

2 CrIS reference truth

We can derive a definition of reference truth from a basic form of the CrIS calibration equation, with details depending on assumptions about instrument behavior. Suppose r_{es} is high resolution earth scene radiance, r_{ict} high resolution black-body radiance from the internal calibration target, ρ instrument responsivity, and R resampling from high resolution to the instrument sensor grid, $dv = 1/(2 \text{ OPD})$, where OPD is the maximum optical path difference.

If r is some arbitrary high resolution radiance, we might expect that $R\rho r \approx \rho Rr$. Figure 2 shows the difference for a typical earth scene, and figure 3 the difference for an ICT (black body) look. Suppose we interpret this as $R\rho r_{\text{ict}} \approx \rho Rr_{\text{ict}}$ for ICT looks, but $R\rho r_{\text{es}} \neq \rho Rr_{\text{es}}$ for earth scenes. Calibration of the on-axis optical path of a Michaelson interferometer can be represented as

$$r_{\text{cal}}^{\text{LR}} = r_{\text{ict}}^{\text{LR}} \frac{ES - SP}{IT - SP} \quad (7)$$

where $r_{\text{cal}}^{\text{LR}}$ is calibrated radiances, $r_{\text{ict}}^{\text{LR}}$ is expected radiance from the internal calibration target, and ES , IT , and SP are uncalibrated spectra for earth scene, internal calibration target, and space looks, respectively. Note that all values in equation 7 are at the “sensor grid” $dv = 1/(2 \text{ OPD})$.

Let $ES \approx R\rho(r_{\text{es}} + r_{\text{sp}})$, $IT \approx R\rho(r_{\text{ict}} + r_{\text{sp}})$, and $SP \approx R\rho r_{\text{sp}}$, where r_{es} , r_{ict} , and r_{sp} are high resolution approximations to the true radiances, ρ is responsivity, and R is resampling from the high resolution to the sensor grid dv . Let $r_{\text{ict}}^{\text{LR}} = R(r_{\text{ict}})$. Substituting this into (7) gives

$$\begin{aligned} r_{\text{cal}}^{\text{LR}} &\approx r_{\text{ict}}^{\text{LR}} \frac{R\rho(r_{\text{es}} + r_{\text{sp}}) - R\rho r_{\text{sp}}}{R\rho(r_{\text{ict}} + r_{\text{sp}}) - R\rho r_{\text{sp}}} \\ &= r_{\text{ict}}^{\text{LR}} \frac{R\rho r_{\text{es}}}{R\rho r_{\text{ict}}} \end{aligned} \quad (8)$$

$$\approx r_{\text{ict}}^{\text{LR}} \frac{R\rho r_{\text{es}}}{\rho Rr_{\text{ict}}} \quad (9)$$

$$= \frac{R\rho r_{\text{es}}}{\rho} = r_{\text{resp}} \quad (10)$$

We go from equation 8 to 9 because we have assumed responsivity commutes at least approximately with resampling for the ICT look. Equation 10 is the