Modeling CrIS Nonlinearity **** DRAFT ****

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October 5, 2016

We consider the definition of reference truth for measurements made with a Michelson interferometer, taking into account relatively small (or possibly non-existant) effects such as filter position and potential mathematical artifacts. The immediate application is defining reference truth and a corresponding calibration equation for the for the CrIS instrument.

1 Michelson Interferometer

Figure 1 shows a basic Michelson interferometer. Let $r_{\rm in}(\nu)$ be incoming radiance as a function of frequency ν , δ mirror displacement, and $r_{\rm out}(\nu,\delta)$ radiance on the path to the detector. In practice the signal from the detector is the product of incoming radiance, beam-splitter efficiency, and detector responsivity. But suppose for the moment that we have a perfect beam splitter and mirrors, and that there are no filters. Then radiance $r_{\rm out}$ on the path to the detector can be represented as

$$r_{\text{out}}(\nu, \delta) = r_{\text{in}}(\nu)(1 + \cos 2\pi\nu\delta)/2 \tag{1}$$

including a term $r_{\rm in}(\nu)/2$ that depends only on ν . Integrating over frequency, we have

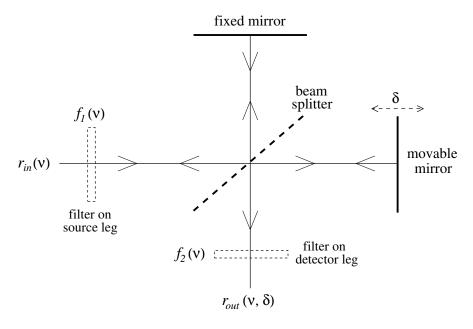


Figure 1: Michelson interferometer with filters

$$r_{\text{out}}(\delta) = \frac{1}{2} \int_{\nu=0}^{\inf} r_{\text{in}}(\nu) d\nu + \frac{1}{2} \int_{\nu=0}^{\inf} r_{\text{in}}(\nu) \cos(2\pi\nu\delta) d\nu$$
 (2)

This is the continuous interferogram as a function of displacement δ . We want the consider the AC' and DC components separately.

$$r_{\text{\tiny DC}}(\delta) = \frac{1}{2} \int_{\nu=0}^{\inf} r_{\text{\tiny in}}(\nu) d\nu, \quad r_{\text{\tiny AC}}(\delta) = \frac{1}{2} \int_{\nu=0}^{\inf} r_{\text{\tiny in}}(\nu) \cos(2\pi\nu\delta) d\nu \tag{3}$$

 $r_{\mbox{\tiny DC}}$ is a function of the scene, while $r_{\mbox{\tiny AC}}$ is a function of both the scene and mirror position. For $\delta=0$ (zero mirror displacement) the two terms are identical.

Figure 2 shows sample transfer functions, taking radiance to voltage. $G_1(r)$ and $G_2(r)$ are linear, of the form G(r) = br + c, for some b and c. For CrIS c is Vinst, a DC bias value, while b depends on analog gain and detector properties. $G_3(r)$ is a plausible arbitrary nonlinear transfer function.

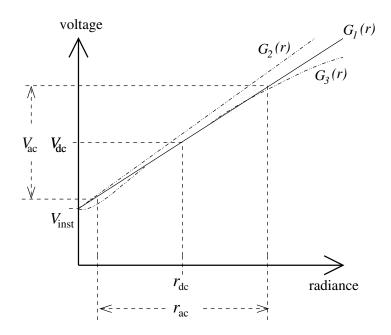


Figure 2: Gain Function