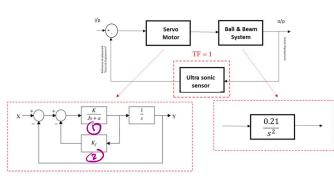


Steps:

For the unity feedback block diagram shown:



Block diagram of Stevo Motor

Transfer function of Ball & Beam System

$$\text{loop 1}$$

$$C.L.S = \frac{\frac{K}{Js+a}}{1 + \frac{KK_f}{Js+a}} = \frac{K}{Js+a + KK_f}$$

$$\therefore \text{Closed loop system} = \frac{K}{Js^2 + (a + KK_f)s + K}$$

$$\underline{\text{Loop 2:}} \quad C.L.S = \frac{\frac{K}{Js^2 + (a + KK_f)s}}{1 + \frac{K}{Js^2 + (a + KK_f)s}} = \frac{K}{Js^2 + (a + KK_f)s + K}$$

$$\frac{Y(s)}{X(s)} = \frac{K}{Js^2 + (a + KK_f)s + K}$$

$$F(s) : \text{open loop system} = \frac{12}{Js^2 + (a + KK_f)s + K} \cdot \frac{0.21}{s^2}$$

K : proportionality gain of motor = responsiveness / torque gain

K_f : friction / damping coefficient

J : Inertia

a : viscous damping coefficient

$$\text{From description: } \frac{\omega_n^2}{s^2 + 2s\omega_n s + \omega_n^2} \cdot \frac{0.21}{s^2}$$

$$\frac{12}{Js^2 + (a + KK_f)s + K} \cdot \frac{0.21}{s^2} \div J$$

$$\frac{K/J}{s^2 + \frac{(a + KK_f)}{J}s + K/J} \cdot \frac{0.21}{s^2}$$

$$\therefore \omega_n^2 = \frac{K}{J} \quad 2s\omega_n = \frac{a + KK_f}{J}$$

$$\therefore \omega_n = \sqrt{\frac{K}{J}} \quad \therefore s = \frac{a + KK_f}{2J\omega_n}$$

$$= \frac{a + KK_f}{2J\sqrt{\frac{K}{J}}} \\ = \frac{a + KK_f}{2\sqrt{KJ}}$$

ID = 13001577

$$\therefore \omega_n = 77$$

$$77 = \sqrt{\frac{K}{J}}$$

$$\& s = 0.8 = \frac{a + KK_f}{2\sqrt{KJ}}$$

$$5929 = \frac{K}{J}$$

$$\& 2 = \frac{a + KK_f}{2\sqrt{KJ}}$$

$$J = 1 \text{ kg/m}^2 \quad \& \quad \alpha = 1 \text{ N.m/rad.sec}$$

$$\therefore K = 5929 \text{ rad.v/s}$$

$$L = \frac{1 + 5929 K_F}{2 \sqrt{5929}}$$

$$ISU = 1 + 5929 K_F$$

$$K_F = \frac{153}{5929} \text{ v.s/rad}$$

$$\therefore G(s) = \frac{5929}{s^2 + 77s + 5929} \cdot \frac{0.21}{s^2} \leftarrow \text{Feed Forward Transfer Function}$$

$$= \frac{124s.09}{s^2(s^2 + 77s + 5929)} = \frac{N(s)}{D(s)}$$

$$\text{Closed loop system: } \frac{G(s)}{1 + G(s)} = \frac{\frac{N(s)}{D(s)}}{1 + \frac{N(s)}{D(s)}} = \frac{N(s)}{D(s) + N(s)}$$

$$H(s) : \text{closed loop system} = \frac{124s.09}{s^2(s^2 + 77s + 5929) + 124s.09}$$

Inputs on $G(s)$:

Analysis of $G(s)$ \rightsquigarrow using Final Value Theorem

$$\text{Steady state} = \lim_{s \rightarrow 0} s G(s) = \frac{124s.09}{s(s^2 + 77s + 5929)} = \infty \text{ for impulse}$$

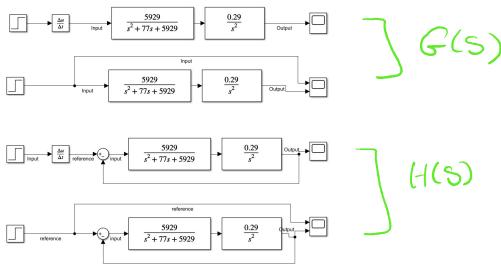
$$\text{Steady State} \lim_{s \rightarrow 0} s G(s) \left(\frac{1}{s}\right) = \frac{124s.09}{s^2(s^2 + 77s + 5929)} = \infty \text{ for step input}$$

* Expected as Function integrates the input making it increase linearly with s and exponentially with step input

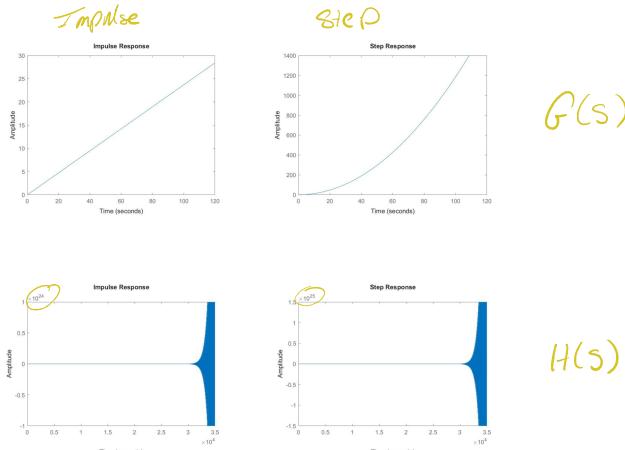
Analysis on $H(s)$: Total TF function

$$H(s) = \frac{124s.09}{s^2(s^2 + 77s + 5929) + 124s.09}$$

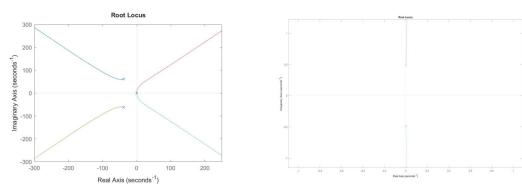
* Grows infinitely as the term of s^1 is missing (Hurwitz Criterion) for both impulse and step inputs, but will also be oscillating.



The feedback introduced a pole in the right plane (the Real part) and so for any input (impulse/Step) the output grows exponentially in addition to also having an imaginary part and so introducing oscillations. So overall the response is worse as the system is now unstable.



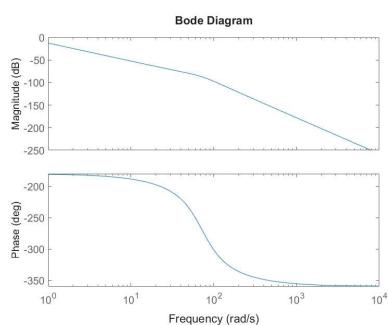
- * Gain adjustment will deteriorate the system's stability as 2 of the poles with increase of K , will move further into the right plane making it more unstable.



12us.09

$$s^2(s^2 + 77s + 5929) + 12us.09$$

System's phase is less than -180° at
Magnitude = 1 \therefore System is unstable



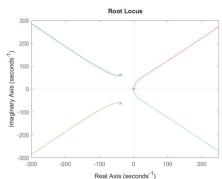
$$124S \cdot 09$$

$$\frac{1}{S^2 \cdot (S^2 + 77S + 5929)}$$

$$= G(s)$$

Poles of open loop : $S^2(S^2 + 77S + 5929)$

$$\begin{aligned} S &= 0 \quad n=2 \\ S &= -38.5 + 66.68j \\ S &= -38.5 - 66.68j \end{aligned}$$



Using a PD Controller: A PD controller is needed since the poles move to the right hand plane in the root locus.

$$K_d = 100$$

$$K_p = 10$$

$$\text{New openloop: } \frac{124S \cdot 09(100S + 10)}{S^2(S^2 + 77S + 5929)}$$

$$\text{New closed loop: } \frac{124S \cdot 09(100S + 10)}{S^4 + 77S^3 + 5929S^2 + 124S \cdot 09S + 124S \cdot 09}$$

Poles: $S = -0.01$ $S = -27.21$ $S = -24.9 \pm j62.88$ Conjugate poles

\therefore all in L.H.P \therefore Stable

From the open loop : System is 2nd type

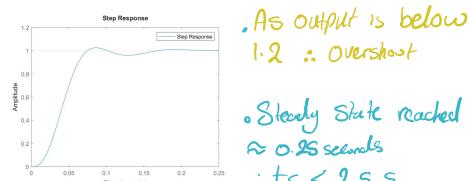
\therefore ζ_{ss} for Step & ramp = 0

$$\zeta_{ss} \text{ for Parabola} \rightarrow \zeta_{ss} = \frac{1}{1 + \text{open loop}}$$

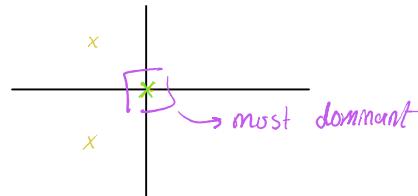
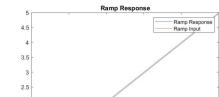
$$\zeta_{ss} = \frac{S^2(S^2 + 77S + 5929)}{S^3(S^2 + 77S + 5929) + 124S \cdot 09(100S + 10)}$$

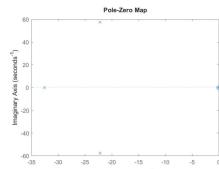
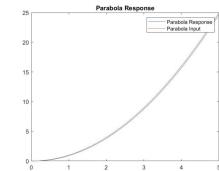
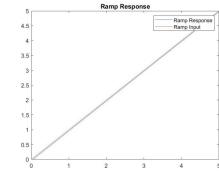
$$\zeta_{ss} = \frac{0 + 5929}{0 + (124S \cdot 09)(10)} = 0.4762$$

Using MATLAB:

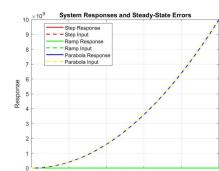


- Steady State reached ≈ 0.25 seconds
- $\therefore t_s < 2.5$ s





From the PZmap
one can see that all
poles are in the L.H.P.
 \therefore System is stable



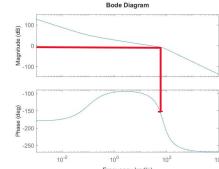
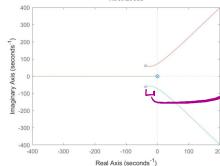
Numerical Steady-State Errors:
Step: 1.1102e-16
Ramp: 0
Parabolic: 0.49178
Step is practically zero
Ramp is zero
Parabolic E_{ss} is extremely close to value computed

Note: The steady state errors were computed numerically @ $t = 100000$

```
ans = struct with fields:
    RiseTime: 0.0432
    TransientTime: 0.1515
    SettlingTime: 0.1515
    SettlingMargin: 3.9001
    SettlingMax: 1.0051
    SettlingMin: 0.9949
    Overshoot: 2.5124
    Undershoot: 0
    Peak: 1.0251
    PeakTime: 0.0852
```

Overshoot: 2.51 %
Settling time: 0.1515 s
Peak time: 0.0852 s
Rise time: 0.0432 s

The root locus has changed significantly as the poles
at zero now are on the left side \therefore stable
and for the corresponding values of K in $K+KL(s) = 0$
 \therefore The system is stable.



Note that for Magnitude plot = 2 the
Corresponding phase is larger than -180°
 \therefore System is stable

Lead Compensator design:

$$\text{Compensator: } K \frac{(s+2)}{(s+p)} \boxed{\frac{124s.09}{s^2(s^2+77s+5929)}} = G(s)$$

$$M_p = 20\% \quad t_s = 2.58$$

$$\zeta = \sqrt{\frac{\ln^2(0.2)}{\pi^2 + \ln^2(0.2)}} = 0.456$$

$$t_s = \frac{4.6}{\zeta \omega_n} = 2.5 (0.456) \omega_n = 4.6 \quad \omega_n = 4.035 \text{ rad/s}$$

$$1 + \frac{K(s+2) 124s.09}{s^2(s^2+77s+5929)(s+p)} = 0$$

$$s^4 + 77s^3 + 5929s^2(s+p) + 124s.09 K s + 124s.09 Z = 0$$

$$\delta^4 + 77\delta^3 + 5929\delta^2(\delta + p) + 1245.09K\delta + 1245.09Z = 0$$

$$\delta^5 + 77\delta^4 + 5929\delta^3 + p\delta^4 + 77p\delta^3 + 5929p\delta^2 + 1245.09K\delta + 1245.09Z = 0$$

$$\delta^5 + (77+p)\delta^4 + (5929+p)\delta^3 + 5929p\delta^2 + 1245.09K\delta + 1245.09Z = 0$$

assume pole = 120

$$+\delta^5 + 197\delta^4 + 6049\delta^3 + 711480\delta^2 + 1245.09K\delta + 1245.09Z = 0$$

$$+(\delta^3 + (a+b+c)\delta^2 + (ab+ac+bc)\delta + abc)(\delta^2 + 3.68\delta + 16.28) = 0$$

$$\delta^4 - 77+p = (a+b+c) + 3.68 \quad \text{[1]}$$

$$\delta^3 - 5929+p = 16.28 + 3.68(a+b+c) + (ab+ac+bc)$$

$$\delta^2 - 5929p = 16.28(a+b+c) + 3.68(ab+ac+bc) \quad \text{[2]}$$

$$\delta^1 - 1245.09K = 16.28(ab+ac+bc) + 3.68abc \quad \text{[3]}$$

$$\delta^0 - 1245.09Z = 16.28abc \quad \text{[4]}$$

From [1] \rightarrow [2]

$$(a+b+c) = 77+p - 3.68 = 73.32+p$$

[5]

$$[1] \rightarrow [3] \quad \& \quad [6] \rightarrow [3]$$

$$5929+p = 16.28 + 3.68(73.32+p) + (ab+ac+bc)$$

$$5929+p - 16.28 - 269.8176 - 3.68p = (ab+ac+bc)$$

$$-2.68p + 5642.9024 = (ab+ac+bc) \quad \text{[7]}$$

$$[7] \rightarrow [4] \quad \& \quad [5] \rightarrow [4]$$

$$1245.09K = 16.28[-2.68p + 5642.9024] + 3.68abc$$

$$1245.09K = -43.6304p + 91866.48 + 3.68abc$$

$$1245.09K + 43.6304p - 91866.48 = 3.68abc \quad \div 3.68$$

$$338.34K + 11.856p - 24963.71 = abc$$

$$1245.09Z = 16.28[338.34K + 11.856p - 24963.71]$$

$$Z = 0.013075 \quad \text{[8]}$$

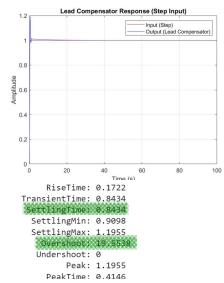
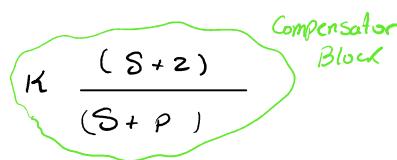
$$Z = 4.4241K + 0.1550172P - 326.4$$

Using MATLAB plugging values into equation (trial & error)

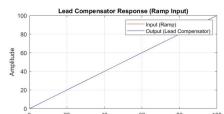
K : Proportionality = 360

Z : Zero = 0.1

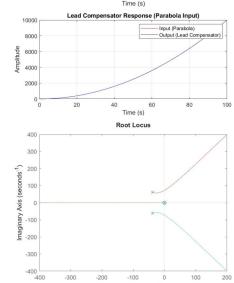
P : Pole = 10



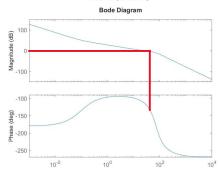
Note that the error is zero since the System type is 2



As System is of type 2 it can track ramp & Parabola too.



From the locus we can see that the System is stable since all poles are on the left hand plane.



Note that for Magnitude plot = 2 the Corresponding phase is larger than -180°
 \therefore System is stable