





$$\overline{E_k} = \frac{3kT}{2}$$





1

0

—

25

345



2





$$E_{\text{thermal}} = \frac{3NkT}{2}$$

$$E_{\text{thermal}} = \frac{3nRT}{2}$$

forbid





1 = 101 + 011011













*Expansion*

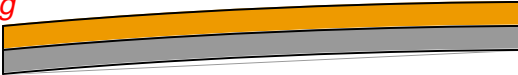


copper



iron

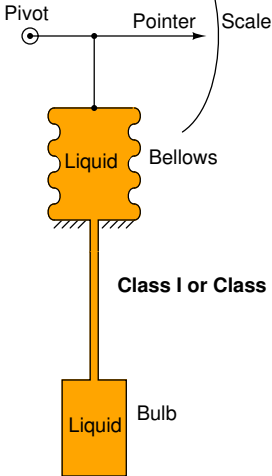
*Bending*

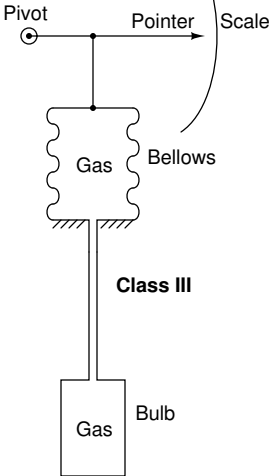


copper

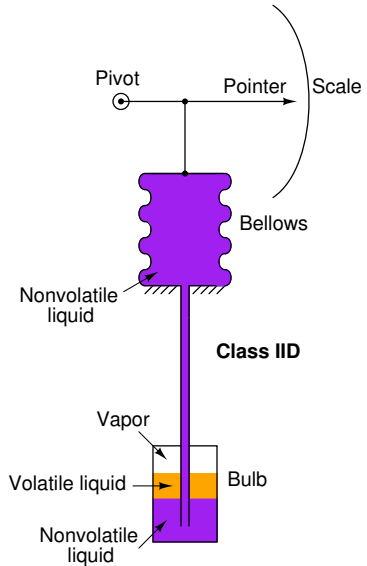
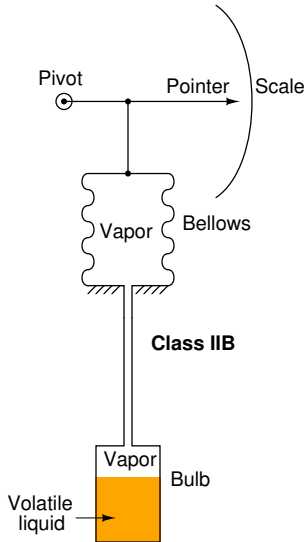
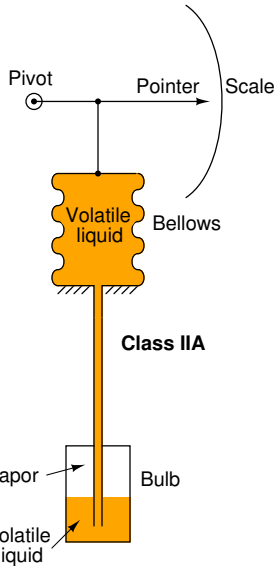
iron







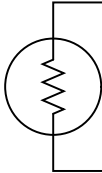








Thermistor  
or  
RTD



Ohmmeter



*Practical [1 + 1] Design*



1999





$AR = 100221 + 10.00392)(35000000)$

APR 1002 [140.132]

APR 10 2015

THE 1520S

$$R_I = R_{ref}(1 + A I^2 + B I^3 - 100 I^3 + C I^4)$$

200







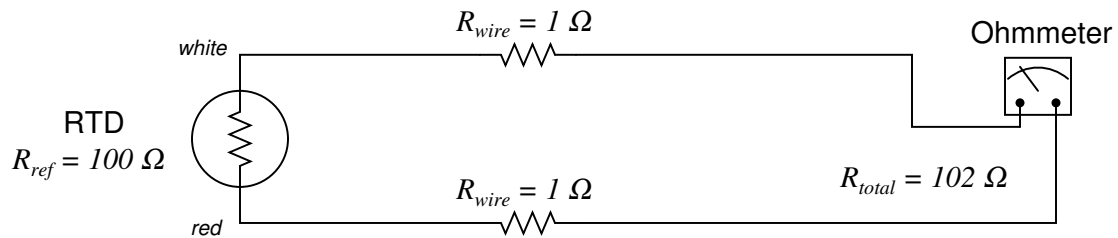
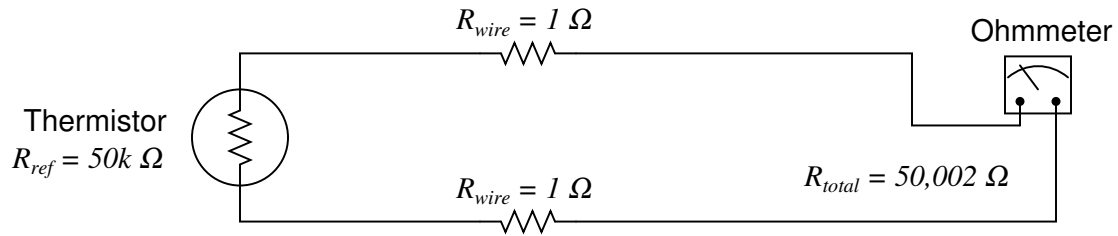
BRAD + BIL

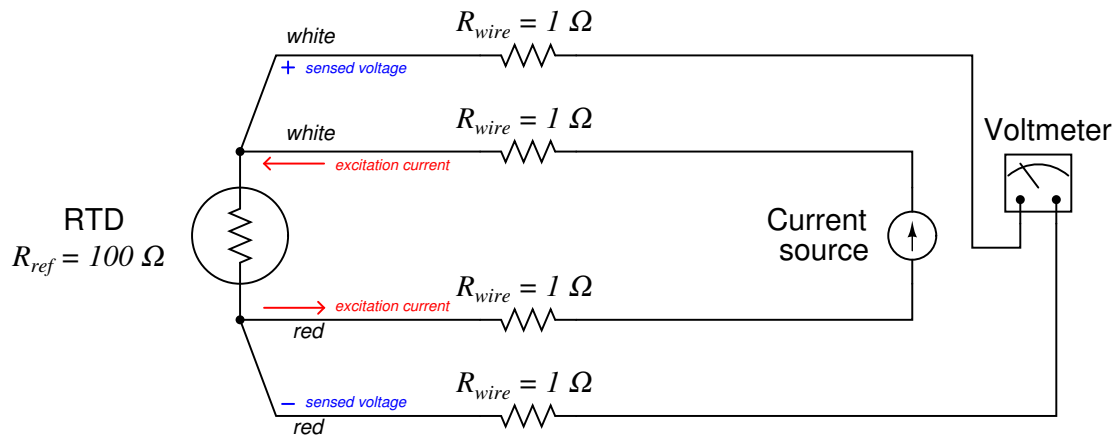


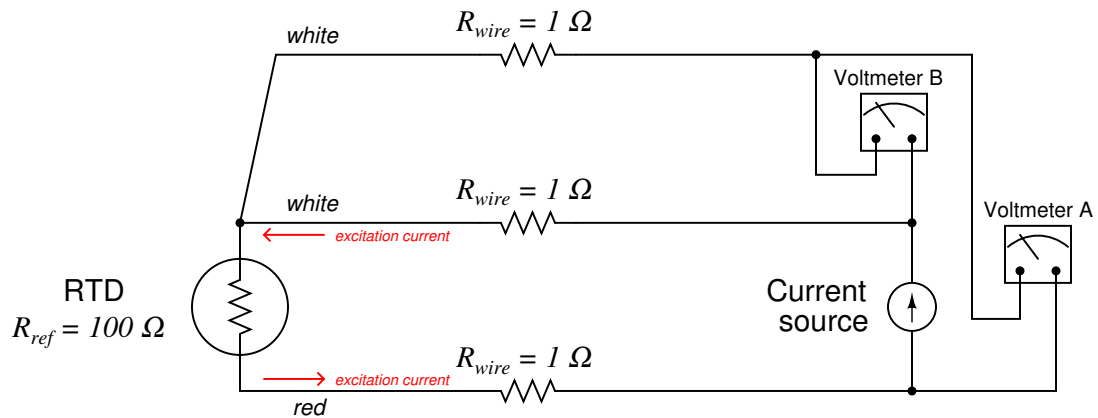






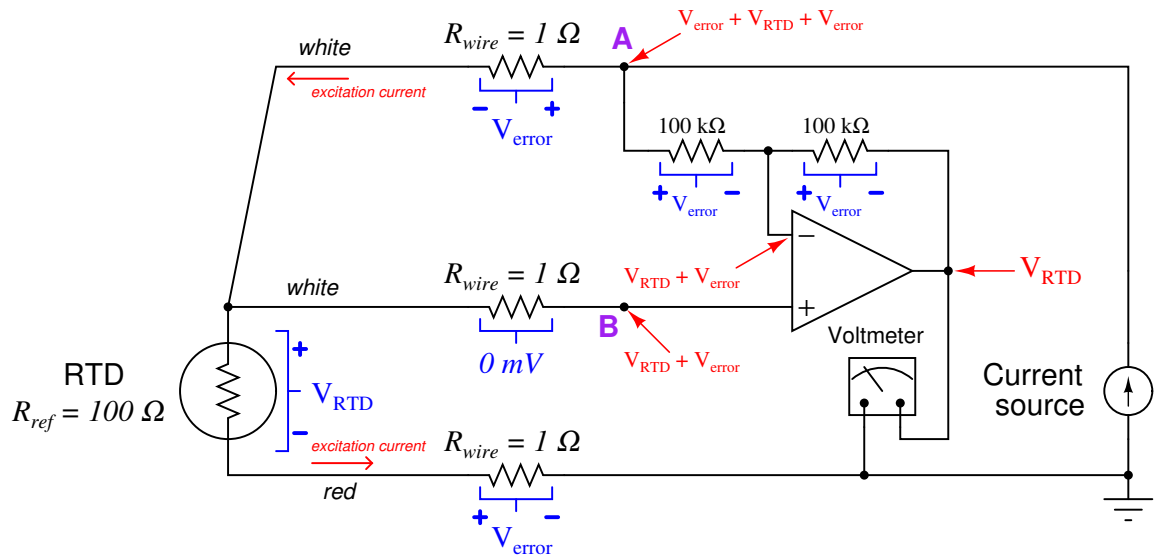








$V_{RD} = V_{meter(A)} - V_{meter(B)}$



Vaporwave

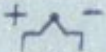


Vaporwave





WORLD



1

2

3

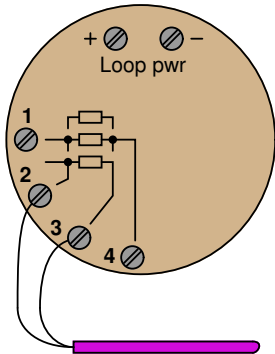
4

P

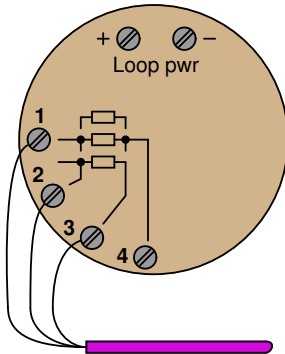




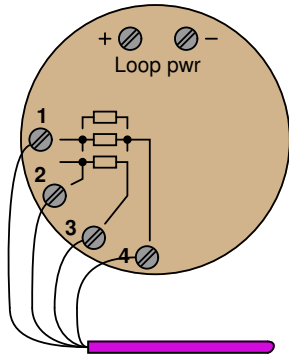
Transmitter connection  
to 2-wire RTD sensor



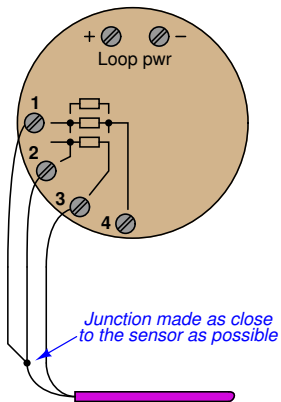
Transmitter connection  
to 3-wire RTD sensor



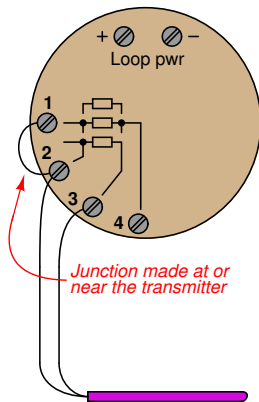
Transmitter connection  
to 4-wire RTD sensor



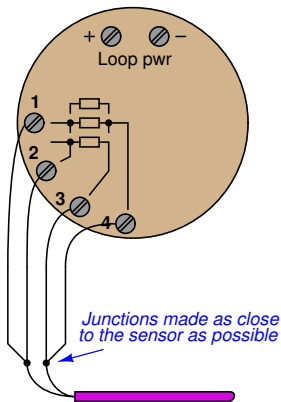
### Correct way to use a 3-wire transmitter on a 2-wire RTD



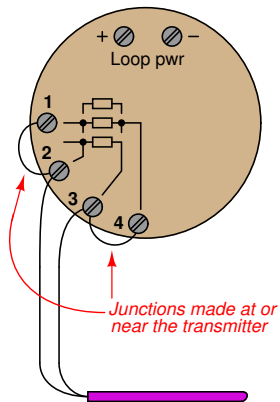
### Incorrect way to use a 3-wire transmitter on a 2-wire RTD



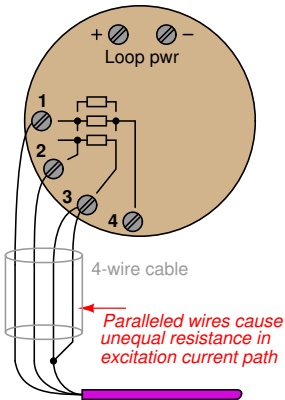
### Correct way to use a 4-wire transmitter on a 2-wire RTD



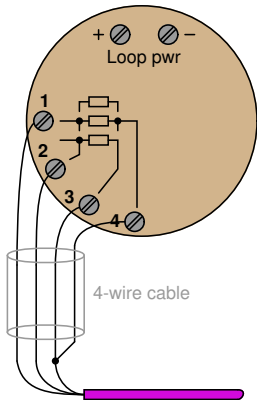
### Incorrect way to use a 4-wire transmitter on a 2-wire RTD



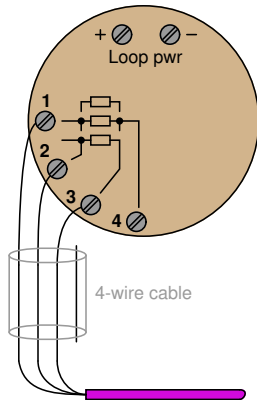
# Incorrect way to use a 3-wire transmitter on a 3-wire RTD



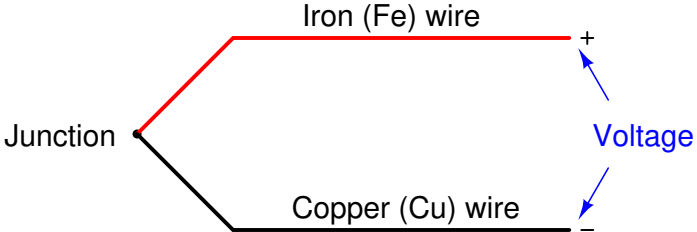
## Correct way to use a 4-wire transmitter on a 3-wire RTD



## Correct way to use a 3-wire transmitter on a 3-wire RTD



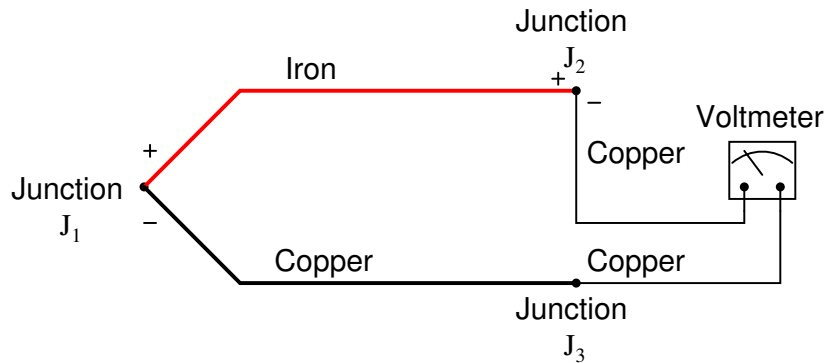














www.viviparous

V  
I

—

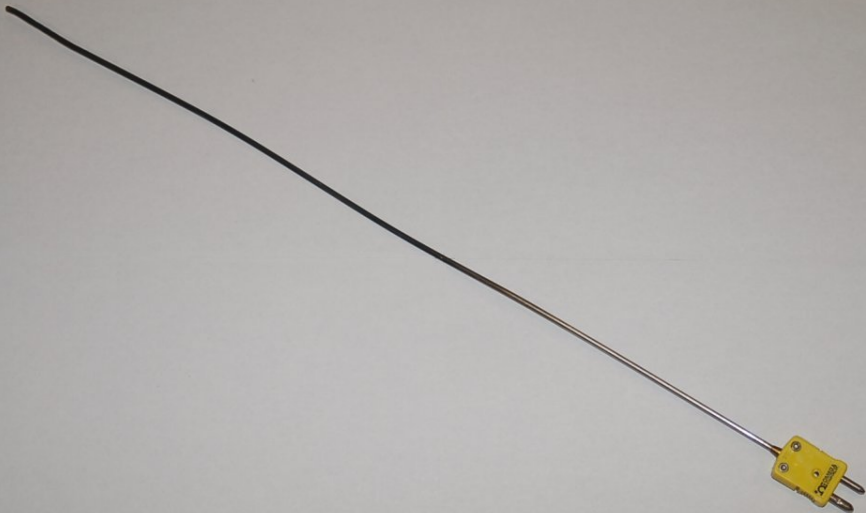
V  
I

mpc

vi

vd

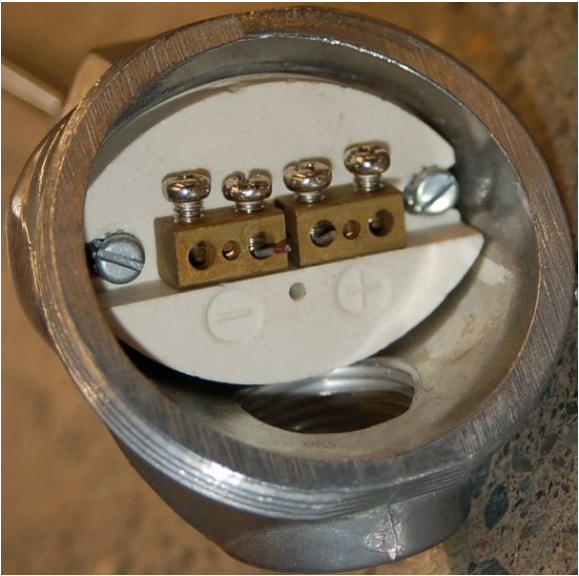
Type	Positive wire <i>characteristic</i>	Negative wire <i>characteristic</i>	Plug	Temp. range
T	Copper (blue) <i>yellow colored</i>	Constantan (red) <i>silver colored</i>	Blue	−300 to 700 °F
J	Iron (white) <i>magnetic, rusty?</i>	Constantan (red) <i>non-magnetic</i>	Black	32 to 1400 °F
E	Chromel (violet) <i>shiny finish</i>	Constantan (red) <i>dull finish</i>	Violet	32 to 1600 °F
K	Chromel (yellow) <i>non-magnetic</i>	Alumel (red) <i>magnetic</i>	Yellow	32 to 2300 °F
N	Nicrosil (orange)	Nisil (red)	Orange	32 to 2300 °F
S	Pt90% - Rh10% (black)	Platinum (red)	Green	32 to 2700 °F
B	Pt70% - Rh30% (grey)	Pt94% - Rh6% (red)	Grey	32 to 3380 °F



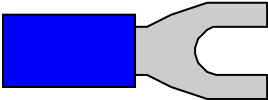




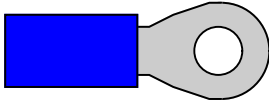


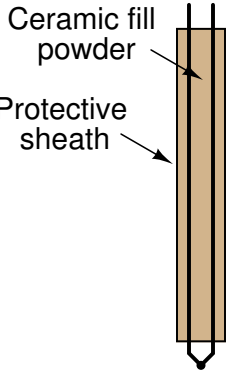


*Fork terminal*



*Ring terminal*

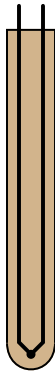




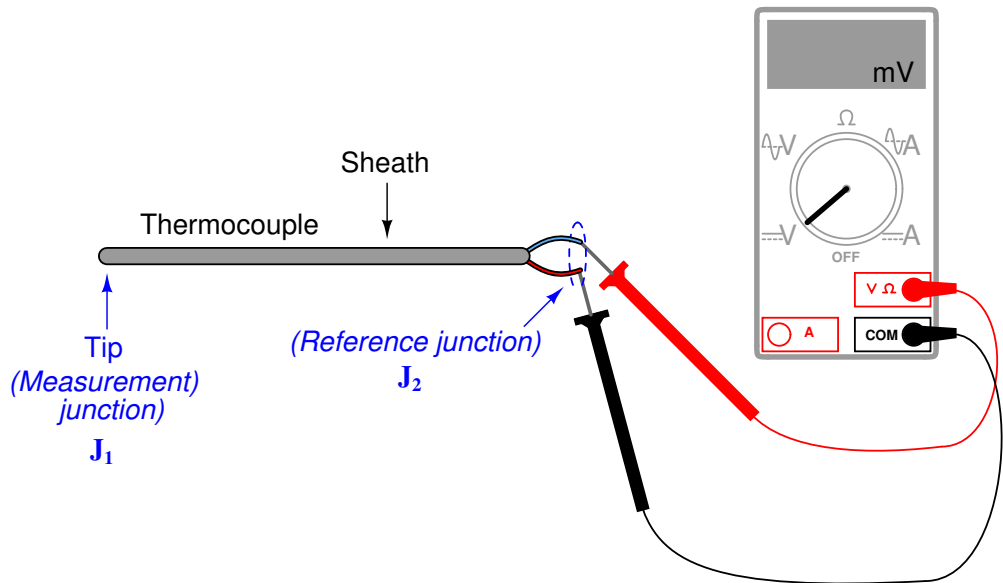
Exposed  
tip



Grounded  
tip



Ungrounded  
tip







$v_1$

$\rightarrow$

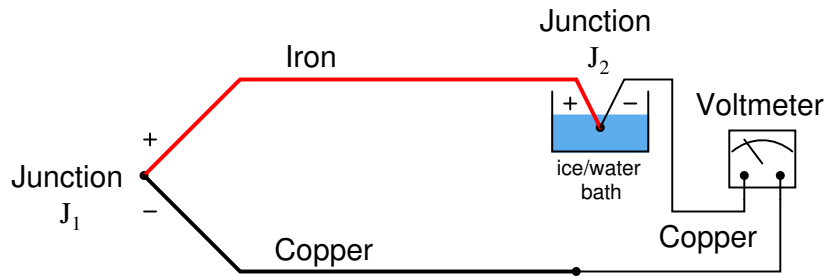
$v_2$

$+$

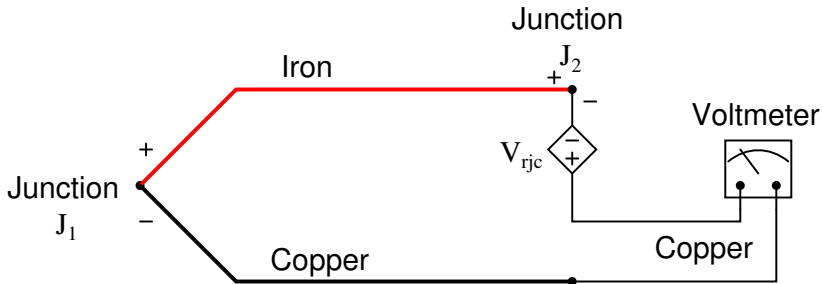
$v_1 + v_2$







*Compensating for the effects of  $J_2$   
using a “reference junction compensation”  
source to generate a counter-voltage*



WPC

WPC

==

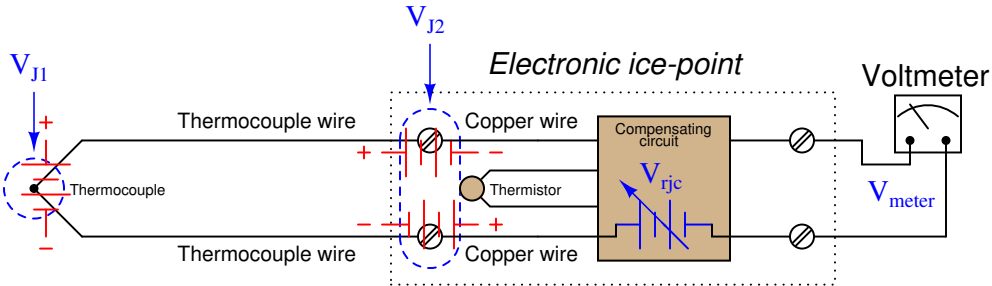
WQ

$$V_{\text{meter}} = V_{x1} - V_{x2} + V_{x3}$$

$$V_{\text{meter}} = V_{x1} + 0 \quad \text{If } V_{x2} = V_{x2}$$

A pixelated, grayscale image of the text 'Vx1'. The characters are rendered in a blocky, digital font style. The 'V' is the largest and most prominent, followed by a smaller 'x' and a '1'. The image has a low-resolution, dithered appearance with various shades of gray and black pixels.





*Example values:*

$$T_{J1} = 570^{\circ}\text{F (type J)}$$

$$V_{J1} = 16.266 \text{ mV}$$

$$T_{J2} = 69^{\circ}\text{F (type J)}$$

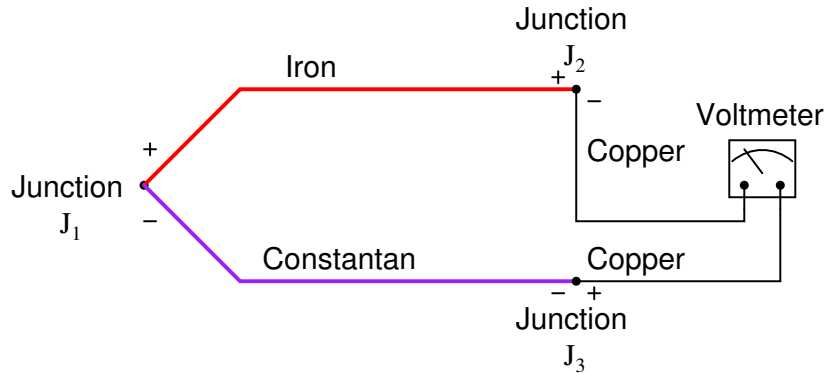
$$V_{J2} = 1.048 \text{ mV}$$

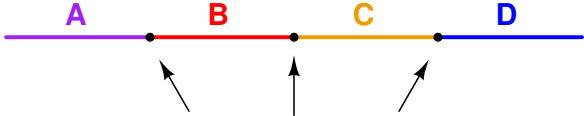
$$V_{rjc} = 1.048 \text{ mV}$$

$$V_{meter} = V_{J1} - V_{J2} + V_{rjc}$$

$$V_{meter} = 16.266 \text{ mV} - 1.048 \text{ mV} + 1.048 \text{ mV}$$

$$V_{meter} = \mathbf{16.266 \text{ mV (equivalent to } 570^{\circ}\text{F)}}$$





*If all junctions are at the same temperature, it is equivalent to . . .*



Junctions A-B-C-D

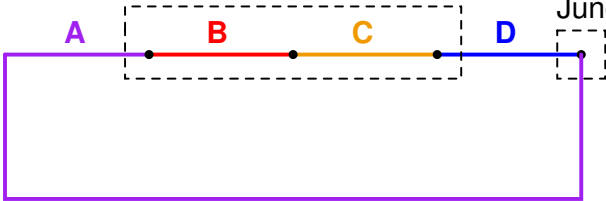
Junction D-A

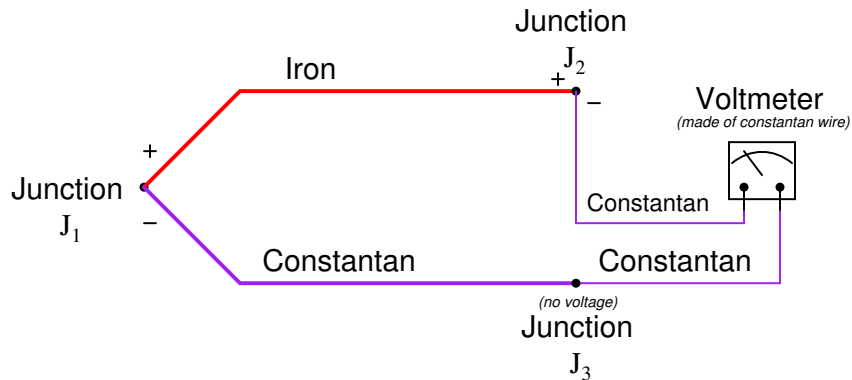
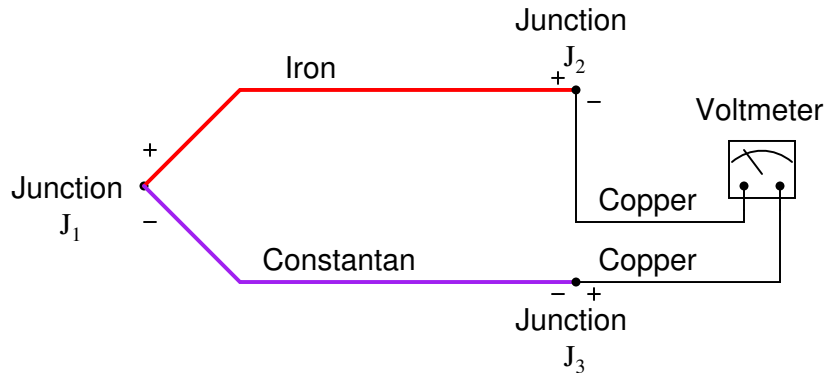
A

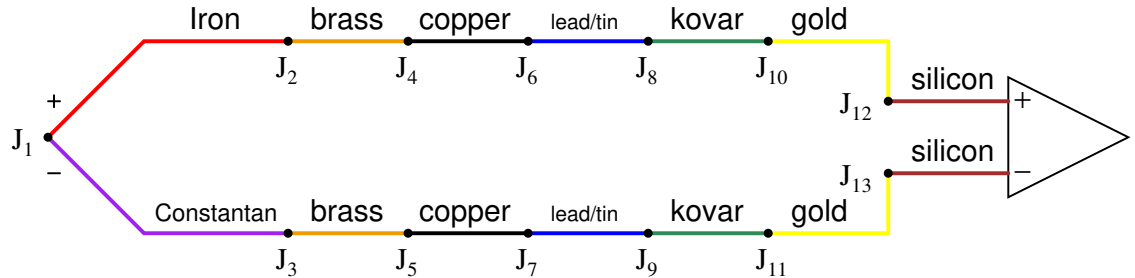
B

C

D









15



10



mpes

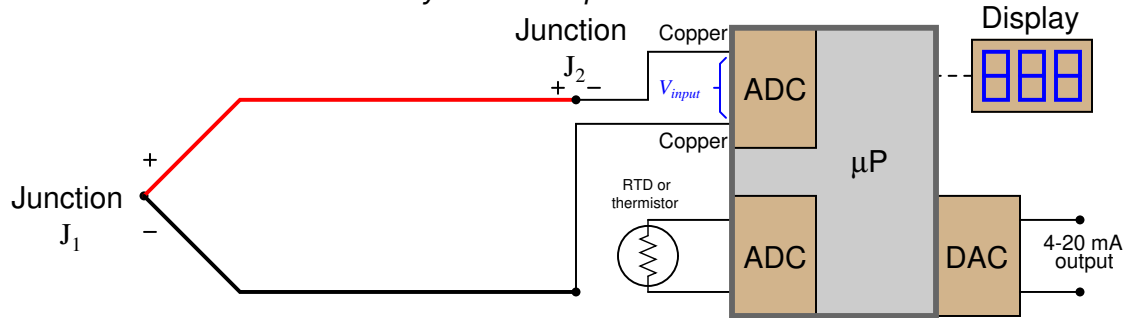
—

vx1

+

0

*Compensating for the effects of  $J_2$   
using a second input channel to sense  
ambient temperature and correcting  
mathematically in the computer*



*Vivamus* *et* *amemus* *et* *ludamus*

compensated total =  $V_{\text{mvt}} + V_{\text{sc}}$

$$\text{Component total} = \sqrt{v_1} + \sqrt{v_2}$$

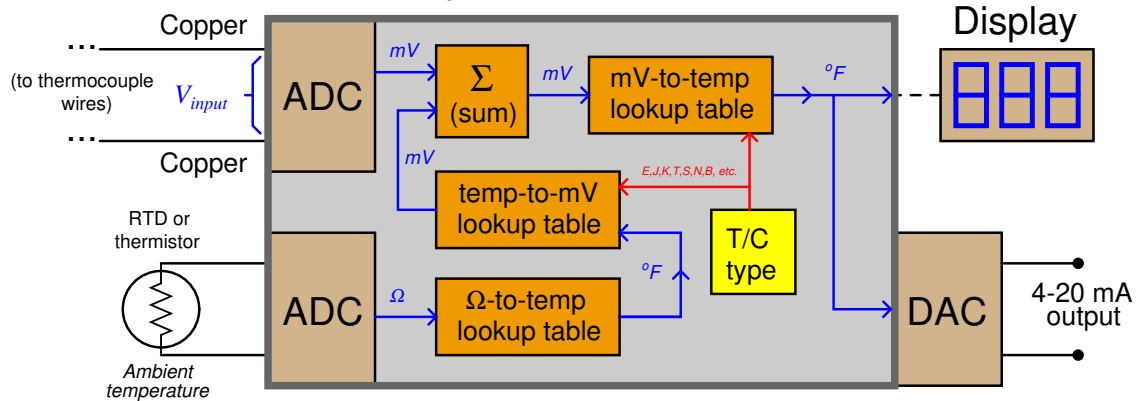
$$\text{compensated total} = V_1 - V_2 + V_3$$

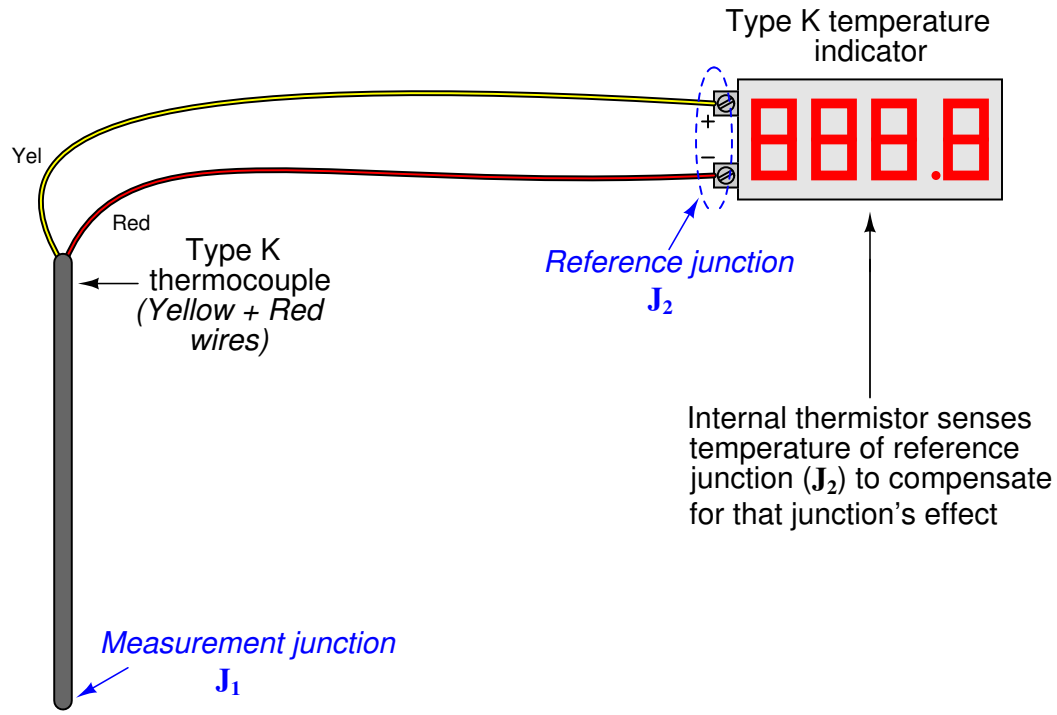


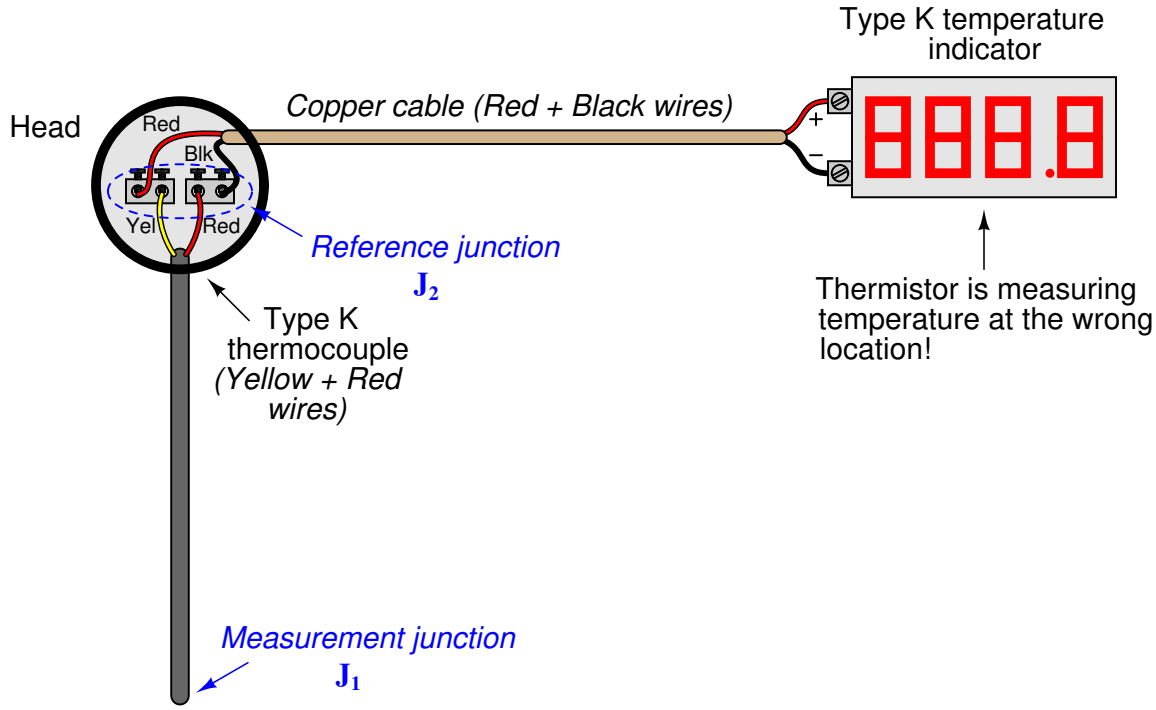
compensated total  $V_1 + 0$

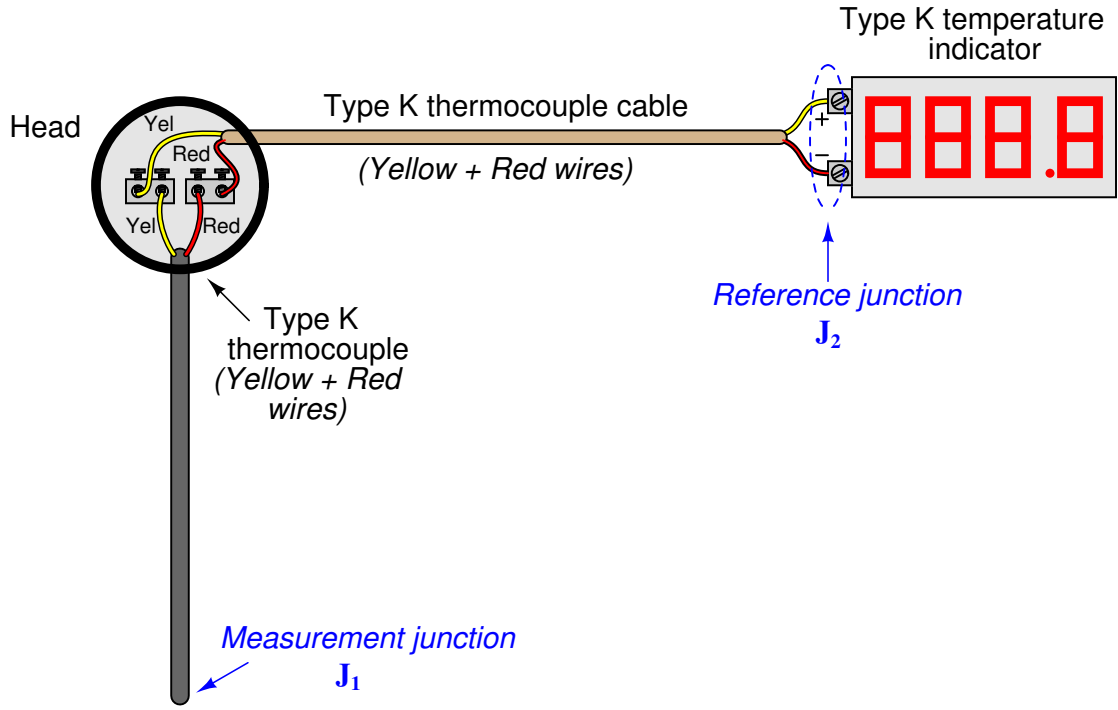
Computerized

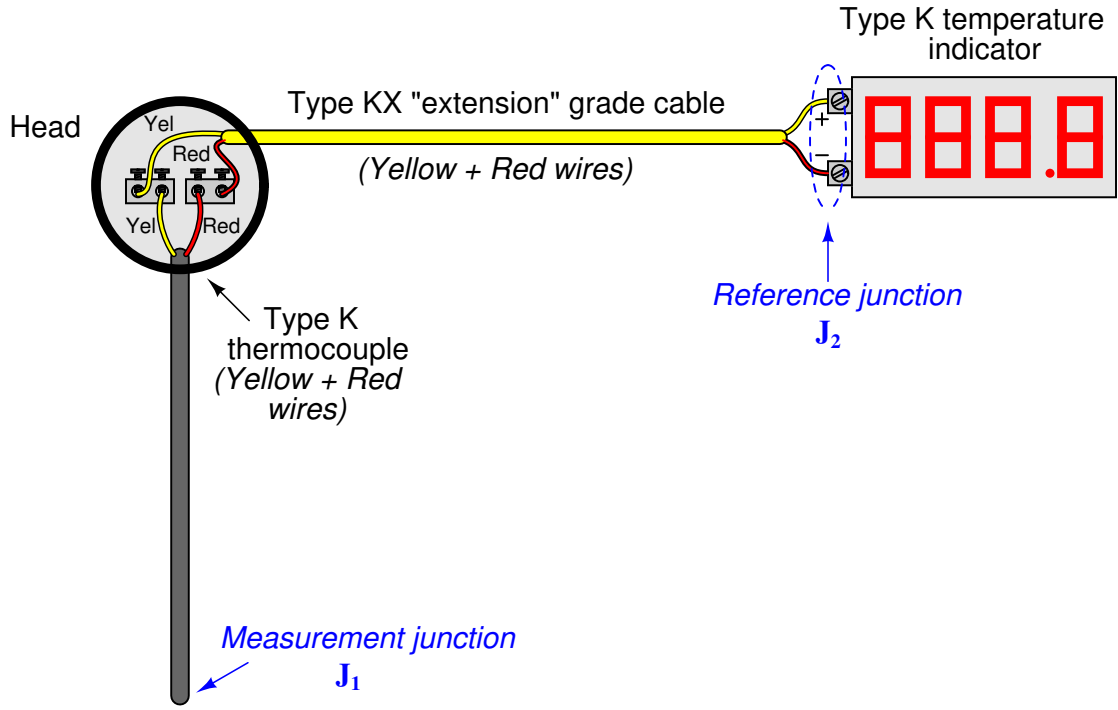
# Digital ("smart") thermocouple temperature transmitter

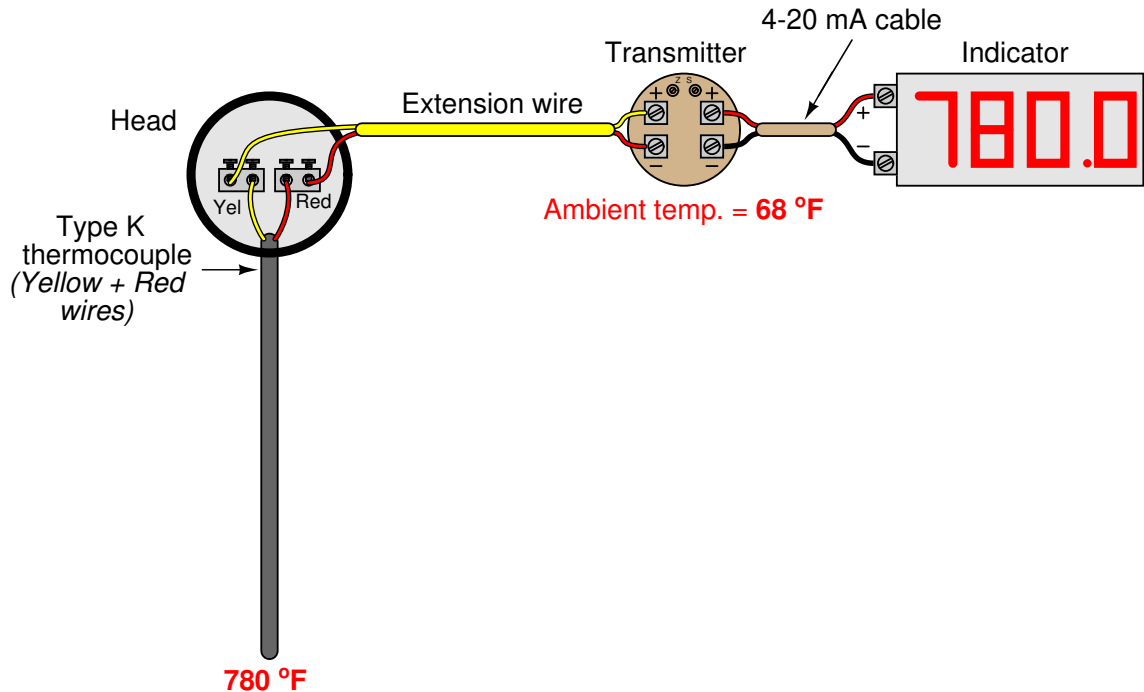




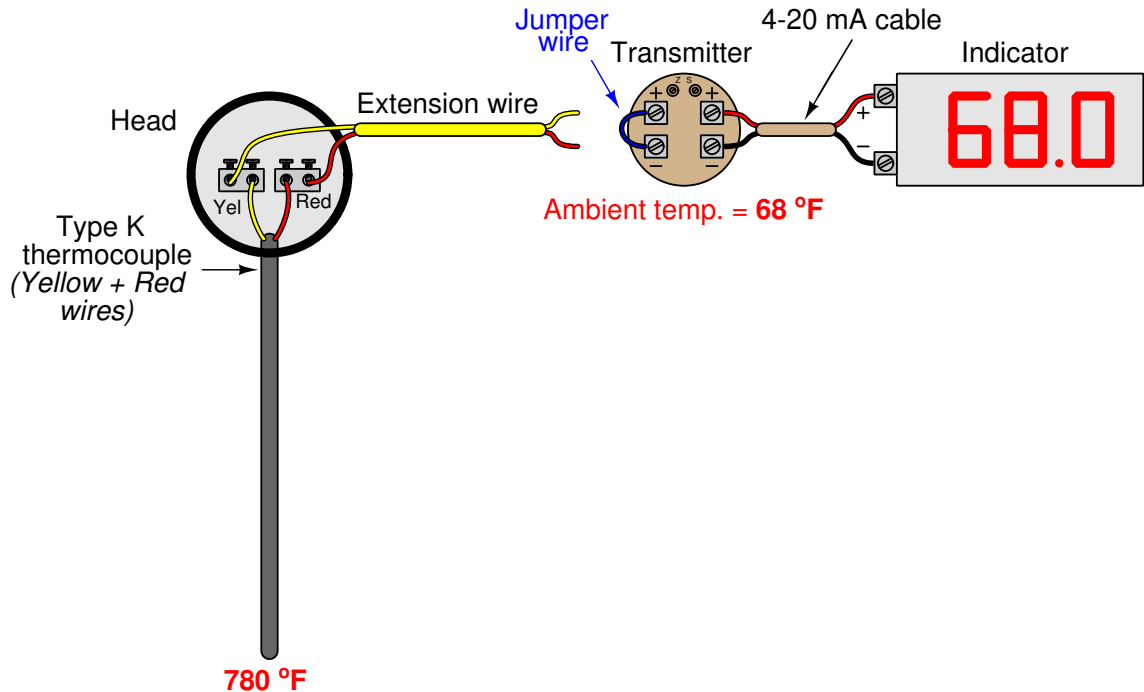












*never*

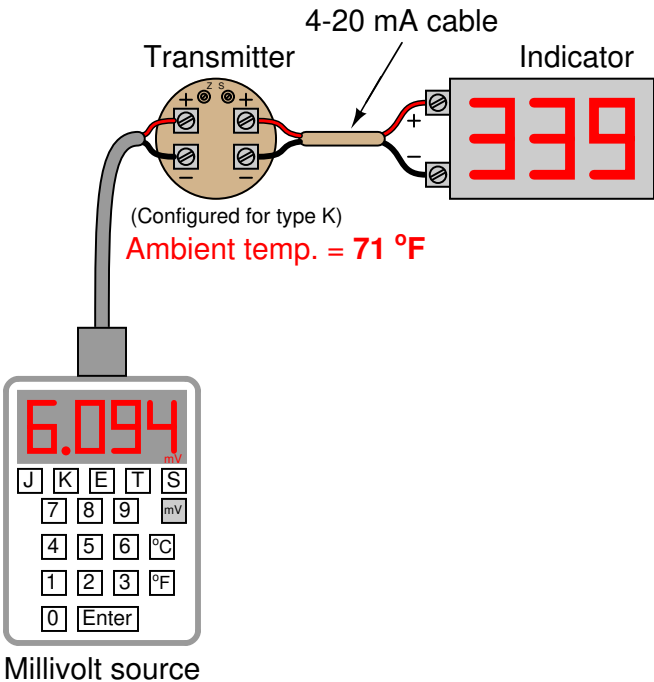
$= 0 +$

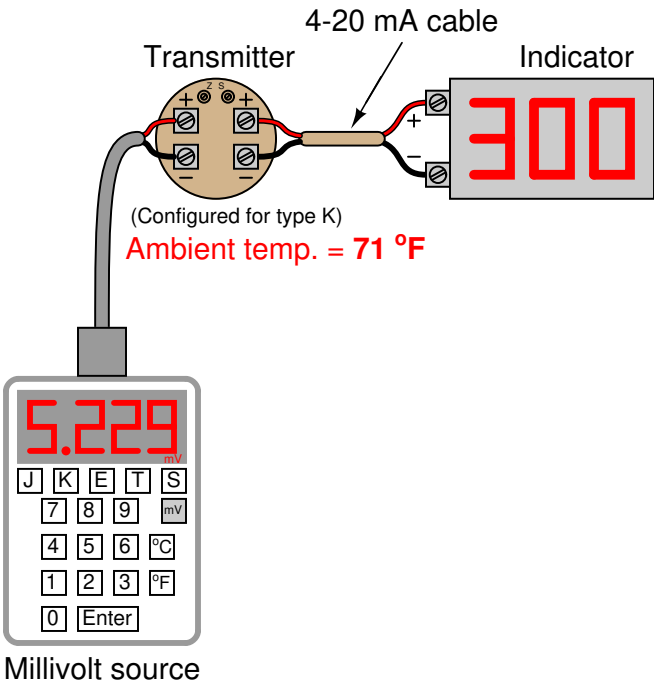
*xc*

never

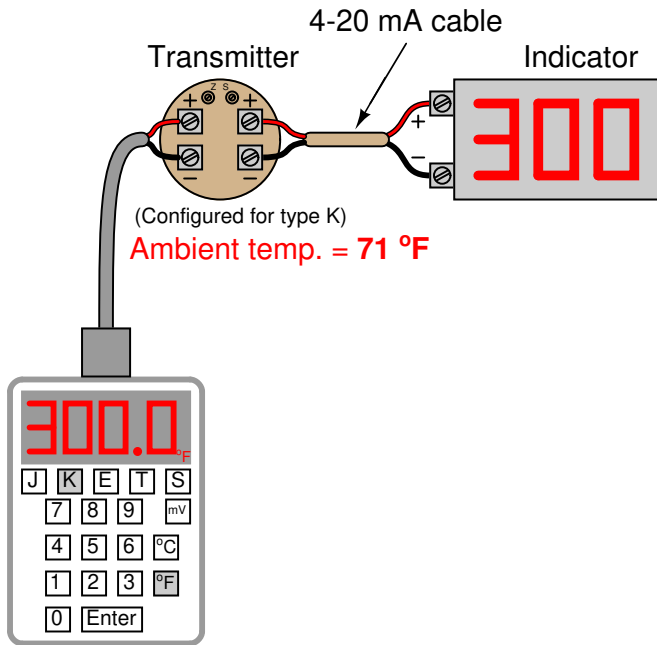


is









Thermocouple simulator

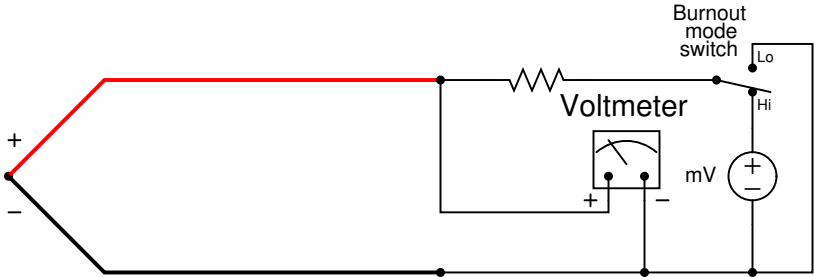
SOURCE

TC Type S

2650.0°F

Int. Ref. 70.8°F ITS-90 14.910mV==





$$\frac{dQ}{dt} = e\sigma AT^4$$











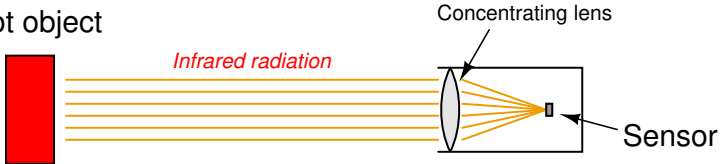




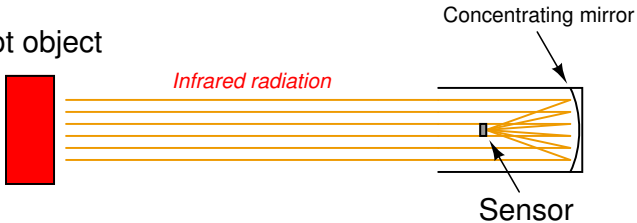


# Two designs of non-contact pyrometer

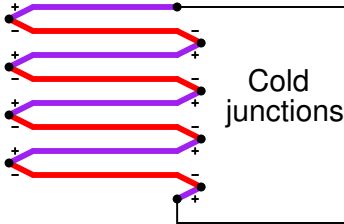
Hot object



Hot object



Hot  
junctions



Cold  
junctions

Thermopile output

Target temperature (K)	Millivolt output
4144 K	34.8 mV
3866 K	26.6 mV
3589 K	19.7 mV
3311 K	14.0 mV
3033 K	9.9 mV
2755 K	6.6 mV
2478 K	4.2 mV
2200 K	2.5 mV
1922 K	1.4 mV
1644 K	0.7 mV

4144 K

---

3033 K

=

1.3663

$$\left(\frac{4144\text{ K}}{3033\text{ K}}\right)^4 = 1.3663^4 = 3.485$$

345/99 IDV 345 IDV









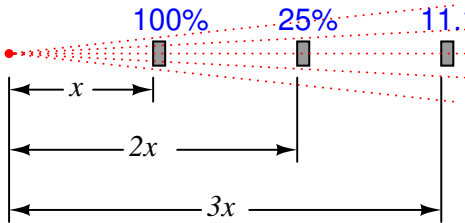
*Relative power received at sensors*

100%

25%

11.1%

Point-source  
of radiation



A

=

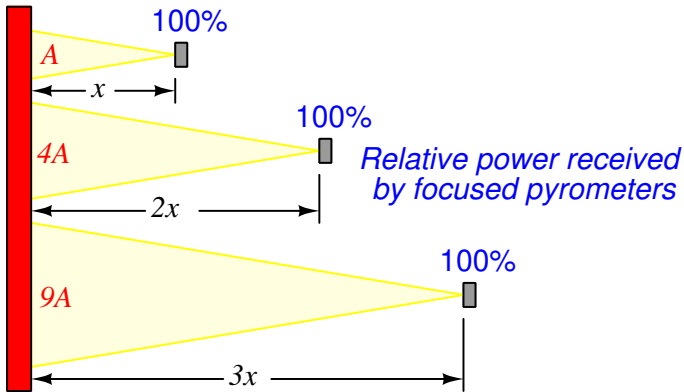
$\pi D^2$

\_\_\_\_\_

4

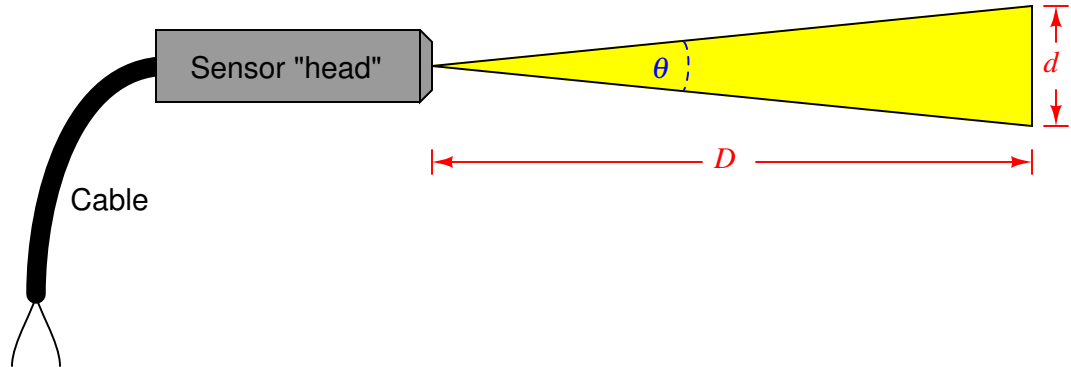


Target object  
(e.g. furnace wall)



*5:1 Field-Of-View (FOV)  
11° viewing angle*

$$\frac{D}{d} = \frac{5}{1} \quad \theta \approx 11^\circ$$









$$\frac{D}{d} = \frac{1}{2 \tan \left( \frac{\theta}{2} \right)}$$

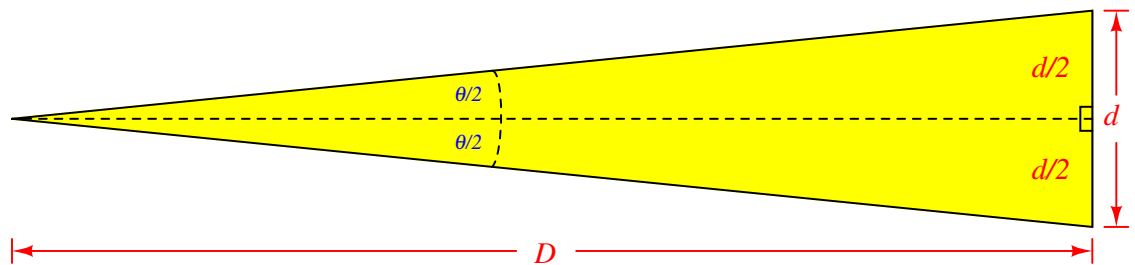
$$\theta = 2 \tan^{-1} \left( \frac{d}{2D} \right)$$

Distance ratio	Angle (approximate)
1:1	53°
2:1	30°
3:1	19°
5:1	11°
7:1	8°
10:1	6°









$$\tan\left(\frac{\theta}{2}\right) = \frac{d/2}{D} = \frac{d}{2D}$$



$$\tan\left(\frac{\theta}{2}\right) = \frac{d}{2D}$$

$$\frac{2D}{d} = \frac{1}{\tan\left(\frac{\theta}{2}\right)}$$

$$\frac{D}{d} = \frac{1}{2 \tan \left( \frac{\theta}{2} \right)}$$

$$\tan^{-1}\left[\tan\left(\frac{\theta}{2}\right)\right]=\tan^{-1}\left(\frac{d}{2D}\right)$$

$$\frac{\theta}{2} = \tan^{-1} \left( \frac{d}{2D} \right)$$

$$\theta = 2 \tan^{-1} \left( \frac{d}{2D} \right)$$

°F

152



68.1

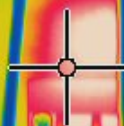
 **FLIR**

Dist = 3.4 Trefl = 122  $\epsilon$  = 0.95

Spot 145  
Difference  
Sp - Ref 84.7

°F

149



 FLIR

Dist = 3.4 Trefl = 122  $\epsilon$  = 0.95

74.7



Spot 68.4 °F

68.6

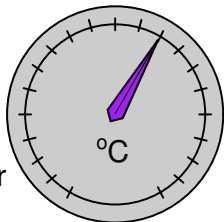


**FLIR**

Dist = 1.0 Trefl = 68.0  $\epsilon$  = 0.95

61.3

Thermometer



Compression fitting

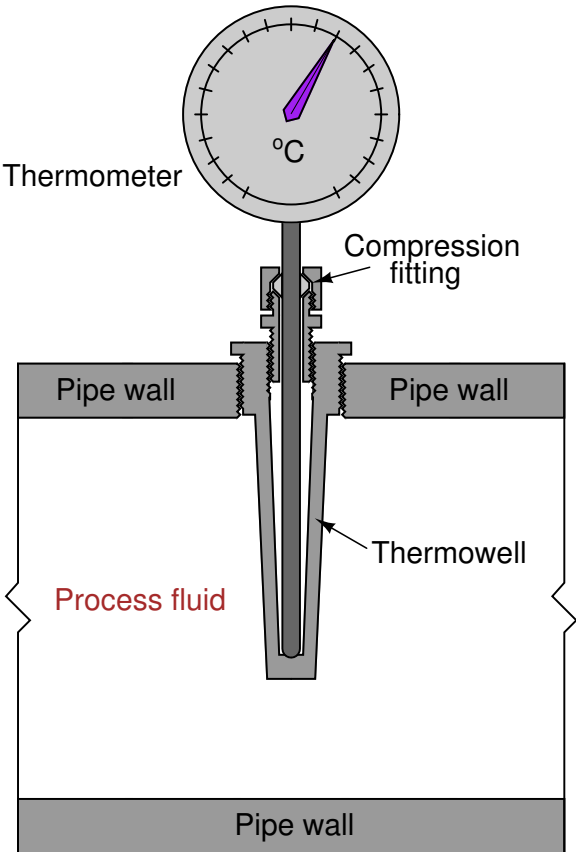
Pipe wall

Pipe wall

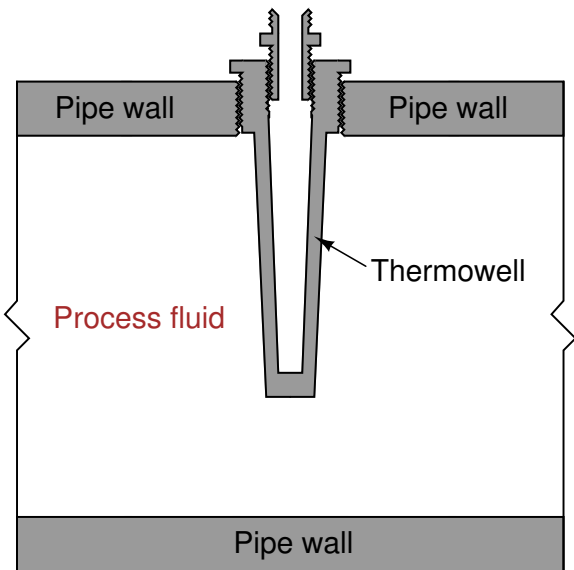
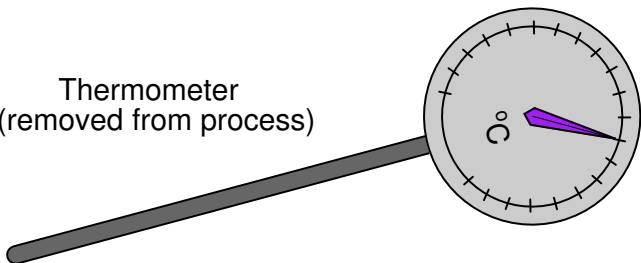
Thermowell

Process fluid

Pipe wall



Thermometer  
(removed from process)











do

---

di

=

eo

Adi





