A new approach for designing dynamic balanced serial mechanisms

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Abstract

Balancing is an important issue related to the design of mechanical systems in general, and also parallel mechanisms, in particular. In fact, the performance of parallel mechanisms associated to specific applications depends on the choice of the balancing method, namely, either static or dynamic, either passive or active, whether it is valid for a given trajectory or even for any motion. The main contribution of this work is to highlight the importance of the dynamic modelling process in order to achieve the compensation conditions associated to the chosen balancing technique. Due to the fact that parallel mechanisms have highly complex structures, the use of dynamic formalisms that employ redundant generalized coordinates, in association with the successive coupling of additional balancing elements to the original system model, can bring remarkable benefits. Additionally, this book chapter also discusses the impact of the dynamic model, developed in accordance with the methodology shown here, for the control strategy of parallel mechanisms. Finally, the simulation results demonstrates how effective is the presented methodology for the planar 5-bar with revolute joints (5R).

KEYWORDS: Dynamic balancing, serial mechanisms

1 Introduction and literature review

2 Mothodology

- 2.1 Static Balancing
- 2.2 Dynamic Balancing

3 Applying the technique

$$\mathbb{M}(\mathbf{q})\ddot{\mathbf{q}} + \mathbf{v}(\mathbf{q}, \dot{\mathbf{q}}) + \mathbf{g}(\mathbf{q}) = \mathbf{u} \tag{1}$$

For a 3-DOF serial mechanism:

$$\mathbb{M} = \begin{bmatrix}
D_{11} & D_{12} & D_{13} \\
D_{12} & D_{22} & D_{23} \\
D_{13} & D_{23} & D_{33}
\end{bmatrix}$$
(2)

$$\mathbf{v} = \begin{bmatrix} D_{111} & D_{122} & D_{133} \\ D_{211} & D_{222} & D_{233} \\ D_{311} & D_{322} & D_{333} \end{bmatrix} \begin{bmatrix} \dot{q}_1^2 \\ \dot{q}_2^2 \\ \dot{q}_3^2 \end{bmatrix} + 2 \begin{bmatrix} D_{112} & D_{113} & D_{123} \\ D_{212} & D_{213} & D_{223} \\ D_{312} & D_{313} & D_{323} \end{bmatrix} \begin{bmatrix} \dot{q}_1 \dot{q}_2 \\ \dot{q}_1 \dot{q}_3 \\ \dot{q}_2 \dot{q}_3 \end{bmatrix}$$
(3)

$$g = \begin{bmatrix} D_1 & D_2 & D_3 \end{bmatrix}^\top \tag{4}$$

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$$\mathbf{q} = \begin{bmatrix} q_1 & q_2 & q_3 \end{bmatrix}^\top \tag{5}$$

$$\mathbf{u} = \begin{bmatrix} u_1 & u_2 & u_3 \end{bmatrix}^\top \tag{6}$$

For a rotational joint we call $q_i = \theta_i$ and $u_i = \tau_i$, and for a prismatic joint we call $q_i = d_i$ and $u_i = f_i$.

3.1 3-DOF RRR planar serial mechanism

$$\begin{cases}
D_1 = g[(m_1l_{g1} + m_2l_1 + m_3l_1)c(\theta_1) + (m_2l_{g2} + m_3l_2)c(\theta_1 + \theta_2) + m_3l_{g3}c(\theta_1 + \theta_2 + \theta_3)] \\
D_2 = g[(m_2l_{g2} + m_3l_2)c(\theta_1 + \theta_2) + m_3l_{g3}c(\theta_1 + \theta_2 + \theta_3)] \\
D_3 = g[m_3l_{g3}c(\theta_1 + \theta_2 + \theta_3)]
\end{cases}$$
(7)

Static balancing:

$$\begin{cases}
D_1 = 0 \\
D_2 = 0 \\
D_3 = 0
\end{cases}
\Rightarrow
\begin{cases}
l_{g1} = -\frac{l_1(m_2 + m_3)}{m_1} \\
l_{g2} = -\frac{l_2 m_3}{m_2} \\
l_{g3} = 0
\end{cases}$$
(8)

Static balanced mechanism:

Static balanced mechanism:
$$\begin{cases}
D_{11} = J_{x_1} + J_{x_2} + J_{x_3} + m_2 l_1^2 + m_3 (l_1^2 + l_2^2) + \frac{l_1^2 (m_2 + m_3)^2}{m_1} + \frac{l_2^2 m_3^2}{m_2} \\
D_{22} = J_{x_2} + J_{x_3} + m_3 l_2^2 + \frac{l_2^2 m_3^2}{m_2} \\
D_{33} = J_{x_3} \\
D_{12} = D_{22} \\
D_{13} = D_{23} = D_{33} \\
v = 0 \\
g = 0
\end{cases} \tag{9}$$

Coupling 4 discs:

$$\begin{cases}
D'_{11} = D_{11} + J_{x_4} + J_{x_5} + J_{x_6} + J_{x_7} \\
D'_{22} = D_{22} + J_{x_4} + J_{x_5}\beta^2 + J_{x_6} + J_{x_7} \\
D'_{33} = D_{33} + J_{x_6} + J_{x_7}\gamma^2 \\
D'_{12} = D_{12} + J_{x_4} + J_{x_5}\beta + J_{x_6} + J_{x_7} \\
D'_{13} = D_{13} + J_{x_6} + J_{x_7}\gamma \\
D'_{23} = D'_{13} \\
v' = 0
\end{cases}$$
(10)

Dynamic balancing:

$$\begin{cases}
D'_{12} = 0 \\
D'_{13} = 0 \\
D'_{23} = 0
\end{cases}
\Rightarrow
\begin{cases}
\beta = -\frac{J_{x_2} + J_{x_3} + J_{x_4} + J_{x_6} + J_{x_7} + m_3 l_2^2 + \frac{m_3^2 l_2^2}{m_2}}{J_{x_5}} \\
\gamma = -\frac{J_{x_3} + J_{x_6}}{J_{x_7}}
\end{cases} (11)$$

Dynamic balanced mechanism:

$$\begin{cases} \tau_1 = k_1 \ddot{\theta}_1 \\ \tau_2 = k_2 \ddot{\theta}_2 \\ \tau_3 = k_3 \ddot{\theta}_3 \end{cases} \tag{12}$$

Being:

$$\begin{cases}
k_{1} = J_{x_{1}} + J_{x_{2}} + J_{x_{3}} + J_{x_{4}} + J_{x_{5}} + J_{x_{6}} + J_{x_{7}} + m_{2}l_{1}^{2} + m_{3}(l_{1}^{2} + l_{2}^{2}) + \frac{l_{1}^{2}(m_{2} + m_{3})^{2}}{m_{1}} + \frac{l_{2}^{2}m_{3}^{2}}{m_{2}} \\
k_{2} = J_{x_{2}} + J_{x_{3}} + J_{x_{4}} + J_{x_{6}} + J_{x_{7}} + m_{3}l_{2}^{2} + \frac{l_{2}^{2}m_{3}^{2}}{m_{2}} + \frac{\left(J_{x_{2}} + J_{x_{3}} + J_{x_{4}} + J_{x_{6}} + J_{x_{7}} + m_{3}l_{2}^{2} + \frac{m_{3}^{2}l_{2}^{2}}{m_{2}}\right)^{2}}{J_{x_{5}}} \\
k_{3} = \frac{(J_{x_{3}} + J_{x_{6}})(J_{x_{3}} + J_{x_{6}} + J_{x_{7}})}{J_{x_{7}}}
\end{cases} (13)$$

3.2 $3-DOF\ RRR\ spatial\ serial\ mechanism$

$$\begin{cases}
D_1 = 0 \\
D_2 = g[(m_2 l_{g2} + m_3 l_2) c(\theta_2) + m_3 l_{g3} c(\theta_2 + \theta_3)] \\
D_3 = g[m_3 l_{g3} c(\theta_2 + \theta_3)]
\end{cases}$$
(14)

Static balancing:

$$\begin{cases}
D_1 = 0 \\
D_2 = 0 \\
D_3 = 0
\end{cases} \Rightarrow \begin{cases}
l_{g2} = -\frac{l_2 m_3}{m_2} \\
l_{g3} = 0
\end{cases}$$
(15)

Static balanced mechanism:

$$\begin{cases} D_{11} = J_{yz} \mathsf{s}^2(\theta_2) + J_{y3} \mathsf{s}^2(\theta_2 + \theta_3) + J_{z_1} + J_{z_2} \mathsf{c}^2(\theta_2) + J_{z_3} \mathsf{c}^2(\theta_2 + \theta_3) + m_3 (l_1 + l_2 \mathsf{c}(\theta_2))^2 + \frac{(m_2 l_1 - m_3 l_2 \mathsf{c}(\theta_2))^2}{m_2} \\ D_{22} = J_{x_2} + J_{x_3} + m_2 l_2^2 + \frac{l_2^2 m_3^2}{m_2} \\ D_{33} = J_{x_3} \\ D_{12} = D_{13} = 0 \\ D_{23} = D_{33} \\ D_{211} = -\frac{1}{2} \Big((J_{y_2} - J_{z_2}) \mathsf{s}(2\theta_2) + (J_{y_3} - J_{z_3} - m_3 l_2^2 (1 + \frac{m_3}{m_2})) \mathsf{s}(2\theta_2 + 2\theta_3) \Big) \\ D_{311} = \frac{1}{2} \Big((J_{z_3} - J_{y_3}) \mathsf{s}(2\theta_2 + 2\theta_3) \Big) \\ D_{111} = D_{122} = D_{133} = D_{222} = D_{233} = D_{322} = D_{333} = 0 \\ D_{112} = -D_{211} \\ D_{113} = -D_{311} \\ D_{123} = D_{212} = D_{213} = D_{223} = D_{312} = D_{313} = D_{323} = 0 \\ \mathfrak{g} = \emptyset \end{cases}$$

$$(16)$$

Coupling 2 discs:

$$\begin{cases} D'_{11} = D_{11} + J_{y_4} s^2(\theta_2 + \theta_2) + J_{y_5} s^2(\beta\theta_2 + \theta_2) + J_{z_4} c^2(\theta_2 + \theta_2) + J_{z_5} c^2(\beta\theta_2 + \theta_2) \\ D'_{22} = D_{22} + J_{x_4} + J_{x_5} \\ D'_{33} = D_{33} + J_{x_4} + J_{x_5} \beta^2 \\ D'_{12} = D'_{13} = 0 \\ D'_{23} = D_{23} + J_{x_4} + J_{x_5} \beta \end{cases}$$

$$\begin{cases} D'_{211} = D_{211} \\ D'_{311} = D_{311} \\ D'_{111} = D'_{122} = D'_{133} = D'_{222} = D'_{233} = D'_{322} = D'_{333} = 0 \\ D'_{112} = D_{112} + \frac{1}{4} \left((J_{y_4} - J_{z_4}) s(2\theta_2 + 2\theta_3) + (J_{y_5} - J_{z_5}) s(2\beta\theta_2 + 2\theta_3) \right) \\ D'_{123} = D'_{113} + \frac{1}{4} \left((J_{y_4} - J_{z_4}) s(2\theta_2 + 2\theta_3) + (J_{y_5} - J_{z_5}) s(2\beta\theta_2 + 2\theta_3) \right) \\ D'_{123} = D'_{212} = D'_{213} = D'_{223} = D'_{312} = D'_{313} = D'_{323} = 0 \end{cases}$$

Dynamic balancing:

$$\begin{cases}
D'_{23} = 0 \\
D'_{211} = 0 \\
D'_{311} = 0 \\
D'_{112} = 0 \\
D'_{113} = 0
\end{cases}
\Rightarrow
\begin{cases}
\beta = -\frac{J_{x_3} + J_{x_4}}{J_{x_5}} \\
J_{y_2} = J_{z_2} \\
J_{y_3} = J_{z_3} + m_3 l_2^2 (1 + \frac{m_3}{m_2}) \\
J_{y_4} = J_{z_4} \\
J_{y_5} = J_{z_5}
\end{cases} (18)$$

Dynamic balanced mechanism:

$$\begin{cases} \tau_1 = k_1 \ddot{\theta}_1 \\ \tau_2 = k_2 \ddot{\theta}_2 \\ f_3 = k_3 \ddot{d}_3 \end{cases} \tag{19}$$

Being:

$$\begin{cases}
k_{1} = J_{z_{1}} + J_{z_{2}} + J_{z_{3}} + J_{z_{4}} + J_{z_{5}} + m_{2}l_{1}^{2} + m_{3}(l_{1}^{2} + l_{2}^{2}) + \frac{l_{1}^{2}m_{3}^{2}}{m_{2}} \\
k_{2} = J_{x_{2}} + J_{x_{3}} + J_{x_{4}} + J_{x_{5}} + m_{3}l_{2}^{2} + \frac{l_{1}^{2}m_{3}^{2}}{m_{2}} \\
k_{3} = \frac{(J_{x_{3}} + J_{x_{4}})(J_{x_{3}} + J_{x_{4}} + J_{x_{5}})}{J_{x_{5}}}
\end{cases} (20)$$

3.3 3-DOF RRP spatial serial mechanism (SCARA)

$$\begin{cases}
D_1 = g[(m_1l_{g1} + m_2l_1 + m_3l_1)c_1 + m_2l_{g2}c_{1+2}] \\
D_2 = g[m_2l_{g2}c_{1+2}] \\
D_3 = 0
\end{cases}$$
(21)

Static balancing:

$$\begin{cases}
D_1 = 0 \\
D_2 = 0 \\
D_3 = 0
\end{cases} \Rightarrow \begin{cases}
l_{g1} = -\frac{l_1(m_2 + m_3)}{m_1} \\
l_{g2} = 0
\end{cases}$$
(22)

Static balanced mechanism:

$$\begin{cases}
D_{11} = J_{x_1} + J_{x_2} + J_{x_3} + m_2 l_1^2 + m_3 l_1^2 + \frac{l_1^2 (m_2 + m_3)^2}{m_1} \\
D_{22} = J_{x_2} + J_{x_3} \\
D_{33} = m_3 \\
D_{12} = D_{22} \\
D_{13} = D_{23} = 0 \\
v = 0 \\
g = 0
\end{cases}$$
(23)

Coupling 2 discs:

$$\begin{cases}
D'_{11} = D_{11} + J_{x_4} + J_{x_5} \\
D'_{22} = D_{22} + J_{x_4} + J_{x_5} \beta^2 \\
D'_{33} = D_{33} \\
D'_{12} = D_{12} + J_{x_4} + J_{x_5} \beta \\
D'_{13} = 0 \\
D'_{23} = 0 \\
v' = 0
\end{cases}$$
(24)

Dynamic balancing:

$$D'_{12} = 0 \Rightarrow \beta = -\frac{J_{x_2} + J_{x_3} + J_{x_4}}{J_{x_5}} \tag{25}$$

Dynamic balanced mechanism:

$$\begin{cases} \tau_1 = k_1 \ddot{\theta}_1 \\ \tau_2 = k_2 \ddot{\theta}_2 \\ f_3 = k_3 \ddot{d}_3 \end{cases}$$
 (26)

Being:

$$\begin{cases}
k_1 = J_{x_1} + J_{x_2} + J_{x_3} + J_{x_4} + J_{x_5} + m_2 l_1^2 + m_3 l_1^2 + \frac{l_1^2 (m_2 + m_3)^2}{m_1} \\
k_2 = \frac{(J_{x_2} + J_{x_3} + J_{x_4})(J_{x_2} + J_{x_3} + J_{x_4} + J_{x_5})}{J_{x_5}} \\
k_3 = m_3
\end{cases}$$
(27)

4 Conclusions

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