

Robotics project

## Invisible Arm (Gripper)



**Team 6**

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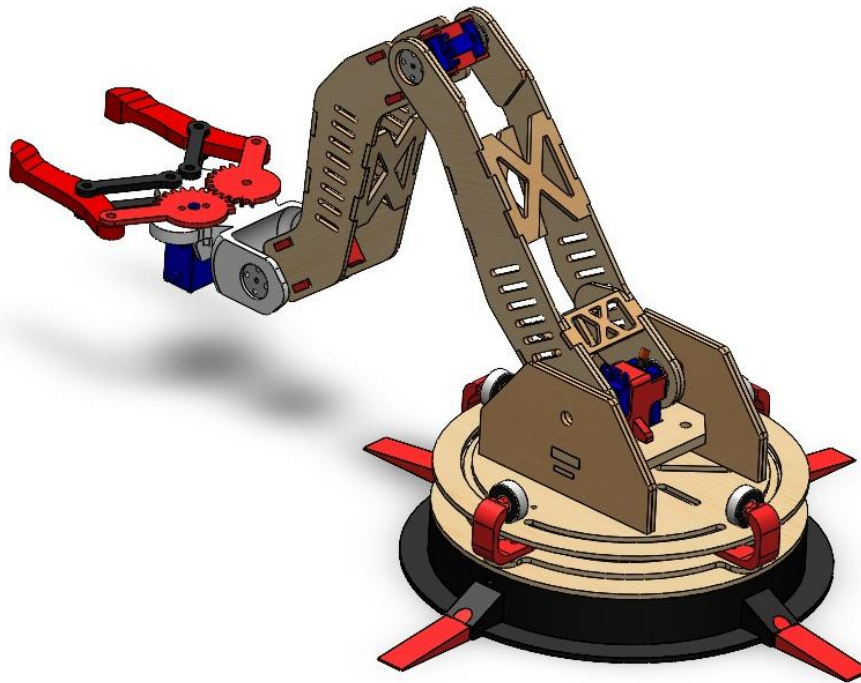
## **1. Introduction**

Robotics has become an essential part of modern industry, automating tasks to improve efficiency, precision, and safety. One of the most widely used robotic components is the gripper arm, designed to mimic the human hand in grasping and manipulating objects. These arms are commonly used in manufacturing, packaging, and assembly lines to handle materials with accuracy and speed. Gripper arms come in various designs, such as mechanical, pneumatic, or vacuum-based, depending on the application. Their integration into production systems reduces labor costs and increases productivity. As technology advances, robotic grippers continue to evolve, offering smarter and more adaptive solutions.

## **2. Description**

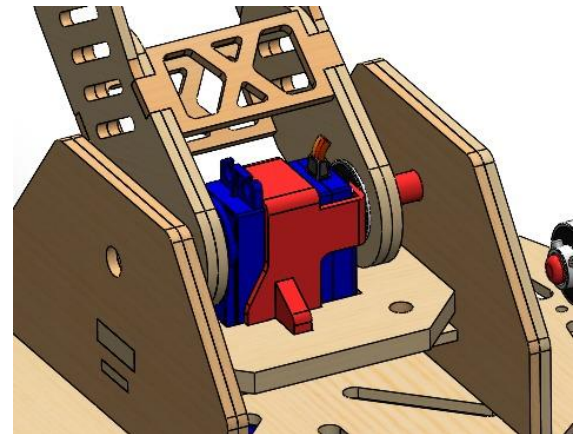
Gripper arm designed for industrial applications. Our design includes a multi-jointed arm structure with rotational joints, powered by servo motors, allowing for a wide range of motion. The base is circular, it offers 360-degree rotation for enhanced flexibility. The gripper at the end features a gear-driven mechanism, enabling it to open and close precisely to grasp various objects. This type of robotic arm is commonly used for pick-and-place tasks, material handling, or light assembly operations. The structure is modular and fabricated from wood, laser-cut, and 3-D printing making it ideal for prototyping and educational use.

### 3. CAD Design

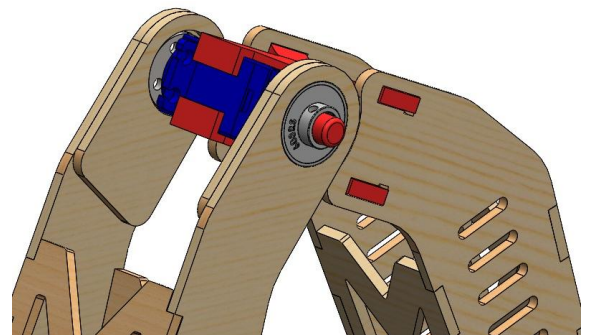


#### 3.1. Servo Holder Assembly

Regarding the servo mounts, we used custom 3D-printed parts designed in CAD software to precisely fit the servo shape while maintaining high strength. These mounts act as the main structural support between the linkages, ensuring the servo is firmly fixed and able to handle the applied loads.

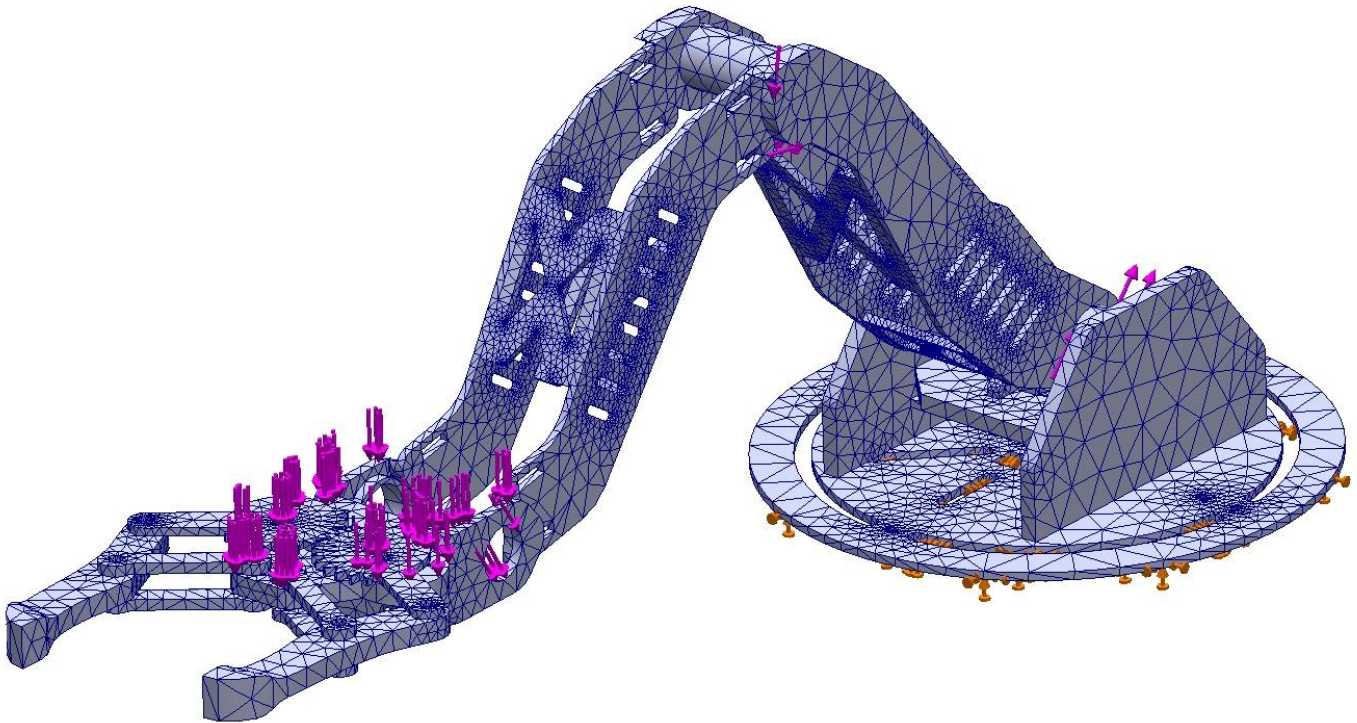


In addition, Bearings were incorporated to allow smooth rotational motion between the linkages. It was accounted for this in the design of the servo's triple-holder, which connects the two linkages. The bearing was integrated into this holder to enable free movement between the linkages without friction to reduce the mechanical load on the servo.

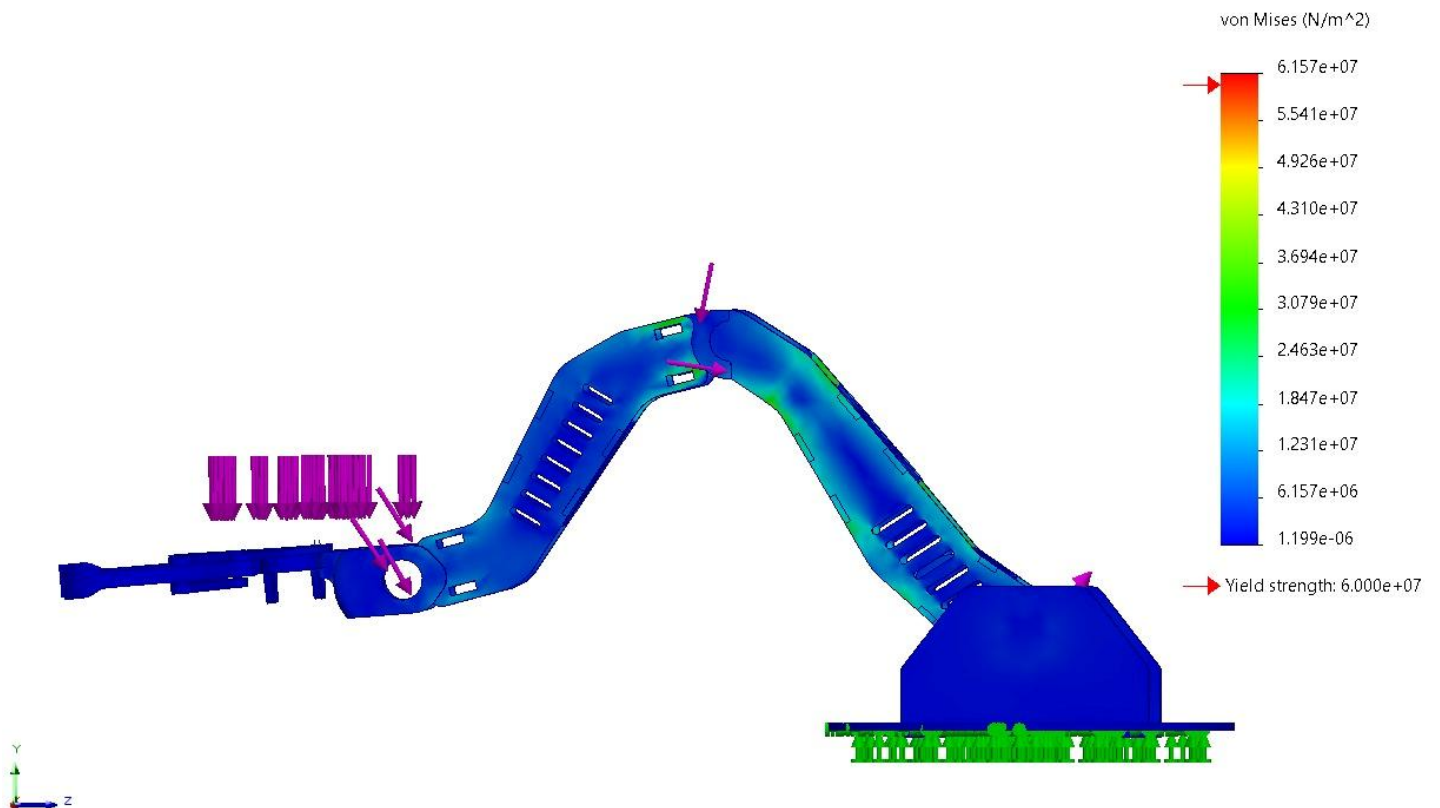


## 3.2. FEA

### 3.2.1. Force Distribution and Meshing

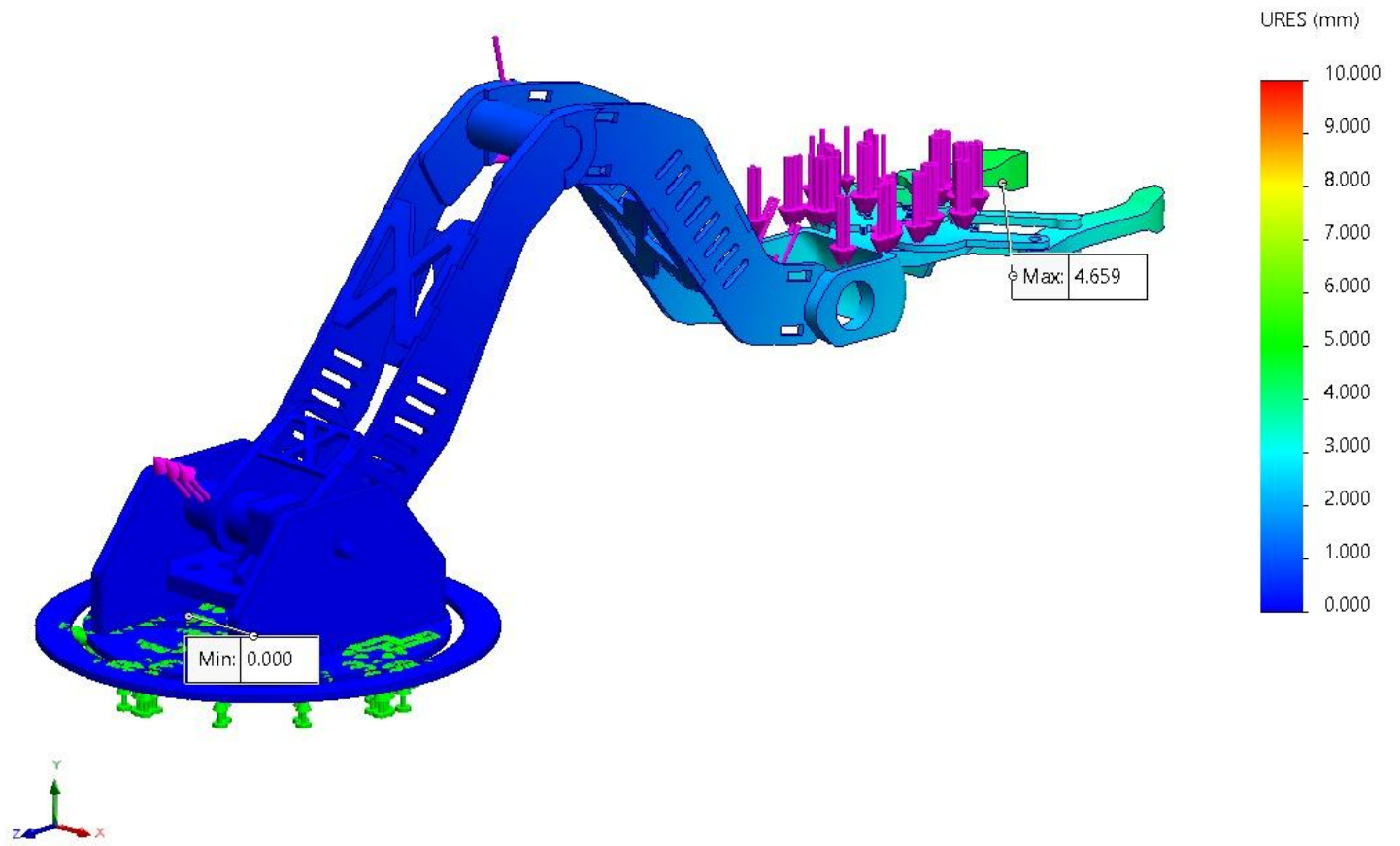


### 3.2.2. Stress Analysis





### 3.2.3. Displacement Analysis



## 4. Roboanalyzer

In this section, we used RoboAnalyzer, a 3D model-based simulation tool, to visualize and verify the forward and inverse kinematics of our robotic arm.

We modeled a 3-degree-of-freedom robotic manipulator consisting of three revolute joints (R-R-R), each represented as a link in RoboAnalyzer. The following links were defined:

- Link 1: Base to first joint.
- Link 2: First joint to second joint.
- Link 3: Second joint to end effector

These values were based on the same dimensions used in our CAD and MATLAB calculations.

We performed simulations to observe:

- Forward Kinematics: By inputting joint angles ( $\theta_1$ ,  $\theta_2$ ), we confirmed the resulting end-effector position matches the theoretical calculations from MATLAB.
- Inverse Kinematics (via Trial): By varying end-effector positions, we observed the corresponding joint configurations, verifying the arm's range and limitations.
- Workspace Visualization: RoboAnalyzer helped us visualize the full reach of the manipulator and ensured that our design satisfies the task requirements.

These simulations were crucial for validating our mathematical model before implementing the physical prototype.

The screenshot displays the Inverse Kinematics software interface. At the top, the 'Inverse Kinematics' title bar is visible. Below it, the 'Select Robot: 3R Articulated' dropdown is set to '3R Articulated'. The main workspace shows a 3D model of a 3R articulated robot with three joints (purple, yellow, and blue) and a red end effector. The joints are labeled with their respective axes:  $\theta_1$  (base),  $\theta_2$  (middle), and  $\theta_3$  (end). The end effector position is labeled  $(x, y, z)$ .

On the right side, the 'Browser' panel shows the '3D Model' and 'Graph' tabs. Below it, the 'Analyses' panel is active, showing 'Time (s)' set to 1.00 and 'No. of Steps' set to 100. The 'FKin' and 'IDyn' buttons are highlighted, and the 'IKin' button is selected.

The 'Analysis Complete' button is visible in the center. Below it, the 'Solution1' panel shows the following joint angles:

- Theta1 (deg): 8.1761
- Theta2 (deg): 13.1338
- Theta3 (deg): -1.7394

The 'Show' button is visible below the solution values.

The 'Solution2' panel shows the following joint angles:

- Theta1 (deg): 8.1761
- Theta2 (deg): 11.4334
- Theta3 (deg): 1.6614

The 'Show' button is visible below the solution values.

The 'Solution3' panel shows the following joint angles:

- Theta1 (deg): 8.1761
- Theta2 (deg): 13.0948
- Theta3 (deg): -1.6614

The 'Show' button is visible below the solution values.

The 'Solution4' panel shows the following joint angles:

- Theta1 (deg): 8.1761
- Theta2 (deg): 11.3944
- Theta3 (deg): 1.7394

The 'Show' button is visible below the solution values.

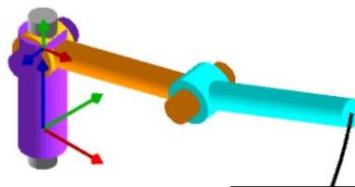
At the bottom right, a large blue 'Update' button is visible, followed by a large black bracket and a table of numerical values:

0.949797	-0.278678	0.142215
0.136463	-0.040039	-0.989836
0.28154	0.95955	0
0	0	0

Joint No	Joint Type	Joint Offset (b) m	Joint Angle (theta) deg	Link Length (a) m	Twist Angle (alpha) deg	Initial Value (V) deg or m	Final Value (V) deg or m
1	Revolute	0.1	Variable	0.001	90	0	90
2	Revolute	0	Variable	0.2	0	0	90
3	Revolute	0	Variable	0.2	0	0	90

Joint	Position	Velocity	Acceleration	Jerk
0	0.949797	-0.278678	0.142215	0.386904
1	0.136463	-0.040039	-0.989836	0.055589
2	0.28154	0.95955	0	0.184751
3	0	0	0	1

- **Link 1**



0.989836	0	0.142215	0.00099
0.142215	0	-0.989836	0.000142
0	1	0	0.1
0	0	0	1

Joint No	Joint Type	Joint Offset (b) m	Joint Angle (theta) deg	Link Length (a) m	Twist Angle (alpha) deg	Initial Value (Jv) deg or m	Final Value (Jv) deg or m
1	Revolute	0.1	Variable	0.001	90	0	90
2	Revolute	0	Variable	0.2	0	0	90
3	Revolute	0	Variable	0.2	0	0	90

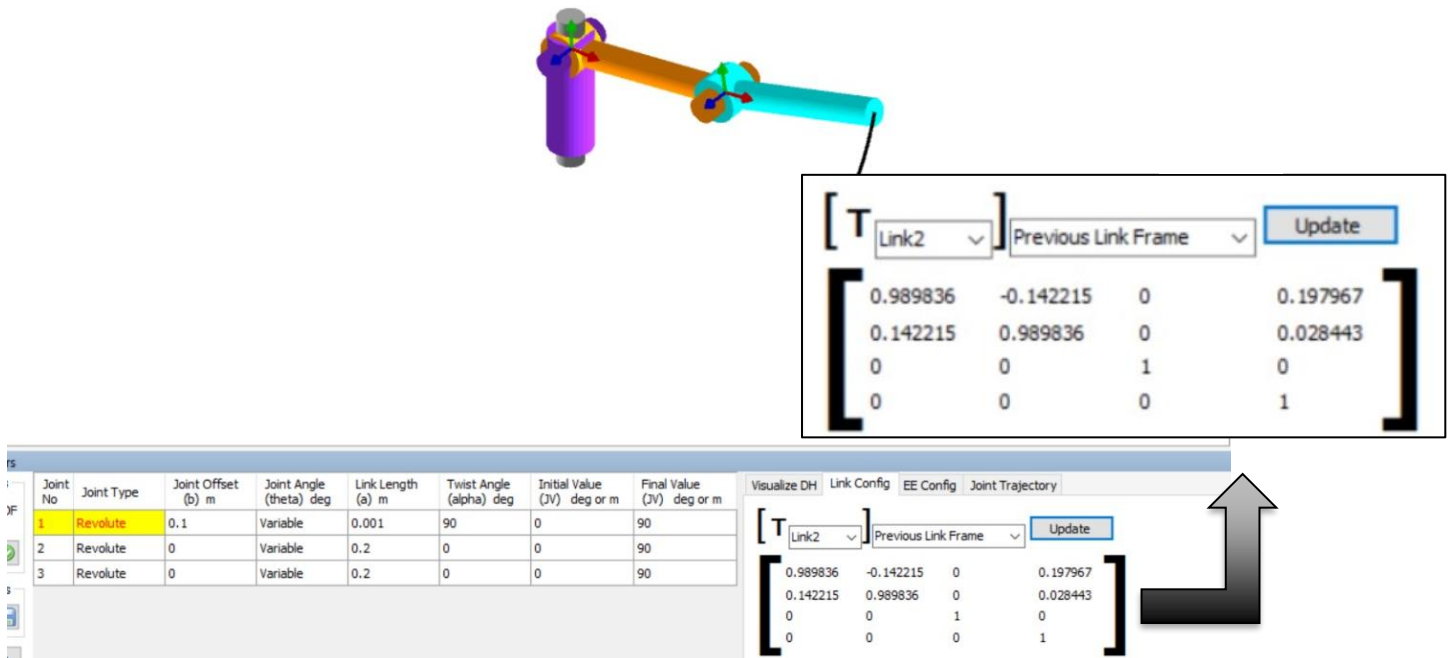
Visualize DH Link Config EE Config Joint Trajectory

[ T Link1 Previous Link Frame Update ]

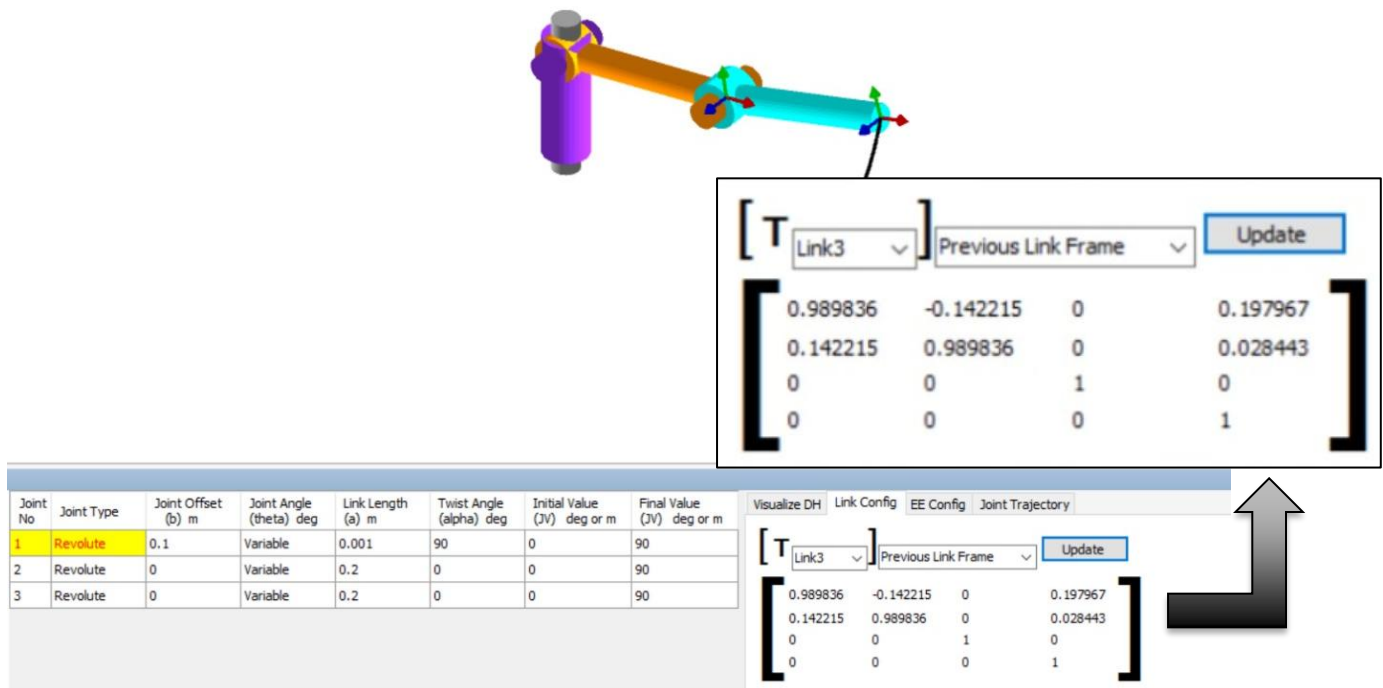
0.989836	0	0.142215	0.00099
0.142215	0	-0.989836	0.000142
0	1	0	0.1
0	0	0	1



## - Link 2



## - Link 3



## 5. MATLAB Calculations

```
syms L_1 L_2 theta_1 theta_2 XE YE
L1 = 0.22;
L2 = 0.208;
XE_RHS = L_1*cos(theta_1) + L_2*cos(theta_1+theta_2)
YE_RHS = L_1*sin(theta_1) + L_2*sin(theta_1+theta_2)
XE_MLF = matlabFunction(XE_RHS, 'Vars', [L_1 L_2 theta_1 theta_2]);
YE_MLF = matlabFunction(YE_RHS, 'Vars', [L_1 L_2 theta_1 theta_2]);
t1_degs_row = linspace(0,90,100);
t2_degs_row = linspace(-180,180,100);
[tt1_degs,tt2_degs] = meshgrid(t1_degs_row,t2_degs_row);
tt1_rads = deg2rad(tt1_degs);
tt2_rads = deg2rad(tt2_degs);
X_mat = XE_MLF(L1,L2,tt1_rads,tt2_rads);
Y_mat = YE_MLF(L1,L2,tt1_rads,tt2_rads);
plot_XY_given_theta_2dof(tt1_degs,tt2_degs,X_mat,Y_mat,(L1+L2))
E_EQ = XE == XE_RHS;
YE_EQ = YE == YE_RHS;
S = solve([E_EQ YE_EQ], [theta_1 theta_2])
simplify(S.theta_1)
simplify(S.theta_2)
TH1_MLF{1} = matlabFunction(S.theta_1(1), 'Vars', [L_1 L_2 XE YE]);
TH1_MLF{2} = matlabFunction(S.theta_1(2), 'Vars', [L_1 L_2 XE YE]);
TH2_MLF{1} = matlabFunction(S.theta_2(1), 'Vars', [L_1 L_2 XE YE]);
TH2_MLF{2} = matlabFunction(S.theta_2(2), 'Vars', [L_1 L_2 XE YE]);
[xmat,yamat] = meshgrid(0:0.01:0.4,0:0.01:0.4);
tmp_th1_mat = TH1_MLF{1}(L1,L2,xmat,yamat);
tmp_th2_mat = TH2_MLF{1}(L1,L2,xmat,yamat);
tmp_th1_mat = rad2deg(tmp_th1_mat);
tmp_th2_mat = rad2deg(tmp_th2_mat);
th1_mat = NaN(size(tmp_th1_mat));
th2_mat = NaN(size(tmp_th2_mat));

tf_mat = imag(tmp_th1_mat) == 0;
th1_mat(tf_mat) = real(tmp_th1_mat(tf_mat));

tf_mat = imag(tmp_th2_mat) == 0;
th2_mat(tf_mat) = real(tmp_th2_mat(tf_mat));
plot_theta_given_XY_2dof(xmat,yamat,th1_mat,th2_mat)
the_J = jacobian([XE_RHS YE_RHS],[theta_1 theta_2])
function plot_theta_given_XY_2dof(X_mat,Y_mat,theta_1_mat_degs,...
                                theta_2_mat_degs)

xlab_str = 'X (m)';
ylab_str = 'Y (m)';
```

```

figure;
hax(1) = subplot(1,2,1);
    contourf(X_mat, Y_mat, theta_1_mat_degs);
    clim(hax(1), [-180 180]);
    colormap(gca,'jet'); colorbar
    xlabel(xlab_str, 'Interpreter', 'tex');
    ylabel(ylab_str, 'Interpreter', 'tex');
    title(hax(1), '\theta_1', 'Interpreter', 'tex')
    axis('equal')
hax(2) = subplot(1,2,2);
    contourf(X_mat, Y_mat, theta_2_mat_degs);
    clim(hax(2), [-180 180]);
    colormap(gca,'jet'); colorbar
    xlabel(xlab_str, 'Interpreter', 'tex');
    ylabel(ylab_str, 'Interpreter', 'tex');
    title(hax(2), '\theta_2', 'Interpreter', 'tex')
    axis('equal')

end

function
plot_XY_given_theta_2dof(theta_1_mat_degs,theta_2_mat_degs,...
                        X_mat,Y_mat,a_cmax)

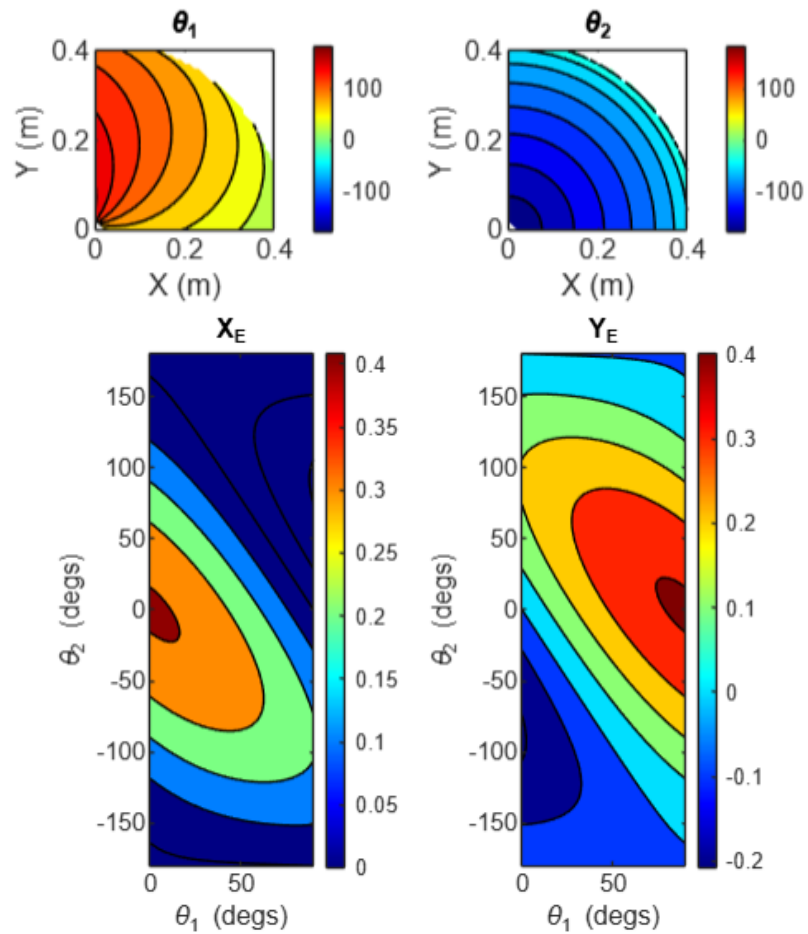
xlab_str = '\theta_1 (deg)';
ylab_str = '\theta_2 (deg)';

figure;
hax(1) = subplot(1,2,1);
    contourf(theta_1_mat_degs, theta_2_mat_degs, X_mat);
    clim(hax(1), [0 a_cmax]);
    colormap(gca,'jet'); colorbar
    xlabel(xlab_str, 'Interpreter', 'tex');
    ylabel(ylab_str, 'Interpreter', 'tex');
    title(hax(1), 'X_E', 'Interpreter', 'tex')
hax(2) = subplot(1,2,2);
    contourf(theta_1_mat_degs, theta_2_mat_degs, Y_mat);
    clim(hax(1), [0 a_cmax]);
    colormap(gca,'jet'); colorbar
    xlabel(xlab_str, 'Interpreter', 'tex');
    ylabel(ylab_str, 'Interpreter', 'tex');
    title(hax(2), 'Y_E', 'Interpreter', 'tex')

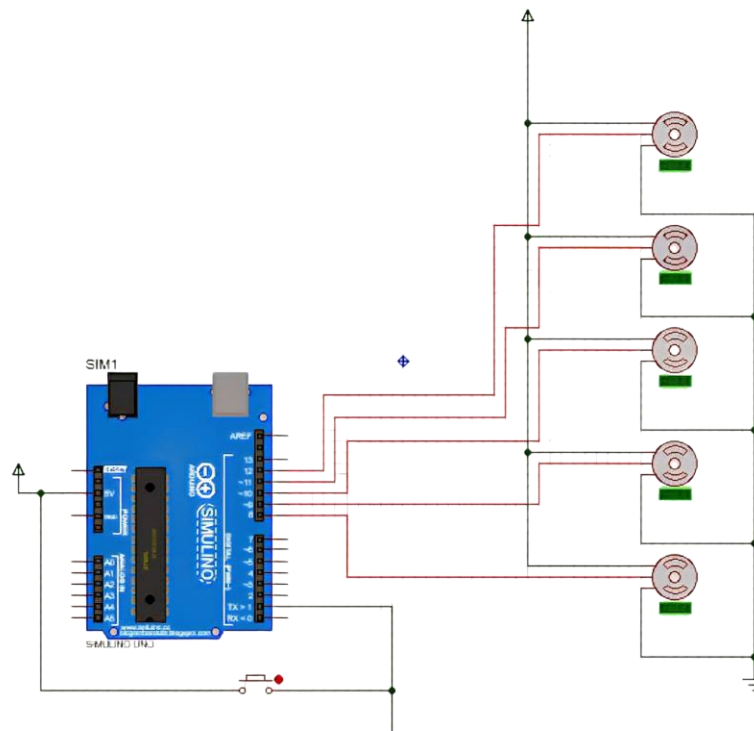
end

```

## 6. Contours and Results

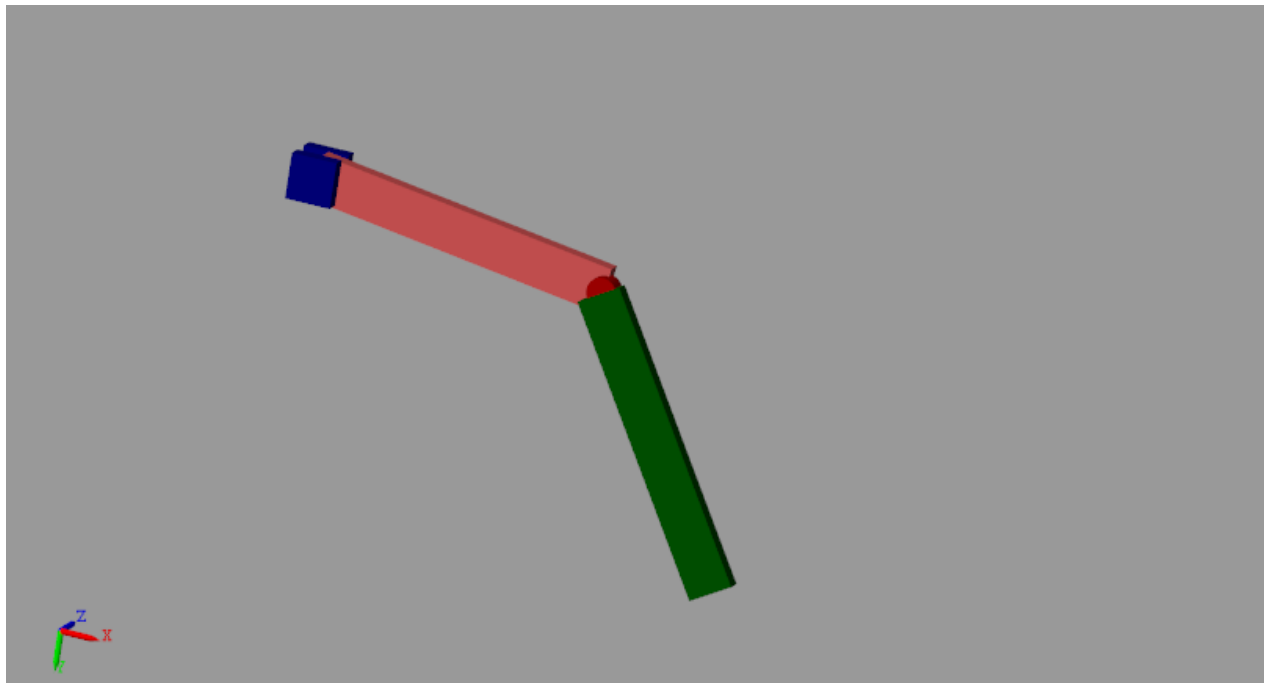
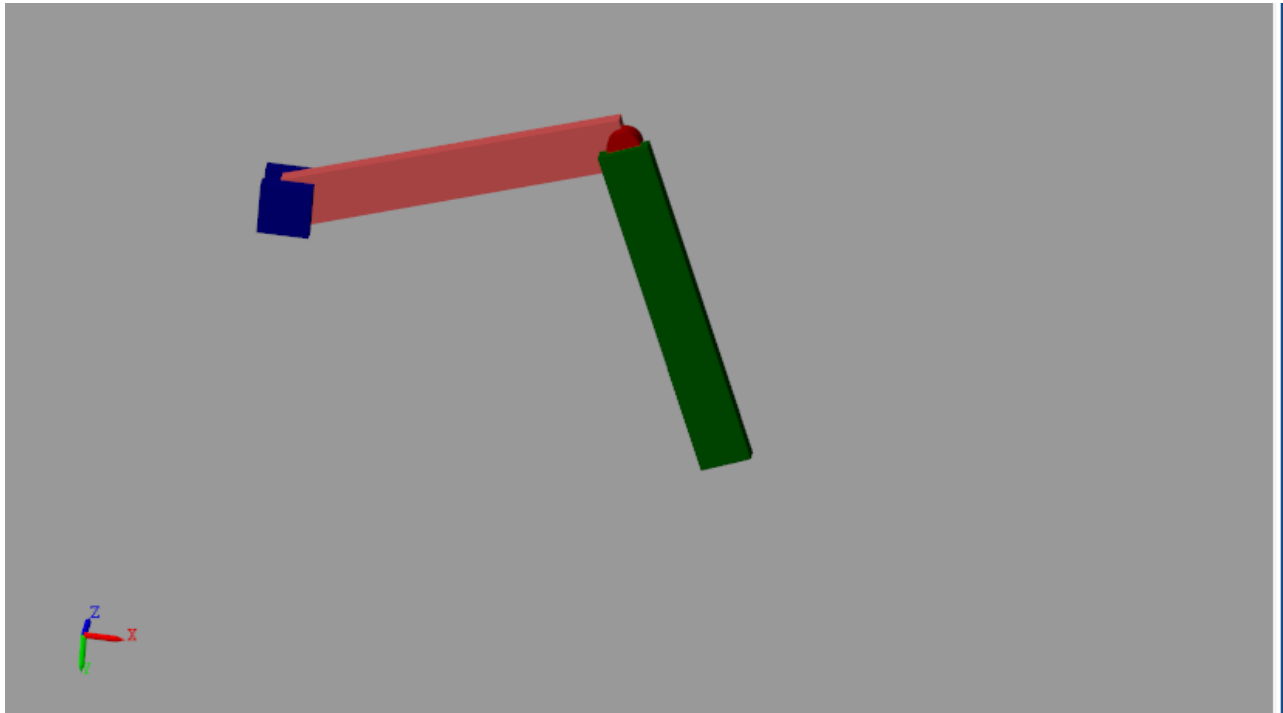


## 7. Wiring Diagram

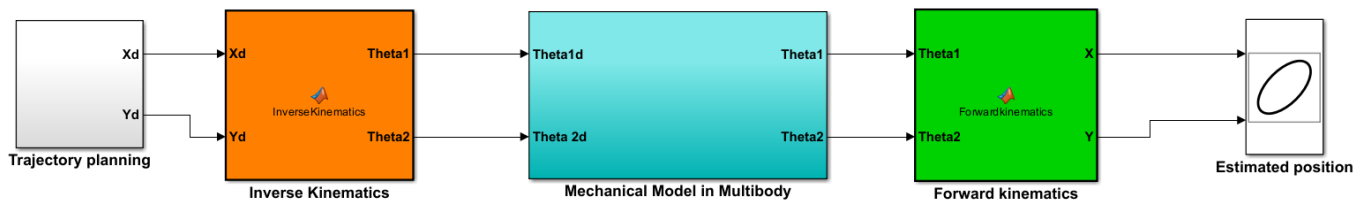
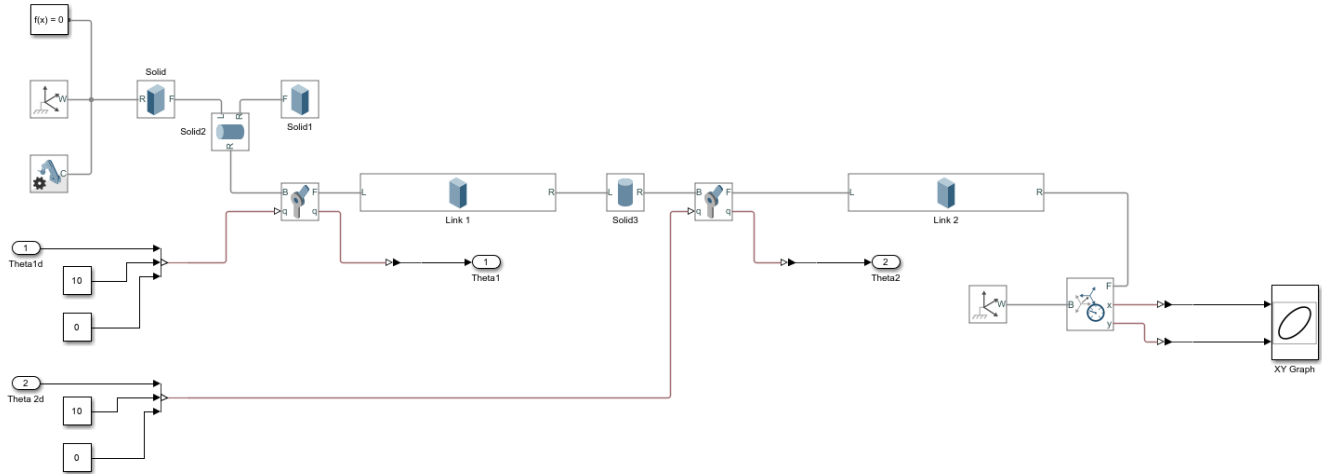


## 8. Simulink

### - Trajectory



## - Mechanical model in multibody



## 9. Torque calculations

$L2=20 \text{ cm}$

$M_{box}=0.3 \text{ Kg}$

$L1=20.8 \text{ cm}$

$M_{joint}=0.08 \text{ Kg}$

$M_{link2}=0.215 \text{ Kg}$

$$T2 = (L2 * M_{box}) + \left(\frac{1}{2} * L2 * M_{link2}\right)$$

$$T1 = ((L1 + L2) * M_{box}) + \left(\left(L1 + \frac{L2}{2}\right) * M_{link2}\right) + (L1 * M_{joint2}) + \left(\frac{L1}{2} * M_{link2}\right)$$

$$T1 = 22.1 \text{ Kg/cm}$$

$$T2 = 8.15 \text{ Kg/cm}$$

