

# IRIS Quadrotor Model

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## 1 CAD Model

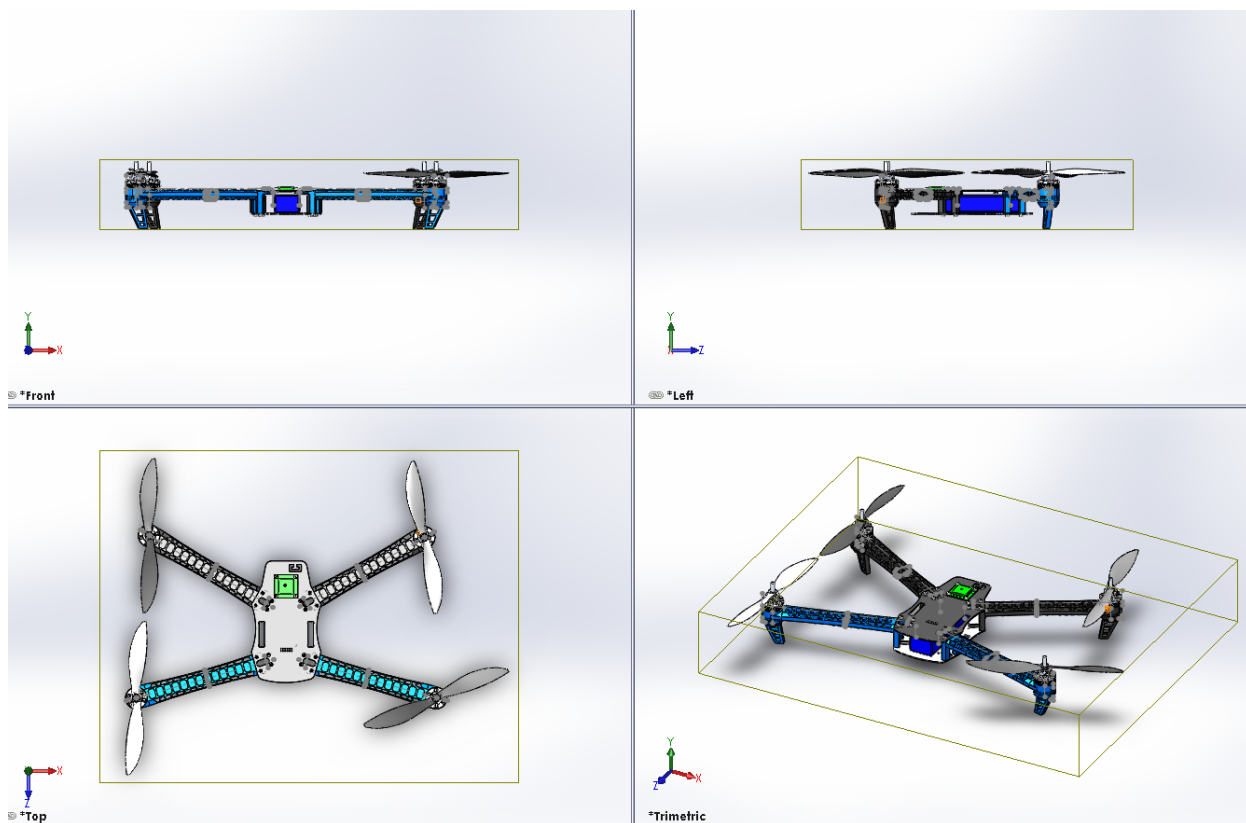


Figure 1: IRIS CAD Model

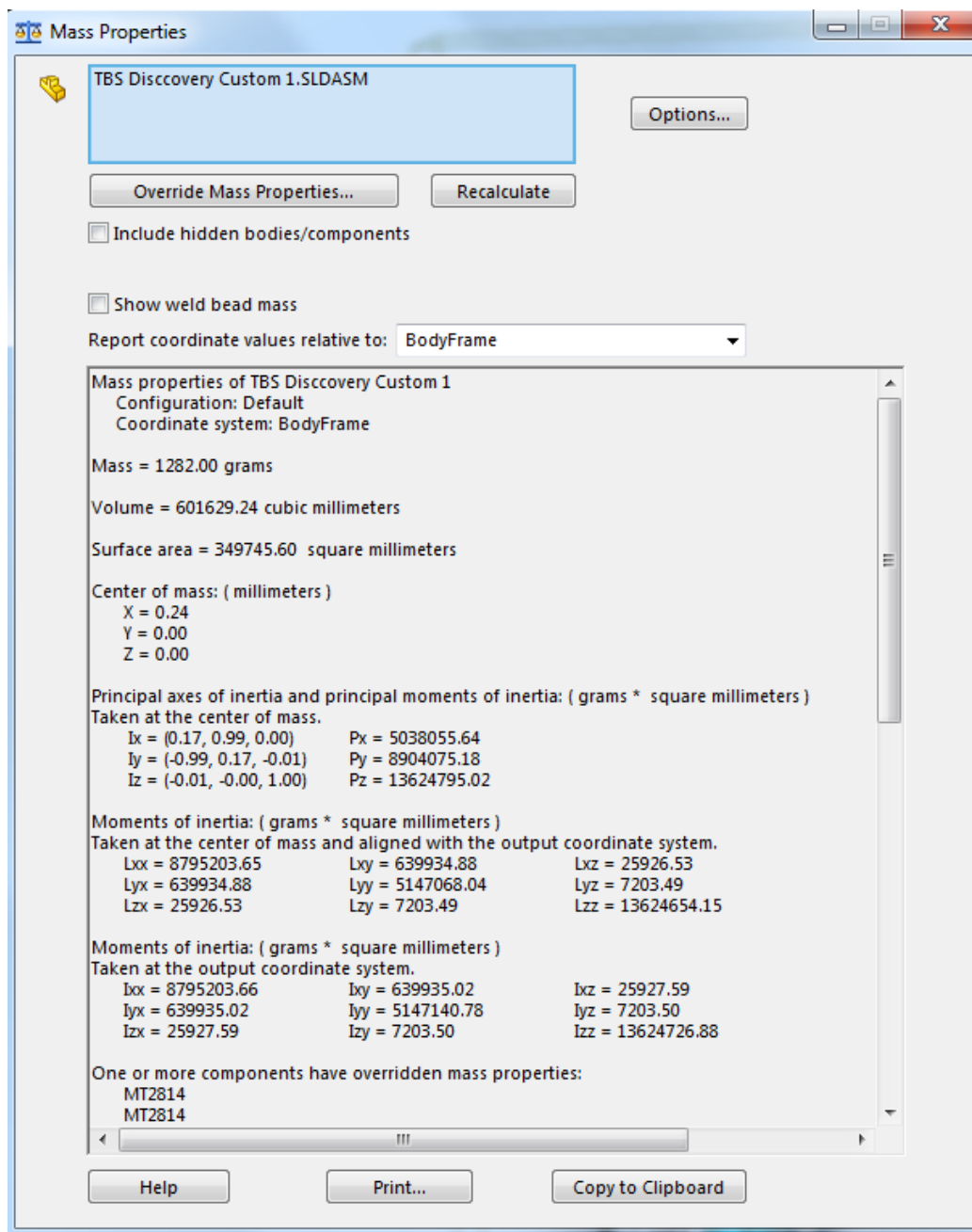


Figure 2: Inertial Matrix of IRIS Quadrotor from Solidworks

## 2 Motion Equations

### 2.1 Parameters for Quadrotor Model

$m$ : Mass of Quadrotor;

$\mathbf{I}$ : Inertial Matrix with respect to Body Frame;

$L$ : Distance from the axis of rotation of the rotors to the center of mass of the Quadrotor;

$r$ : Propeller Radius;

$rpm\_min$ : Minimum Rotation Speed of motor;

$rpm\_max$ : Maximum Rotation Speed of motor;

$k_F$ : Thrust Coefficient;

$k_M$ : Moment Coefficient;

$k_m$ : Motor Gain;

Controller Gains:  $\mathbf{k}_x, \mathbf{k}_v, \mathbf{k}_\Omega, \mathbf{k}_R$ ;

For IRIS Quadrotor:

$$m = 1282 \text{ g}$$

$$\mathbf{I} = \begin{bmatrix} 8795203.66 & 639935.02 & 25927.59 \\ 639935.02 & 5147140.78 & 7203.50 \\ 25927.59 & 7203.50 & 13624726.88 \end{bmatrix} g \cdot mm^2$$

$$L = 252.33 \text{ mm}$$

$$r = 127 \text{ mm}$$

$$k_F = 1.5693 \times 10^{-7} \text{ N/RPM}^2$$

$$k_M = -2.7848 \times 10^{-6} \text{ N} \cdot mm / \text{RPM}^2$$

$$k_m = 20 \text{ s}^{-1}$$

### 2.2 Newton's Equations of Motion

$$m\ddot{\mathbf{r}} = \begin{bmatrix} 0 \\ 0 \\ -mg \end{bmatrix} + \mathbf{R} \begin{bmatrix} 0 \\ 0 \\ F_1 + F_2 + F_3 + F_4 \end{bmatrix}$$

Define the first input  $u_1$  to be

$$u_1 = \sum_{i=1}^4 F_i$$

Here in the equation:

$\mathbf{r}$  is Position Vector in Inertial Frame;

$\mathbf{R}$  is Rotation Matrix which we use  $Z - X - Y$  Euler angles to model the rotation of the Quadrotor in the World Frame;

$F_i = k_f w_i^2$  is Thrust produced by each motor;

$w_i$  is rotor speed;

## 2.3 Euler's Equations of Motion

$$\mathbf{I} \begin{bmatrix} \dot{p} \\ \dot{q} \\ \dot{r} \end{bmatrix} = \begin{bmatrix} F_1 l_{1x} - F_2 l_{2x} + F_3 l_{3x} - F_4 l_{4x} \\ -F_1 l_{1y} + F_2 l_{2y} + F_3 l_{3y} - F_4 l_{4y} \\ M_1 + M_2 - M_3 - M_4 \end{bmatrix} - \begin{bmatrix} p \\ q \\ r \end{bmatrix} \times \mathbf{I} \begin{bmatrix} p \\ q \\ r \end{bmatrix}$$

with

$$\mathbf{I} = \begin{bmatrix} I_{xx} & I_{xy} & I_{xz} \\ I_{yx} & I_{yy} & I_{yz} \\ I_{zx} & I_{zy} & I_{zz} \end{bmatrix}$$

or we could write

$$\mathbf{I} \begin{bmatrix} \dot{p} \\ \dot{q} \\ \dot{r} \end{bmatrix} = \begin{bmatrix} l_{1x} & -l_{2x} & l_{3x} & -l_{4x} \\ -l_{1y} & l_{2y} & l_{3y} & -l_{4y} \\ \gamma & \gamma & -\gamma & -\gamma \end{bmatrix} \begin{bmatrix} F_1 \\ F_2 \\ F_3 \\ F_4 \end{bmatrix} - \begin{bmatrix} p \\ q \\ r \end{bmatrix} \times \mathbf{I} \begin{bmatrix} p \\ q \\ r \end{bmatrix}$$

Define the second input  $\mathbf{u}_2$  to be

$$\mathbf{u}_2 = \begin{bmatrix} l_{1x} & -l_{2x} & l_{3x} & -l_{4x} \\ -l_{1y} & l_{2y} & l_{3y} & -l_{4y} \\ \gamma & \gamma & -\gamma & -\gamma \end{bmatrix} \begin{bmatrix} F_1 \\ F_2 \\ F_3 \\ F_4 \end{bmatrix} = \begin{bmatrix} u_2 \\ u_3 \\ u_4 \end{bmatrix}$$

Here is the equation:

$p, q, r$ : Components of Angular Velocity of the robot in Body Frame;

$l_{ix}$ : The Arm of Force of thrust  $F_i$  about  $x$  axis;

$l_{iy}$ : The Arm of Force of thrust  $F_i$  about  $y$  axis

$M_i = k_m w_i^2$ : Moment produced by each motor;

$\gamma = \frac{k_m}{k_f}$ : Relationship between Lift and Drag;

### 3 State Space Equation

A nonlinear system can be described by the following differential equations:

$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}) + \mathbf{g}(\mathbf{x}, \mathbf{u})$$

We could linearize it to get state space equation:

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u}$$

with initial conditions  $\mathbf{x}(0) = \mathbf{x}_0$

For quadrotor, we define its state vector  $\mathbf{X}$  to be

$$\mathbf{X} = [x \ y \ z \ \phi \ \theta \ \psi \ \dot{x} \ \dot{y} \ \dot{z} \ p \ q \ r]^T$$

$(x, y, z)$  are Position in Inertial frame,  $(\phi, \theta, \psi)$  are Orientation,  $(\dot{x}, \dot{y}, \dot{z})$  are Linear Velocity in Inertial frame,  $(p, q, r)$  are components of Angular Velocity in Body frame. Especially,

$$\begin{bmatrix} p \\ q \\ r \end{bmatrix} = \begin{bmatrix} \cos(\theta) & 0 & -\cos(\phi)\sin(\theta) \\ 0 & 1 & \sin(\phi) \\ \sin(\theta) & 0 & \cos(\phi)\cos(\theta) \end{bmatrix} \begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix}$$

The inputs  $\mathbf{u}$  as defined in section 2.2 and 2.3 are:

$$\mathbf{u} = [u_1 \ u_2 \ u_3 \ u_4]^T$$

Equilibrium State:

$$\begin{aligned} \mathbf{X}_0 &= [x_0 \ y_0 \ z_0 \ 0 \ 0 \ \psi_0 \ 0 \ 0 \ 0 \ 0 \ 0 \ 0]^T \\ \mathbf{u}_0 &= [mg \ 0 \ 0 \ 0]^T \end{aligned}$$

We first write the state vector as below:

$$\mathbf{X} = [x_1 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ x_7 \ x_8 \ x_9 \ x_{10} \ x_{11} \ x_{12}]^T$$

Then we write the state equations:

$$\begin{aligned}
f_1(\mathbf{x}, \mathbf{u}) &= \dot{x}_1 = x_7 \\
f_2(\mathbf{x}, \mathbf{u}) &= \dot{x}_2 = x_8 \\
f_3(\mathbf{x}, \mathbf{u}) &= \dot{x}_3 = x_9 \\
f_4(\mathbf{x}, \mathbf{u}) &= \dot{x}_4 = x_{10} \cos(x_5) + x_{12} \sin(x_5) \\
f_5(\mathbf{x}, \mathbf{u}) &= \dot{x}_5 = x_{10} \frac{\sin(x_4) \sin(x_5)}{\cos(x_4)} + x_{11} - x_{12} \frac{\cos(x_5) \sin(x_4)}{\cos(x_4)} \\
f_6(\mathbf{x}, \mathbf{u}) &= \dot{x}_6 = -x_{10} \frac{\sin(x_5)}{\cos(x_4)} + x_{12} \frac{\cos(x_5)}{\cos(x_4)} \\
f_7(\mathbf{x}, \mathbf{u}) &= \dot{x}_7 = \frac{u_1}{m} (\cos(x_6) \sin(x_5) + \cos(x_5) \sin(x_4) \sin(x_6)) \\
f_8(\mathbf{x}, \mathbf{u}) &= \dot{x}_8 = \frac{u_1}{m} (\sin(x_6) \sin(x_5) - \cos(x_6) \cos(x_5) \sin(x_4)) \\
f_9(\mathbf{x}, \mathbf{u}) &= \dot{x}_9 = -g + \frac{u_1}{m} \cos(x_4) \cos(x_5) \\
f_{10}(\mathbf{x}, \mathbf{u}) &= \dot{x}_{10} = \frac{I_{xy}u_3 - I_{yy}u_2}{I_{xy}^2 - I_{xx}I_{yy}} \\
f_{11}(\mathbf{x}, \mathbf{u}) &= \dot{x}_{11} = \frac{I_{xy}u_2 - I_{xx}u_3}{I_{xy}^2 - I_{xx}I_{yy}} \\
f_{12}(\mathbf{x}, \mathbf{u}) &= \dot{x}_{12} = \frac{u_4}{I_{zz}}
\end{aligned}$$

Then we get  $A$  and  $B$  matrix:

$$\mathbf{A} = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & g \sin(\psi_0) & g \cos(\psi_0) & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -g \cos(\psi_0) & g \sin(\psi_0) & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

$$\mathbf{B} = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ \frac{1}{m} & 0 & 0 & 0 \\ 0 & \frac{-I_{yy}}{I_{xy}^2 - I_{xx}I_{yy}} & \frac{I_{xy}}{I_{xy}^2 - I_{xx}I_{yy}} & 0 \\ 0 & 0 & 0 & 0 \\ 0 & \frac{I_{xy}}{I_{xy}^2 - I_{xx}I_{yy}} & \frac{-I_{xx}}{I_{xy}^2 - I_{xx}I_{yy}} & 0 \\ 0 & 0 & 0 & \frac{1}{I_{zz}} \end{bmatrix}$$

For the measurement  $\mathbf{y} = \mathbf{C}\mathbf{x}$ ,  $\mathbf{C}$  is an Identity matrix of dimension 12;

## References

- [1] T.Lee, M.Leok and N.McClamroch,"Geometric Tracking Control of a Quadrotor UAV on SE(3)," Atlanta, GA, USA, December 2010
- [2] N.Michael, D.Mellinger, Q.Lindsey, and V.Kumar, "The grasp multiple micro uav testbed," IEEE Robotics and Automation Magazine, 2010