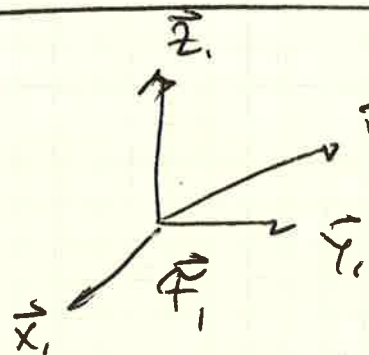


Derivatives of vectors (1.4)



$$\vec{r} = \vec{F}_1^T \vec{r}_1$$

↑ evolution of \vec{r}
 2100% dependent on
 view/frame of reference

now define

$$\dot{\vec{r}} \triangleq \lim_{\delta t \rightarrow 0} \frac{\delta \vec{r}}{\delta t}$$

$$\delta \vec{r} \triangleq \vec{F}_1^T (\vec{r}_1(t + \delta t) - \vec{r}_1(t))$$

$$\Rightarrow \dot{\vec{r}} = \vec{F}_1^T \dot{\vec{r}}_1 = \vec{F}_1^T \begin{bmatrix} \dot{x}_{1,1} \\ \dot{y}_{1,1} \\ \dot{z}_{1,1} \end{bmatrix}$$

since $\dot{\vec{x}}_1, \dot{\vec{y}}_1, \dot{\vec{z}}_1 = 0$ why - inertial
 i.e. if frame is ~~moving~~ w.r.t inertial
 say on a S/C or A/C, $\dot{\vec{x}}_1, \dot{\vec{y}}_1, \dot{\vec{z}}_1 \neq 0$

Notice ~~a~~ $(\dot{\vec{r}}) = \vec{F}_1^T (\dot{\vec{r}}_1)$

$$= \vec{F}_1^T (\ddot{\vec{r}}_1 + \dot{\vec{r}}_1)$$

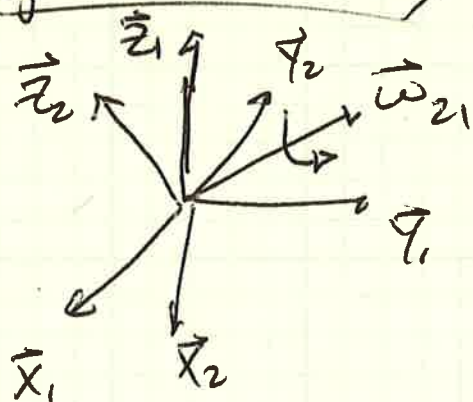
$$= \dot{\vec{a}}\vec{r} + \vec{a}\vec{r}$$

$$(\vec{a} + \vec{b}) = \vec{a} + \vec{b}$$

$$(\vec{a} \cdot \vec{b}) = \vec{a} \cdot \vec{b} + \vec{a} + \vec{b}$$

$$(\vec{a} \times \vec{b}) = \vec{a} \times \vec{b} + \vec{a} \times \vec{b}$$

Angular Velocity (1.4.1)



\vec{r}_2 is rotating about $\vec{\omega}_{21}$ at some instant relative to \vec{r}_1

$|\vec{\omega}_{21}| = \omega_{21}$ is rotational speed

$\vec{\omega}_{21}$ = rotational direction

} at some instant in time

= principal axes

$$\text{Now } \vec{\omega}_{21} = \lim_{\delta t \rightarrow 0} \vec{a}(\delta t) \frac{\phi(\delta t)}{\delta t}$$

since $\vec{\omega}_{21}$ is \vec{a} at that instant between $t = t$ and $t + \delta t$

~~well~~ $\vec{\omega}_{21}$

Now, consider some vector \vec{v} in \vec{F}_1

$$\Rightarrow \vec{v}_{rot} = \vec{C}_{12} \vec{F}_1^T \vec{C}_{12} \vec{v}$$

$$= \vec{F}_1^T [\cos \phi \mathbb{I} + (1 - \cos \phi) \hat{a} \hat{a}^T + \sin \phi \hat{a}^\times] \vec{v}$$

when δt is small $\Rightarrow \phi(\delta t) \approx$ small

$$\Rightarrow \sin \phi \approx \phi \text{ and } \cos \phi \approx 1$$

$$\Rightarrow \vec{v}(t + \delta t) = \vec{F}_1^T [1 + \hat{a}^\times \phi] \vec{v}(t)$$

$$\text{or } \vec{v}(t + \delta t) - \vec{v}(t) = \vec{F}_1^T [\hat{a}^\times \phi] \vec{v}$$

$$\text{and } \dot{\vec{v}} = \lim_{\delta t \rightarrow 0} \frac{\vec{v}(t + \delta t) - \vec{v}(t)}{\delta t}$$

$$= \vec{F}_1^T \hat{a}^\times \frac{\phi(\delta t)}{\delta t} \vec{v}$$

$$= \vec{F}_1^T \vec{\omega}_{21} \times \vec{v} = \vec{\omega}_{21} \times \vec{v}$$

true for $\vec{x}_1, \vec{y}_1, \vec{z}_1$

$$\Rightarrow \vec{\dot{x}}_2 = \vec{\omega}_{21} \times \vec{x}_2$$

$$\vec{\dot{y}}_2 = \vec{\omega}_{21} \times \vec{y}_2 \text{ or } \vec{\dot{F}}_2^T = \vec{\omega}_{21} \times \vec{F}_2^T$$

$$\vec{\dot{z}}_2 = \vec{\omega}_{21} \times \vec{z}_2$$

now $\vec{r} = \vec{F}_1^T r_1 = \vec{F}_2^T r_2$

denote

$$\dot{\vec{r}} = \vec{F}_1^T \dot{r}_1, \quad \dot{\vec{r}} = \vec{F}_2^T \dot{r}_2$$

$\dot{\vec{r}}$
 $\frac{d}{dt}$ of \vec{r}
 viewed
 from \vec{F}_1^T

$\dot{\vec{r}}$
 $\frac{d}{dt}$ of \vec{r}
 viewed from \vec{F}_2^T

$$\Rightarrow \dot{\vec{r}} = \vec{F}_2^T \dot{r}_2 + \dot{\vec{F}}_2^T r_2$$

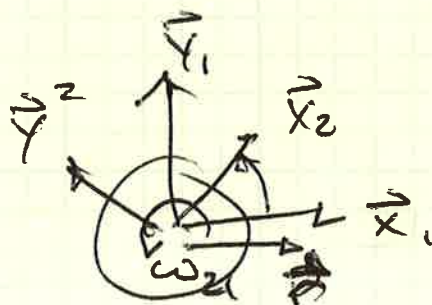
$$= \dot{r}_2 + \vec{\omega}_{21} \times \vec{F}_2^T r_2$$

$$\dot{\vec{r}} = \dot{r}_2 + \vec{\omega}_{21} \times \vec{r}$$

\uparrow
 absolute
 derivative

\uparrow
 relative
 derivative

apparent motion due
 to rotating frame



Ant on
 a record

\dot{r}_2 is a spiral

\dot{r}_2 is going ~~straight~~ straight out
 \vec{X}_2

Now

$$\vec{\omega}_{21} = \vec{F}_2^T \omega_{21}$$

$$\begin{aligned} \dot{\vec{r}} &= \vec{F}_1^T \dot{r}_1 = \vec{F}_2^T \dot{r}_2 + \vec{F}_2^T \omega_{21}^X r_2 \\ &= \vec{F}_2^T (r_2 + \omega_{21}^X r_2) \end{aligned}$$

$$\dot{\vec{r}} = \vec{F}_1^T r_1 = \vec{F}_2^T [\dot{r}_2 + \omega_{21}^X r_2]$$

$$\begin{aligned} \vec{F}_2^T &= \vec{F}_1^T C_{12} \\ \vec{F}_2^T C_{21} &= \vec{F}_1^T \\ \vec{F}_1^T &= C_{11} \vec{F}_1 \end{aligned}$$

$$= \vec{F}_1^T C_{12} [\dot{r}_2 + \omega_{21}^X r_2]$$

$$\Rightarrow \dot{r}_1 = C_{12} [\dot{r}_2 + \omega_{21}^X r_2]$$

use this to find \dot{C}_{21} Let $\vec{r} = \text{const. vector in } \vec{F}_1$

$$\Rightarrow \dot{\vec{r}} = 0 \quad \dot{\vec{r}}_1 = \vec{F}_1^T \dot{r}_1 = 0$$

$$\Rightarrow \dot{r}_2 + \omega_{21}^X r_2 = 0$$

$$r_2 = C_{21} r_1$$

$$\Rightarrow \dot{C}_{21} r_1 + \cancel{C_{21} \dot{r}_1} + \omega_{21}^X C_{21} r_1 = 0$$

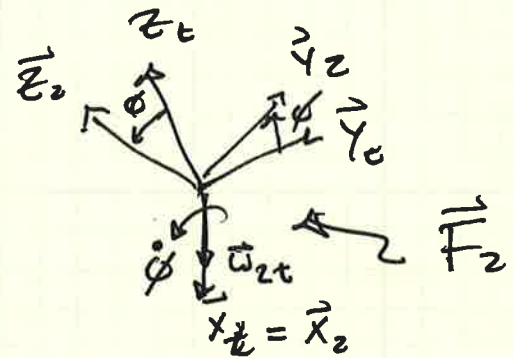
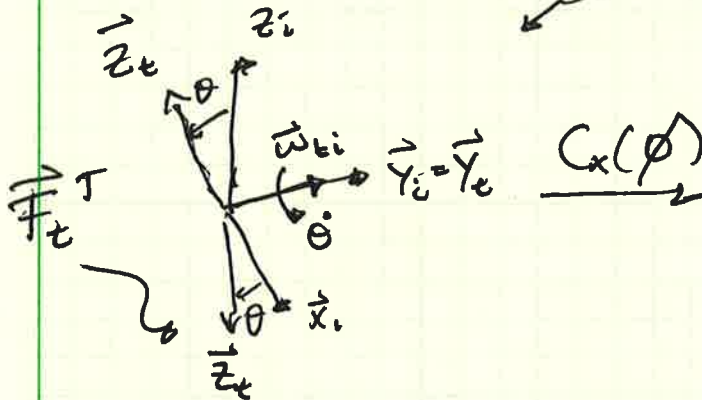
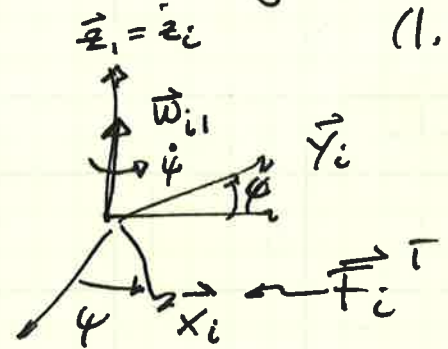
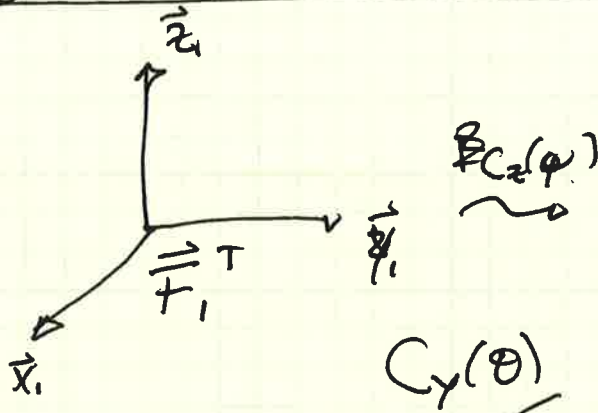
$$\Rightarrow [\dot{C}_{21} + \omega_{21}^X C_{21}] r_1 = 0$$

$$\Rightarrow \cancel{C_{21}} \left[\dot{C}_{21} = -\omega_{21}^X C_{21} \right]$$

since \vec{r}_2 is arbitrary

$$\text{and } \left[\omega_{21}^X = -\dot{C}_{21} C_{21}^T = -\dot{C}_{21} C_{12} \right]$$

Angular Velocity in Terms of Euler Angle Rates (1.4.2)



So, $\vec{\omega}_{i1} = \vec{F}_i^T \begin{bmatrix} 0 \\ 0 \\ \dot{\psi} \end{bmatrix} = \vec{F}_2^T C_x(\phi) C_y(\theta) \begin{bmatrix} 0 \\ 0 \\ \dot{\psi} \end{bmatrix}$

↑
angular velocity
of i frame wrt 1 frame in \vec{F}_2^T coords

$$\vec{\omega}_{t1} = \vec{F}_t^T \begin{bmatrix} 0 \\ \dot{\theta} \\ 0 \end{bmatrix} = \vec{F}_2^T C_x(\phi) \begin{bmatrix} 0 \\ \dot{\theta} \\ 0 \end{bmatrix}$$

$$\vec{\omega}_{2t} = \vec{F}_2^T \begin{bmatrix} \dot{\phi} \\ 0 \\ 0 \end{bmatrix}$$

and $\vec{\omega}_{21} = \vec{\omega}_{2t} + \vec{\omega}_{t1} + \vec{\omega}_{i1}$

$$\Rightarrow \omega_{21} = \begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} + C_x(\phi) \begin{bmatrix} 0 \\ \dot{\theta} \\ 0 \end{bmatrix} + C_x(\phi) C_y(\theta) \begin{bmatrix} 0 \\ 0 \\ \dot{\psi} \end{bmatrix}$$

$$\Rightarrow \omega_{21} = \begin{bmatrix} 1 & 0 & -s\theta \\ 0 & c\phi & s\phi c\theta \\ 0 & -s\phi & c\phi c\theta \end{bmatrix} \begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix}$$

$$\Rightarrow \begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = \begin{bmatrix} 1 \\ c\theta \end{bmatrix} \frac{1}{c\theta} \begin{bmatrix} c\theta & s\phi s\theta & c\phi s\theta \\ 0 & c\phi c\theta & -s\phi c\theta \\ 0 & s\phi & c\phi \end{bmatrix} \omega_{21}$$

Notice $\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix}$ is undefined when $\theta = \pm 90^\circ$

Angular Velocity in terms of Quaternion Rates

(1.4.3)

$$\omega_{21}^X = -\dot{C}_{21} C_{21}^T$$

$$C_{21} = (2\eta^2 - 1) \mathbf{1} + 2\epsilon\epsilon^T - 2\eta\epsilon^x$$

but $\epsilon^x \epsilon^x = \epsilon\epsilon^T - \epsilon^T \epsilon \mathbf{1}$

and $\epsilon^T \epsilon + \eta^2 = 1 \Rightarrow \eta^2 = 1 - \epsilon^T \epsilon$

$$\Rightarrow 2(\epsilon^T \epsilon + \eta^2)$$

$$\Rightarrow 2(1 - \epsilon^T \epsilon) \mathbf{1} + 2\epsilon\epsilon^T - 2\eta\epsilon^x$$

$$= 2 - 2\epsilon^T \epsilon \mathbf{1}$$

$$= 2(\underbrace{\mathbf{1} - \epsilon^T \epsilon \mathbf{1} + \epsilon\epsilon^T}_{\epsilon^x \epsilon^x}) - 2\eta\epsilon^x$$

$$\Rightarrow C_{21} = [2(1 - \epsilon^T \epsilon) - 1] \mathbf{1} + 2\epsilon\epsilon^T - 2\eta\epsilon^x$$

$$= [1 - 2\epsilon^T \epsilon] \mathbf{1} + 2\epsilon\epsilon^T - 2\eta\epsilon^x$$

$$= \mathbf{1} + 2(\epsilon\epsilon^T - \epsilon^T \epsilon \mathbf{1}) - 2\eta\epsilon^x$$

$$\underline{C_{21} = \mathbf{1} + 2\epsilon^x \epsilon^x - 2\eta\epsilon^x}$$

$$\Rightarrow \dot{C}_{21} = 2 [\dot{e}^x e^x + e^x \dot{e}^x - \dot{\eta} e^x - \eta \dot{e}^x]$$

now $\frac{1}{2} \dot{C}_{21} C_{21} = (e^x \dot{e})^x - \eta \dot{e}^x + \dot{\eta} e^x$

comes in handy ~~comes in~~ handy

lots of algebra...

$$\Rightarrow \omega_{21}^x = -2 [(e^x \dot{e})^x - \eta \dot{e}^x + \dot{\eta} e^x]$$

$$\text{or } \omega_{21} = 2(\eta \mathbb{1} - e^x) \dot{e} - 2e \dot{\eta}$$

$$\Rightarrow \begin{bmatrix} \omega_{21} \\ 0 \end{bmatrix} = 2 \begin{bmatrix} (\eta \mathbb{1} - e^x) & -e \\ e^T & \eta \end{bmatrix} \begin{bmatrix} \dot{e} \\ \dot{\eta} \end{bmatrix}$$

↓

$$\text{Since } e^T e + \eta^2 = 1$$

$$\Rightarrow \frac{d}{dt} (e^T e + \eta^2) = 0$$

$$\Rightarrow \underbrace{\dot{e}^T e + e^T \dot{e}}_{= \text{to cancel}} + 2\eta \dot{\eta} = 0$$

$$\Rightarrow \cancel{e^T \dot{e}} + 2e^T \dot{e} + 2\eta \dot{\eta} = 0$$

$$\Rightarrow \underline{e^T \dot{e} + \eta \dot{\eta} = 0}$$

Now inverting

$$\Rightarrow \begin{bmatrix} \ddot{e} \\ \dot{e} \end{bmatrix} = \frac{1}{2} \begin{bmatrix} (\gamma \mathbf{1} + e^x) & e \\ -e^T & \gamma \end{bmatrix} \begin{bmatrix} w_{z1} \\ 0 \end{bmatrix}$$

or

$$\begin{aligned} \ddot{e} &= \frac{1}{2} (\gamma \mathbf{1} + e^x) w_{z1} \\ \dot{e} &= -\frac{1}{2} e^T w_{z1} \end{aligned} \left. \begin{array}{l} \text{no trig} \\ \text{and} \\ \text{no singularity} \end{array} \right\}$$

How will we use this?

Ex given $\vec{w}_{z1} = \text{const} = \vec{F}_1^T \begin{bmatrix} 1.5 \\ +1.5 \\ 1 \end{bmatrix} \frac{\text{rad}}{\text{s}}$

and $\psi_0 = 10^\circ$ $\theta_0 = -5^\circ$ $\phi_0 = 20^\circ$ — initial conditions

$$\begin{aligned} \Rightarrow C_{z10} &= C_x(\phi_0) C_y(\theta_0) C_z(\psi_0) \\ &= C_x(20^\circ) C_y(-5^\circ) C_z(10^\circ) \\ &= \end{aligned}$$

Matlab code

Find ϵ_0 and η_0

$$\eta_0 = \sqrt{\frac{\text{trace}(C_{20}) + 1}{2}}$$

$$\epsilon_{10} = \frac{C_{230} - C_{320}}{4\eta_0}$$

$$\epsilon_{20} = \frac{C_{310} - C_{130}}{4\eta_0} \quad \epsilon_0 = \begin{bmatrix} \epsilon_{10} \\ \epsilon_{20} \\ \epsilon_{30} \end{bmatrix}$$

$$\epsilon_{30} = \frac{C_{120} - C_{210}}{4\eta_0}$$

$$\eta_0 = \quad \epsilon_0 =$$

For Fuel $e(t)$, $\eta(t)$, θ , $\phi(t)$

need to integrate use ODE 45