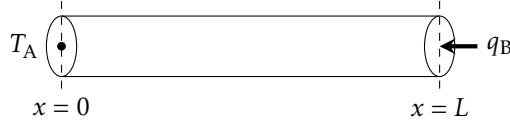




Case 1

Consider a $L = 1.00$ m long rod with a thermal conductivity of $k = 1.0 \text{ W m}^{-1} \text{ K}^{-1}$. The left end of the rod is maintained at a constant temperature of $T_A = 50.0^\circ\text{C}$, while the right end is heated at a constant inward flux of $q_B = 2.0 \text{ W m}^{-2}$. Heat is generated within the rod at a rate of $\dot{Q} = 100.0 \text{ W m}^{-3}$. It is desired to determine the steady-state temperature profile in the rod.



The above problem may be described by the 1D heat equation with the following boundary conditions: In these equations, \mathbf{n} is the outward normal vector (so $-\mathbf{n}$ points inwards), and \mathbf{q} is the diffusive heat flux (i.e., $\mathbf{q} = -k\nabla T$).

$$0 = -\nabla \cdot (-k\nabla T) + \dot{Q} \quad (1)$$

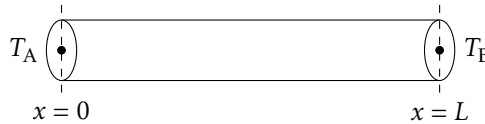
$$T|_{x=0} = T_A \quad (2)$$

$$-\mathbf{n} \cdot \mathbf{q}|_{x=L} = +q_B \quad (3)$$

Note that the sign of q_B in Equation 3 is positive because the heat flux points inwards. Because flux-type boundary conditions are defined with respect to the normal vector, the sign of flux-type boundary conditions dictates whether the flux enters or exits the domain, and not whether the flux points towards the positive or negative coordinates.

Case 2

Consider a $L = 1.00$ m long rod with a thermal conductivity of $k = 1.0 \text{ W m}^{-1} \text{ K}^{-1}$. The left end of the rod is maintained at a constant temperature of $T_A = 50.0^\circ\text{C}$, while the right end is at a constant temperature of $T_B = 60.0^\circ\text{C}$. Heat is generated within the rod at a rate of $\dot{Q} = 100.0 \text{ W m}^{-3}$. It is desired to determine the steady-state temperature profile in the rod.



The above problem may be described by the 1D heat equation with the following boundary conditions:

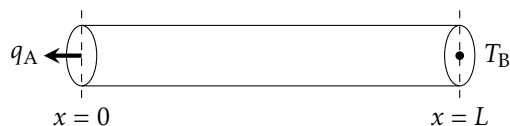
$$0 = -\nabla \cdot (-k\nabla T) + \dot{Q} \quad (4)$$

$$T|_{x=0} = T_A \quad (5)$$

$$T|_{x=L} = T_B \quad (6)$$

Case 3

Consider a $L = 1.00$ m long rod. The left end of the rod loses heat at a constant flux of $q_A = 2.0 \text{ W m}^{-2}$, while the right end is held at a constant temperature of $T_B = 50.0^\circ\text{C}$.



The thermal conductivity k of the rod is non-constant and depends on the temperature as given by Equation 7. Moreover, the linear heat generation \dot{Q} varies with the position in the rod as given by Equation 8. It is desired to determine the steady-state temperature profile in the rod.

$$k = 1.0 + 0.01T + 500T^{-1} \quad k [=] \text{ W m}^{-1} \text{ K}^{-1}; T [=] \text{ K} \quad (7)$$

$$\dot{Q} = 10.0 + 10.0x^{0.5} - 2.0x^{1.5} \quad \dot{Q} [=] \text{ W m}^{-3}; x [=] \text{ m} \quad (8)$$

The above problem may be described by the 1D heat equation with the following boundary conditions:

$$0 = -\nabla \cdot (-k\nabla T) + \dot{Q} \quad (9)$$

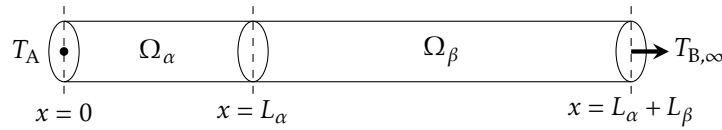
$$-\mathbf{n} \cdot \mathbf{q}|_{x=0} = -q_A \quad (10)$$

$$T|_{x=L} = T_B \quad (11)$$

Case 4

Two rods, the first with a length of $L_\alpha = 0.5 \text{ m}$ and the second with a length of $L_\beta = 1.0 \text{ m}$, are joined end-to-end to form a longer rod. The first rod has a thermal conductivity of $k_\alpha = 1.0 \text{ W m}^{-1} \text{ K}^{-1}$ and a linear heat generation of $\dot{Q}_\alpha = 500.0 \text{ W m}^{-3}$. The second rod has a thermal conductivity of $k_\beta = 5.0 \text{ W m}^{-1} \text{ K}^{-1}$ and does not generate heat (i.e., $\dot{Q}_\beta = 0$).

The left end of the combined rod is held at a constant temperature of $T_A = 50^\circ \text{C}$, while the right end is exposed to a cooling fluid at $T_{B,\infty} = 10^\circ \text{C}$. The heat flux on the right end follows Newton's law of cooling with a heat transfer coefficient of $h_B = 5.0 \text{ W m}^{-2} \text{ K}^{-1}$. It is desired to determine the steady-state temperature profile in the rod.



The above problem may be described by the 1D heat equation with the following boundary conditions:

$$0 = -\nabla \cdot (-k_\alpha \nabla T) + \dot{Q}_\alpha \quad \text{in } \Omega_\alpha \quad (12)$$

$$0 = -\nabla \cdot (-k_\beta \nabla T) + \dot{Q}_\beta \quad \text{in } \Omega_\beta \quad (13)$$

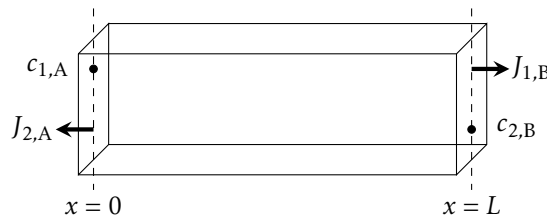
$$T|_{x=0} = T_A \quad (14)$$

$$-\mathbf{n} \cdot \mathbf{q}|_{x=L_\alpha+L_\beta} = -h_B (T|_{x=L_\alpha+L_\beta} - T_{B,\infty}) \quad (15)$$

Observe the formulation of Newton's law of cooling as a boundary condition. If heat exits the tip of the rod, then the tip must be warmer than the surroundings (i.e., $T|_{x=L_\alpha+L_\beta} > T_{B,\infty}$). The quantity $(T|_{x=L_\alpha+L_\beta} - T_{B,\infty})$ is therefore positive. However, the right-hand side of Equation 15 must be negative since heat is leaving the boundary, thus a negative sign is included.

Case 5

Two chemical species, referred to as species 1 and 2, diffuse in a tank of length $L = 1.00 \text{ m}$. At the left end of the tank, the concentration of species 1 is held at $c_{1,A} = 0.10 \text{ mol m}^{-3}$, while the outward flux of species 2 is $J_{2,A} = 0.002 \text{ mol m}^{-2} \text{ s}^{-1}$. At the right end of the tank, the outward flux of species 1 is $J_{1,B} = 0.003 \text{ mol m}^{-2} \text{ s}^{-1}$, while the concentration of species 2 is held at $c_{2,B} = 0.40 \text{ mol m}^{-3}$.



Species 1 has a diffusion coefficient of $D_1 = 0.050 \text{ m}^2 \text{ s}^{-1}$, while species 2 has a much lower diffusion coefficient of $D_2 = 0.006 \text{ m}^2 \text{ s}^{-1}$. A chemical reaction exists wherein species 1 is converted to species 2 via the following second-order reaction. The rate constant is $0.07 \text{ m}^3 \text{ mol}^{-1} \text{ s}^{-1}$. It is desired to determine the steady-state concentration profiles of both species.

$$\dot{R}_{1 \rightarrow 2} = k_{1 \rightarrow 2} c_1 c_2 \quad (16)$$

The above problem may be described by the 1D diffusion equation with the following boundary conditions:

$$0 = -\nabla \cdot (-D_1 \nabla c_1) - \dot{R}_{1 \rightarrow 2} \quad (17)$$

$$0 = -\nabla \cdot (-D_2 \nabla c_2) + \dot{R}_{1 \rightarrow 2} \quad (18)$$

$$c_1|_{x=0} = c_{1,A} \quad (19)$$

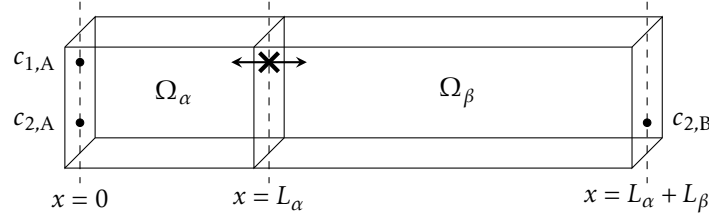
$$-\mathbf{n} \cdot \mathbf{J}_2|_{x=0} = J_{2,A} \quad (20)$$

$$-\mathbf{n} \cdot \mathbf{J}_1|_{x=L} = J_{1,B} \quad (21)$$

$$c_2|_{x=L} = c_{2,B} \quad (22)$$

Case 6

A tank is divided into two sections by a membrane. The section on the left is $L_\alpha = 0.50 \text{ m}$ long, while the section on the right is $L_\beta = 1.00 \text{ m}$ long. Two chemical species are injected on the left side of the tank. The concentration of species 1 is held at $c_{1,A} = 0.30 \text{ mol m}^{-3}$, while that of species 2 is $c_{2,A} = 0.20 \text{ mol m}^{-3}$. The membrane, however, prevents species 1 from entering the right section of the tank, so species 1 is found only on the left section. The concentration of species 2 on the right side of the tank is $c_{2,B} = 0.10 \text{ mol m}^{-3}$.



Species 1 has a diffusion coefficient of $D_1 = 0.050 \text{ m}^2 \text{ s}^{-1}$, while species 2 has a much lower diffusion coefficient of $D_2 = 0.006 \text{ m}^2 \text{ s}^{-1}$. A chemical reaction exists wherein species 1 is converted to species 2 via the following second-order reaction. The rate constant is $0.40 \text{ m}^3 \text{ mol}^{-1} \text{ s}^{-1}$. It is desired to determine the steady-state concentration profiles of both species.

$$\dot{R}_{1 \rightarrow 2} = k_{1 \rightarrow 2} c_1 c_2 \quad (23)$$

The above problem may be described by the 1D diffusion equation with the following boundary conditions:

$$0 = -\nabla \cdot (-D_1 \nabla c_1) - \dot{R}_{1 \rightarrow 2} \quad \text{in } \Omega_\alpha \quad (24)$$

$$0 = -\nabla \cdot (-D_2 \nabla c_2) + \dot{R}_{1 \rightarrow 2} \quad \text{in } \Omega_\alpha, \Omega_\beta \quad (25)$$

$$c_1|_{x=0} = c_{1,A} \quad (26)$$

$$c_2|_{x=0} = c_{2,A} \quad (27)$$

$$-\mathbf{n} \cdot \mathbf{J}_1|_{x=L_\alpha} = 0 \quad (28)$$

$$c_2|_{x=L_\alpha+L_\beta} = c_{2,B} \quad (29)$$