

第8章 场效应晶体管(FETs)

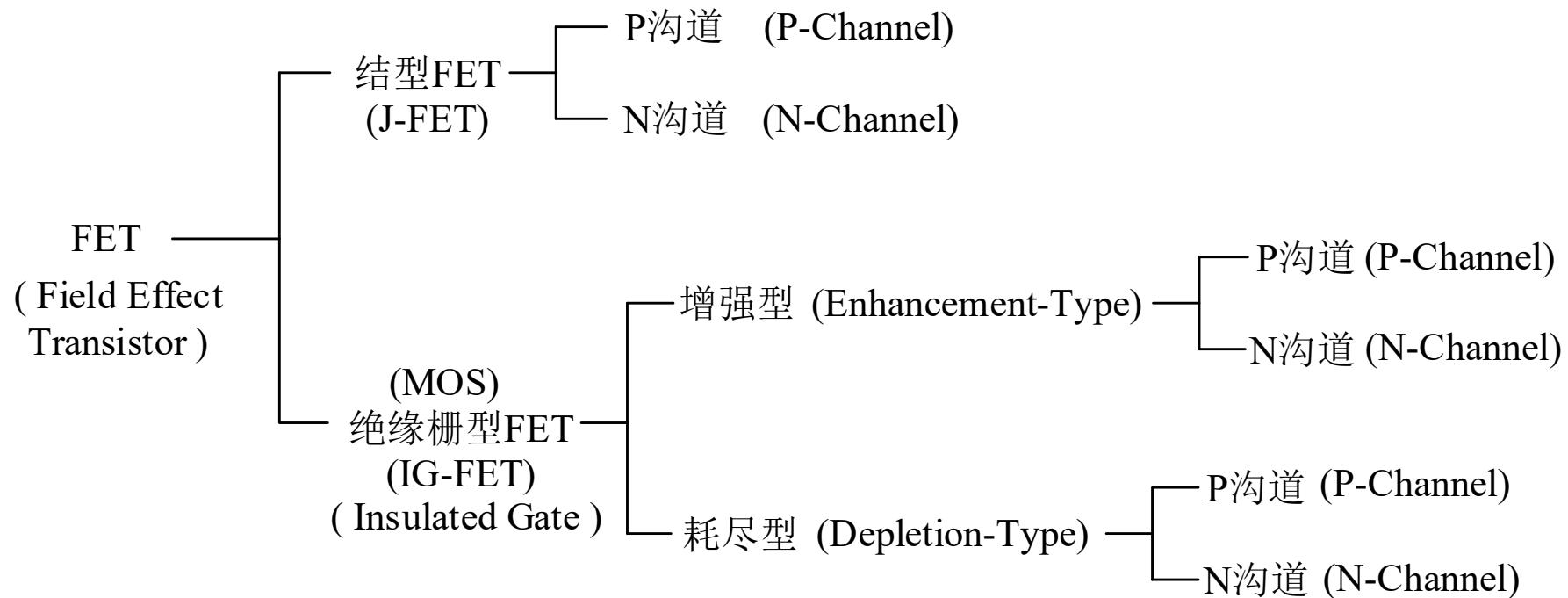
场效应晶体管基础

场效应晶体管放大电路的构成及其分析

8.1 场效应晶体管基础

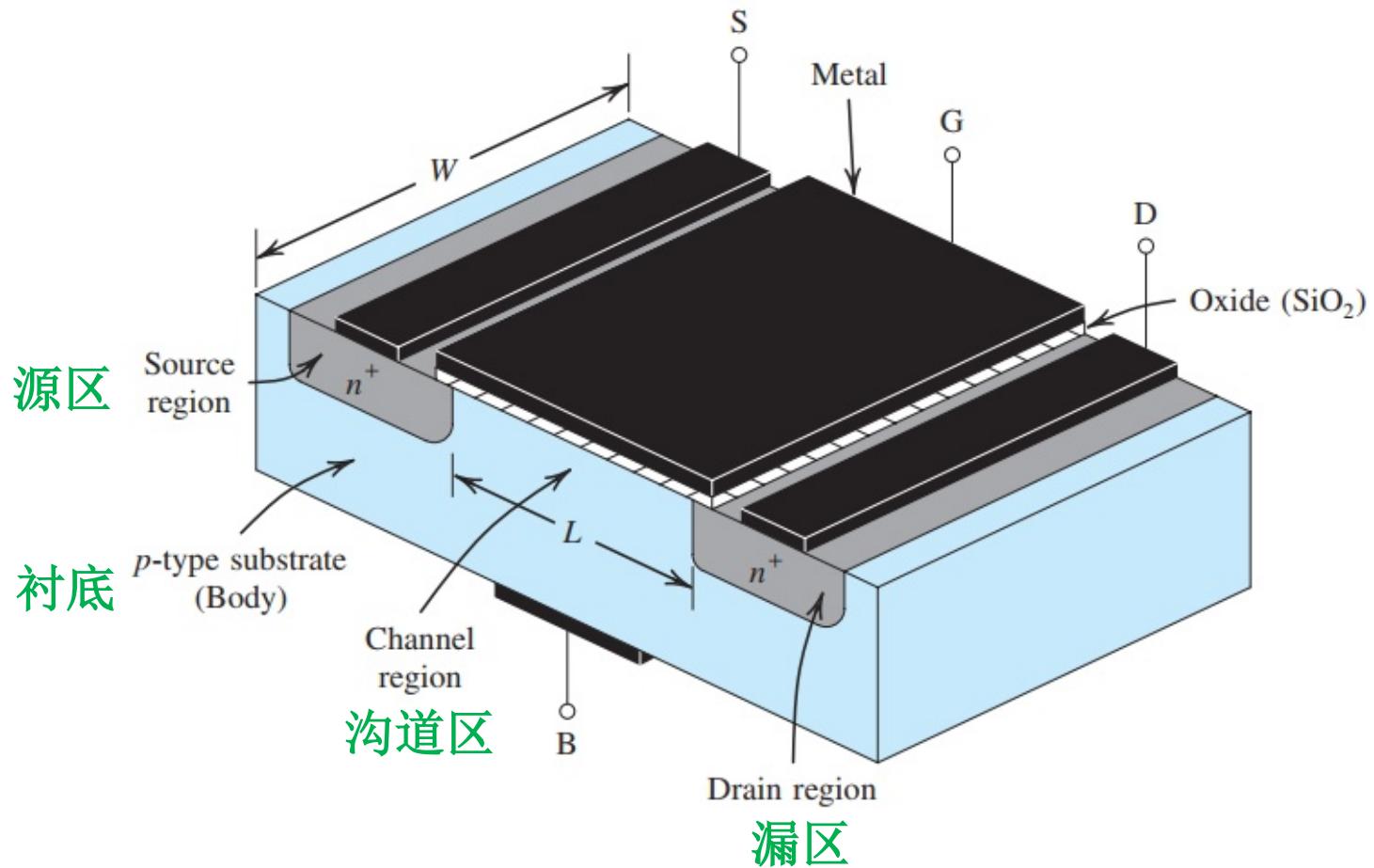
8.1.1 场效应晶体管的结构、工作原理及其电路符号

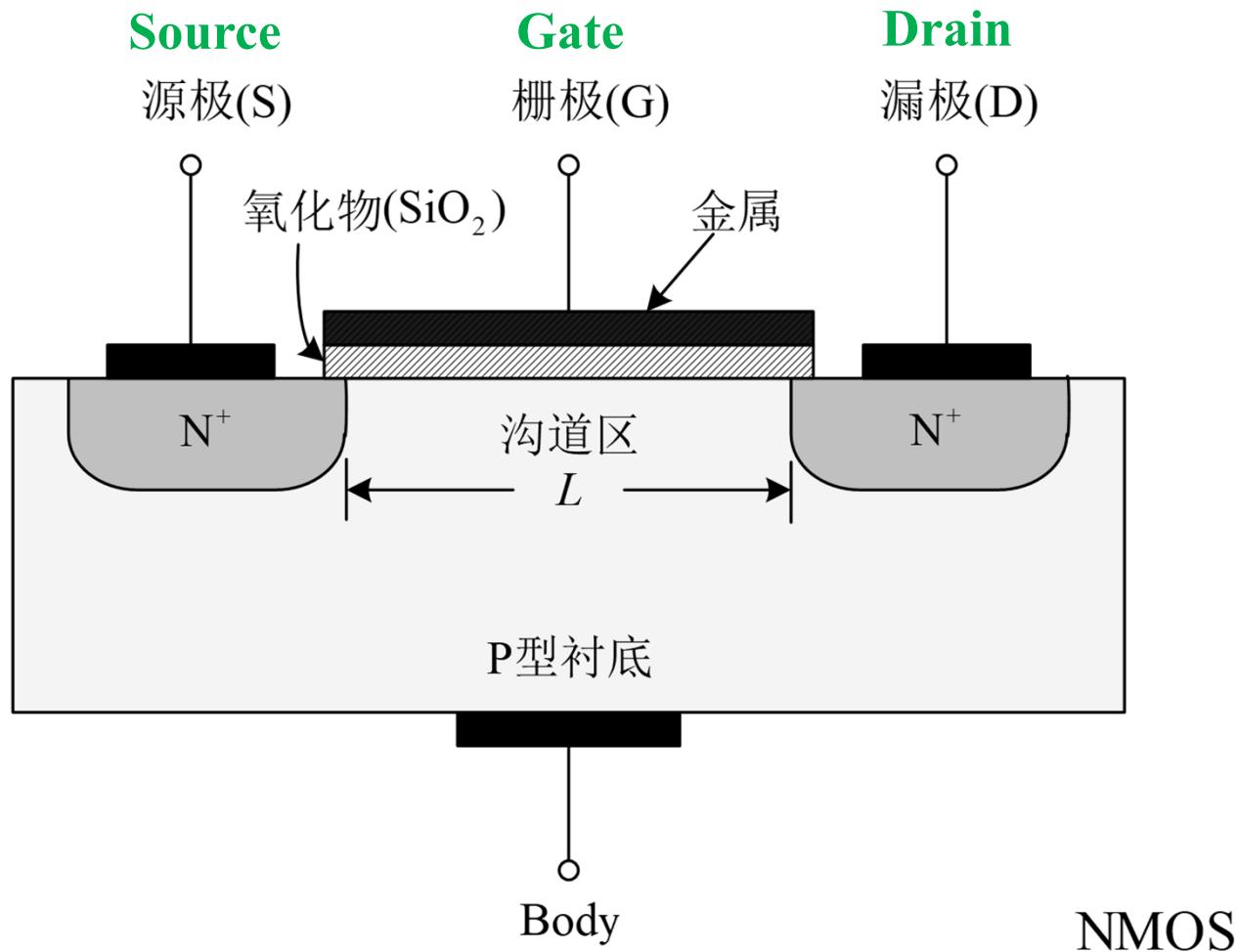
单极型管：噪声小、抗辐射能力强、低电压工作

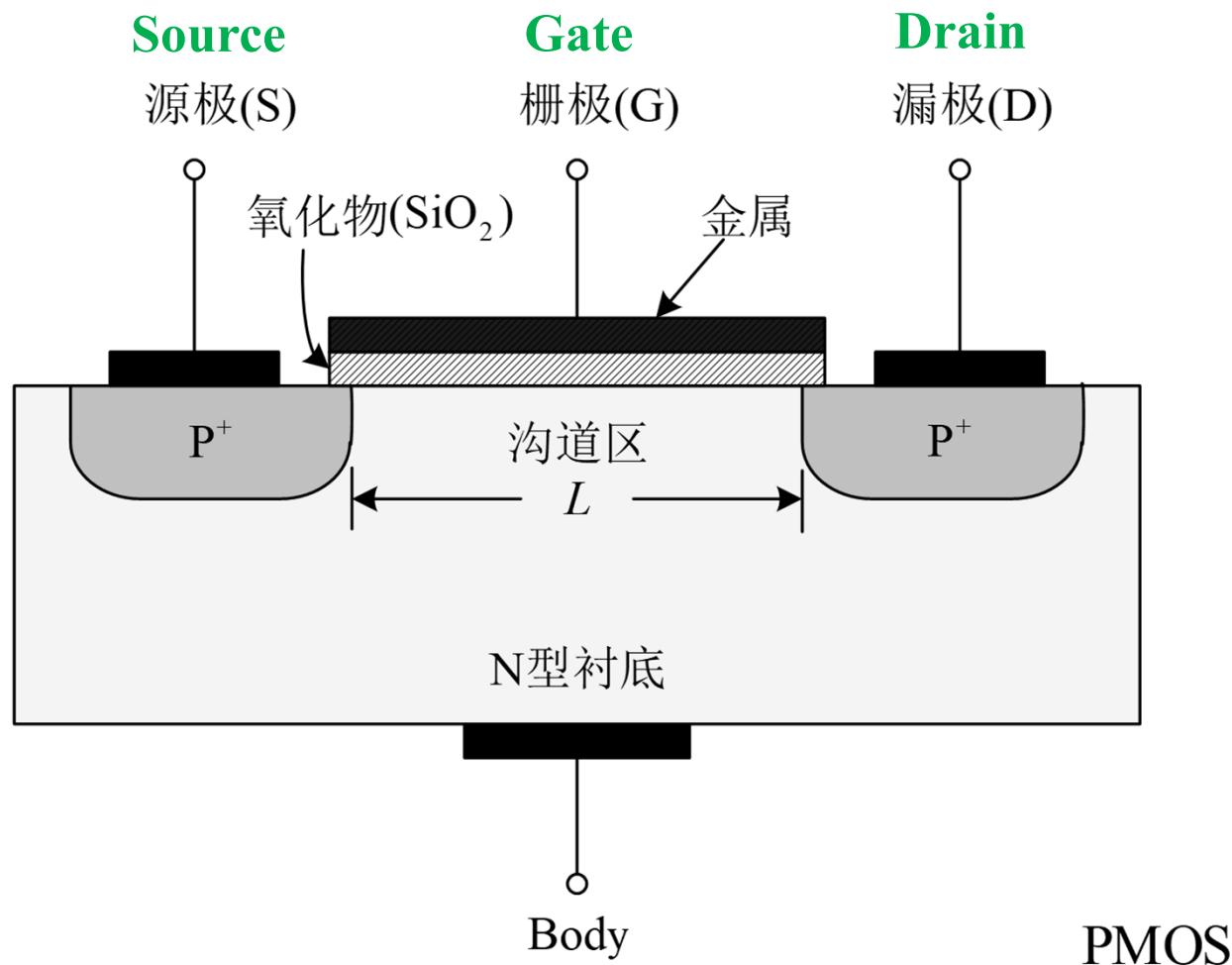


一、场效应晶体管的结构

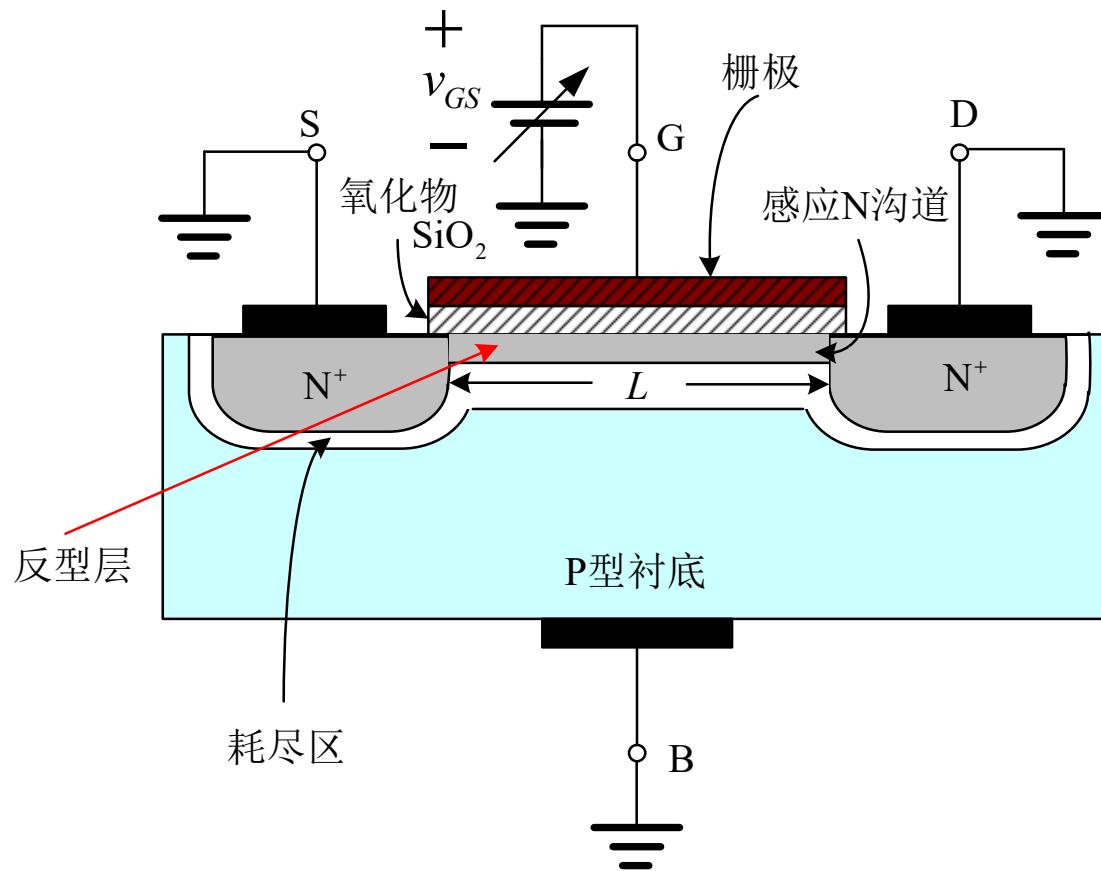
1、绝缘栅型场效应晶体管的结构



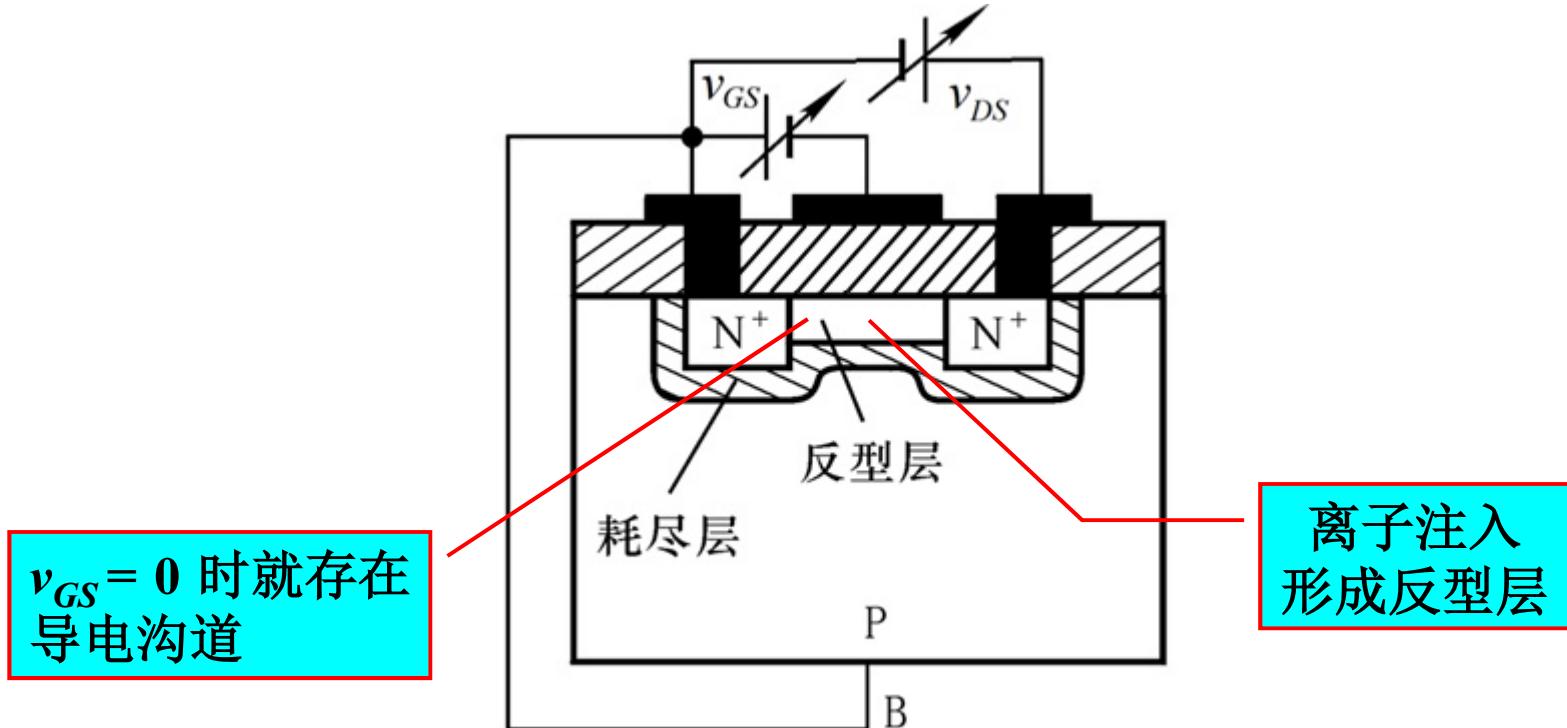




(a) N沟道增强型



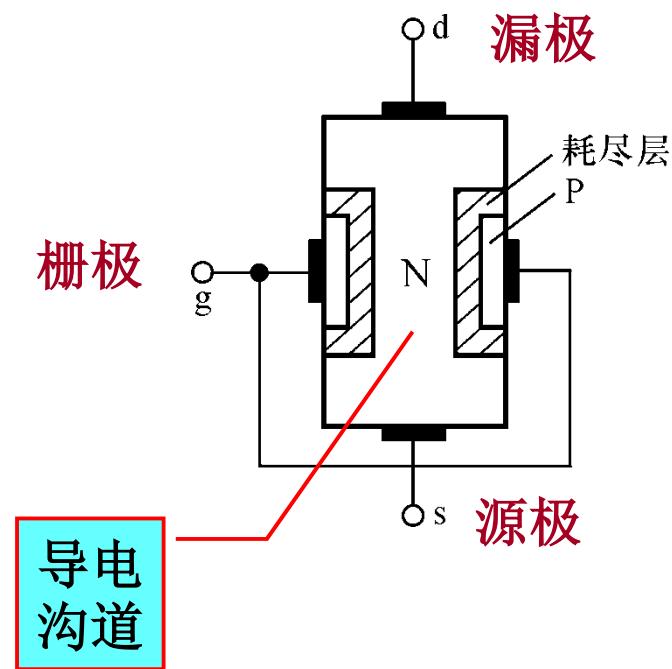
(b) N沟道耗尽型



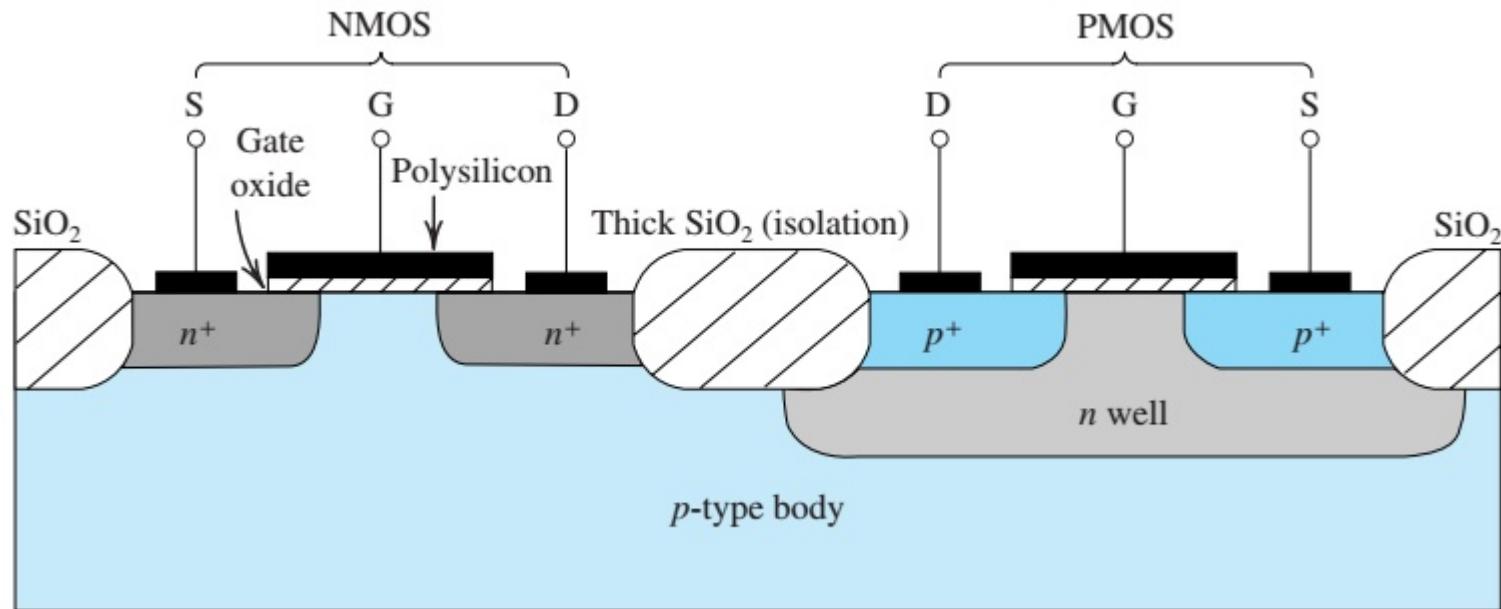
耗尽型NMOS管在 $V_{GS} > 0$ 、 $V_{GS} < 0$ 、 $V_{GS} = 0$ 时均可存在导电沟道。

2、结型（Junciton-FET）场效应管的结构

N沟道结型
场效应晶体管



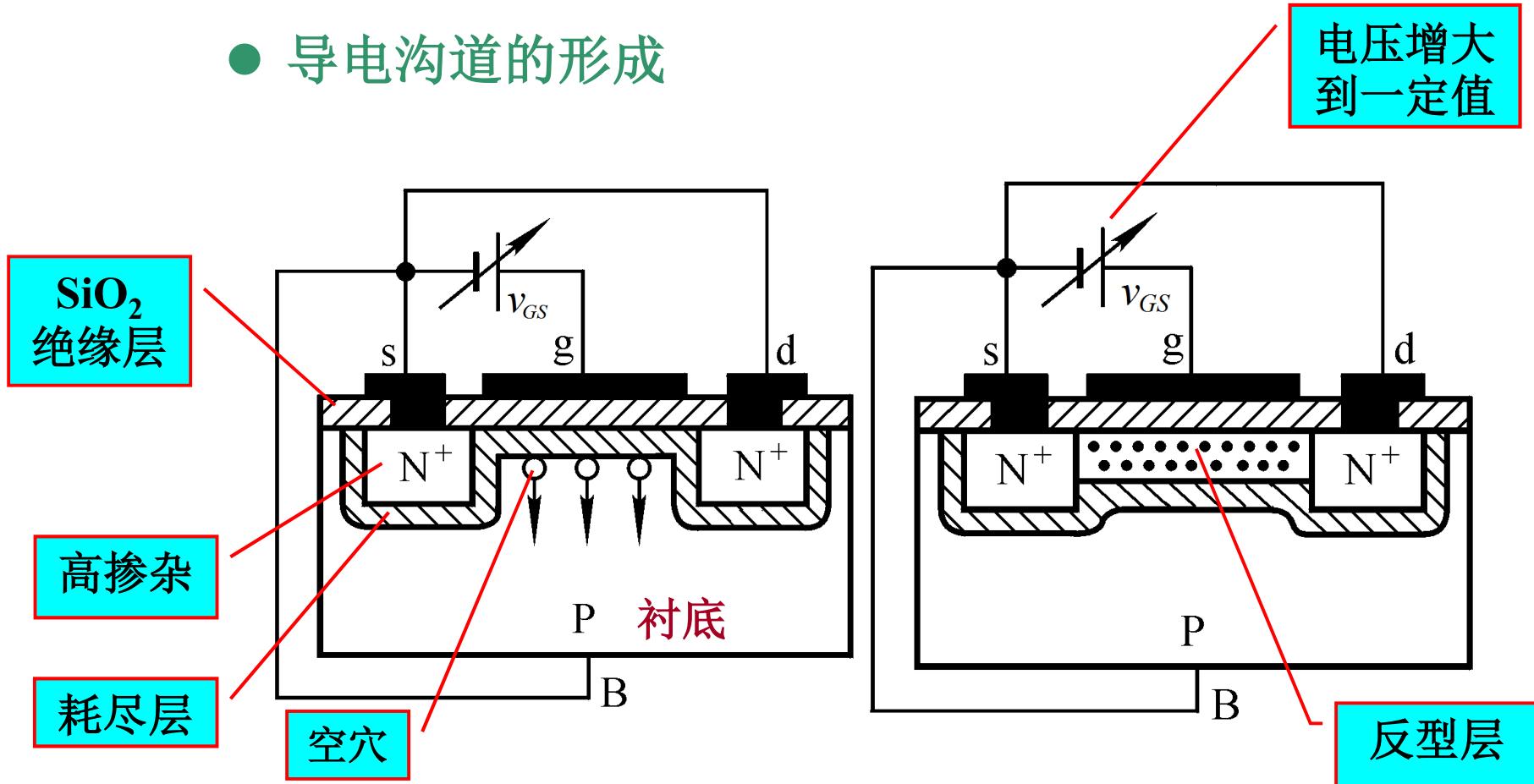
3、Complementary MOS (CMOS) 的结构



二、场效应晶体管的工作原理

1、N沟道增强型MOSFET的工作原理

● 导电沟道的形成

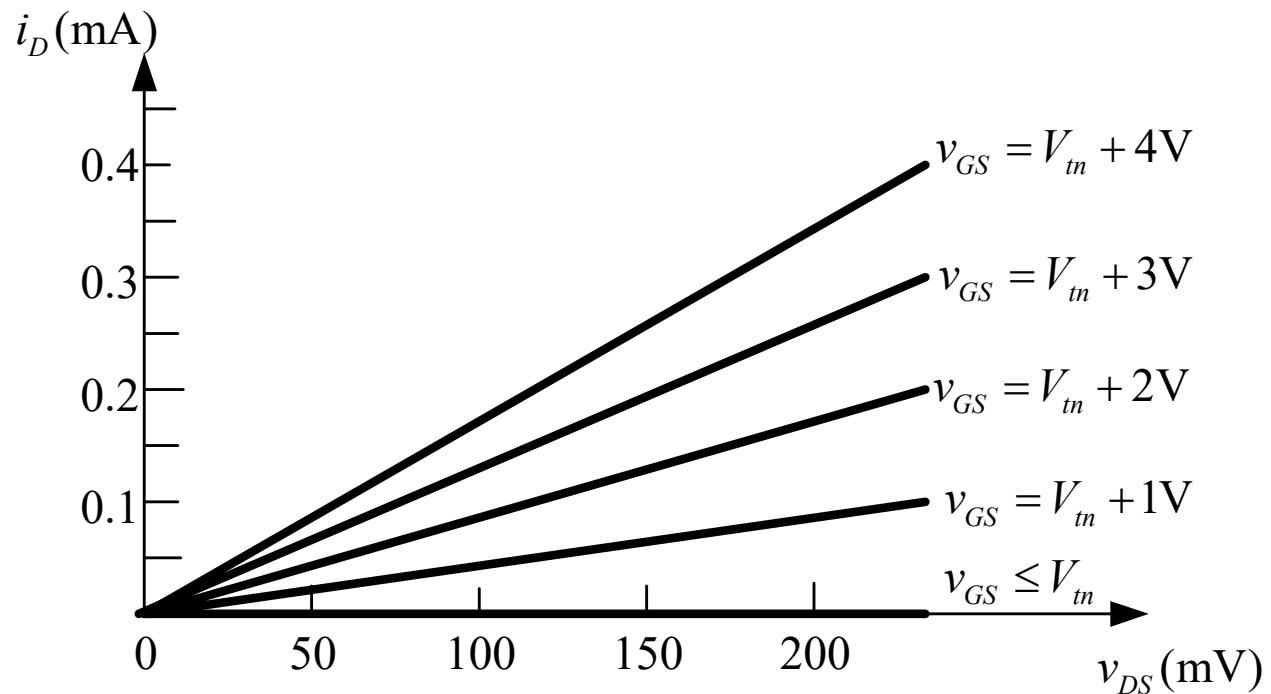


V_{GS} 增大，N型反型层将变厚变长。当反型层将两个N区相接时，形成N型导电沟道（简称N沟道）。

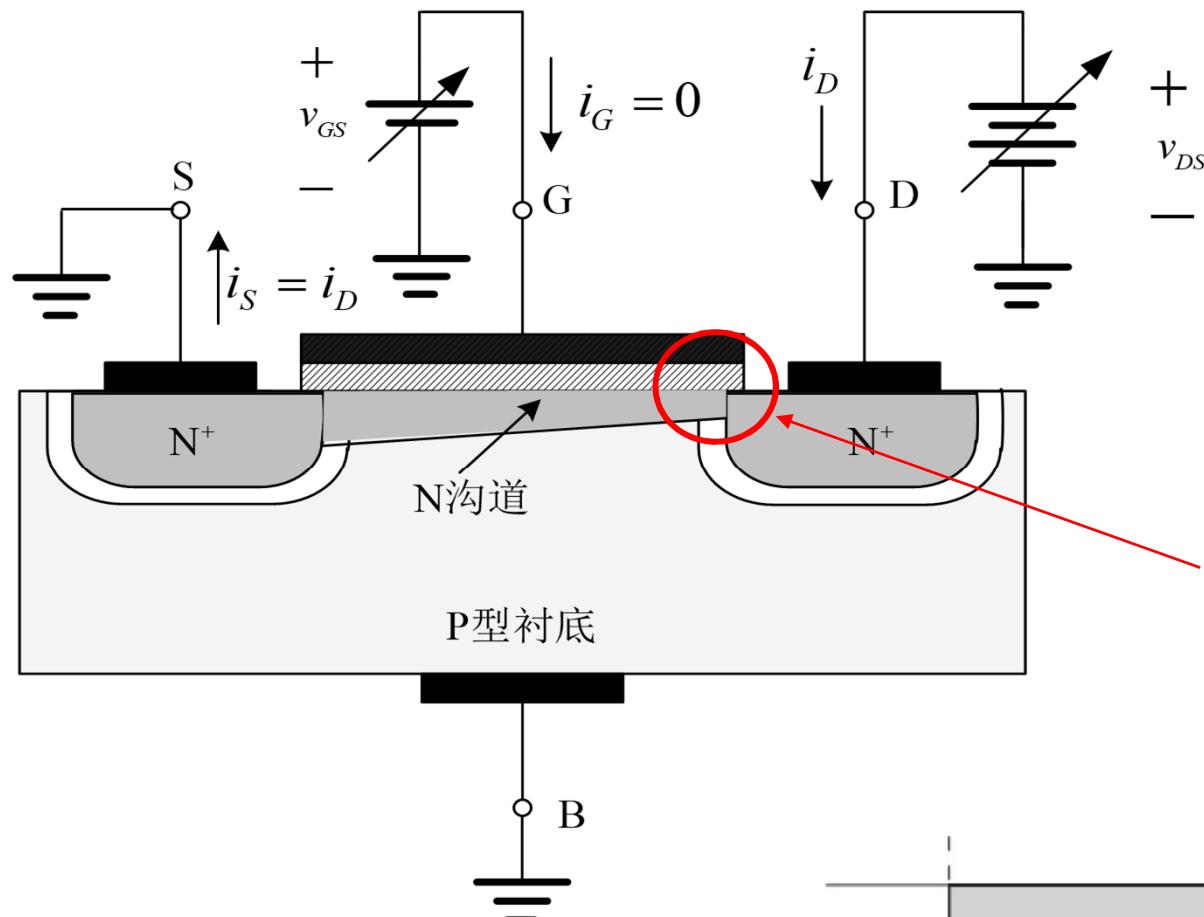
特点：

- (1) 由电子形成的反型层称N沟道，对应为NMOS；由空穴构成的反型层称P沟道，对应为PMOS。
- (2) 对于NMOS，反型层形成的先决条件是 $v_{GS} > V_{tn}$ (开启电压，阈值电压， threshold voltage)。 V_{tn} 的大小取决于场效应管的工艺参数。 SiO_2 绝缘层越薄，两N⁺区的掺杂浓度越高，衬底掺杂浓度越低， V_{tn} 就越小。
- (3) 对于NMOS， v_{GS} 越大，反型层的电子浓度就越大，沟道的导电能力也就越强，在同样的 v_{DS} 作用下，漏极与源极之间的电流相应也越大。
- (4) 如果在源漏间加上一个小电压（如100 ~ 200 mV），沟道呈电阻特性。

增强型NMOS管在很小的 v_{DS} 作用下的伏安特性

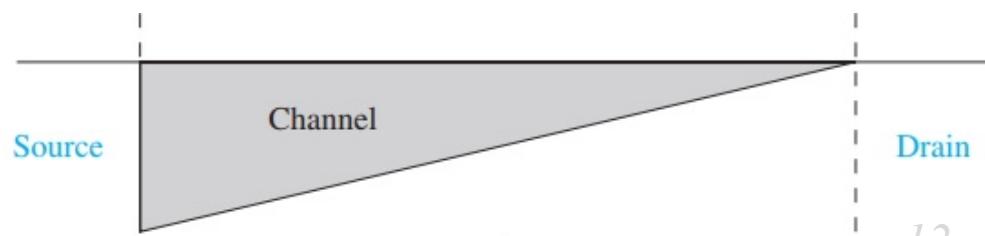


● 沟道夹断 (channel pinch-off)



当该点电压减小到
 $v_{GD} = v_{GS} - v_{DS} = V_{tn}$

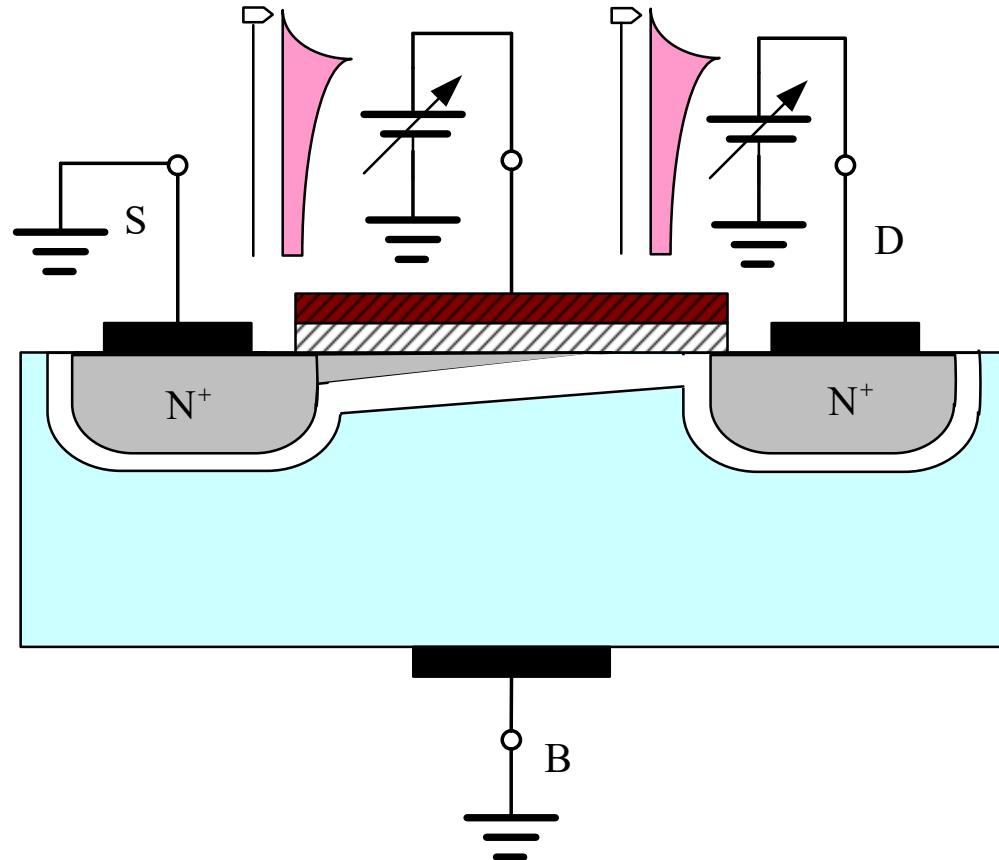
发生沟道夹断



当 $v_{DS} \geq v_{GS} - V_{tn}$ 时，如果继续升高漏极电压，漏极电流达到饱和，不再随漏极电压的升高而增大。

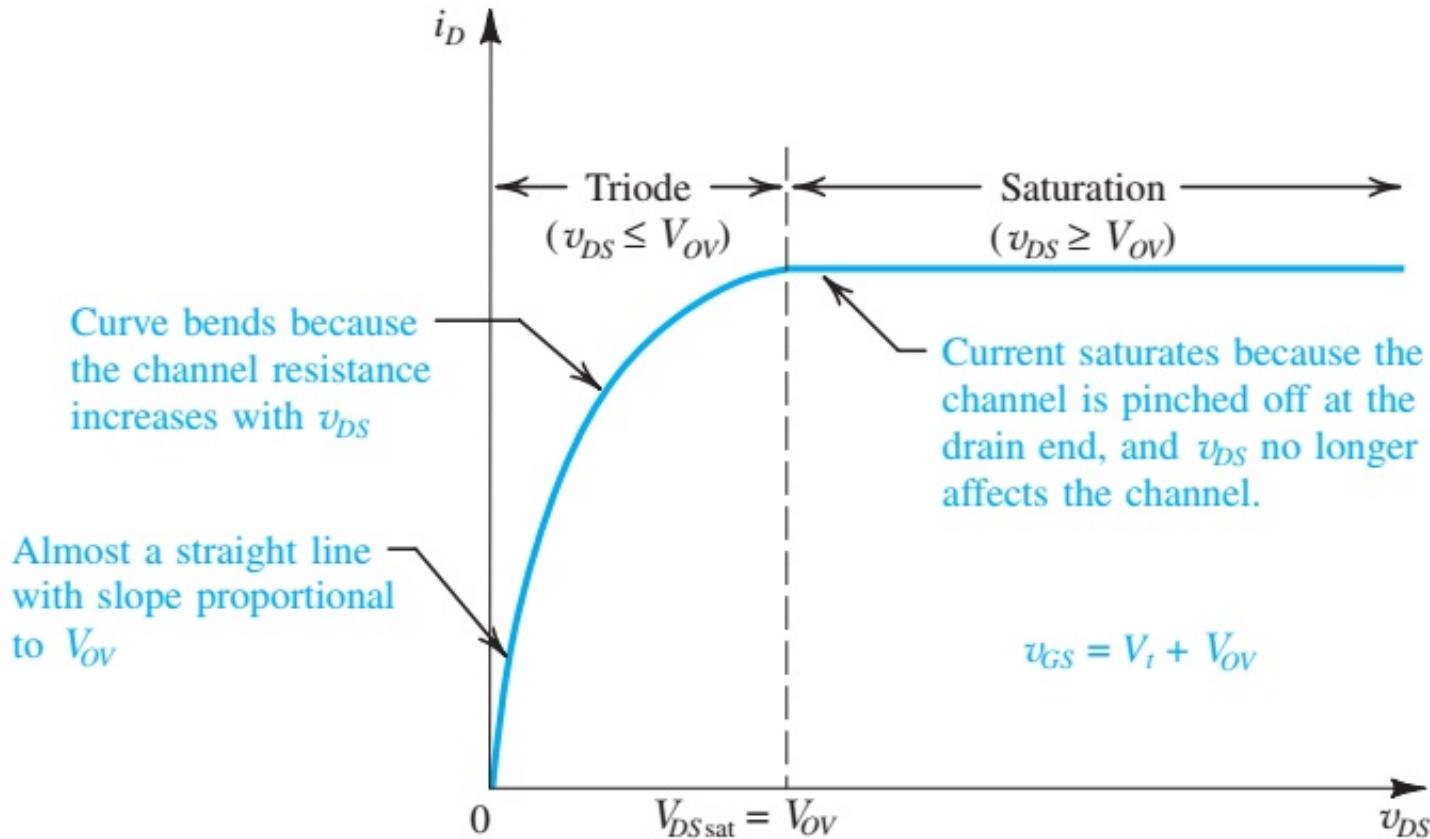
$$v_{OV} = v_{GS} - V_{tn}$$

Effective voltage
Overdrive voltage



随着 v_{DS} 继续升高，沟道夹断的长度增加，沟道长度进一步变短，沟道呈现的阻抗进一步加大，增加的电压基本与沟道增加的阻抗相匹配，漏极电流达到饱和。

● 漏极电流的分析



漏极电流 (以NMOS为例)

变阻区 (triode region) $v_{DS} < v_{GS} - V_{tn}$ 或 $v_{GD} > V_{tn}$

$$i_D = k_n' \frac{W}{L} \left[(v_{GS} - V_{tn}) v_{DS} - \frac{1}{2} v_{DS}^2 \right]$$

饱和区 (saturation region) $v_{DS} \geq v_{GS} - V_{tn}$ 或 $v_{GD} \leq V_{tn}$

$$i_D = \frac{1}{2} k_n' \frac{W}{L} (v_{GS} - V_{tn})^2$$

$$k_n' = \mu_n C_{ox} \quad k_n = k_n' \frac{W}{L}$$

k_n' : the process transconductance parameter

k_n : the transconductance parameter

μ_n : the electron mobility

C_{ox} : the oxide capacitance

W, L : 沟道的宽度和长度



注意

对于增强型PMOS管， $V_{tp} < 0$ $v_{GS} < 0$ $v_{DS} < 0$

变阻区 (triode region) $v_{DS} > v_{GS} - V_{tp}$ 或 $v_{GD} < V_{tp}$

$$|v_{DS}| < |v_{GS}| - |V_{tp}| \text{ 或 } |v_{GD}| > |V_{tp}|$$

$$i_D = k_p' \frac{W}{L} \left[(v_{GS} - V_{tp}) v_{DS} - \frac{1}{2} v_{DS}^2 \right]$$

饱和区 (saturation region) $v_{DS} \leq v_{GS} - V_{tp}$ 或 $v_{GD} \geq V_{tp}$

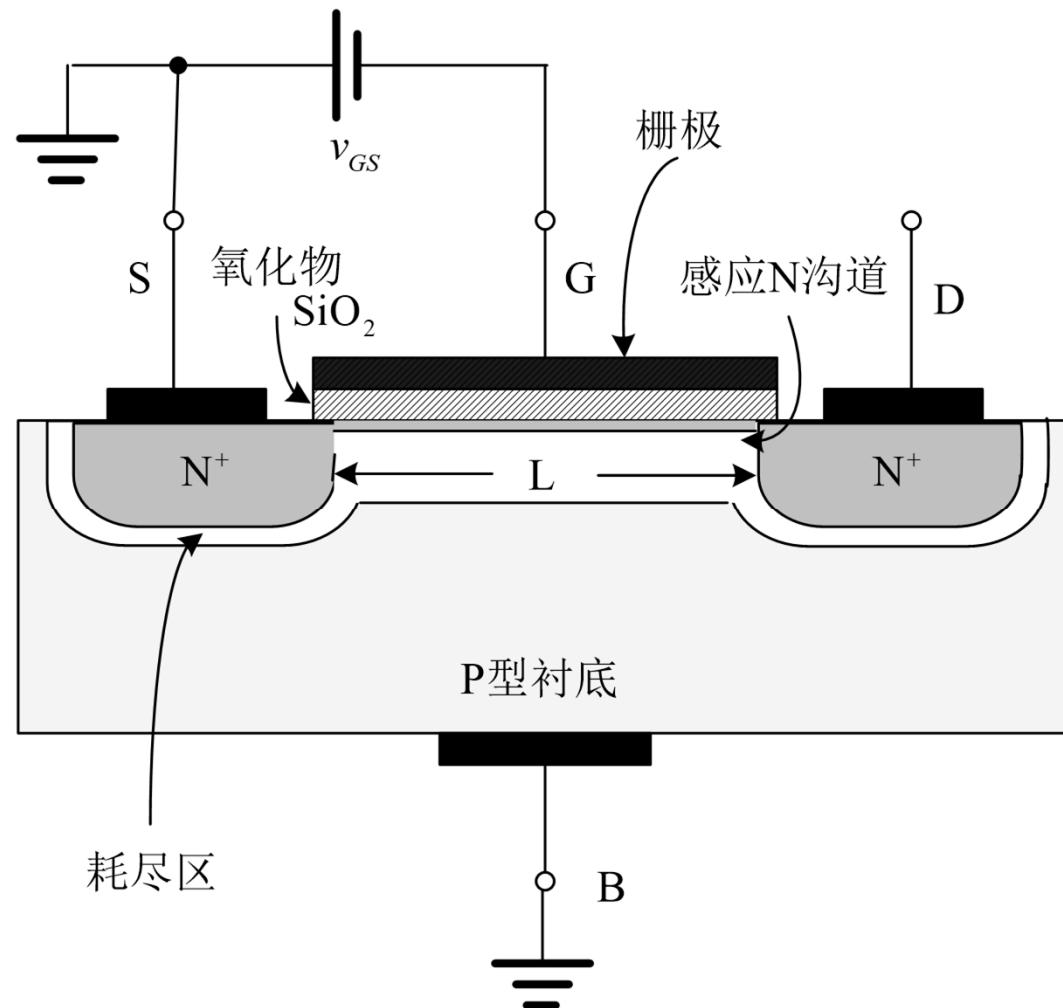
$$|v_{DS}| \geq |v_{GS}| - |V_{tp}| \text{ 或 } |v_{GD}| \leq |V_{tp}|$$

$$i_D = \frac{1}{2} k_p' \frac{W}{L} (v_{GS} - V_{tp})^2$$

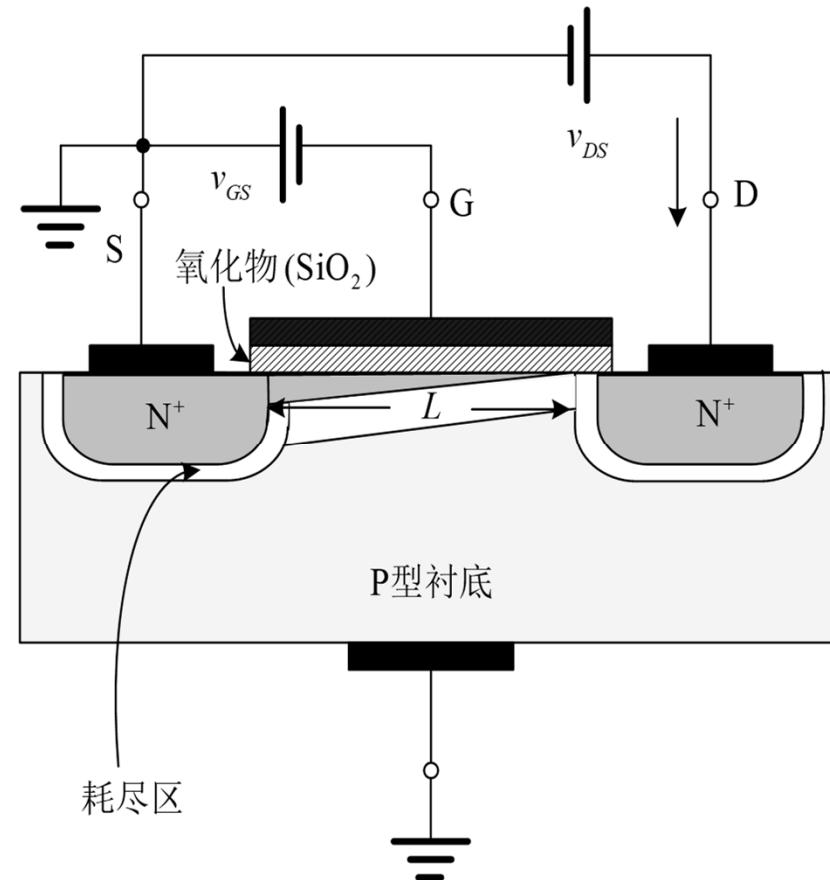
2、N沟道耗尽型MOSFET的工作原理

- 通道夹断（沟道消失）（进入截止区）

夹断电压 $V_{GS}(\text{off})$

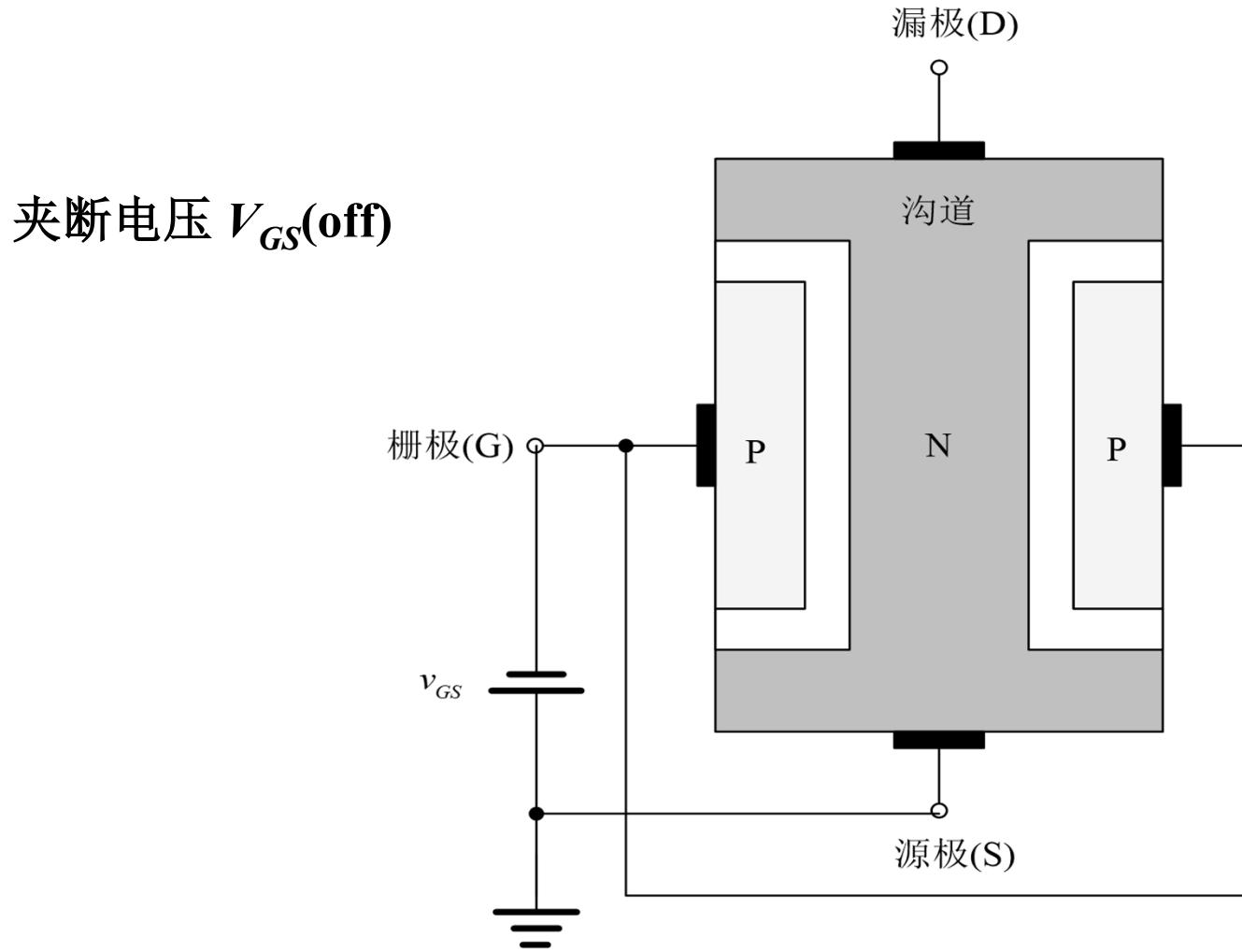


● 预夹断（进入饱和区）

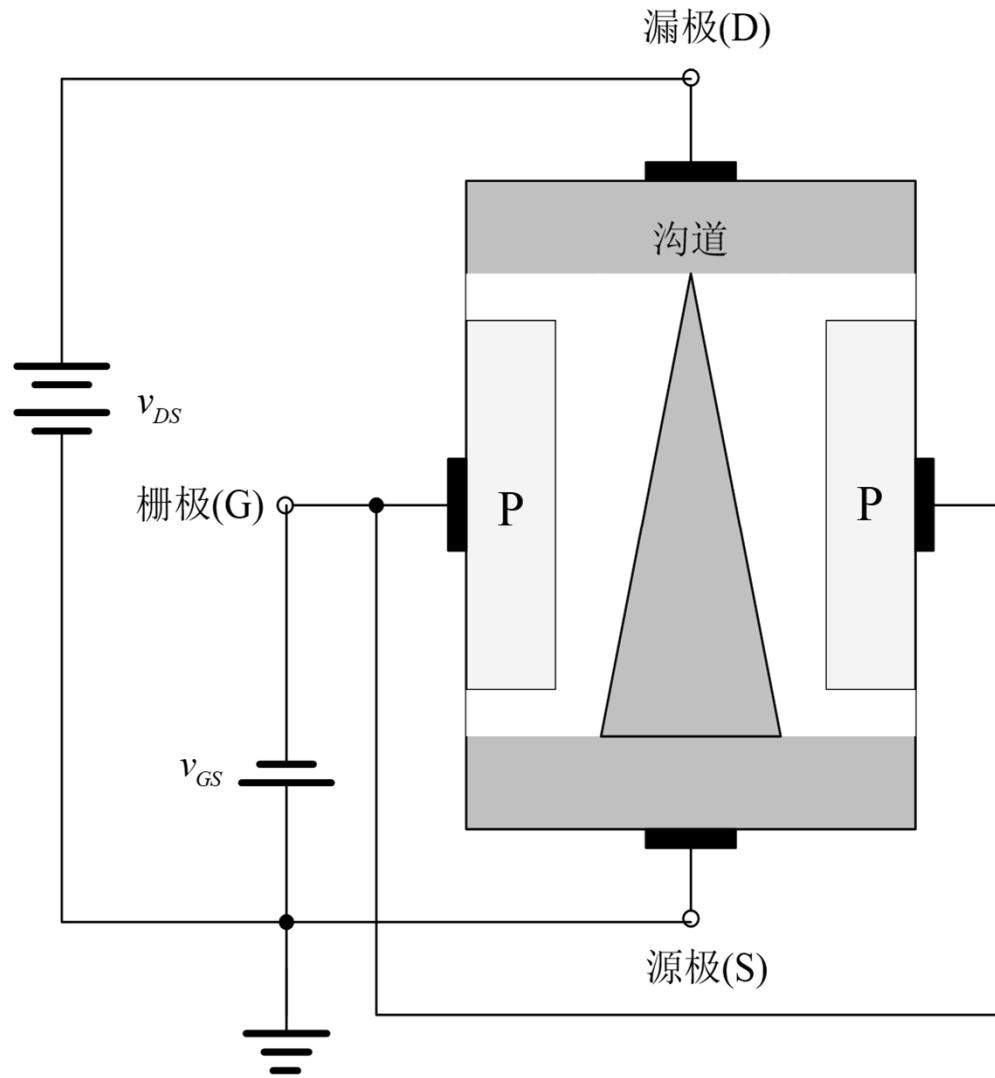


3、结型场效应管的工作原理

- 通道夹断（沟道消失）（进入截止区）

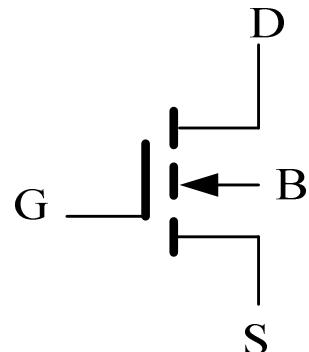


● 预夹断（进入饱和区）

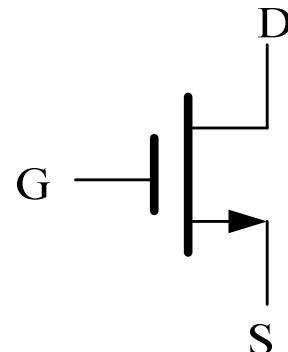


三、场效应晶体管的符号

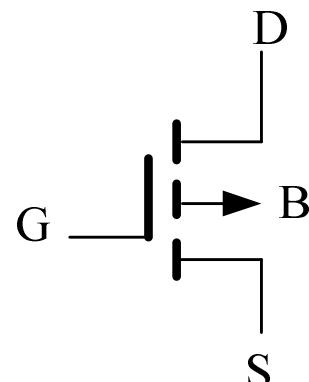
1、增强型（MOSFET）



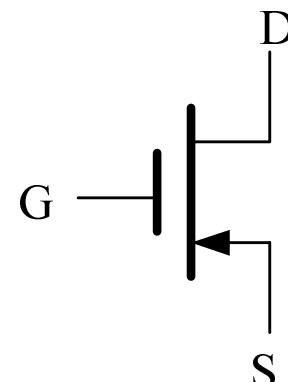
N沟道



简化符号

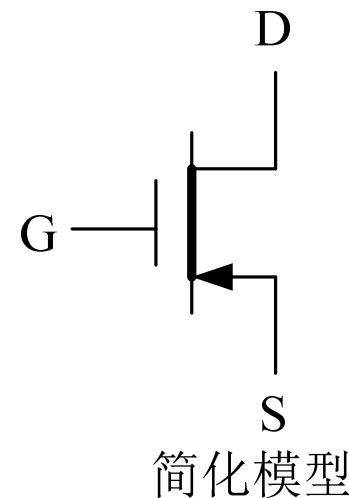
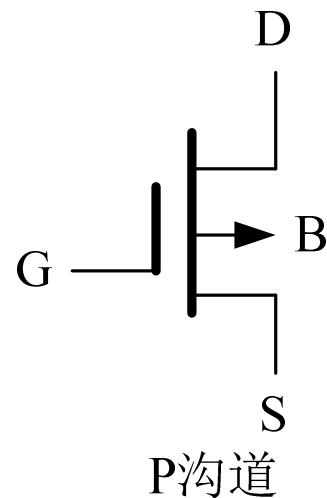
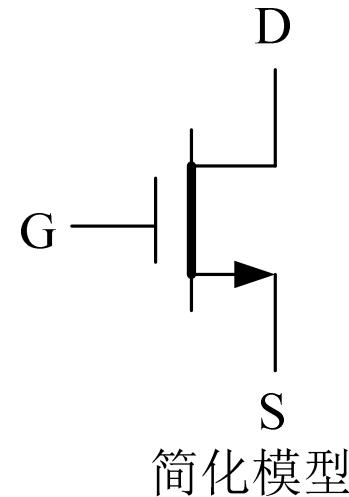
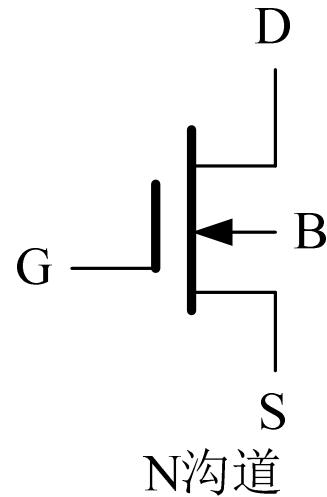


P沟道

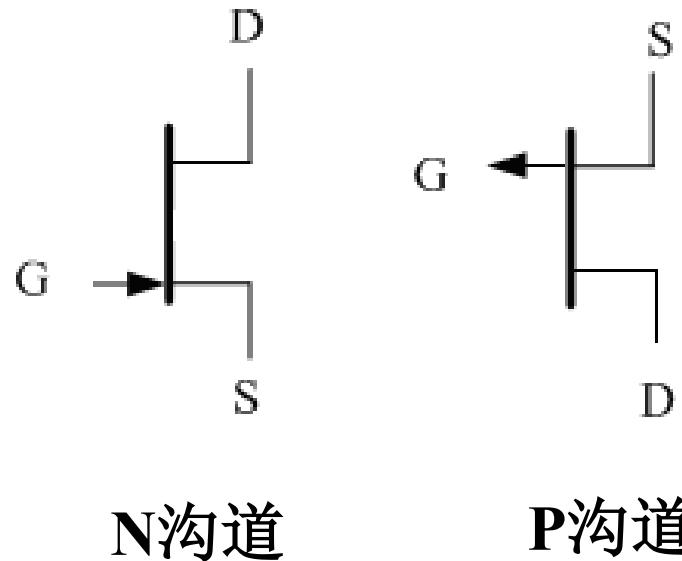


简化符号

2、耗尽型（MOSFET）



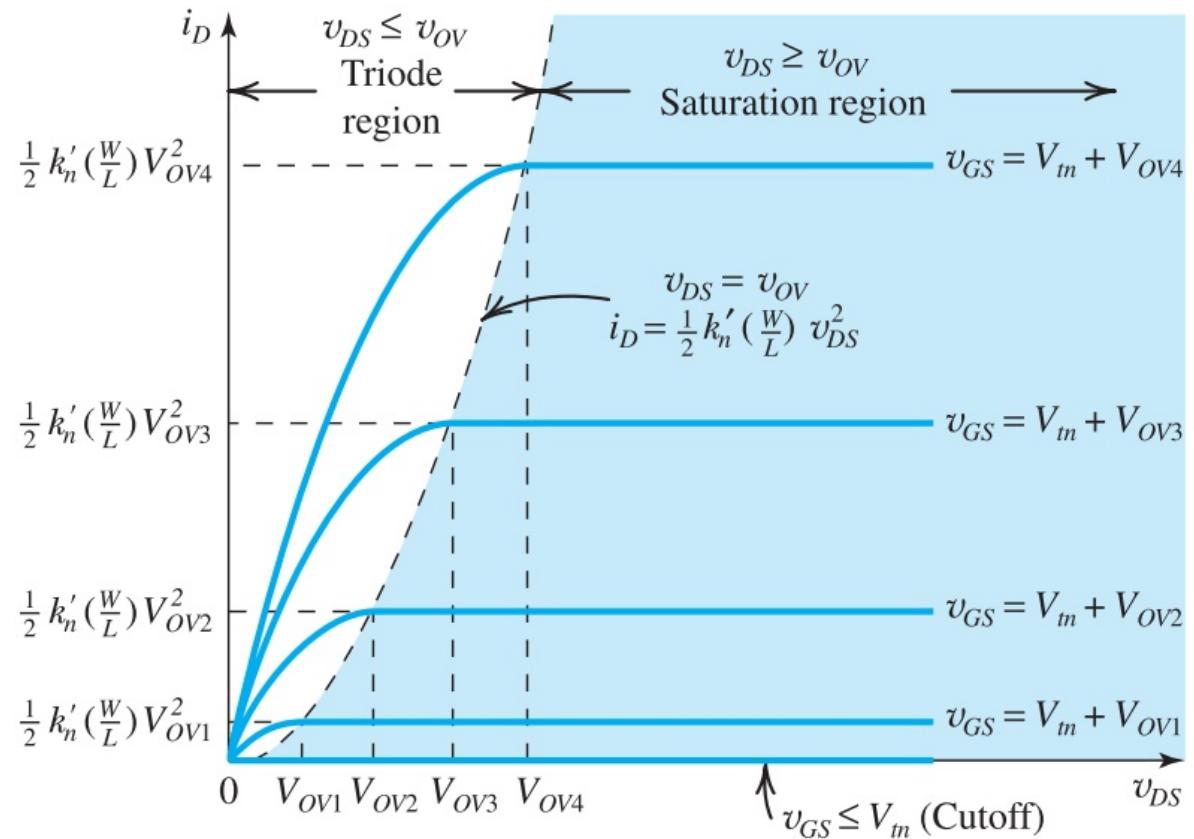
3、结型场效应晶体管（J-FET）



8.1.2 场效应晶体管的电路特性

一、输出特性

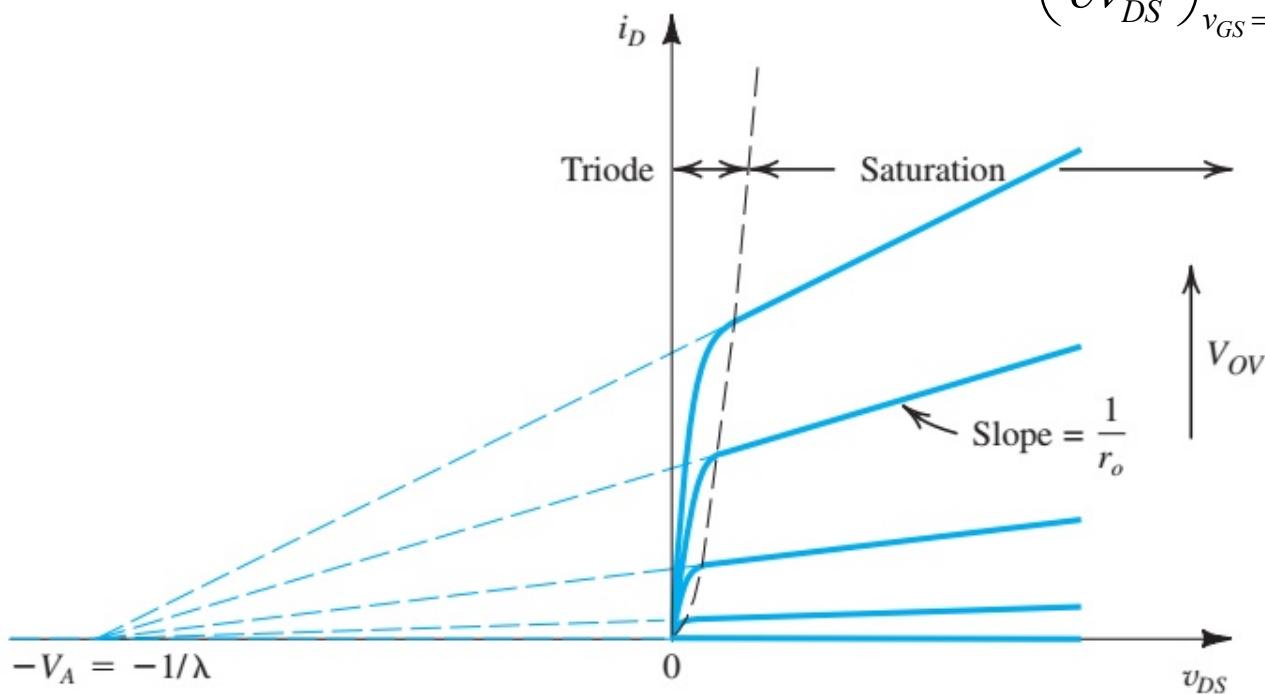
增强型NMOS管
输出特性曲线



若考慮沟道長度調制效應

(channel-length modulation)

$$r_o \equiv \left(\frac{\partial i_D}{\partial v_{DS}} \right)_{v_{GS}=\text{Const}}^{-1} = \frac{V_A}{I_D}$$

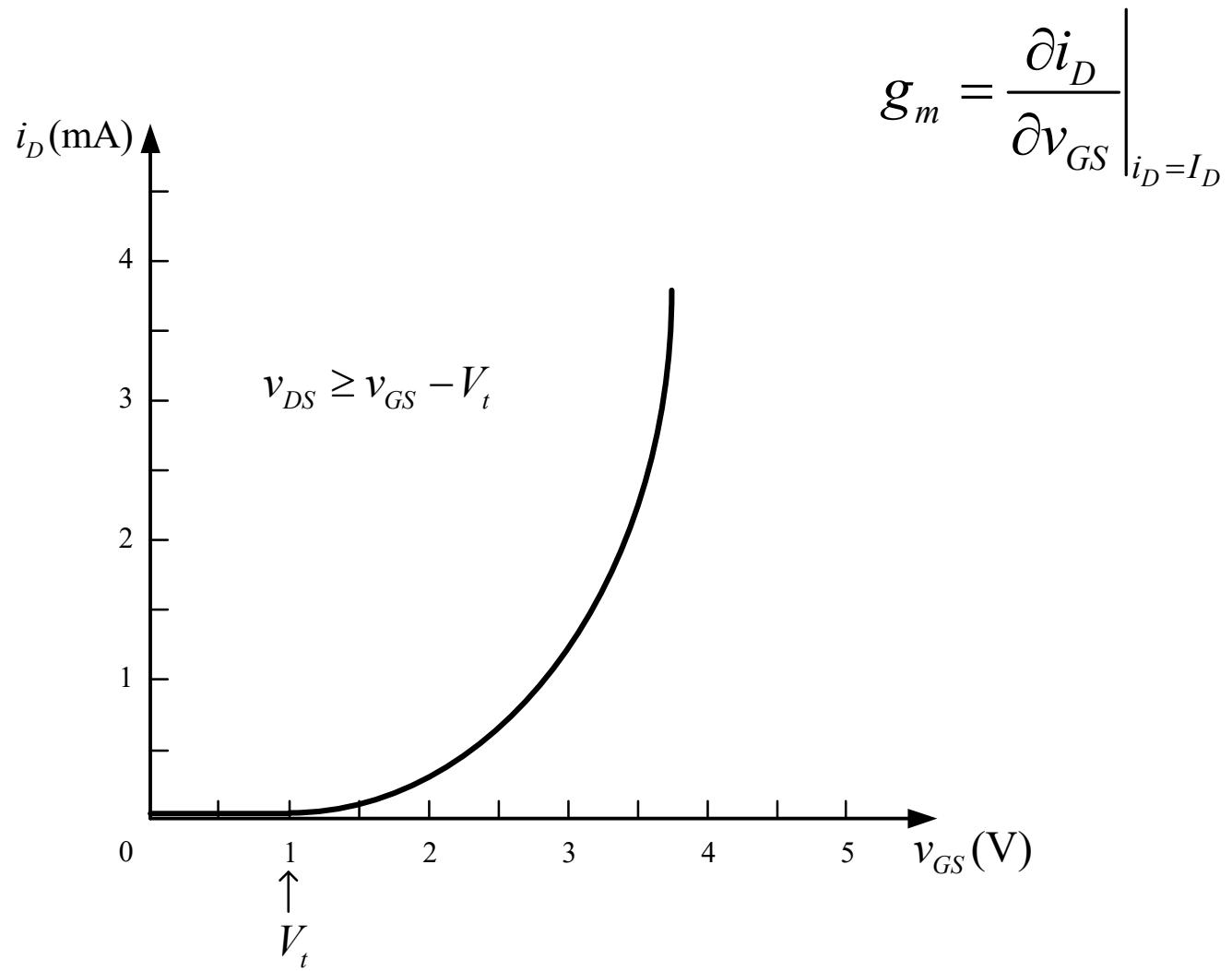


NMOS管 $i_D = \frac{1}{2} k_n' \frac{W}{L} (v_{GS} - V_{tn})^2 (1 + \lambda v_{DS})$ $\lambda = \frac{1}{V_A} > 0$

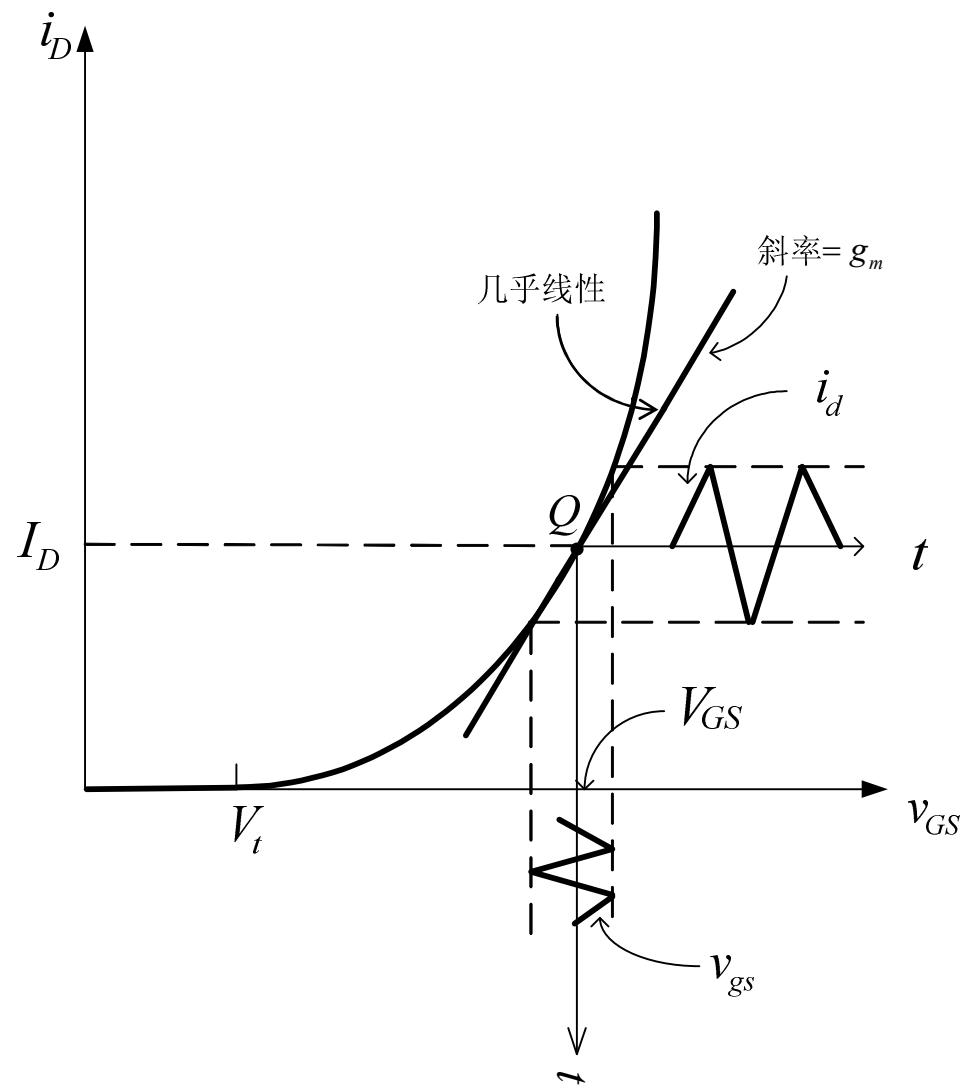
PMOS管 $i_D = \frac{1}{2} k_p' \frac{W}{L} (v_{GS} - V_{tp})^2 (1 + \lambda v_{DS})$ $\lambda = \frac{1}{V_A} < 0$

二、转移特性

增强型NMOS管
转移特性曲线



场效应管工作点的确定



三、场效应管（FET）的参数

- 直流参数：

$V_{GS(\text{th})} / V_t$ ：开启电压（增强型MOSFET特有的参数），当 V_{DS} 为一固定值时，能够产生漏极电流 I_D 所需的 $|V_{GS}|$ 最小值。

$V_{GS(\text{off})}$ ：夹断电压（耗尽型MOSFET特有的参数），当 V_{DS} 为一固定值时，使 I_D 减小到一个微小值时所需的 V_{GS} 值。

I_{DSS} ：饱和漏极电流，当 $V_{GS} = 0$ ，场效应管发生预夹断时的漏极电流。

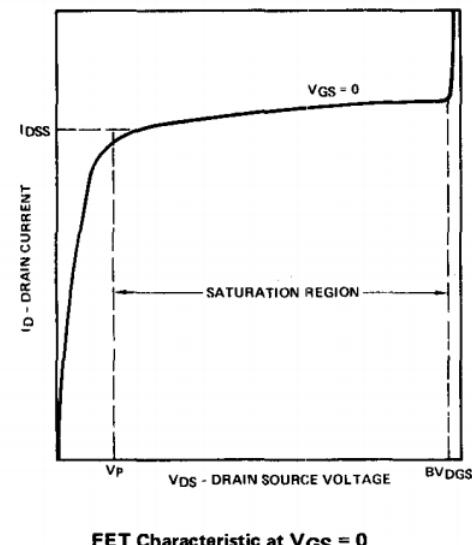
R_{GS} ：直流输入电阻， $V_{DS} = 0$ 时， V_{GS} 与 I_G 的比值。

$V_{(\text{BR})DS}$ ：漏源击穿电压

$V_{(\text{BR})GS}$ ：栅源击穿电压

- 交流参数：

g_m 、 r_o 、 C_{GS} 、 C_{GD} 、 C_{DS}



8.1.3 中频等效电路模型

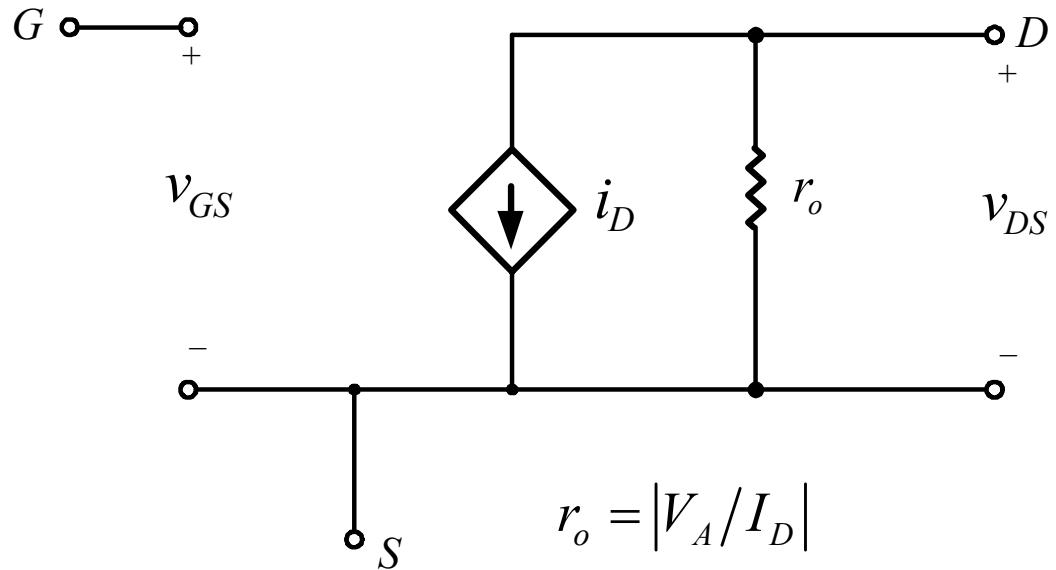
一、大信号模型

$$i_D = \frac{1}{2} k_n' \frac{W}{L} (v_{GS} - V_{tn})^2$$

也可写为

$$i_D = I_{DSS} \left(1 - \frac{v_{GS}}{V_{tn}} \right)^2$$

其中 $I_{DSS} = \frac{1}{2} k_n' \frac{W}{L} V_{tn}^2$



二、小信号模型

$$v_{GS} = V_{GS} + v_{gs}$$

$$\begin{aligned} i_D &= \frac{1}{2} k_n' \frac{W}{L} (v_{GS} - V_t)^2 = \frac{1}{2} k_n' \frac{W}{L} (V_{GS} + v_{gs} - V_{tn})^2 \\ &= \frac{1}{2} k_n' \frac{W}{L} (V_{GS} - V_{tn})^2 + k_n' \frac{W}{L} (V_{GS} - V_{tn}) v_{gs} + \frac{1}{2} k_n' \frac{W}{L} v_{gs}^2 \end{aligned}$$

若 $\frac{1}{2} k_n' \frac{W}{L} v_{gs}^2 \ll k_n' \frac{W}{L} (V_{GS} - V_{tn}) v_{gs}$ 即 $v_{gs} \ll 2(V_{GS} - V_{tn})$

→ $i_D \approx \frac{1}{2} k_n' \frac{W}{L} (V_{GS} - V_{tn})^2 + k_n' \frac{W}{L} (V_{GS} - V_{tn}) v_{gs} = I_D + i_d$

$$I_D = \frac{1}{2} k_n' \frac{W}{L} (V_{GS} - V_{tn})^2$$

$$i_d = k_n' \frac{W}{L} (V_{GS} - V_{tn}) v_{gs}$$

1、 π 型等效电路

$$i_d = k_n' \frac{W}{L} (V_{GS} - V_{tn}) v_{gs}$$

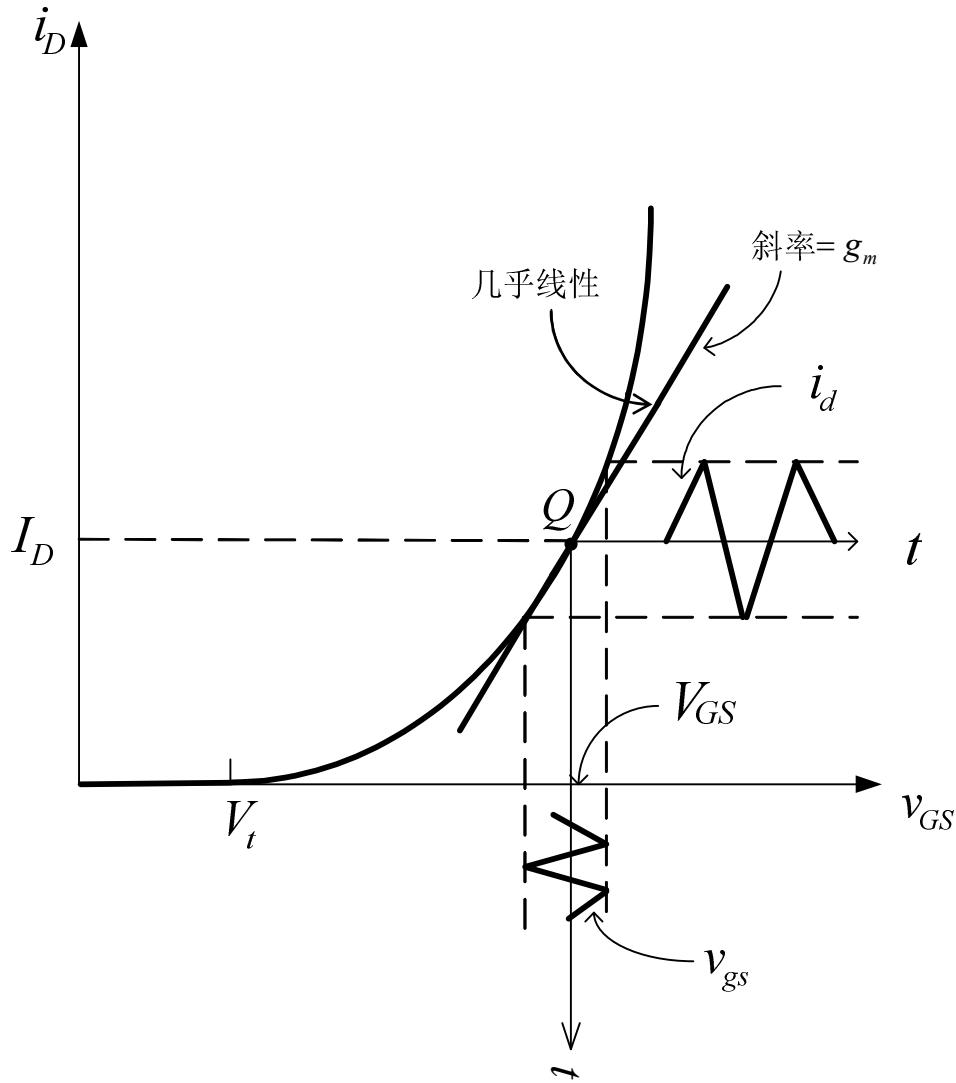
$$g_m = \left. \frac{\partial i_d}{\partial v_{GS}} \right|_{i_D=I_D} = \frac{i_d}{v_{gs}} = k_n' \frac{W}{L} (V_{GS} - V_{tn}) = k_n V_{OV}$$

其中 $k_n = k_n' \frac{W}{L}$, $V_{OV} = V_{GS} - V_{tn}$

代入 $I_D = \frac{1}{2} k_n' \frac{W}{L} (V_{GS} - V_{tn})^2$

又可得 $g_m = \frac{I_D}{(V_{GS} - V_{tn})/2}$

对照三极管 $g_m = \frac{I_C}{V_T}$

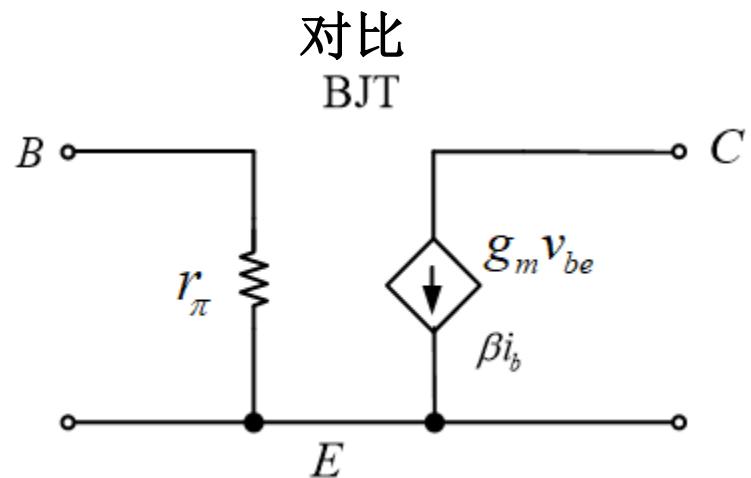
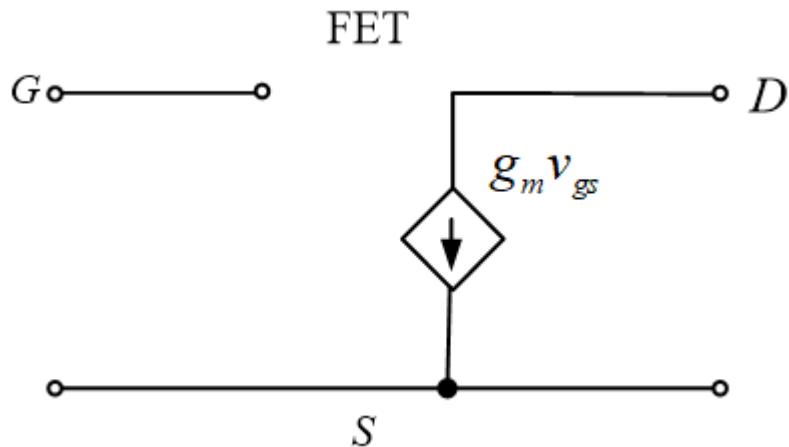


g_m 是转移特性曲线的斜率，因此：

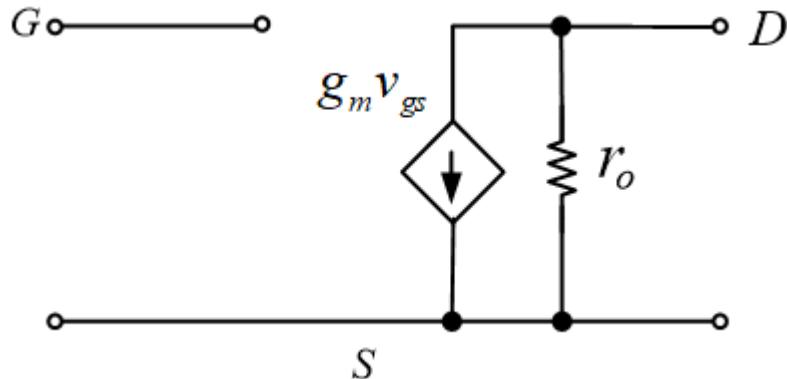
对于**NMOS**管， $g_m > 0$

对于**PMOS**管， $g_m < 0$

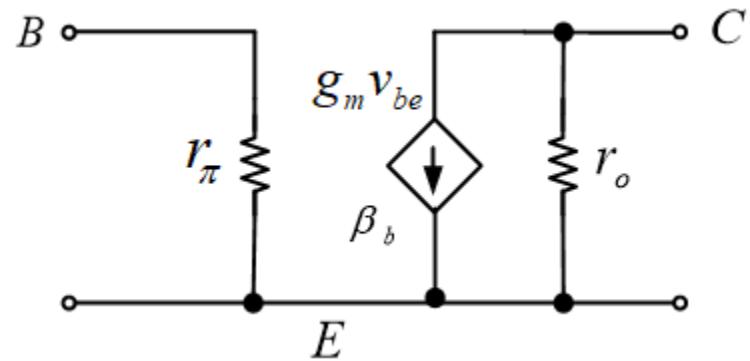
$$i_d = k_n' \frac{W}{L} (V_{GS} - V_{tn}) v_{gs} = g_m v_{gs}$$



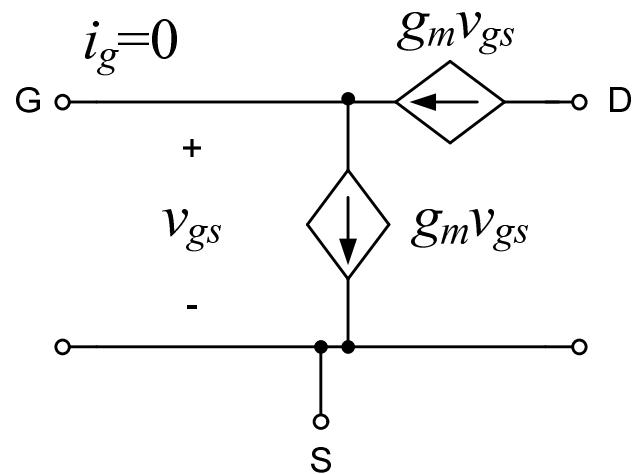
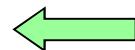
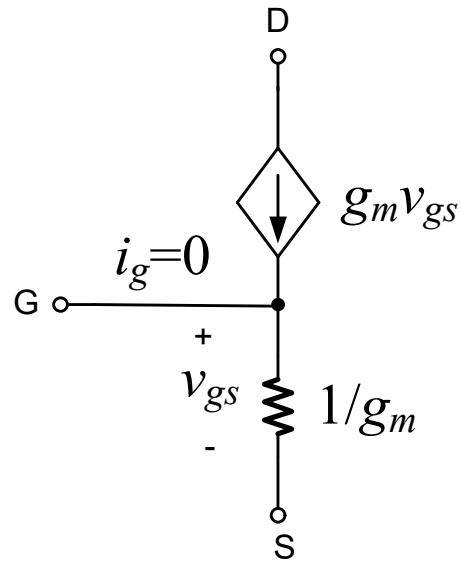
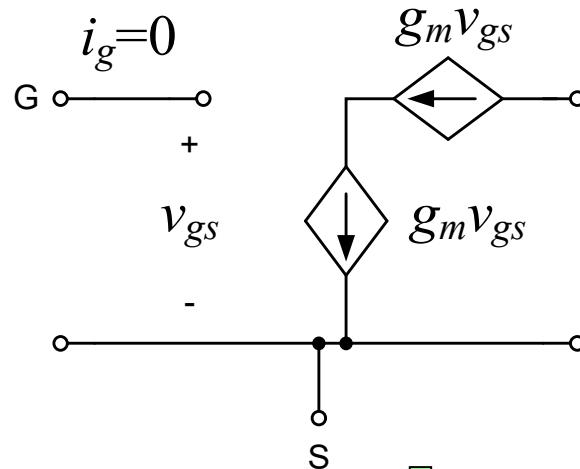
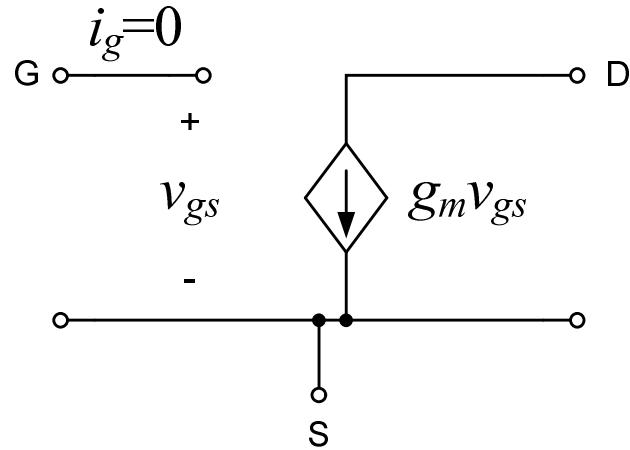
考虑沟道长度调制效应



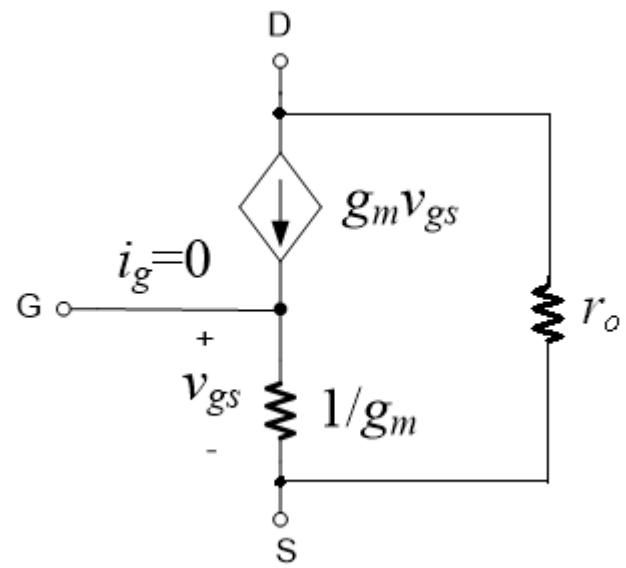
考虑厄利效应



2、T型等效电路



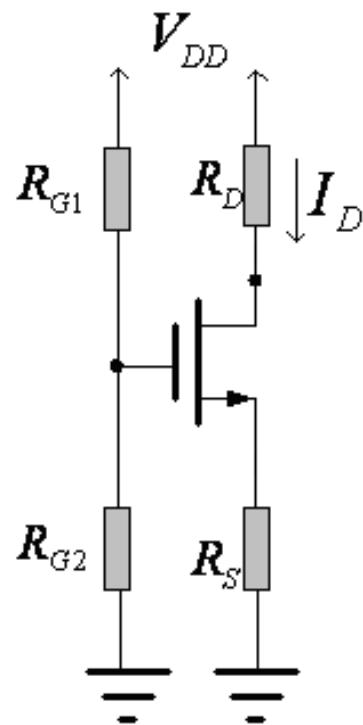
考虑输出电阻的T型等效电路



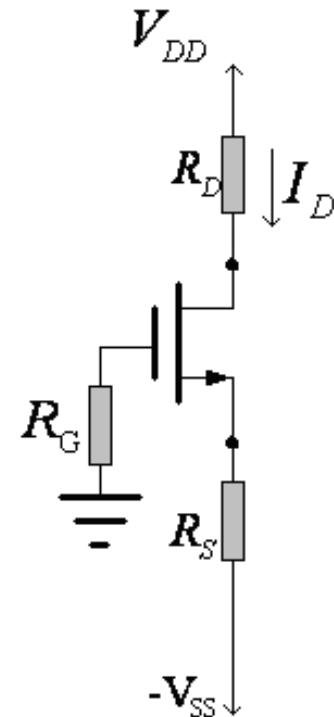
8.2 场效应晶体管放大电路的构成及其分析

8.2.1 直流偏置电路及其分析

一、自给偏置电路

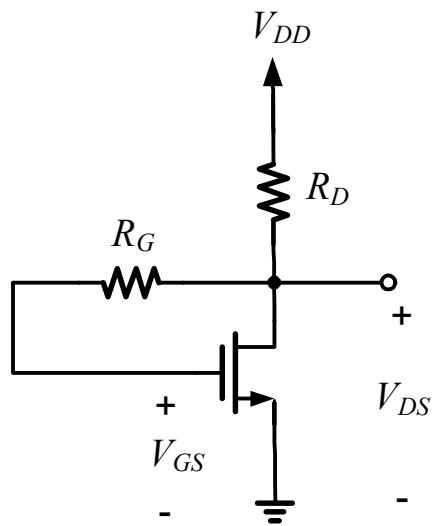


单电源



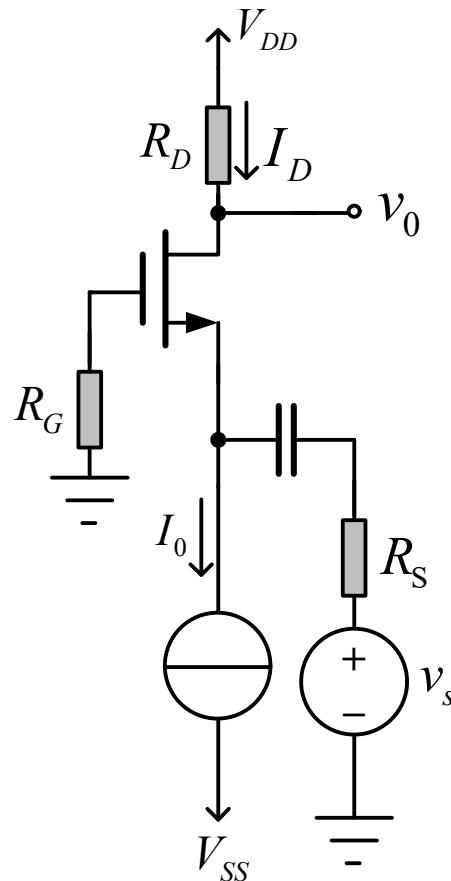
双电源

二、栅源间接反馈电阻的偏置电路

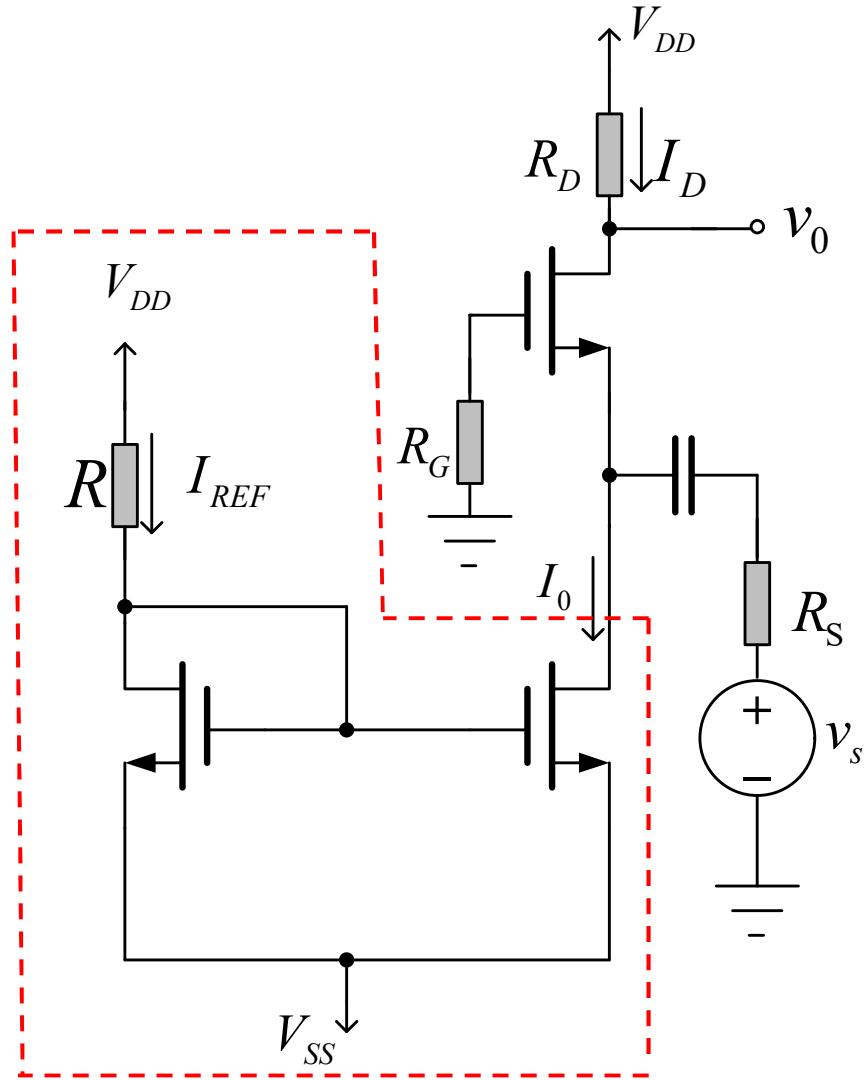


$$V_{DD} = V_{GS} + R_D I_D$$

三、恒流源偏置电路



镜像电流源



$$I_{REF} = \frac{1}{2} k'_n \frac{W}{L} (V_{GS} - V_t)^2$$

$$I_{REF} = \frac{V_{DD} - V_{GS} - V_{SS}}{R}$$

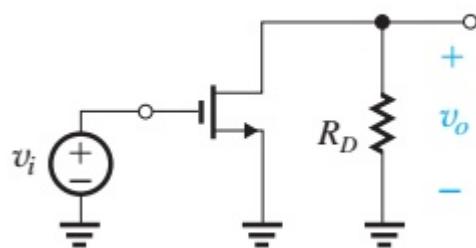
8.2.2 三种接法放大电路的分析计算

一、三种接法

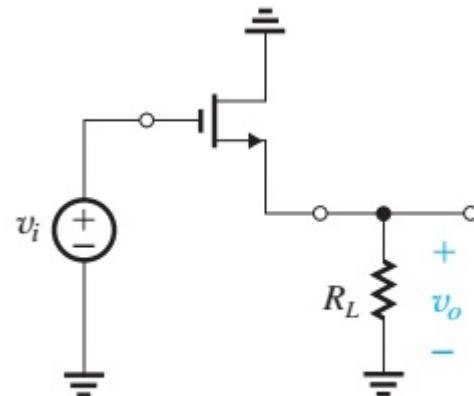
1、共源接法 Common-Source (CS)

2、共漏接法 Common-Drain (CD)

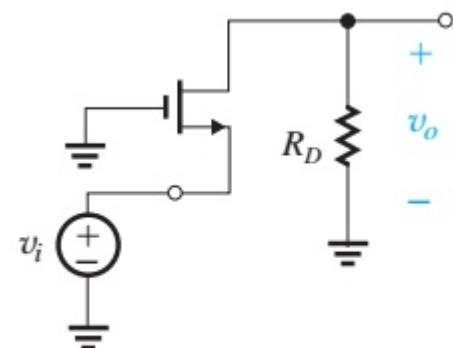
3、共栅接法 Common-Gate (CG)



(a) Common Source (CS)



(c) Common Drain (CD)
or Source Follower



(b) Common Gate (CG)

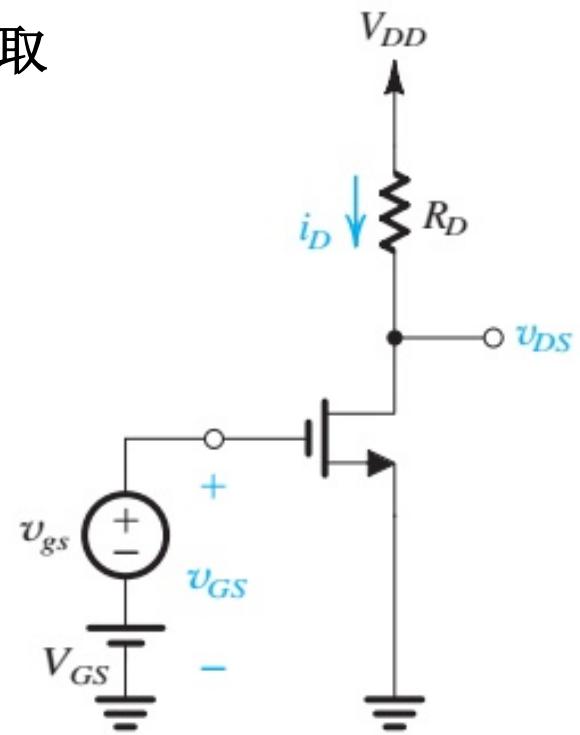
二、直流偏置通路的计算

注意

- 首先，判断MOS管的工作状态，正确选择公式。
- 其次，求解二次方程得到双解，合理取舍。

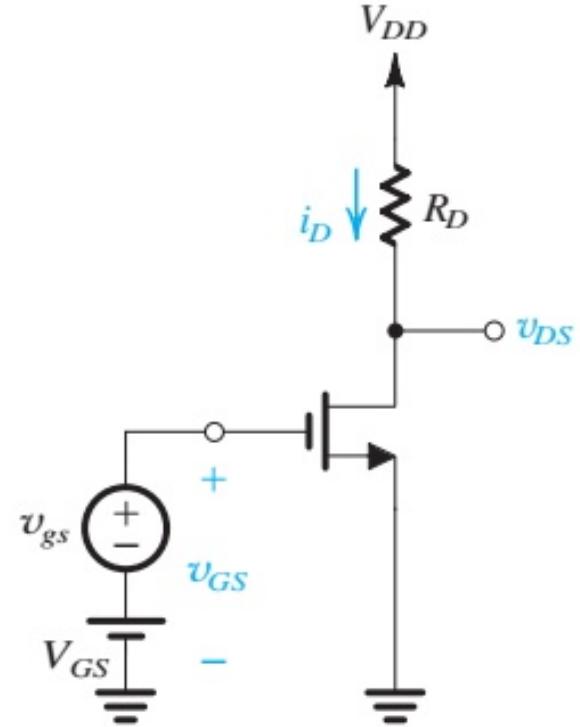
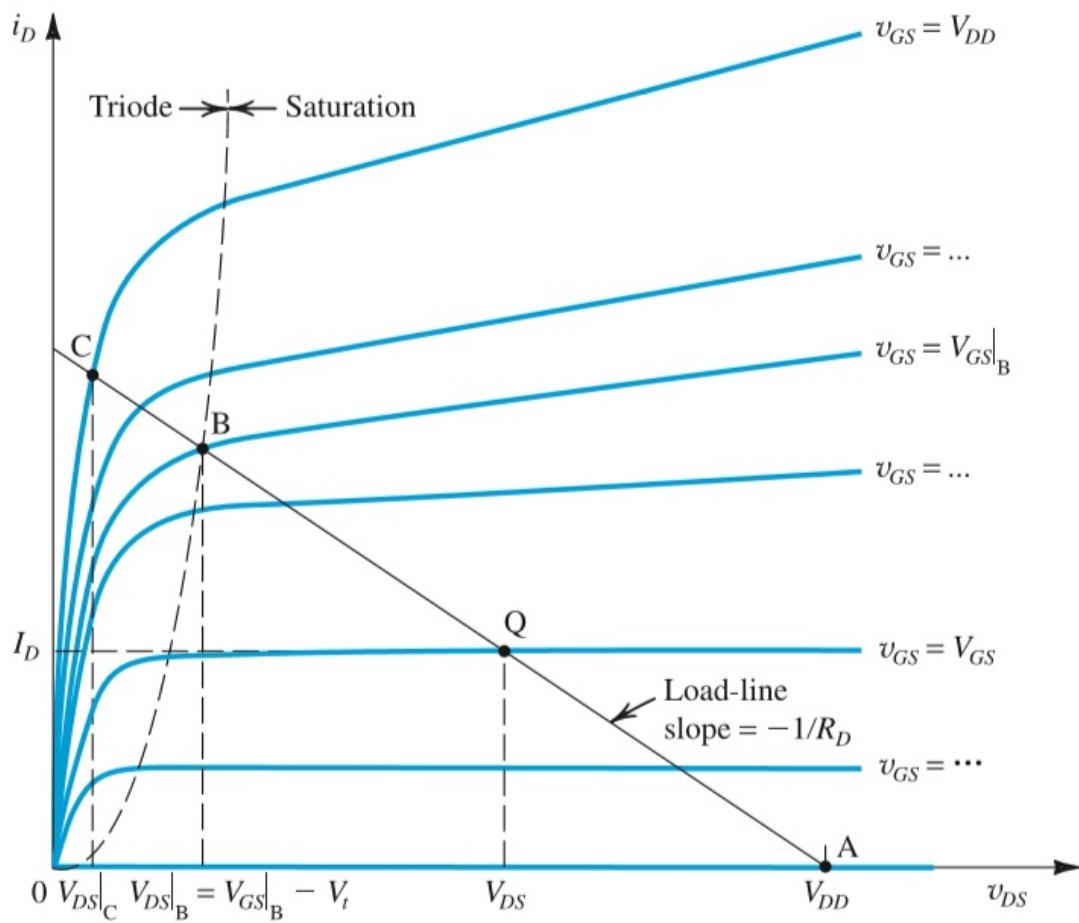
$$I_D = k_n \cdot \frac{W}{L} \left[(V_{GS} - V_{tn}) V_{DS} - \frac{1}{2} V_{DS}^2 \right]$$

$$I_D = \frac{1}{2} k_n \cdot \frac{W}{L} (V_{GS} - V_{tn})^2$$



三、交流通路的计算

1、图解法



2、小信号等效电路法

a、确定跨导 g_m

$$g_m = \frac{i_d}{v_{gs}} = k_n' \frac{W}{L} (V_{GS} - V_{tn})$$

$$g_m = \frac{I_D}{(V_{GS} - V_{tn})/2}$$

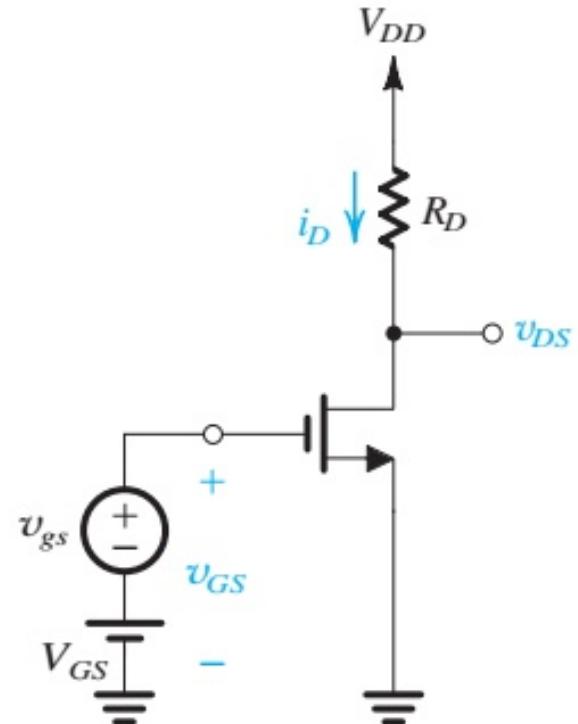
b、电压增益

$$v_{DS} = V_{DD} - R_D i_D = V_{DD} - R_D (I_D + i_d)$$

$$v_{DS} = V_{DD} - R_D I_D - R_D i_d = V_{DS} - R_D i_d$$

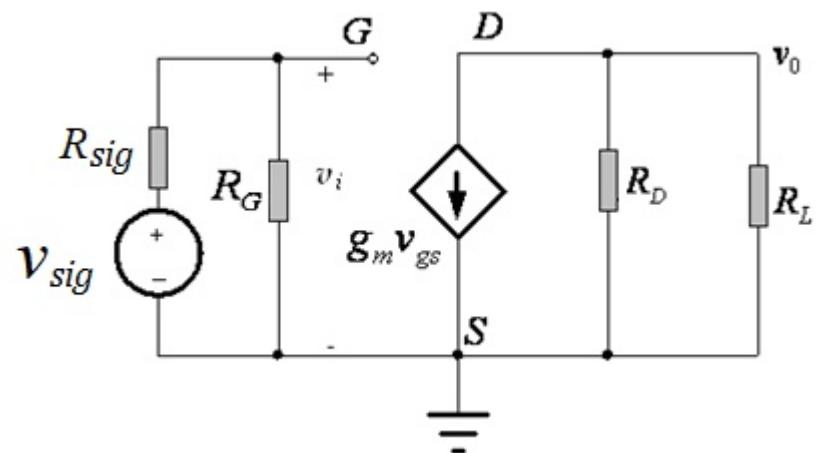
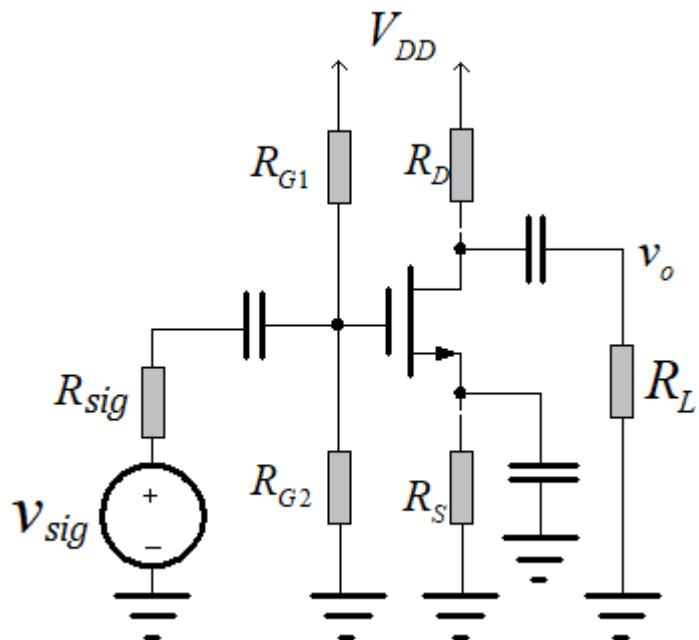
$$v_{ds} = -R_D i_d = -g_m v_{gs} R_D$$

$$A_v = \frac{v_{ds}}{v_{gs}} = -g_m R_D$$

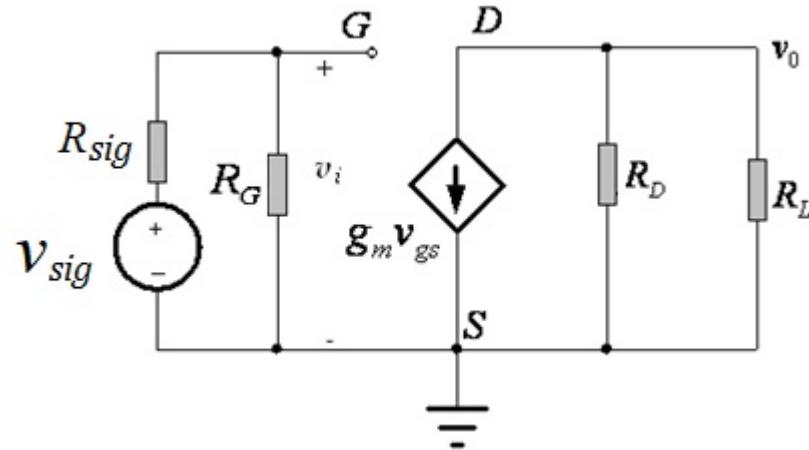


四、三种接法放大电路的计算

1、共源放大器



$$R_G = R_{G1} // R_{G2}$$



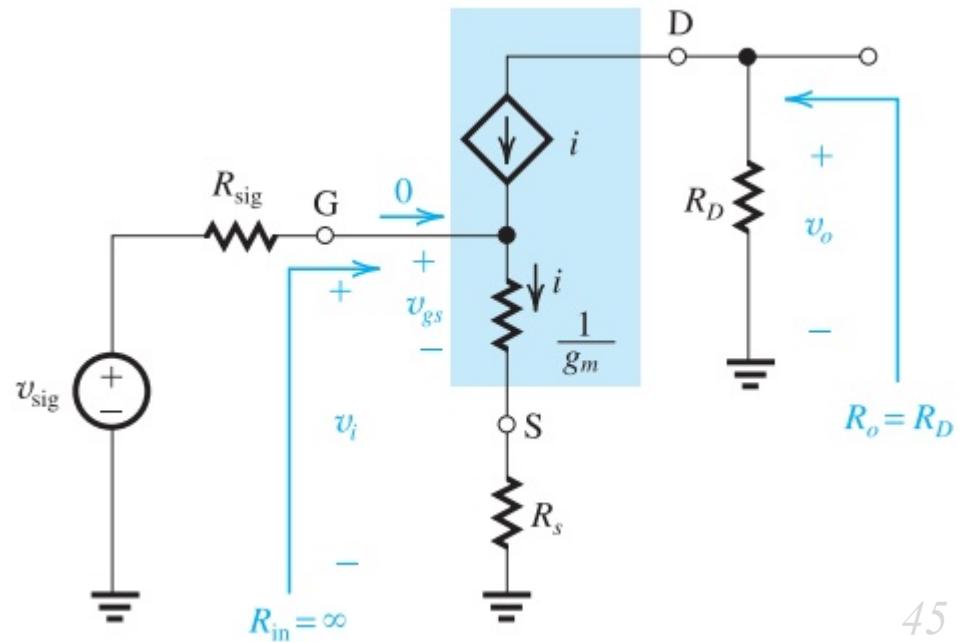
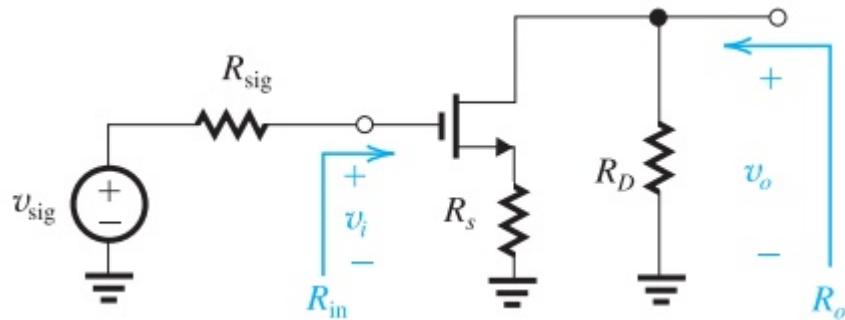
$$A_v = \frac{v_o}{v_i} = -g_m (R_D // R_L)$$

$$A_{vs} = \frac{v_o}{v_{sig}} = \frac{v_i}{v_{sig}} \frac{v_o}{v_i} = -\frac{R_G}{R_{sig} + R_G} g_m (R_D // R_L)$$

$$R_i = R_G$$

$$R_o = R_D$$

➤ 带源极电阻的共源放大器

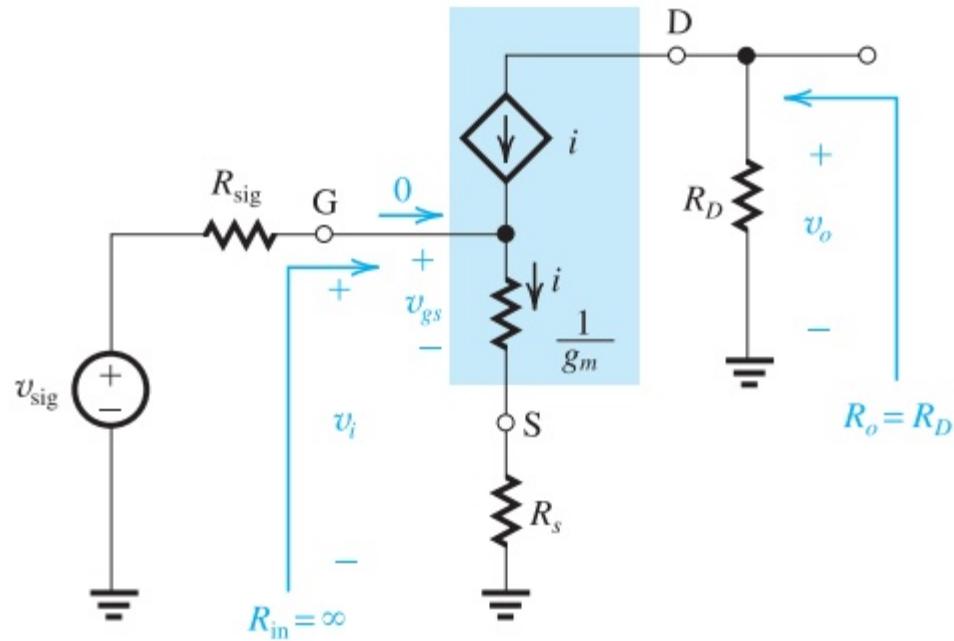


$$A_v = \frac{v_o}{v_i} = \frac{-g_m v_{gs} R_D}{g_m v_{gs} (1/g_m + R_S)} = -\frac{R_D}{1/g_m + R_S}$$

$$A_{vs} = \frac{v_o}{v_{sig}} = \frac{v_o}{v_i} = A_v$$

$$R_i = \infty$$

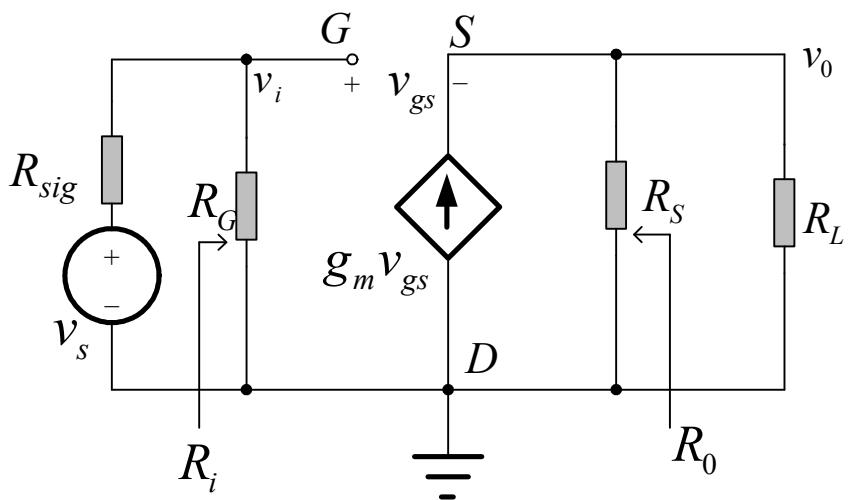
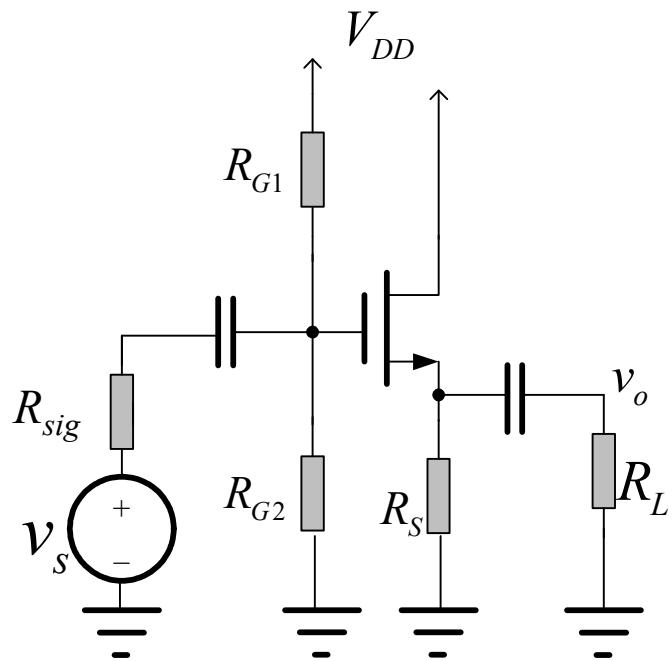
$$R_o = R_D$$



共源放大器特性：

非常高的输入电阻、适中的电压增益和相当高的输出电阻，
频带窄。

2、共漏放大器

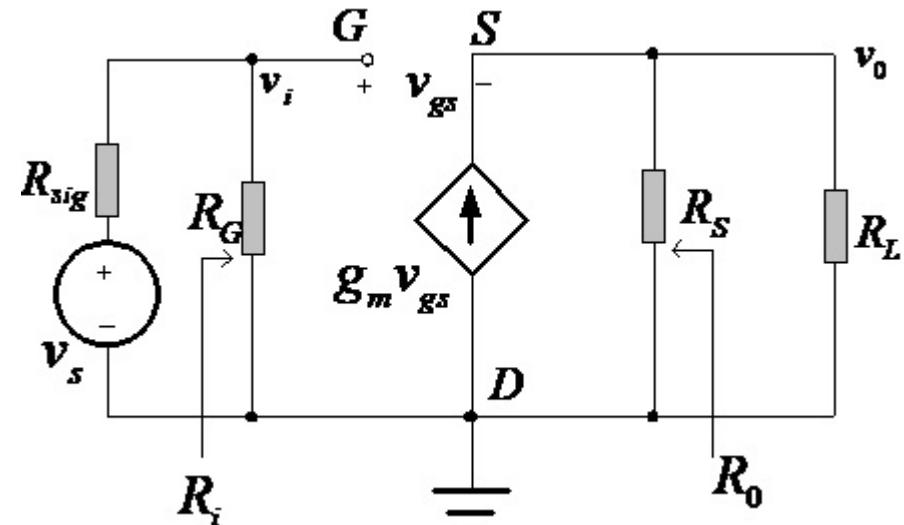


$$A_v = \frac{v_o}{v_i} = \frac{v_o}{v_{gs} + v_o} = \frac{g_m (R_s // R_L)}{1 + g_m (R_s // R_L)}$$

$$A_{vs} = \frac{v_o}{v_{sig}} = \frac{v_i}{v_{sig}} \frac{v_o}{v_i} = \frac{R_G}{R_{sig} + R_G} A_v$$

$$R_i = R_G$$

$$R_o = R_s // \frac{1}{g_m}$$

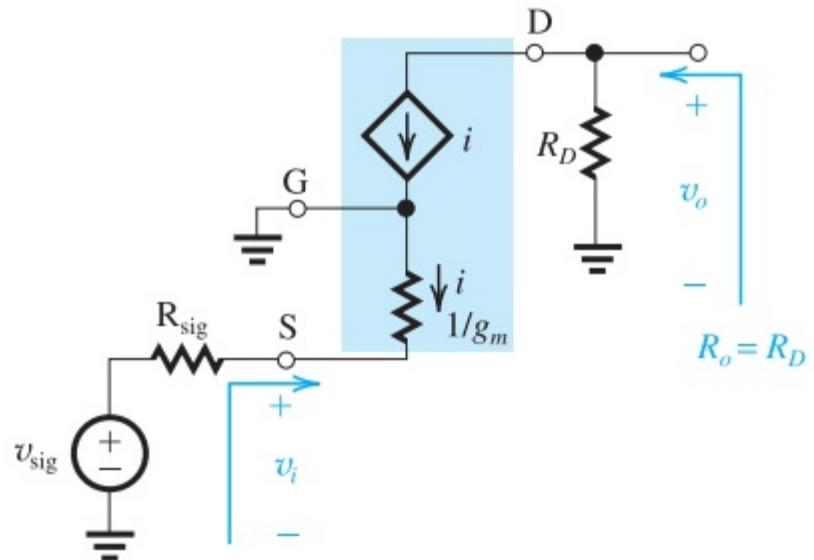
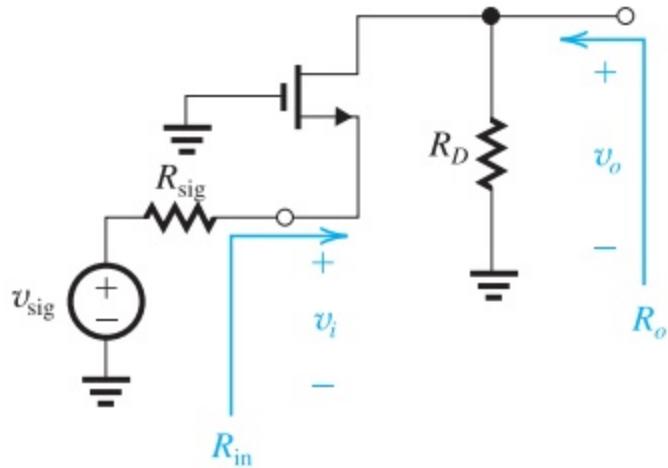


共漏放大器特性：

非常高的输入电阻、相当低的输出电阻和接近于1的电压增益，频带中等。

共漏放大器可作为单位增益的电压缓冲放大器，又称为**源极跟随器**。

3、共栅放大器



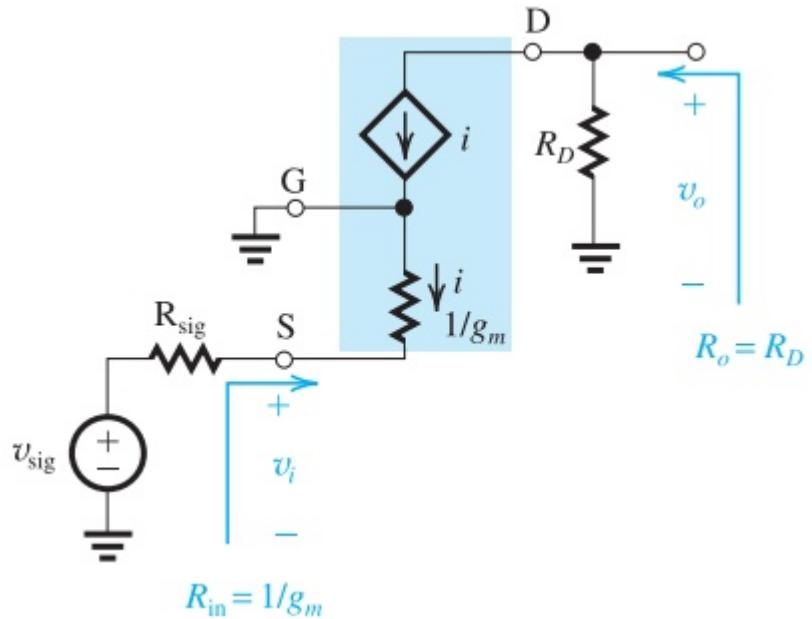
$$R_{\text{in}} = 1/g_m$$

$$A_v = \frac{v_o}{v_i} = \frac{-g_m v_{gs} R_D}{-g_m v_{gs} \times \frac{1}{g_m}} = g_m R_D$$

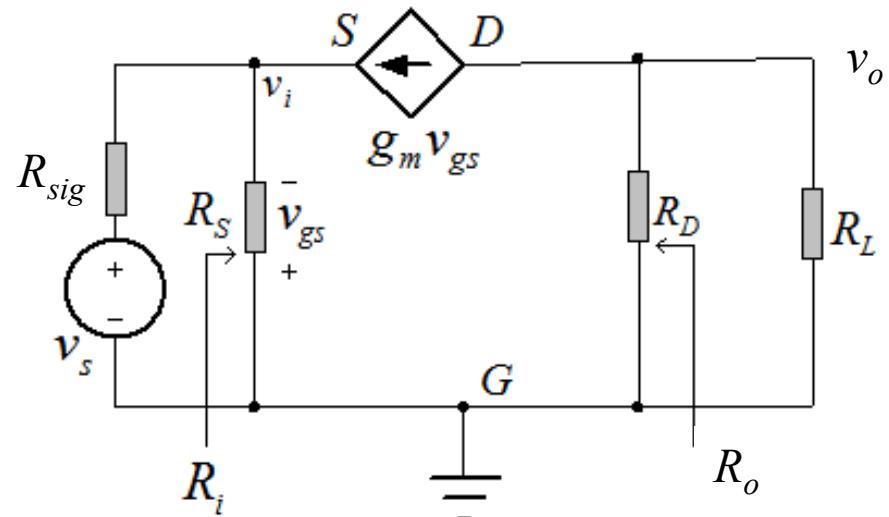
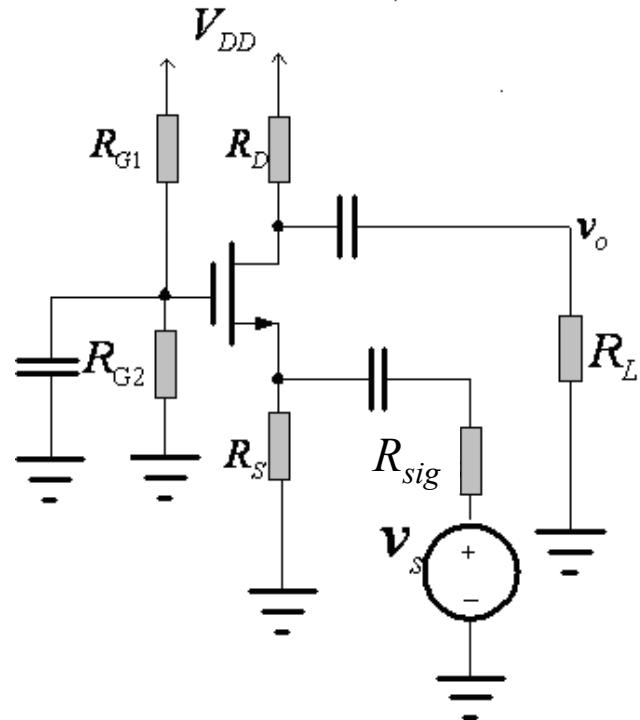
$$A_{vs} = \frac{v_o}{v_s} = \frac{v_i}{v_s} \times \frac{v_o}{v_i} = \frac{-g_m v_{gs} \times \frac{1}{g_m}}{-g_m v_{gs} \times \left(R_{sig} + \frac{1}{g_m} \right)} \times g_m R_D = \frac{R_D}{R_{sig} + 1/g_m}$$

$$R_i = \frac{1}{g_m}$$

$$R_o = R_D$$



➤ 带源极电阻的共栅放大器



$$A_v = \frac{v_o}{v_i} = g_m R_D // R_L$$

$$\begin{aligned} A_{vs} &= \frac{v_o}{v_s} = \frac{v_i}{v_s} \times \frac{v_o}{v_i} = \frac{-v_{gs}}{R_{sig}(-g_m v_{gs} - v_{gs}/R_S) - v_{gs}} \times g_m (R_D // R_L) \\ &= \frac{g_m (R_D // R_L)}{(g_m + 1/R_S) R_{sig} + 1} \end{aligned}$$

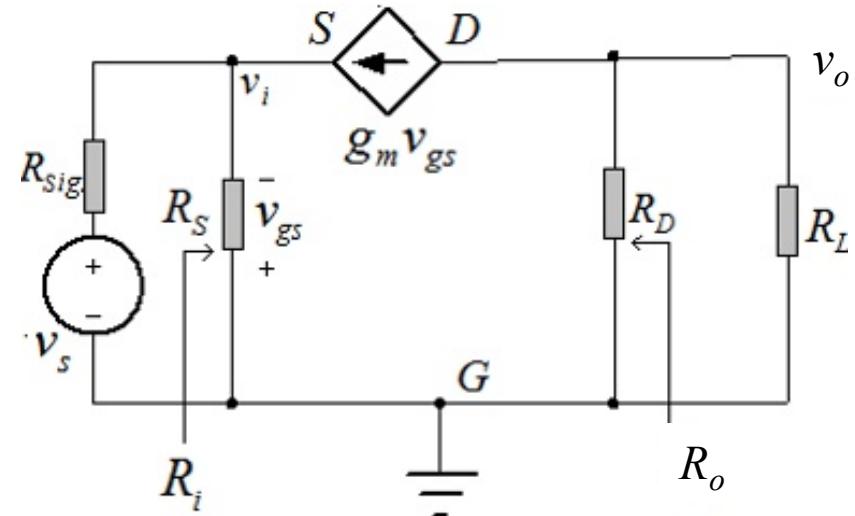
$$R_i = R_S // \frac{1}{g_m}$$

$$R_o \approx R_D$$

共栅放大器特性：

相当低的输入电阻、很大的输出电阻和接近于1的电流增益，且高频特性较好，频带宽。

共栅放大器可作为单位增益的电流缓冲放大器，又称为**电流跟随器**。



三种接法放大电路特性比较

接法	共源	共漏	共栅
A_v	适中	~ 1	适中
A_i	/	/	~ 1
R_i	大	大	小
R_o	大	小	大
频带	窄	中	宽