

Some Lecture Notes for

Statistical Mechanics

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CHAPTER 1

THERMODYNAMICS (TD)

1.1 Postulates and Laws

- TD is motivated by applications: steam engines
- TD deals with macroscopic equilibrium states.

Definition 1.1.1 (Macroscopic state). A description of a system based macroscopic measurements. Temperature, volume, mass, energy, pressure...

A macroscopic state is not infinitely precise. It doesn't refer to a particle.

Definition 1.1.2 (Equilibrium state). A macroscopic state that does NOT change in time. No net transfer of energy or particle or of the system.

Definition 1.1.3 (State function). A function of the small number of quantities that specifies an equilibrium state.

Main Assumption: For every equilibrium state there is a state function called the ENTROPY.

1.1.1 Postulates of TD

1. Existence of S:

$$S \equiv S(U, V, N).$$

The fundamental relation (in the entropy representation)

A macroscopic system has equilibrium states that are characterised uniquely by a small set of extensive variables.

Definition 1.1.4 (Extensive variables). Provides a measure of the size of a system. Answer “how much” questions. (U: energy, V:Volume, N:Number of particle (mass).)

The fundamental relation gives all TD info about the system. (because you can invert the equation above to get U,V,N)

2. **Maximisation:** The values of the extensive variables of an isolated system in the absence of an internal constraint are those that maximise the entropy over the set of all constrained macroscopic states. We have then:

Figure 1.1: Box with removable wall.

$$S(U_A, V_A, N_A, U_B, V_B, N_B)$$

$$U = U_A + U_B$$

same for V, N Removing wall, the values of U_A, V_A, N_A will be such that it maximises S .

3. **Additivity:** The entropy of a composite system is additive over its constituent subsystems.

$$S(X_A, X_B) = S(X_A) + S(X_B)$$

This is not true if there exist long range forces but usually well satisfied.

Hold whenever interactions between particles are much shorter than the system size.

4. **Continuity and Differentiability:** The entropy is a continuous and differentiable function of the extensive parameters. (NOT true at phase transitions.)
5. **Extensivity:** The entropy is an extensive function of its extensive variables.

$$S(\lambda U, \lambda V, \lambda N) = \lambda S(U, V, N) \quad \lambda \in \mathbb{R}$$

(Only holds if surface effects can be neglected.)

6. **Monotonicity:** The entropy is a monotonically increasing function of energy for equilibrium volumes of the energy.

$$\left. \frac{\partial S}{\partial U} \right|_{V,N} > 0$$

(Something funny happens at negative temperature.)

7. **Nernst postulate:** The entropy of any real physical system is non-negative.(Only applies to QM systems. Doesn't apply to f.eks ideal gas.)

Definition 1.1.5 (Temperature in TD).

$$\left(\frac{\partial S}{\partial U} \right)_{N,V} \equiv \frac{1}{T}$$

1.1.2 TD laws

- If two systems are in equilibrium with a third system, they are also in equilibrium with each other. (Their intensive variables are equal)
- Heat is energy and energy is conserved.
- After the release of a constraint in a closed system, the entropy never decreases.
- The entropy of a quantum mechanical system goes to a constant as $T \rightarrow 0$.

0th law: It follows from P.2(maximisation) and P.3(additivity).

$$S = S(U_A, V_A, N_A) + S(U_B, V_B, N_B)$$

$$U_B = U - U_A$$

Calculations

1.2 Small Changes: Inexact and exact differentials

Consider a function of 2 variables $F(x, y)$ The differential of this is:

$$df = \left(\frac{\partial f}{\partial x} \right)_y dx + \left(\frac{\partial f}{\partial y} \right)_x dy \quad (1.1)$$

This is an exact differential.

Exact differential gives a **unique (does not depend on the integration path)** function (up to a constant) when integrated.

$$\int_{(0,0)}^{(x,y)} df = \int_{(0,0)}^{(x,y)} \frac{\partial f}{\partial y} dy + \int_{(0,y)}^{(x,y)} \frac{\partial f}{\partial x} dx$$

Condition for exact differential:

$$\left(\frac{\partial f}{\partial y} \right)_x = \left(\frac{\partial g}{\partial x} \right)_y$$

But not every differential

$$df = f(x, y)dx + g(x, y)dy$$

is exact For instance:

$$dF = -ydx + xdy$$

is not exact. (The integral is path dependant.)

$$\int_{(0,0)}^{(x,y)} dF = \int_{(0,0)}^{(x,0)} -y dx + \int_{(x,0)}^{(x,y)} x dy = xy,$$

$$\int_{(0,0)}^{(x,y)} dF = \int_{(0,0)}^{(0,y)} x dy + \dots$$

Not the same.

We can always find an integrating non unique factor (function) so that

$$dG = r(x, y) dF$$

For

$$dF = -y dx + x dy$$

want

$$dG = (-r(x, y)y) dx + (r(x, y)x) dy$$

$$r = \frac{1}{xy}$$

This is the same thing as used when solving first order diff.equation.

Next: work and heat are not exact.

Conservation of energy: $dU = dQ$ (Heat added) + dW (work done **on** the system) U is a state function so dU is exact. dQ and dW are inexact as they cannot be derived.

Work

$$dW = F_{outer}^{\vec{}} \cdot d\vec{x} > 0 \quad (1.2)$$

$$F_{outer} = -F_{inside}$$

$$dW = -F_{inner} \cdot dx$$

$$dW = -pdV$$

$$-\frac{1}{p} dW = dV$$

Here $-1/p$ plays the role of an integrating factor.

$$\int_{(0,0)}^{(p,v)} = \int_{(0,0)}^{p,0} + \int_{(p,0)}^{p,V} -pdV = -pV$$

$$\int_{(0,0)}^{(p,v)} = \int_{(0,0)}^{(0,v)} -pdV = 0$$

Path dependant work can also be magnetic or electric.

Heat

$$\begin{aligned} dS &= S(U + \text{d}Q, V, N) - S(U, V, N) \\ &= \left(\frac{\partial S}{\partial U} \right)_{(v,N)} \text{d}Q \\ \implies \text{d}Q &= T dS \end{aligned}$$

$$dS = \frac{1}{T} \text{d}Q$$

Conservation of energy

$$dU = \text{d}Q + \text{d}W$$

$$dU = TdS - pdV$$

(N const)

$$\begin{aligned} U &= U(S, V, N) \\ dU &= \left(\frac{\partial U}{\partial S} \right)_{V,N} dS + \left(\frac{\partial U}{\partial V} \right)_{S,N} dV + \left(\frac{\partial U}{\partial N} \right)_{S,V} dN \\ \left(\frac{\partial U}{\partial S} \right)_{V,N} &= T \\ \left(\frac{\partial U}{\partial V} \right)_{S,N} &= -P \\ \left(\frac{\partial U}{\partial N} \right)_{(S,V)} &\equiv \mu \end{aligned}$$

With N varying:

$$dU = TdS - PdV + \mu dN$$

In entropy representation:

$$\begin{aligned} S &= S(U, V, N) \\ dS &= \left(\frac{\partial S}{\partial U} \right)_{(V,N)} dU + \left(\frac{\partial S}{\partial V} \right)_{U,N} dV + \left(\frac{\partial S}{\partial N} \right)_{U,V} dN \end{aligned}$$

$$dS = \frac{1}{T}dV + \frac{P}{T}dV - \frac{\mu}{T}dN$$

1.2.1 TD Processes

For all processes in a closed system,

$$dS \geq 0$$

$dS = 0$ when system is already in equilibrium.

Processes when $dS > 0$ in termed irreversible.

Quasistatic process

Definition 1.2.1. In the limit of infinitesimal changes at an equilibrium system (very slow ideal process)

$$\Rightarrow dS = 0$$

It's an idealisation, doesn't exist.

Heat Engines

Produce work from heat (steam engine).

Such engines are cyclic,

$$dU = 0, \quad dS = 0, \quad dV = 0, \quad dN = 0$$

in a cycle.

$$dU = 0 \implies \mathrm{d}Q + \mathrm{d}W = 0$$

$$\implies -\mathrm{d}W = \mathrm{d}Q$$

$$dS = 0$$

$$T\mathrm{d}Q = 0$$

This shit doesn't do any work, new engine: Need a hot and a cold reservoir (to dump heat)

$$\frac{\mathrm{d}Q_i}{T_i} - \frac{\mathrm{d}Q_o}{T_o} = 0$$

$$\implies \mathrm{d}Q_o = \frac{T_i}{T_o}\mathrm{d}Q_i$$

$$\mathrm{d}Q_i - \mathrm{d}Q_o + \mathrm{d}W = 0$$

$$\implies -\mathrm{d}W = \mathrm{d}Q_i \left(1 - \frac{T_o}{T_i}\right)$$

Efficiency

$$\eta = \frac{-\mathrm{d}W}{\mathrm{d}Q_i} = 1 - \frac{T_o}{T_i} = \frac{T_i - T_o}{T_i}$$

Fridge and Air conditioners

Diagram

Fridges are heat engines run in reverse.

$$\mathrm{d}W + \mathrm{d}Q_I - \mathrm{d}Q_o = 0 \quad (dU = 0)$$

$$\frac{\mathrm{d}Q_I}{T_I} - \frac{\mathrm{d}Q_o}{T_o} \quad dS = 0$$

Coefficient of Performance is

$$COP_{cooling} = \frac{-\mathrm{d}Q_o}{\mathrm{d}W}$$

$$\implies \mathrm{d}Q_I = T_I \frac{\mathrm{d}Q_o}{T_o}$$

$$\left(\mathrm{d}W + \left(\frac{T_I}{T_o} - 1 \right) \mathrm{d}Q_o \right) = 0$$

Reduce efficiency as $T_o \rightarrow 0$.

Heat Pumps

Same as re Fridgerators, but inside of fridge is outside of the house.

$$COP_{heating} = \frac{\mathrm{d}Q_I}{\mathrm{d}W} = \frac{1}{1 - \frac{T_o}{T_I}} = \frac{T_I}{T_I - T_o}$$

with

$$\mathrm{d}Q_o = \frac{T_o}{T_I} \mathrm{d}Q_I$$

$$\mathrm{d}W + \mathrm{d}Q_I - \frac{T_o}{T_I} \mathrm{d}Q_I = 0$$

$$\mathrm{d}W = \mathrm{d}Q_I \left(\frac{T_o}{T_I} - 1 \right)$$

For a non-reversible engine:

$$dS = \frac{\mathrm{d}Q_I}{T_I} - \frac{\mathrm{d}Q_o}{T_o} + \mathrm{d}A$$

A is the positive entropy generated in a cycle.

1.3 TD Potentials

Fundamental relation:

$$S = S(U, V, N) \text{ or } U = U(S, V, N)$$

from this we can derive all TD.

Example 1.3.1 (Ideal Gas).

$$S = Nk_B \left(\frac{3}{2} \ln\left(\frac{V}{N}\right) + \ln\left(\frac{V}{N}\right) + \ln X \right)$$

where X is independent of U, V, N

$$\begin{aligned} \frac{1}{T} &= \frac{\partial S}{\partial U}_{V,N} = \frac{3}{2} Nk_B \frac{1}{U} \\ \implies U &= \frac{3}{2} Nk_B T \\ \frac{P}{T} &= \frac{\partial S}{\partial V}_{U,N} = \frac{Nk_B}{V} \\ \implies PV &= Nk_B T \\ -\frac{\mu}{T} &= \frac{\partial S}{\partial N}_{U,V} = \frac{S}{N} - Nk_B \frac{5}{2} \frac{1}{N} = \frac{S}{N} - \frac{5}{2} k_B \\ \implies S &= \frac{5}{2} k_B N - \frac{\mu N}{T} \end{aligned}$$

These are all equations of states, not fundamental relations.

How can we extract TD info at constant T, P etc. ?

$$T = \frac{\partial U}{\partial S}_{V,N} - \frac{\partial U}{\partial V}_{S,N}$$

1.3.1 Legendre Transform

Given $y = y(x)$ let's call $\frac{\partial y}{\partial x} = p$

$$\tilde{y}(p)$$

Try $\tilde{y} = y$ and make a table.

Useless, no way to know where on the x-axis.

$$\begin{array}{cc} p & y \\ \dots & \dots \end{array}$$

Second try: replace \tilde{y} by the y-intercept of the curved tangent. This works, but requires $\frac{\partial y}{\partial x}$ monotonic (as temperature is).

$$y - \tilde{y} = px$$

$$\tilde{y} = y - px$$

Example 1.3.2.

$$y = x^2$$

$$p = \frac{\partial y}{\partial x} = 2x \implies x = \frac{p}{2}$$

$$\tilde{y}(p) = y - px = x^2 - px = \frac{p^2}{2} - p\frac{p}{2} = -\frac{p^2}{2}$$

Inverse:

$$y(x) = \tilde{y} + px = -\frac{p^2}{2} + px = -\frac{(2x)^2}{2} + 2x^2 = x^2$$

Differentials:

$$d\tilde{y} = dy - p dx - x dp = -x dp$$

$$dy = d\tilde{y} + x dp + p dx = p dx$$

Switches and negative.

1.3.2 Helmholtz free energy

$$U = U(S, V, N)$$

want a function of T, V, N that gives all TD info.

$$T = \frac{\partial U}{\partial S}_{V,N}$$

$$F = U - TS$$

eliminate U, S in favour of T, V, N

$$= F(T, V, N)$$

(is a fundamental relation.)

$$dF = dU - T dS - S dT$$

recall $dU = T dS - P dV + \mu dN$

$$= -S dT - P dV + \mu dN$$

$$\implies -S = \frac{\partial F}{\partial T}_{V,N} \quad -P = \frac{\partial F}{\partial V}_{T,N} \quad \mu = \frac{\partial F}{\partial N}_{T,V}$$

1.3.3 Enthalpy

P instead of v .

$$p = - \left(\frac{\partial U}{\partial V} \right)_{S,N}$$

$$H = U + PV$$

want to eliminate V

$$= H(S, P, N)$$

$$dH = TdS + VdP + \mu dN$$

$$T = \frac{\partial H}{\partial S}_{P,N} \quad V = \frac{\partial H}{\partial P}_{S,N} \quad \mu = \frac{\partial H}{\partial N}_{S,P}$$

For experiments at constant P, N Then

$$dH = TdS = \delta Q$$

or

$$dH = \delta Q$$

(No integrating factor since it's one dimensional.)

1.3.4 Gibbs free energy

Double Legendre transform: replace S with T and replace V by P .

$$G = U - TS + PV = G(T, P, N)$$

$$dG = -SdT + VdP + \mu dN$$

$$-S = \frac{\partial G}{\partial T}_{P,N}, \quad V = \frac{\partial G}{\partial P}_{T,N} \quad \mu = \frac{\partial G}{\partial N}_{P,T}$$

1.3.5 Summary

- Energy: $U(S, V, N)$
- Helmholtz $F(T, V, N) = U - TS$
- Enthalpy $H(S, P, N) = U + PV$
- Gibbs: $G(T, P, N) = U - TS + PV$
- $f(S, V, \mu) = U - \mu N$
- Grand potential (Landau potential) : $\Omega(T, V, \mu) = U - TS - \mu N$
- $f(S, P, \mu) = U + PV - \mu N$
- $f(T, P, \mu) = U - TS + PV - \mu N$

1.4 Extensivity

From the postulate,

$$S(\lambda U, \lambda V, \lambda N) = \lambda S(U, V, N)$$

in systems where surface effect can be neglected.

Assume that it holds: For energy:

$$U(\lambda S, \lambda V, \lambda N) = \lambda U(S, V, N)$$

Now vary λ : Differentiate w.r.t λ and let $\lambda = 1$

$$\begin{aligned} \text{LHS} &= \frac{\partial}{\partial \lambda} U(\lambda S, \lambda V, \lambda N) = \frac{\partial}{\partial(\lambda S)} U(\lambda S, \lambda V, \lambda N) \left(\frac{\partial(\lambda S)}{\partial \lambda} \right)_{\lambda=1} + \frac{\partial}{\partial(\lambda V)} U(\lambda S, \lambda V, \lambda N) \left(\frac{\partial(\lambda V)}{\partial \lambda} \right)_{\lambda=1} \\ &\quad + \frac{\partial}{\partial(\lambda N)} U(\lambda S, \lambda V, \lambda N) \\ \text{RHS} &= U(S, V, N) \\ \implies TS - PV + \mu N &= U \quad \text{Euler's equation} \end{aligned} \tag{1.3}$$

For the entropy equation:

$$S = \frac{U}{T} + \frac{P}{T}V - \frac{\mu}{T}N.$$

Same stuff.

1.4.1 Gibbs-Duhem relation

Euler's equation:

$$U = TS - PV + \mu N$$

differentiate:

$$dU = \underbrace{TdS - PdV + \mu dN}_{dU} + SdT - VdP + Nd\mu$$

$$\implies 0 = SdT - VdP + Nd\mu \tag{1.4}$$

So changes in T, P, N are not independent for an extensive system.

For instance:

$$d\mu = -\frac{S}{N}dT + \frac{V}{N}dP$$

1.4.2 TD Potentials and Extensivity

$$\text{Euler's Equation } U = TS - PV + \mu N$$

$$\text{Helmholtz } F = U - TS = -PV + \mu N$$

$$\text{Enthalpy } H = U + PV = TS + \mu N$$

$$\text{Gibbs } G = U - TS + PV = \mu N$$

$$f(T, P, \mu) = U - TS + PV - \mu N = 0 \quad \text{Check on extensivity}$$

1.5 TD identities

Derivatives: What is held constant matters!

Ideal gas:

$$U = \frac{3}{2}Nk_B T, \quad PV = Nk_B T$$

$$\frac{\partial U}{\partial V}_{T,N} = 0$$

$$\frac{\partial U}{\partial V}_{P,N} = \frac{\partial}{\partial V} \left(\frac{3}{2}PV \right)_{P,N} = \frac{3}{2}P$$

$$\frac{\partial U}{\partial V}_{S,N} = -P$$

Other TD potentials

$$dF = -SdT - PdV + \mu dN$$

See previous section for derivatives. We are often interested in quantities like

$$\frac{\partial V}{\partial P}_{T,N} = \left(\frac{\partial^2 G}{\partial P^2} \right)_{T,N} = -V\kappa_T$$

1.5.1 Standard Quantities

Coefficient of thermal expansion:

$$\alpha \equiv \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_{P,N} \quad (1.5)$$

Isothermal compressibility:

$$\kappa_T = -\frac{1}{V} \left(\frac{\partial V}{\partial P} \right)_{T,N} \quad (1.6)$$

The negative sign in front is because most substance shrink when applying pressure.

Specific heat at constant pressure:

$$C_p = \frac{T}{N} \left(\frac{\partial S}{\partial T} \right)_{P,N} \quad (1.7)$$

Specific heat at constant volume:

$$C_v = \frac{T}{N} \left(\frac{\partial S}{\partial T} \right)_{V,N} \quad (1.8)$$

Heat capacity: = specific heat $\times N$

1.5.2 Maxwell Relations

For N constant:

$$dU = TdS - PdV$$

because dU is an exact differential (orders of derivative doesn't matter):

$$\left(\frac{\partial T}{\partial V} \right)_{S,N} = - \left(\frac{\partial P}{\partial S} \right)_{V,N}$$

From

$$dF = -SdT - PdV + \mu dN$$

$$\frac{\partial S}{\partial V}_{V,N} = \frac{\partial P}{\partial T}_{V,N}$$

and from unnamed potential:

$$\left(\frac{\partial T}{\partial P} \right)_{S,N} = \left(\frac{\partial V}{\partial S} \right)_{P,N}$$

1.6 Manipulating partial derivatives as Jacobians

Jacobian:

$$\frac{\partial(U, V)}{\partial(x, y)} \equiv \begin{bmatrix} \frac{\partial U}{\partial x} & \frac{\partial U}{\partial y} \\ \frac{\partial V}{\partial x} & \frac{\partial V}{\partial y} \end{bmatrix} = \frac{\partial U}{\partial x} \frac{\partial V}{\partial y} - \frac{\partial U}{\partial y} \frac{\partial V}{\partial x} \quad (1.9)$$

can be extended to any number of variables by adding rows and columns.

Property of Jacobians

$$\begin{aligned} \frac{\partial(U, V)}{\partial(x, y)} &= - \frac{\partial(V, U)}{\partial(x, y)} \\ &= - \frac{\partial(U, V)}{\partial(y, x)} = \frac{\partial(V, U)}{\partial(y, x)} \end{aligned}$$

1.6.1 Connection to partial derivatives

$$\frac{\partial(U, y)}{\partial(x, y)} = \begin{bmatrix} \frac{\partial U}{\partial x} & \frac{\partial U}{\partial y} \\ \frac{\partial y}{\partial x} & \frac{\partial y}{\partial y} \end{bmatrix} = \left(\frac{\partial U}{\partial x} \right)_y$$

So

$$\left(\frac{\partial F}{\partial T} \right)_{V, N} = \frac{\partial(F, V, N)}{\partial(T, V, N)}$$

Chain rule:

$$\begin{aligned} \frac{\partial(U, V)}{\partial(x, y)} &= \frac{\partial(U, V)}{\partial(r, s)} \frac{\partial(r, s)}{\partial(x, y)} \\ &= \begin{vmatrix} U_r & U_s \\ V_r & V_s \end{vmatrix} \cdot \begin{vmatrix} r_x & r_y \\ s_x & s_y \end{vmatrix} \\ &= \begin{vmatrix} U_r r_x + U_s s_x & U_r r_y + U_s s_y \\ V_r r_x + V_s s_x & V_r r_y + V_s s_y \end{vmatrix} \end{aligned}$$

Using rule:

$$\det(AB) = \det(A)\det(B)$$

An identity:

$$\frac{\partial(U, V)}{\partial(x, y)} \frac{\partial(a, b)}{\partial(c, d)} = \frac{\partial(u, v)}{\partial(c, d)} \frac{\partial(a, b)}{\partial(x, y)}$$

chain rule gives:

$$\begin{aligned} \frac{\partial(U, V)}{\partial(x, y)} \frac{\partial(a, b)}{\partial(c, d)} &= \frac{\partial(U, V)}{\partial(r, s)} \frac{\partial(r, s)}{\partial(x, y)} \frac{\partial(a, b)}{\partial(r, s)} \frac{\partial(r, s)}{\partial(c, d)} \\ &= \frac{\partial(U, V)}{\partial(r, s)} \frac{\partial(r, s)}{\partial(c, d)} \frac{\partial(a, b)}{\partial(r, s)} \frac{\partial(r, s)}{\partial(x, y)} \\ &= \frac{\partial(U, V)}{\partial(c, d)} \frac{\partial(a, b)}{\partial(x, y)} \end{aligned}$$

Reciprocals:

$$\frac{\partial(U, V)}{\partial(U, V)} = \begin{vmatrix} \frac{\partial U}{\partial U} & \frac{\partial U}{\partial V} \\ \frac{\partial V}{\partial U} & \frac{\partial V}{\partial V} \end{vmatrix} = \begin{vmatrix} 1 & 0 \\ 0 & 1 \end{vmatrix}$$

chain rule:

$$\begin{aligned} 1 &= \frac{\partial(U, V)}{\partial(U, V)} = \frac{\partial(U, V)}{\partial(x, y)} \frac{\partial(x, y)}{\partial(U, V)} \\ &\implies \left(\frac{\partial U}{\partial x} \right)_y = \frac{\partial(U, y)}{\partial(x, y)} \\ &= \left(\frac{\partial(x, y)}{\partial(U, y)} \right)^{-1} \end{aligned}$$

Example 1.6.1.

$$\left(\frac{\partial P}{\partial T}\right)_{V,N}$$

in terms standard quantities. Standard quantities:

$$\alpha = \left(\frac{\partial V}{v\partial T}\right)_{P,N}$$

$$K_T = -\frac{1}{V} \left(\frac{\partial V}{\partial P}\right)_{T,N}$$

$$C_p = \frac{T}{N} \left(\frac{\partial S}{\partial T}\right)_{P,N}$$

$$\begin{aligned} \left(\frac{\partial P}{\partial T}\right)_{V,N} &= \frac{\partial(P, V, N)}{\partial(T, V, N)} = \frac{\partial(P, V, N)}{\partial(P, T, N)} \underbrace{\frac{\partial(P, T, N)}{\partial(T, V, N)}}_{-\partial(V, T, N)} - \left(\frac{\partial V}{\partial T}\right)_{P,N} \left(\frac{\partial P}{\partial V}\right)_{T,N} \\ &= \frac{1}{V} \left(\frac{\partial V}{\partial T}\right)_{P,N} \frac{1}{-\frac{1}{V} \left(\frac{\partial V}{\partial P}\right)_{T,N}} \\ &= \frac{\alpha}{\kappa_T} \end{aligned}$$

Example 1.6.2. $\left(\frac{\partial T}{\partial P}\right)_{H,N}$ in terms of std. quantities.

$$\begin{aligned} \left(\frac{\partial T}{\partial P}\right)_{H,N} &= \frac{\partial(T, H, N)}{\partial(P, H, N)} = \frac{\partial(T, H, N)}{\partial(T, P, N)} \frac{\partial(T, P, N)}{\partial P, H, N} = -\frac{\partial(H, T, N)}{\partial(P, T, N)} \frac{\partial(T, P, N)}{\partial(H, P, N)} = \frac{\left(\frac{\partial H}{\partial P}\right)_{T,N}}{\left(\frac{\partial H}{\partial T}\right)_{P,N}} \\ &= \frac{V(T\alpha - 1)}{NC_p} \end{aligned}$$

$$dH = TdS + VdP + \mu dN$$

$$\left(\frac{\partial H}{\partial P}\right)_{T,N} = T \left(\frac{\partial S}{\partial P}\right)_{T,N} + V = V - T \left(\frac{\partial V}{\partial T}\right)_{P,N}$$

Want $\left(\frac{\partial S}{\partial P}\right)_{T,N}$ Maxwell relation

$$-SdT + VdP + \mu dN = 0$$

$$\implies \left(\frac{\partial S}{\partial P}\right)_{T,N} = -\left(\frac{\partial V}{\partial T}\right)_{P,N}$$

$$\left(\frac{\partial H}{\partial T}\right)_{P,N} = T \left(\frac{\partial S}{\partial T}\right)_{P,N}$$

$$dH = TdS \implies \Delta H = T\Delta S$$

$$\frac{\Delta H}{\Delta T} = \frac{T\Delta}{\Delta T} = \frac{T(S(T + \Delta T) - S(T))}{\Delta T}$$

$$\frac{\Delta H}{\Delta T} = \frac{T\Delta S}{\Delta T}$$

Which T ? $T, T + \Delta T$ or something else? Check an arbitrary $T + g\Delta T$

$$\frac{\Delta H}{\Delta T} = \frac{(T + g\Delta T)\Delta S}{\Delta T} = \frac{T\Delta S}{\Delta T} + g\Delta S \rightarrow 0 \quad \text{when } \Delta \rightarrow 0$$

$$\left(\frac{\partial H}{\partial T}\right)_{P,N} = T \left(\frac{\partial S}{\partial T}\right)_{P,N}$$

Example 1.6.3 (C_p and C_v).

$$\begin{aligned} C_v &= \frac{T}{N} \left(\frac{\partial S}{\partial T}\right)_{V,N} = \frac{T}{N} \frac{\partial(S, V, N)}{\partial(T, V, N)} \\ &= \frac{T}{N} \frac{\partial(S, V, N)}{\partial(T, P, N)} \underbrace{\frac{\partial(T, P, N)}{\partial(T, V, N)}}_{\frac{\partial(P, T, N)}{\partial(V, T, N)} = \frac{1}{\left(\frac{\partial V}{\partial P}\right)_{T,N}}} \\ &= -\frac{T}{NVK_T} \frac{\partial(S, V, N)}{\partial(T, P, N)} \end{aligned}$$

$$\begin{aligned} \frac{\partial(S, V, N)}{\partial(T, P, N)} &= \left(\frac{\partial S}{\partial T}\right)_{P,N} \left(\frac{\partial V}{\partial P}\right)_{T,N} - \left(\frac{\partial V}{\partial T}\right)_{P,N} \left(\frac{\partial S}{\partial P}\right)_{T,N} \\ &= \frac{NVC_P\kappa_T}{T} + (\alpha V)^2 \\ \Rightarrow C_V &= \frac{-T}{NVK_T} \left(\frac{-NVC_P\kappa_T}{T} + (\alpha V)^2 \right) \end{aligned}$$

or

$$C_P = C_V + \frac{T\alpha^2 V}{NK_T}$$

1.7 Extrema Principles

TD postulate: $S = S(U, V, N, X)$ (N unconstrained extensive variable), is maximized for U, V, N constant as a function of X . X is the position of the wall. In equilibrium:

$$\frac{\partial S}{\partial X}_{U,V,N,X_0} = 0$$

X_0 is the equilibrium value.

$$\frac{\partial^2 S}{\partial x^2}_{U,V,N,X_0} < 0$$

since entropy is max.

Similarly, $U = U(S, V, N, X)$ is minimized for S, V, N constant.

Proof. Near equilibrium at constant V and N

$$dS = \frac{\partial S}{\partial U}_{V,N,X_0,U_0} dU + \frac{\partial S}{\partial X}_{U,V,N,X_0} dX + \frac{1}{2} \left(\frac{\partial^2 S}{\partial X^2} \right)_{U,V,N,X_0} dX^2$$

$$\implies dU = T dS - \frac{T}{2} \left(\frac{\partial^2 S}{\partial X^2} \right)_{U,V,N,X_0} dX^2$$

For S, V, N constant:

$$dU = -\frac{T}{2} \left(\frac{\partial^2 S}{\partial X^2} \right)_{U,V,N,X_0} dX^2 > 0$$

U has a minimum in equilibrium for S, V, N constant. □

Process is where entropy is constant and system minimises energy by doing work on the surroundings.

1.7.1 Helmholtz Free Energy F

F is minimal in equilibrium for constant T, V, N

A big box with system inside and within the system there's a movable wall with a piston connected to the wall which goes outside of the system and the box. Outside the system inside the box is the reservoir, can exchange heat, but with V, N constant. In equilibrium:

$$\frac{\partial(U + U_R)}{\partial X} = 0 \quad \text{for const. } V + V_R, N + N_R, S + S_R$$

where U is system energy.

$$\frac{\partial^2}{\partial X^2}(U + U_R) > 0$$

Entropy is conserved: $\frac{\partial(S+S_R)}{\partial X} = 0$

$$F = U - TS$$

$$\begin{aligned} \frac{\partial F}{\partial X} &= \frac{\partial U}{\partial X} - \frac{\partial}{\partial X}(T_R S) = \frac{\partial U}{\partial X} - T_R \frac{\partial S}{\partial X} \\ &= \frac{\partial U}{\partial X} + T_R \frac{\partial S_R}{\partial X} \end{aligned}$$

Since reservoir can't do work or anything

$$T dS = dU$$

so

$$\begin{aligned} &= \frac{\partial}{\partial X}(U + U_R) = 0 \\ \frac{\partial^2 F}{\partial X^2} &= \frac{\partial^2 U}{\partial X^2} + \frac{\partial^2 U_R}{\partial X^2} = \frac{\partial^2}{\partial X^2}(U + U_R) > 0 \end{aligned}$$

The max work that can be extracted:

$$dF = -SdT + dW + \mu dN$$

with $dW = -PdV + dW'$ and dW' is other work For constant T, V, N

$$dF = dW'$$

Free energy Enthalpy and Gibbs free energy are also minimized in equilibrium (see 15.3 and 15.4, Swendsen.)

1.7.2 Exergy

$$dU = TdS - PdV + dW_X + \mu dN$$

dW_X is work on system by moving internal wall. For constant T, P, N , G is minimized

$$dG = -SdT + VdP + \mu dN + dW_X$$

$$\implies dG = dW_X$$

at $P = P_0, T = T_0$ standard $T_0 = \text{room temp}, P_0 = 1\text{atm}$.

$$\text{Exergy} = G(T_0, P_0, X) - G(T_0, P_0, X_0)$$

This is the amount of work that can be extracted at standard pressure and temperature. (Important in engineering for machines in real environment.)

1.8 Stability Conditions

1.8.1 Composite system

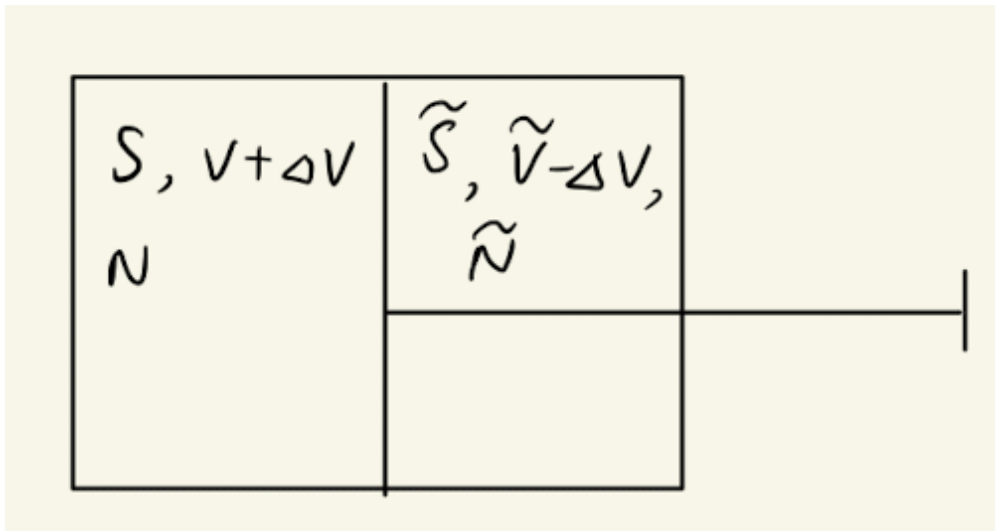


Figure 1.2: Composite system

Using the additivity postulate:

$$\Delta U = U(S, V + \Delta V, N) + \tilde{U}(\tilde{S}, \tilde{V} - \Delta V, \tilde{N}) - (U(S, V, N) + U(\tilde{S}, \tilde{V}, \tilde{N})) \geq 0 \quad (1.10)$$

The second term is the equilibrium energy, and it's minimised.

Specialise to identical systems:

$$\tilde{U} = U$$

Then

$$\Delta U = U(S, V + \Delta V, N) - U(S, V - \Delta V, N) - 2U(S, V, N) \geq 0$$

For ΔV infinitesimal:

$$\begin{aligned} & \frac{\partial^2 U}{\partial V^2} (\Delta V)^2 \\ \Rightarrow & \left(\frac{\partial^2 U}{\partial V^2} \right)_{S,N} \geq 0 \\ dU = & TdS - PdV + \mu dN \\ \frac{\partial U}{\partial V}_{S,V} = & -P \\ \left(\frac{\partial^2 U}{\partial^2} \right)_{S,N} = & -\frac{1}{\left(\frac{\partial V}{\partial P} \right)_{S,V}} \\ = & \frac{1}{VK_s} \geq 0 \\ & K_s > 0 \end{aligned} \quad (1.11)$$

where K_s is the isentropic compressibility.

1.8.2 Heat Transfer

$$\Delta U = U(S + \Delta S, V, N) - U(S - \Delta S, V, N) - 2U(S, V, N) \geq 0$$

$$\left(\frac{\partial^2 U}{\partial S^2} \right)_{V,N} \geq 0$$

$$\left(\frac{\partial U}{\partial S} \right)_{V,N} = T \implies$$

$$\left(\frac{\partial^2 U}{\partial S^2} \right)_{V,N} = \left(\frac{\partial T}{\partial S} \right)_{V,N} = \left[\left(\frac{\partial S}{\partial T} \right)_{V,N} \right]^{-1}$$

$$= \left[\frac{N}{T} \frac{T}{N} \left(\frac{\partial S}{\partial T} \right)_{V,N} \right]^{-1} \geq 0$$

1.8.3 Volume Exchange for Helmholtz Free Energy

$$\Delta F = F(T, V + \Delta V, N) - F(T, V - \Delta V, N) - 2F(T, V, N) \geq 0$$

$$\left(\frac{\partial^2 F}{\partial V^2} \right)_{T,N} \geq 0$$

$$\implies \left(\frac{\partial F}{\partial V} \right)_{T,N} = -P$$

$$\left(\frac{\partial^2 F}{\partial V^2} \right)_{T,N} = \left(\frac{\partial P}{\partial V} \right)_{T,N} = \left[v \frac{1}{-v} \left(\frac{\partial V}{\partial P} \right)_{T,N} \right]^{-1}$$

$$\frac{1}{V K_T} \geq 0$$

$$\implies K_T \geq 0$$

1.8.4 Heat Exchange for Enthalpy

$$H(S + \Delta S, P, N) - H(S - \Delta S, P, N) - 2H(S, P, N) \geq 0$$

$$\implies \left(\frac{\partial^2 H}{\partial S^2} \right)_{P,N} \geq 0$$

$$\left(\frac{\partial H}{\partial S} \right)_{P,N} = T$$

$$\left(\frac{\partial^2 H}{\partial S^2} \right)_{P,N} = \left[\left(\frac{\partial S}{\partial T} \right)_{P,N} \right]^{-1} \geq 0$$

$$\implies C_p \geq 0$$

The stability conditions that we have derived so far are only valid for **extensive** variables!

1.8.5 What about intensive variables?

We use TD relations.

$$\left(\frac{\partial F}{\partial T}\right)_{V,N} = -S, \quad \left(\frac{\partial^2 F}{\partial T^2}\right)_{V,N} = -\left(\frac{\partial S}{\partial T}\right) = \frac{-1}{\left(\frac{\partial^2 U}{\partial S^2}\right)_{V,N}} < 0$$

$$\left(\frac{\partial U}{\partial S}\right)_{V,N} = T, \quad \left(\frac{\partial^2 U}{\partial S^2}\right)_{V,N}$$

so

$$\left(\frac{\partial^2 F}{\partial T^2}\right)_{V,N} < 0 \quad (1.12)$$

1.8.6 Van der Waal's gas

Ideal gas:

$$F = -Nk_B T \left[\ln\left(\frac{V}{N}\right) + \frac{3}{2} \ln(k_B T) + X \right]$$

Free, non-interacting particles

Include interactions "treated crudely":

The interaction has two main effects:

1. Energy is lowered by the mean interaction energy $\propto \frac{N}{V}$ per particle.
2. The hard-core potential restricts the volume to $V \rightarrow V - Nb$

$$F_{VDW} = -Nk_B T \left[\ln\left(\frac{V - Nb}{N}\right) + \frac{3}{2} \ln(k_B T) + X \right] - a \frac{N^2}{V}$$

where a (measure of attraction) and b (hard-core) are constants. This is an extensive system, meaning we could use the Euler's equation.

Pressure:

$$P = -\left(\frac{\partial F}{\partial V}\right)_{T,N} = \frac{Nk_B T}{V - Nb} + a \frac{N^2}{V^2}$$

Stability:

$$\left(\frac{\partial^2 F}{\partial V^2}\right)_{T,N} \geq$$

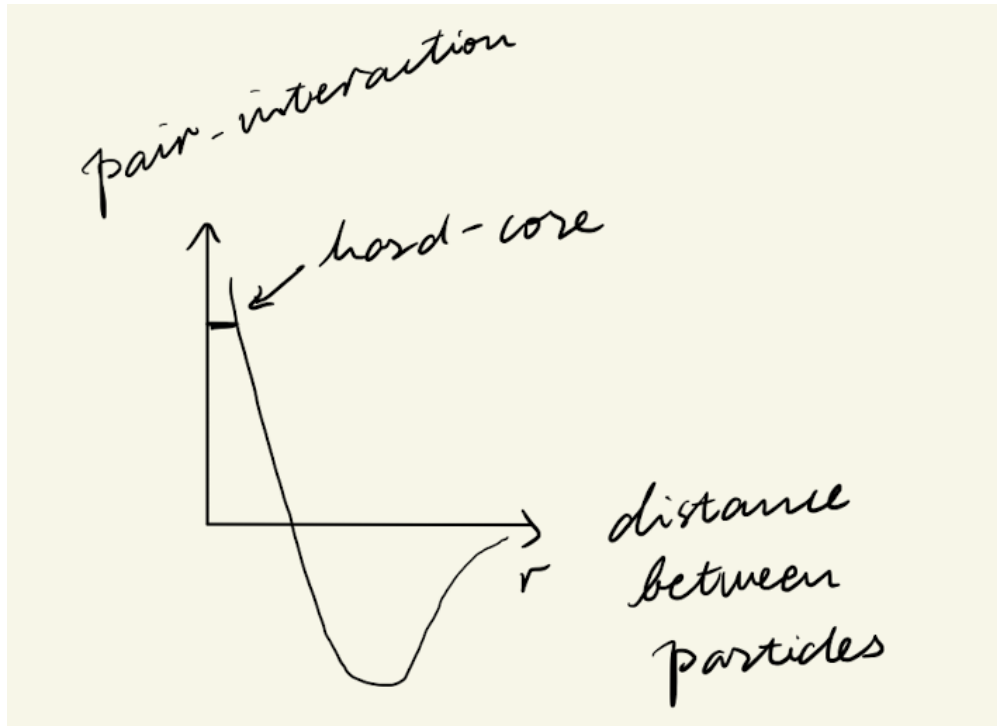


Figure 1.3: Van der Waal interaction model.

$$\left(\frac{\partial F}{\partial V}\right)_{T,N} = -P$$

$$\left(\frac{\partial^2 F}{\partial V^2}\right)_{T,N} = -\left(\frac{\partial P}{\partial V}\right)_{T,N} > 0$$

$$\Rightarrow \left(\frac{\partial P}{\partial V}\right)_{T,N} < 0$$

The highlighted part is unstable since $\left(\frac{\partial P}{\partial V}\right)_{T,N} \geq 0$.

Want to calculate the critical temperature T_c :

$$\left(\frac{\partial P}{\partial V}\right)_{T,N} = 0 = \left(\frac{\partial^2 P}{\partial V^2}\right)_{T,N} = 0$$

$$\frac{\partial P}{\partial V} = \frac{-Nk_B T}{(V - Nb)^2} + 2a \frac{N^2}{V^3} = 0$$

$$\Rightarrow Nk_B T V^3 = 2aN^2(V - Nb)^2$$

$$\left(\frac{\partial^2 P}{\partial V^2}\right) = \frac{2Nk_B T}{(V - Nb)^3} - 6a \frac{N^2}{V^4} = 0$$

$$\Rightarrow 2Nk_B T V^4 = 6aN^2(V - Nb)^3$$

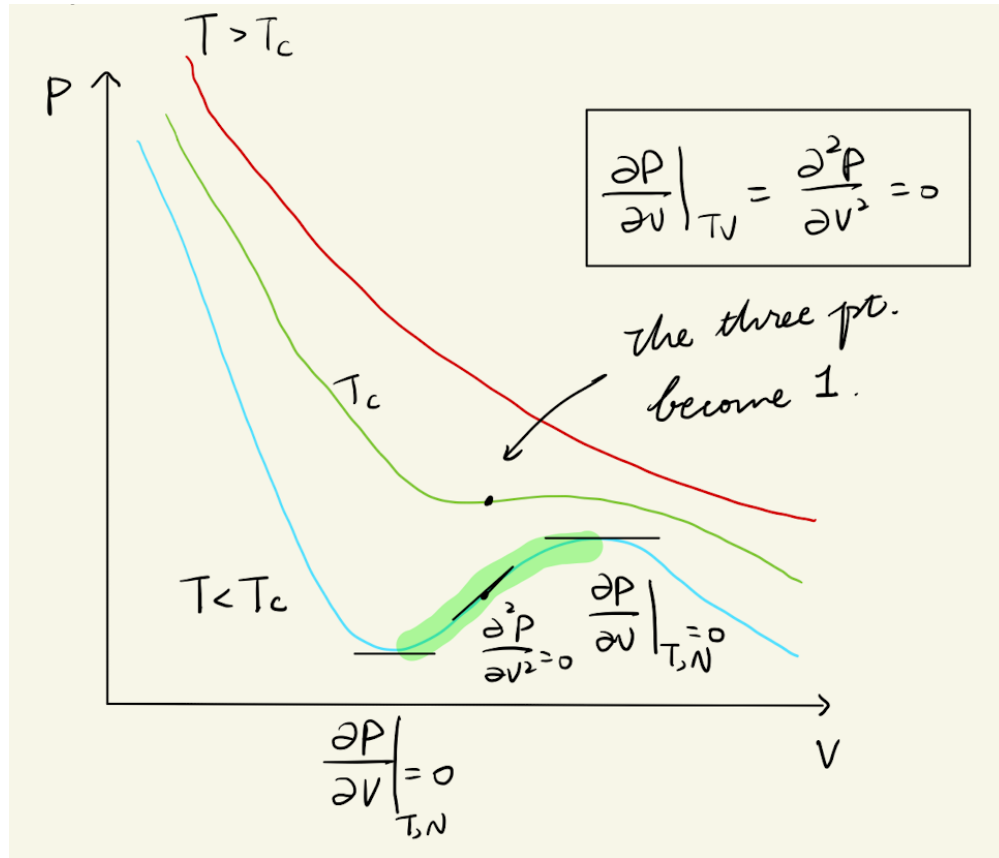


Figure 1.4: Pressure vs Volume diagram.

Combine:

$$2V = 3(V - Nb)$$

and

$$k_B T_c = \frac{2aN^2(3Nb - Nb)^2}{N(3Nb)^3} = \frac{8}{27} \frac{a}{b}$$

$$P_c = \frac{N_k B T}{V_c - Nb} - a \frac{N^2}{V_c^2} = \frac{1}{27} \frac{a}{b^2}$$

$$\frac{P_c V_c}{N k_B T_c} = \frac{3}{8}$$

Ideal gas: 1

insert **Fig.4** Both unphysical, unstable.

$$P = - \left(\frac{\partial F}{\partial V} \right)_{T,N}$$

$$\left(\frac{\partial P}{\partial V}\right)_{T,N} = -\left(\frac{\partial^2 F}{\partial V^2}\right)_{T,N} < 0$$

For stability.

$$V = \left(\frac{\partial G}{\partial P}\right)_{T,N}$$

$$\left(\frac{\partial V}{\partial P}\right)_{T,N} = \left(\frac{\partial^2 G}{\partial P^2}\right)_{T,N} < 0$$

second derivative of intensive variable less than 0 for stability.

insert Fig.5 Cap: Van der Waal's gas at $T < T_C$ Stability

$$\left(\frac{\partial^2 F}{\partial V^2}\right)_{T,N} > 0 \Rightarrow \left(\frac{\partial P}{\partial V}\right)_{T,N} < 0$$

This is violated on D-F. Assumption of homogeneity breaks down. The homogeneous solution is unstable (unphysical. NOT realised) on D-F.

insert Fig.6 Maxwell construct: Choose a line which crosses the graph 3 times which also divides the area into 2 equal parts. In the region B-H there are 3 possible values for V given a P (one is unphysical (DF), but there are still two to choose from.) TD stable state at const. P, T, N minimises **Gibbs free energy**. Calculate G ! Van der Waal's gas is extensive:

$$U = TS - PV + \mu N$$

$$G = U - TS + PV = \mu N$$

Recall Gibbs-Duhem relation:

$$d\mu = -\left(\frac{S}{N}\right)dT + \left(\frac{V}{N}\right)dP = \frac{V}{N}dP$$

$$\Rightarrow G = \int dG = \int d\mu N = \int dPV$$

Area under the curve.

$$V = \left(\frac{\partial G}{\partial P}\right)_{T,N}$$

At C, G there are two phases that coexists: V_C and V_G Since V_C is bigger than V_G , so V_C describes a gas phase and V_G describes a liquid phase.

insert Fig.8 and 9

$$\rho_C = \frac{N}{V_C}, \quad \rho_G = \frac{N}{V_G}$$

1.8.7 Phases

C-phase: V_C volume fraction $\frac{V_C}{V} = X_C$ G-phase: V_G volume fraction $\frac{V_G}{V} = X_G$

$$\implies V_C + V_G = V \implies X_C + X_G = 1$$

Total number of particles:

$$N = V_C \rho_C^* + V_G \rho_G^*$$

$$\frac{N}{V} = X_C \rho_C^* + X_G \rho_G^*$$

Set $X_G = 1 - X_C$, $\frac{N}{V}$

$$\rho = X_C \rho_C^* + (1 - X_C) \rho_G^*$$

$$X_C = \frac{\rho - \rho_G^*}{\rho_C^* - \rho_G^*}, \quad X_G = 1 - X_C$$

insert Fig.10 From Helmholtz Free energy, $T < T_C$

insert Fig.11

$$P = - \left(\frac{\partial F}{\partial V} \right)_{T, N}$$

insert Fig.12

1.8.8 Clausius-Clapeyron

Assume extensivity \implies Gibbs-Duhem relation

$$d\mu = -\frac{S}{N}dT + \frac{V}{N}dP = -sdT + \frac{1}{n}dP$$

where $s \equiv \frac{S}{N}$, $n \equiv \frac{N}{V}$

Liquid

$$\mu_2^l - \mu_1^l = -s(T_2^l - T_1^l) + \frac{1}{n^l}(P_2^l - P_1^l)$$

Gas

$$\mu_2^g - \mu_1^g = -s(T_2^g - T_1^g) + \frac{1}{n^g}(P_2^g - P_1^g)$$

l stands for liquid On the coexistence line in equilibrium:

$$\mu_1^l = \mu_1^g$$

same with all other variables. Subtract the eqs:

$$0 = (s^g - s^l)(T_2 - T_1) + \left(\frac{1}{n^l} - \frac{1}{n^g} \right) (P_2 - P_1)$$

$$\implies \frac{P_2 - P_1}{T_2 - T_1} = \frac{s^g - s^l}{T_2 - T_1} = \frac{\frac{1}{n^g} - \frac{1}{n^l}}{\frac{1}{n^g} - \frac{1}{n^l}}$$

$$\implies \left(\frac{\partial P}{\partial T} \right)_{\text{alone coexistence}} = \frac{(s^g - s^l)}{\frac{1}{n^g} - \frac{1}{n^l}}$$

1.9 More particle types: Gibbs Phase Rule

$$dU = TdS - PdV + \sum_{i=1}^K \mu_i dN_i$$

There are $2 + K$ independent variable. Extensive:

$$U = TS - PV + \sum_{i=1}^k \mu_i N_i$$

Gibbs-Duhem:

$$d\mu = -\frac{S}{N}dT + \frac{V}{N}dP + \sum_{i=1}^k N_i d\mu_i$$

If we have ϕ phases, then there is a Gibbs-Duhem rel. for each phase.

$$0 = S^1 dT^1 - V^1 dP^1 + \sum_{i=1}^k N_i^1 d\mu_i^1$$

phase 1

\vdots

$$0 = S^\phi dT^\phi - V^\phi dP^\phi + \sum_{i=\phi}^k N_i^\phi d\mu_i^\phi$$

phase ϕ

At coexistence:

$$T_1 = T_2 = \dots = T_\phi \quad P_1 = P_2 = \dots = P_\phi \quad \forall i \mu_i^1 = \mu_i^2 = \dots = \mu_i^\phi$$

(Can omit superscript from T,P, and μ_i)

$$0 = S^1 dT - V^1 dP + \sum_{i=1}^k N_i^1 d\mu_i$$

and for all ϕ equations. There are $2 + k$ variables (T, P, μ_i) and ϕ equations. The number of **free variables** at coexistence determines the dimension of the coexistence manifold (multidimensional object).

$$F = 2 + K - \phi$$

Example 1.9.1 ($K=1$).

$$F = 3 - \phi$$

$\phi = 2$ (Two phases coexist) $\implies F = 1$ (line) $\phi = 3$ (Three phases coexist) $\implies F = 0$ (point)
 $\phi = 4$ cannot coexist.

Example 1.9.2 (Binary Alloy (Two types of atoms)).

$$K = 2$$

$$F = 4 - \phi$$

Here 4 phases can coexist at a point, 3 along a line and 2 on a surface.

1.10 3. Law of TD

“The entropy of a (real QM) TD system goes to a constant as $T \rightarrow 0$. ”

Violated for the ideal gas:

$$\begin{aligned} S &= k_B N \left(\frac{3}{2} \ln \left(\frac{U}{N} \right) + \ln \left(\frac{V}{N} \right) \right) + X \\ &= k_B N \left(\frac{3}{2} \ln \left(\frac{3}{2} \frac{N k_B T}{N} \right) + \ln \left(\frac{V}{N} \right) + X \right) \end{aligned}$$

when $T \rightarrow 0$, $S \rightarrow -\infty$

Planck said it's 0, but it's **NOT**!

1.10.1 Consequences

$$dS = \frac{dQ}{T} \quad dQ = c dT$$

$$dS = c \frac{dT}{T}, S(T) - S(0) = \int_0^T dS = \int_0^T \frac{dT}{T} C$$

Taking $T \rightarrow 0$ will give 0 if integral is not diverging. For integral not to diverge $C(T \rightarrow 0) = 0$

Also the thermal expansion coefficient:

$$\alpha = \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_{P,N} = -\frac{1}{V} \left(\frac{\partial S}{\partial P} \right)_{T,N}$$

$$-SdT + VdP.$$

If S goes to a pressure independent const. at $T \rightarrow 0$. Then $\alpha = 0$.

CHAPTER 2

STATISTICAL MECHANICS

2.1 Behaviour for Large N

2.1.1 Binomial Distribution

Probability distribution for flipping coins: 1 coin:

$$1 : 1$$

2 coins:

$$1 : 2 : 1$$

3 coins:

$$1 : 3 : 3 : 1$$

Mean value, increases width increases, maximum (probability) decreases.

$$P(N_{\uparrow}) = \frac{1^{\uparrow} 1^{\downarrow}}{2^N} = \frac{N!}{N_{\uparrow}!(N - N_{\uparrow})!} \frac{1^N}{2^N}$$

What is the characteristic of this distribution when N is large. We need $N!$ for N large

$$N! = \int_0^{\infty} dx x^N e^{-x} = \left(-x^N e^{-x} \Big|_0^{\infty} + N \int_0^{\infty} dx x^{N-1} e^{-x} \quad \text{and so on} \right)$$

Factorial Expansion

$$N! = \int_0^{\infty} dx e^{-x+N \ln(x)} \tag{2.1}$$

Use Laplace's method. For N large Approximate the integrand by its value close to the maximum of the exponent. Set

$$\begin{aligned}
 g(x) &= N \ln(x) - x \\
 \left(\frac{\partial g}{\partial x} \right) &= \frac{N}{x} - 1 = 0 \implies X_0 = N \\
 2 \left(\frac{\partial g}{\partial x} \right) &= -\frac{N}{x^2} \Big|_{x=x_0} = -\frac{1}{N} < 0 \implies x_0 \text{ is a max.} \\
 g(x) &\approx g(x_0) + \left(\frac{\partial g}{\partial x} \right)_{x_0} (x - x_0) + \frac{1}{2} 2 \left(\frac{\partial g}{\partial x} \right)_{x=x_0} (x - x_0)^2 \\
 \implies N! &= \int_0^\infty dx e^{N \ln(N) - N - \frac{1}{2N} (x - N)^2} \\
 &= e^{N \ln(N) - N} \int_0^\infty e^{-\frac{1}{2N} (x - N)^2}
 \end{aligned}$$

For $N \gg \sqrt{(N)}$ width of the Gaussian we can extend the lower limit to $-\infty$ since it's so small.

$$\begin{aligned}
 \implies e^{N \ln(N) - N} \int_{-\infty}^\infty dx e^{-\frac{1}{2N} x^2} \\
 = e^{N \ln(N) - N} \sqrt{2\pi N}
 \end{aligned}$$

Stirling Approximation

$$\ln(N!) = N \ln(N) - N + \frac{1}{2} \ln(2\pi N) \quad (2.2)$$

The last term is often dropped when $N \gg \sqrt{N}$

$$\begin{aligned}
 \ln(P(N_\uparrow)) &= \ln(N_\downarrow) - \ln(N_\uparrow) - \ln((N - N_\uparrow)!) + N_\uparrow \ln(P) + (N - N_\uparrow) \ln(1 - p) \\
 &= N \ln(N) - N - (N_\uparrow \ln(N_\uparrow) - N_\uparrow) - ((N - N_\uparrow) \ln(N - N_\uparrow) - (N - N_\uparrow)) + N_\uparrow \ln(P) + (N - N_\uparrow) \ln(1 - P) \\
 &= N \ln(N) - N_\uparrow \ln(N_\uparrow) - (N - N_\uparrow) \ln(N - N_\uparrow) + N_\uparrow \ln\left(\frac{P}{1 - p}\right) + N \ln(1 - P)
 \end{aligned}$$

Maximum:

$$\begin{aligned}
 \left(\frac{\partial}{\partial N_\uparrow} \right) \ln[P(N_\uparrow)] &\implies -\ln(N_\uparrow) - \frac{N_\uparrow}{N_\uparrow} + \ln(N - N_\uparrow) + 1 + \ln\left(\frac{p}{1 - p}\right) = 0 \\
 \implies \ln\left(\frac{p}{1 - p}\right) &= \ln\left(\frac{N_\uparrow}{N - N_\uparrow}\right) = \ln\left(\frac{N_\uparrow/N}{1 - N_\uparrow/N}\right) \\
 \implies P &= \frac{N_\uparrow}{N} \\
 \implies N_\uparrow^{max} &= NP
 \end{aligned}$$

Location of the max P is NP . Second derivative:

$$\begin{aligned} \left(\frac{\partial^2 \ln(P)}{\partial N_{\uparrow}^2} \right) &= -\frac{1}{N_{\uparrow}} - \frac{1}{N - N_{\uparrow}} \\ &= -\frac{1}{N} \left(\frac{1}{N_{\uparrow}/N} + \frac{1}{1 - N_{\uparrow}/N} \right) = -\frac{1}{N} \left(\frac{1}{(N_{\uparrow}/N)(1 - N_{\uparrow}/N)} \right) \\ &=_{atmax \frac{N_{\uparrow}}{N}=p} -\frac{1}{N} \frac{1}{p(1-p)} \end{aligned}$$

$$\ln(P_N)|_{at \ max} = N \ln N - Np(\ln N + \ln p) - N(1-p)(\ln(N) + \ln(1-P)) + NP \ln(1-p) + N \ln(1-p) = 0$$

$$\begin{aligned} \ln[P(N_{\uparrow})] &= 0 + \underbrace{0}_{\text{first der.}} - \frac{1}{2(Np(1-P))} (N_{\uparrow} - NP)^2 \\ P(N_{\uparrow}) &\approx \textcolor{red}{A} e^{-\frac{1}{2N(1-p)}(N_{\uparrow} - NP)^2} \end{aligned}$$

where $\textcolor{red}{A}$ is the missing normalisation constant.

Gaussian around $NP \propto N$ and standard derivative $\sqrt{NP(1-P)} \propto \sqrt{N}$

The height is $\frac{1}{\sqrt{N}}$.

If we focus on the fraction of coins being head,

$$\begin{aligned} \left\langle \frac{N_{\uparrow}}{N} \right\rangle &= p \\ \left\langle \left(\frac{N_{\uparrow}}{N} \right)^2 \right\rangle - \left\langle \frac{N_{\uparrow}}{N} \right\rangle^2 &= \frac{1}{N^2} NP(1-P) \propto \frac{1}{N} \end{aligned}$$

the mean value becomes a precise statment as $N \rightarrow \infty$

2.1.2 Random Independent Variables

We define a random variable F that takes 2 values

1 with Probability P 0 with probability $1 - P$ Then take N such random variables $F_i \quad i = 1 \dots N$ then

$$N_{\uparrow} = \sum_{i=1}^N F_i$$

The average value of F_i is

$$\begin{aligned} \langle F_i \rangle &= 1P + 0(1-P) = P \\ \langle N_{\uparrow} \rangle &= \left\langle \sum_{i=1}^N F_i \right\rangle = \sum_{i=1}^N \langle F_i \rangle = NP \end{aligned}$$

Deviation from the average:

$$\langle (N_{\uparrow} - NP)^2 \rangle = \langle N_{\uparrow}^2 \rangle - 2NP \langle N_{\uparrow} \rangle + (NP)^2$$

$$\begin{aligned}
\langle N_{\uparrow}^2 \rangle &= \left\langle \left(\sum_{i=1}^N F_i \right)^2 \right\rangle = \left\langle \sum_{i=1}^N F_i \sum_{j=1}^N F_j \right\rangle = \left\langle \sum_{n=0}^N F_i^2 + \sum_{i,j} F_i F_j \right\rangle \\
&= \sum_{i=1}^N \langle F_i^2 \rangle + \sum_{i \neq j} \langle F_i F_j \rangle \\
&= \frac{1}{N^2} NP(1-P)
\end{aligned}$$

2.2 Boltzmann Configurational Entropy

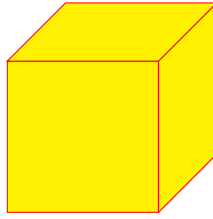


Figure 2.1: A 3D box with $V = L^3$ with N identical particles, labelled by their x -coordinates

"The number of microstates $\propto L^3$ "

Since x_1 has to be in the left of x_2 and same for the other particles:

$$\begin{aligned}
\# \text{ of microstates} &= \int_0^L dx_N L^2 \cdots \int_0^{x_3} dx_2 L^2 \int_0^{x_2} dx_1 L^2 \\
&= L^{2N} \int_0^L dx_N \int_0^{x_N} dx_{N-1} \cdots \int_0^{x_3} dx^2 \int_0^{x_2} dx_1
\end{aligned}$$

Integrating from the right hand side we see a pattern:

$$\begin{aligned}
x_2 &\rightarrow \frac{x_3^2}{2!} \rightarrow \frac{x_4^3}{3!} \cdots \\
&= L^{2N} \frac{L^N}{N!} = \frac{V^N}{N!}
\end{aligned}$$

This is the same result as gotten with first labelling particles and then divide by all permutations of labels.

Assuming all the microstates are equally probable.

$$\begin{aligned}
P(N_A, N_B) &= \frac{\frac{V_A^{N_A}}{N_A!} \frac{V_B^{N_B}}{N_B!}}{\frac{V^N}{N!}} \\
&= \frac{N!}{N_A! N_B!} \left(\frac{V_A}{V} \right)^{N_A} \left(\frac{V_B}{V} \right)^{N_B}
\end{aligned}$$

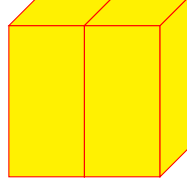


Figure 2.2: 2 boxes.

(Binomial distribution) Boltzmann: All microstates (position here) are equally likely. The most likely macrostate (value of N_A, N_B is the one that corresponds to most microstates: i.e. the max of $P(N_A, N_B)$).

The maximum of $P(N_A, N_B)$ also corresponds to the maximum of

$$k_B \ln \left(P(N_A, N_B) \frac{V^N}{N!} e^{xN} \right) \quad (2.3)$$

S_B Boltzmann Configuration Entropy Boltzmann never actually wrote this.

Equation 2.3 can also be written as

$$k \ln \left(\left(\frac{V_A^{N_A}}{N_A!} \right) e^{xN_A} \frac{V_B^{N_B}}{N_B!} e^{xN_B} \right)$$

The other words, the impossibility of an uncompensated decrease of entropy seems to be reduced to an improbability. (Boltzmann, 1898)

Set $\Omega \equiv \frac{V^N}{N!}$ In equilibrium:

$$S_B = \underbrace{k \ln(P_{max} \Omega e^{xN})}_{k \ln P_{max} + k \ln(\Omega e^{xN})} = k \ln(\Omega_A e^{xN_A}) + k \ln(\Omega_B e^{xN_B})$$

$$LHS = k \ln(\Omega e^{xN}),$$

Note that this has the same form as the right hand side!

So in the TD equilibrium,

$$S = k \ln(\Omega e^{xN}) = k \ln(\Omega) + kxN \quad (2.4)$$

This is additive over its subsystems.

$$S = S_A + S_B$$

$$\Omega = \frac{V^N}{N!} = \frac{\int d^3 q_1 \cdots \int d^3 q_n}{N!} \quad (2.5)$$

To generalise to also include momenta and pick only those configurations that have a total energy E .

$$\Omega(E)\delta E$$

δE is a thin energy shell

$$\frac{1}{N!h^{3N}} = \int d^3q_1 \cdots \int d^3q_N \int d^3p_1 \cdots \int d^3p_N$$

the h^{3N} can be interpreted as the x from before, the reference volume phase space. It's related to the uncertainty, and it's a choice.

Remark 2.2.1.

$$\ln(h^{3N}) = N \ln(h^3)$$

$$\Omega(E)\delta E = \frac{1}{N!h^{3N}} \int d^3q_1 \cdots d^3p_N (\Theta(E + \delta E - H(q_1, \dots, p_N)) - \Theta(E - H(q_1 \cdots p_N))) \quad (2.6)$$

where the $\Theta(x)$ is the Heaviside step function. Expand for small δE

$$= \delta E \frac{1}{N!h^{3N}} \int d^3q_1 \cdots d^3p_N \delta(E - H(q_1 \cdots p_N))$$

$$\Omega(E) = \frac{1}{N!h^{3N}} \int d^3q_1 \cdots d^3p_N \delta(E - H(q_1 \cdots p_N)) \quad (2.7)$$

This is the microcanonical ensemble. (All microstates have the same energy.)

2.3 Equilibrium Stat Mech and Ensembles

After a time the system reaches equilibrium (when the macroscopic states is time independent and is independent of the initial condition.) Microscopic state changes all the time (also in equilibrium)
Microscopic state:

$$Q = \{q_{1x}, q_{1y}, q_{1z}, \dots, q_{Nx}\}$$

$$P = \{p_{1x}, p_{1y}, \dots\}$$

$\{Q, P\}$ has $6N$ components. A microstate is a point in phase-space.

2.3.1 Conserved Quantities

In the approach to equilibrium, not all info about the initial state is lost. If collisions conserve energy, then (total) energy is conserved.

Instead of considering the microstates at different times, evolving from a particular initial condition, we can consider the system at a particular time t , coming from all possible initial conditions with the same energy.

$$\Omega(E) = \frac{1}{N!h^{3N}} \int D\mathbb{Q}D\mathbb{P} \delta(E - H(\mathbb{P} - \mathbb{Q}))$$

$$S = k_B \ln(\Omega(E) \delta E) \tag{2.8}$$

Ensemble average

$$\langle O \rangle_E = \frac{1}{\Omega(E)} \frac{1}{N!h^{3N}} \int D\mathbb{P}D\mathbb{Q} \delta(E - H(\mathbb{P}, \mathbb{Q})) O(\mathbb{P}, \mathbb{Q})$$

2.4 Microcanonical Ensemble

Ideal gas and Maxwell-Boltzmann distribution. Microcanonical ensemble:

$$S = k_B \ln(\Omega)$$

$$\Omega = \Omega(E) \delta E = \int \frac{1}{N! h^{3N}} \int d^3 q_1 \cdots d^3 p_N \delta(E - H(\mathbb{P}, \mathbb{Q})) \delta E$$

Ideal Gas:

$$H = \sum_{n=1}^N \frac{\vec{p}_i^2}{2m}$$

All q 's will be inside the box of volume V .

First the integrals over q 's give V^N (They are independent of the positions, but need to be confined in the box.)

$$\Omega = \frac{V^N}{N! h^{3N}} \delta E \int d^3 p_1 \cdots d^3 p_N \delta(E - \sum_{i=1}^N \frac{\vec{p}_i^2}{2m}) \equiv \frac{V^N}{N! h^{3N}} \delta E$$

Note that it's possible to take any momentum.

Shift:

$$\vec{p}_i' = \frac{\vec{p}_i}{\sqrt{2m}}$$

$$(2m)^{\frac{3N}{2}} \int d^3 p_1' \cdots d^3 p_N' \delta(E - \sum_{i=1}^N \underbrace{\vec{p}_i'^2}_{3N \text{ terms}})$$

Expanding these out and call them r^2

$$r^2 = p_1^2 + p_1^2 + p_1^2 + \dots + p_N^2$$

Switch to hyperspherical coordinates in $3N$ dimensions.

$$I = (2m)^{\frac{3N}{2}} \int d\tilde{\Omega}^{3N-1} \int_0^\infty dr V^{3N-1} \delta(E - r^2)$$

Now use

$$\begin{aligned} \int dx f(x) \delta(g(x)) &= \sum_n \frac{f(x)}{|g'(x)|} \Big|_{x=x_n} \\ \int dr r^{3N-1} \delta(E - r^2) & \\ |g'(r)| = |-2r| = 2r & \end{aligned} \tag{2.9}$$

Zeros of g : $r = \pm\sqrt{E}$ but only $+\sqrt{E}$ is inside the integration range.

Then

$$\int dr r^{3N-1} \delta(E - r^2) = \frac{E^{\frac{3N-1}{2}}}{2E^{1/2}} = \frac{E^{\frac{3N}{2}}}{2}$$

So

$$I = (2m)^{\frac{3N}{2}} \tilde{\Omega}^{3N-1} (2m)^{3N/2} \frac{E^{\frac{3N}{2}-1}}{2}$$

For the **Solid Angle** $\tilde{\Omega}^{d-1}$ in d dimensions We consider a Gaussian Integral and compute it in both hyperspherical and Cartesian coordinates.

$$I = \int d^d r e^{-r^2} = \int d\tilde{\Omega}^{d-1} \int_0^\infty r^{d-1} e^{-r^2}$$

Change variables:

$$t = r^2 \quad dt = 2r dr$$

$$I = \frac{1}{2} \tilde{\Omega}^{d-1} \underbrace{\int_0^\infty t^{\frac{d}{2}-1} e^{-t}}_{\Gamma(\frac{d}{2})}$$

Then in Cartesian coordinates:

$$I = \int_0^\infty dx \cdots \int_{-\infty}^\infty e^{-x_1^2} e^{-x_2^2} \cdots e^{-x_d^2} = \pi^{\frac{d}{2}}$$

$$\tilde{\Omega}^{d-1} = \frac{2\pi^{\frac{d}{2}}}{\Gamma(d/2)} \quad (2.10)$$

$$\Omega = \frac{V^N}{N! h^{3N}} \delta E \tilde{\Omega}^{3N-1} (2m)^{\frac{3N}{2}} \frac{E^{\frac{3N}{2}-1}}{2}$$

where

$$\tilde{\Omega}^{3N-1} = \frac{2\pi^{\frac{3N}{2}}}{\Gamma(\frac{3N}{2})}$$

$$\Omega = \frac{V^N}{N! h^{3N}} \frac{(2\pi m E)^{\frac{3N}{2}}}{\Gamma(\frac{3N}{2})} \frac{dE}{E}$$

Finally the entropy is

$$S = k_B \ln(\Omega) = k_B \ln \left(\left[\frac{V(2\pi m E)^{3/2}}{h^3} \right]^N \frac{dE}{N! \Gamma(3N/2) E} \right)$$

Now use

$$X\Gamma(x) = \Gamma(x+1) \implies \Gamma(3N/2) = \frac{2}{3N} \Gamma\left(\frac{3N}{2} + 1\right)$$

$$S = k_B \left(\ln \left[\frac{V(2\pi m E)^{3/2}}{h^3} \right]^N \right) - k_B (N \ln N - N) - k_B \left(\frac{3N}{2} \ln \left(\frac{3N}{2} - \frac{3N}{2} \right) \right) - k_B \ln \left(\frac{2E}{3N \delta E} \right)$$

where we ignore the last term since it doesn't scale with n .

$$S = N k_B \left[\ln \left(\frac{V}{N} \right) + \frac{3}{2} \ln \left(\frac{E}{N} \right) + \frac{5}{2} + \frac{3}{2} \ln \left(\frac{4\pi m}{3h^2} \right) \right]$$

The Sackur-Tetrode formula for entropy of ideal gas

$$S = Nk_B \left(\frac{5}{2} - \ln \left(\frac{N}{V} \underbrace{\left(\frac{h}{(4\pi m E)^{\frac{1}{2}}}}_{\lambda^3} \right)^{\frac{1}{2}} \right)^3 \right) \quad (2.11)$$

Expected to be valid physically when $V \gg N\lambda^3$

2.5 Maxwell-Boltzmann Distribution

NOTATION: $P \rightarrow$ Probability, $p \rightarrow$ momentum

The probability of one particle having a momentum in one direction being of magnitude p_1 when the total energy is E .

$$P(p_1) = \frac{\text{Volume of phase-space where } p_{1x} = p_1 \text{ and the total energy is } E}{\text{Volume of phase-space with total energy } E}$$

$$= \frac{\text{The surface area of a sphere in } 3N - 1 \text{ dimensions with radius } \sqrt{E - \frac{p_i^2}{2m}}}{\text{surface area of a sphere in } 3N \text{ dimensions with radius } \sqrt{E}}$$

$$= \frac{\pi^{\frac{3N-1}{2}} (2m)^{\frac{3N-1}{2}} \left(E - \frac{p_i^2}{2m}\right)^{\left(\frac{3N-1}{2}-1\right)} \Gamma\left(\frac{3N-1}{2}\right)}{\pi^{3N/2} (2m)^{3N/2} E^{3N/2-1} / \Gamma(3N/2)}$$

$$\frac{\Gamma(3N/2) \left(1 - \frac{p_i^2}{2mE}\right)^{\frac{3N}{2}-\frac{3}{2}}}{\Gamma\left(\frac{3N-1}{2}\right) \sqrt{\pi} \sqrt{2mE}}$$

In general $\frac{p_i^2}{2mE} \ll 1$

$$1 - \frac{p_i^2}{2mE} \approx e^{-\frac{p_i^2}{2mE}}$$

Stating the result without proof:

$$\frac{\Gamma(3N/2)}{\Gamma\left(\frac{3N-1}{2}\right)} \overset{N \rightarrow \text{large}}{\approx} \left(\frac{3N}{2}\right)^{\frac{1}{2}}$$

To show this, use Stirling's formula and that the gamma function is factorial (somehow).

$$P(p_1) = e^{-\frac{\frac{p_i^2}{2mE} \left(\frac{3N}{2}-\frac{3}{2}\right)}{\frac{3N}{2}}} \frac{1}{\sqrt{2\pi \frac{2mE}{3N}}} e^{-\frac{p_i^2}{2\left(\frac{2mE}{3N}\right)}}$$

Gaussian with mean 0, $\sigma^2 = \frac{2mE}{3N}$.

For the ideal gas in TD:

$$E = \frac{3}{2} N k_B T$$

$$\sigma^2 = m k_B T$$

We can in fact define the temperature in statistical mechanics as the width of the momentum distribution and use that definition to establish the equality:

$$E = \frac{3}{2} N k_B T$$

2.6 Flow in Phase-space: Liouville theorem

Ensemble: Several copies of the same system but with different initial conditions. Insert phase space figure. A point in the phase space is one system, an ensemble is many dots in the phase space. Imagine so many copies of the system that on a coarse grained scale h_3N , we can talk about a density of systems.

$$\rho(q_1, \dots, p_N, t)$$

where ρ is the ensemble density.

So the number of systems in the region around $q_1 \dots p_N$ at time t is

$$\rho(Q, \mathbb{P}, t) dQ d\mathbb{P}$$

when time goes on, the system will change (points in phase-space is moving) and so the ensemble density can in principle change.

Paths can't cross, but can merge, because from one point (initial condition) we can only have path. Newton's equations are continuous, so a system (the trajectory, point) moves continuously in phase-space. This means that it does not disappear or reappear suddenly in phase space.

2.6.1 Continuity Equation

“in = out”

$$\frac{\partial \rho}{\partial t} = -\vec{\nabla} \cdot \vec{j}$$

$$\vec{j} = \rho \vec{V}$$

where V is the generalised velocity.

$$\vec{V} = (\dot{q}_1, \dots, \dot{p}_N)$$

Continuity equation in terms of components:

$$\begin{aligned} \frac{\partial \rho}{\partial t} &= \sum_{n=1}^{3N} \left(\frac{\partial(\rho \dot{q}_n)}{\partial q_n} + \frac{\partial(\rho \dot{p}_n)}{\partial p_n} \right) \\ &= \sum_{n=1}^{3N} \left(\left(\frac{\partial \rho}{\partial q_n} \right) \dot{q}_n + \frac{\partial \rho}{\partial p_n} \dot{p}_n + \rho \underbrace{\left(\frac{\partial \dot{q}_n}{\partial q_n} + \frac{\partial \dot{p}_n}{\partial p_n} \right)}_0 \right) \end{aligned}$$

Hamilton eqs of motion:

$$\dot{q}_n = \left(\frac{\partial H}{\partial p_n} \right) \implies \left(\frac{\partial \dot{q}_n}{\partial q_n} \right) = \left(\frac{\partial^2 H}{\partial q_n \partial p_n} \right)$$

using

$$\frac{\partial^2 J}{\partial q_n \partial p_n} = \frac{\partial^2 J}{\partial p_n \partial q_n}$$

How does the density change as we flow with the system?

$$\begin{aligned} & \frac{d}{dt} \rho(q_{1x}(t) \cdot p_{nz}(t), t) \\ &= \frac{\partial \rho}{\partial t} + \sum_{n=1}^{3N} \frac{\partial \rho}{\partial q_n} \dot{q}_n + \frac{\partial \rho}{\partial p_n} \dot{p}_n \\ &= \frac{\partial \rho}{\partial t} - \frac{\partial \rho}{\partial t} = 0 \end{aligned}$$

No local change in density following a Volume element.

Flow in phase-space is as an incompressible liquid (same volume different shape.)

$$\frac{\partial \rho}{\partial t} = - \sum_{n=1}^{3N} \left(\frac{\partial \rho}{\partial q_n} \frac{\partial H}{\partial p_n} - \frac{\partial \rho}{\partial p_n} \frac{\partial H}{\partial q_n} \right) = -\{\rho, H\}$$

Recall $\{\}$ is the Poisson bracket,

$$\{A, B\} = \sum_{n=1}^{3N} \frac{\partial A}{\partial q_n} \frac{\partial B}{\partial p_n} - \frac{\partial A}{\partial p_n} \frac{\partial B}{\partial q_n}$$

which btw is the anticommutator in QM.

In equilibrium we want $\frac{\partial \rho}{\partial t} = 0$

$$\{H, \rho\} = 0$$

Now note that is $\rho = \rho(H)$ Then

$$\{H, \rho(H)\} = \sum_{n=1}^{3N} \left(\frac{\partial H}{\partial q_n} \frac{\partial \rho}{\partial H} \frac{\partial H}{\partial p_n} - \frac{\partial H}{\partial p_n} \frac{\partial \rho}{\partial H} \frac{\partial H}{\partial q_n} \right) = 0$$

That's the microcanonical ensemble (only depends on H) is constant in time.

$$\rho(\mathbb{P}, \mathbb{Q}) = \frac{1}{N! h^{3N}} \rho(E - H(\mathbb{P}, \mathbb{Q}))$$

More generally if there are more of motions c_1, c_2 so that $\{H, C\} = 0$ then

$$\rho = \rho(H, \{c_1\})$$

will also have

$$\begin{aligned} & \frac{\partial \rho}{\partial t} = 0 \\ & \{H, \rho(H, \{c_1\})\} = \sum_{n=1}^{3N} \sum_i \left(\frac{\partial H}{\partial q_n} \frac{\partial c_i}{\partial p_n} \frac{\partial \rho}{\partial c_i} - \frac{\partial H}{\partial p_n} \frac{\partial c_i}{\partial q_n} \frac{\partial \rho}{\partial c_i} \right) \\ & \sum_i \{H, C_i\} \frac{\partial \rho}{\partial c_i} = 0 \implies \frac{\partial \rho}{\partial t} = 0 \end{aligned}$$

2.6.2 The Ergodic Hypothesis

With statistical ensembles ρ we can calculate ensemble averages:

$$\langle f \rangle$$

this is average over different copies of the same system with differential initial conditions. But experimentally we most often measure a single copy over some time

$$\bar{f} = \lim_{t \rightarrow \infty} \frac{1}{t_1 - t_0} \int_{t_0}^{t_1} dt f(t)$$

It holds whenever "the trajectories of (almost every point phase space eventually passes arbitrarily close to every point on the surface of constant energy.)" Proving ergodicity is very hard and has been done only for a few systems: Gas of hard spheres.

Ergodicity is very strict and in practice we might do well with

$$\langle f \rangle = \bar{f} + \text{error}$$

For certain systems $\langle f \rangle \neq \bar{f}$

- Few-body problems: chaos
- Integrable systems: Many-body systems with ∞ number of conservation laws.
- Broken symmetry phases.
- Glasses, very slow dynamics.