

Filter + Amp

toDos :

1. Book consult to understand why the gain is lower than expected
2. Consult on how to use eog sensor properly
3. Transform the data set found today(detail in "Sensor" document) to format easily imported by waveform

Current Design (May 10th)

One bp amplifier + amplifier

G1 = 50 = 34dB

$$F_L = \frac{1}{2\pi R_{IN} C_{IN}} = 0.16Hz$$

$$F_H = \frac{1}{2\pi R_F C_F} = 18.83Hz$$

G2 = 20 = 26dB

Total gain = 1000 = 60dB

V_i = 3500 uv

V_o = 3.5V (simulation) 1.5V (actual)

F_BP : 0.16 - 18.83Hz

Apr 5, 2022

- Actions

Verify whether I have the capacitors

Build and validate the circuit in real life

Detail

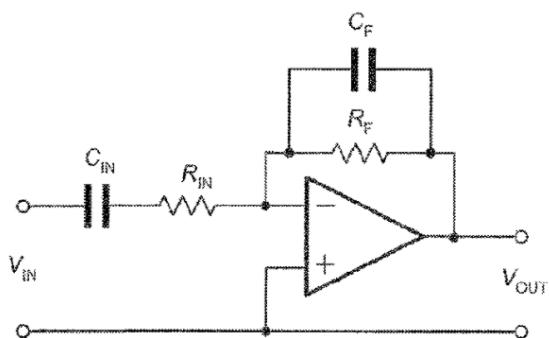


Figure 8.8 Adding capacitors to modify the frequency response of an inverting operational amplifier

(from perusal week 6 op amp)

Since only the frequency between 0.1 and 20Hz is related to eye movement, we will choose a bandpass between 0.1 to 25 Hz.

From ref[2], the typical signal is 50 to 3500 uV, and we want to amplify it to 0~1.5 V
So we need a gain of 428.6. If we choose $R_{IN} = 100\Omega$, $R_F = 42k\Omega$

Higher cutoff frequency :

$$R_F = 42k\Omega$$

$$F_H = \frac{1}{2\pi R_F C_F} = 25Hz$$

$$C_F = \frac{1}{2\pi R_F F_H} = 152nF$$

For simpler circuit, we choose

$$C_F = \frac{1}{2\pi R_F F_H} = 150nF$$

$$F_H = \frac{1}{2\pi R_F C_F} = 25.26Hz$$

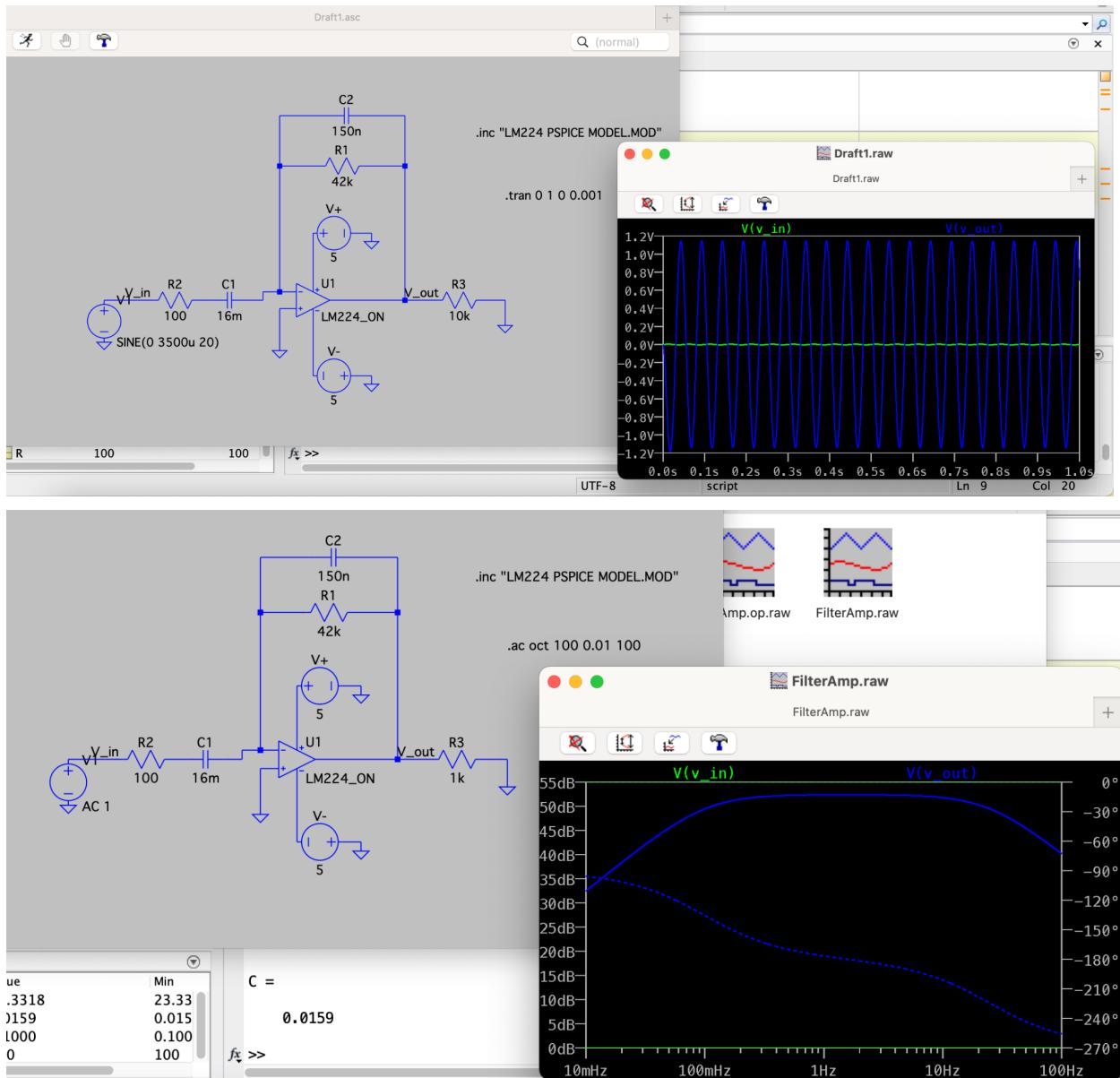
Lower cutoff frequency :

$$R_{IN} = 100\Omega$$

$$F_L = \frac{1}{2\pi R_{IN} C_{IN}} = 0.1Hz$$

$$C_{IN} = \frac{1}{2\pi R_{IN} F_L} = 16mF$$

By simulation, the result is pretty similar to what I expected



Ref

[2] - Deng, L. Y., Hsu, C.-L., Lin, T.-C., Tuan, J.-S., Chang, S.-M. (2010). EOG-based Human–Computer Interface system development. Expert Systems with Applications, 37(4), 3337–3343. doi:10.1016/j.eswa.2009.10.017

May 6, 2022

Issue 1 : The capacitance come in 1mF maximum

> R_{in} must be increased

Issue 2 : We need the output signal to be 5V instead of 1.5V

> Either change R_f or add another amplifier

New Gain : $5V/3500\mu V = 1428$

If we use $R_{in} = 1k\Omega$

$$F_L = \frac{1}{2\pi R_{IN} C_{IN}} = 0.1Hz$$

$$C_{IN} = \frac{1}{2\pi R_{IN} F_L} = 1600\mu F$$

$$R_f = 1428k\Omega$$

$$C_F = \frac{1}{2\pi R_F F_H} = 4.581nF$$

This is a bit too small for our components, and 1.4MOhm may also induce large currents.

New Strategy: use two amplifiers with a same cutoff frequency

New Gain : $\sqrt{1428} = 37.78 = 31.54dB$

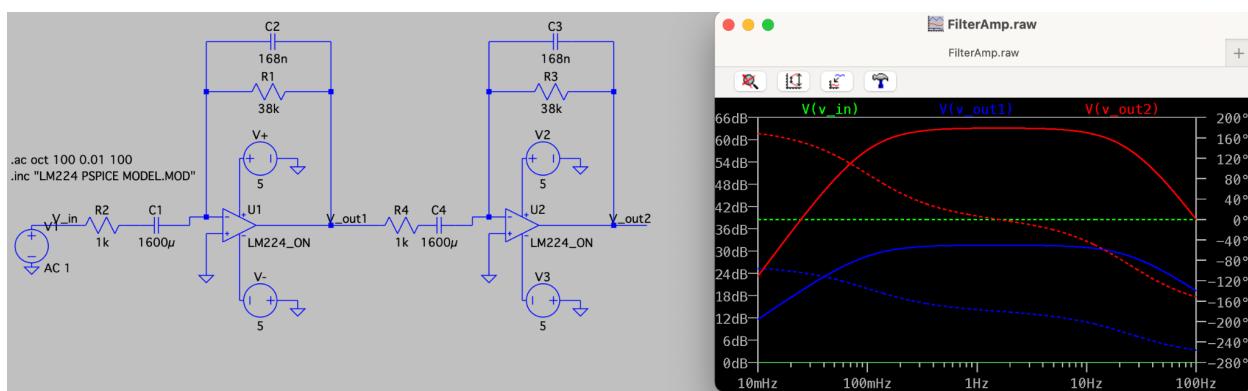
$$R_f = 37.78k\Omega$$

$$C_F = \frac{1}{2\pi R_F F_H} = 168.5nF$$

For simplicity,

Choose $R_f = 38k\Omega$, $C_F = 168nF$

New cut-off $F_H = 24.93Hz$



May 9, 2022

The full circuits were showing that the filt& are amplifying it to 3.5V instead of 5V. I noticed that I haven't truly validated the circuit yet.

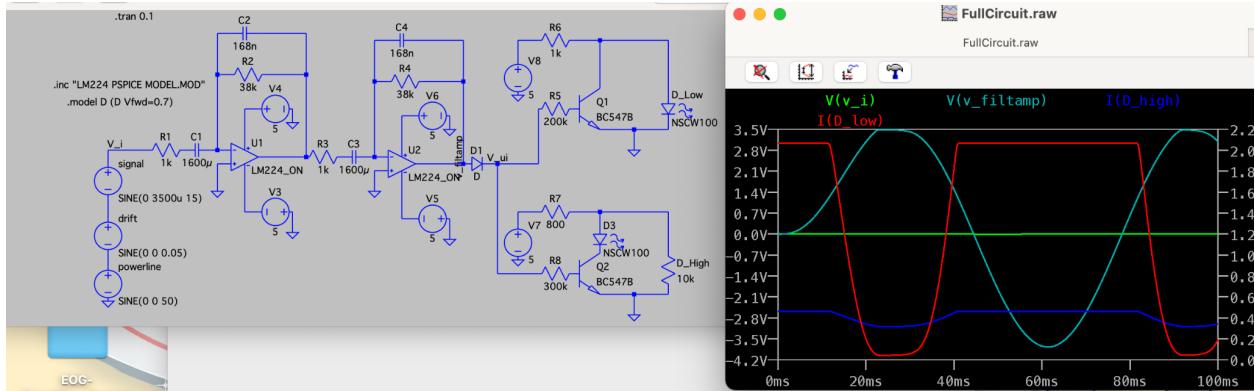
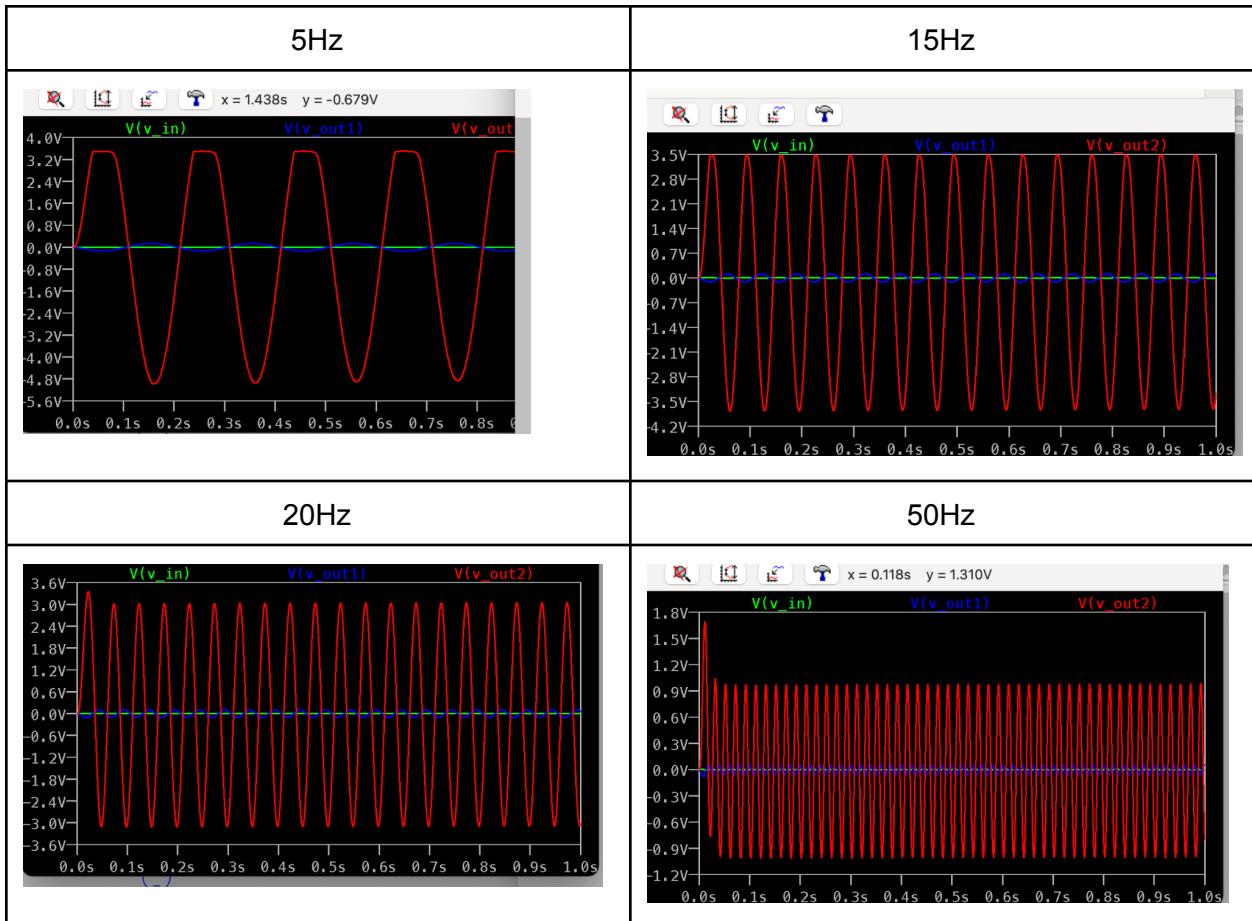


Figure : Result of the full circuit. The magnitude of the incoming signal to the ui was off, hence the threshold was not catered to that.

Testing the filt& circuit with sin wave of 3500uV magnitude, at 5 to 15 Hz, the output is consistent at around 3.5V. At 20 Hz, the output is starting to attenuate.

At a powerline frequency of 50 Hz, we can see that the output is lower than 1V, which I think is satisfactory for. If the actual magnitude is larger than the signal, we may need to redesign the filter again. **Clearly, the calculations did not end up as I have anticipated, we will need a better understanding of the issue, probably bringing it up for consultation.**



Future actions:

1. Reset the thresholds of the ui to suit this new gain.
 2. May need a peak detector to capture the average signal value.
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May 10, 2022

Building circuit

For ease of building, I have simplified some of the components, which altered the gain and cutoff frequencies in the first op amp. I have also removed the filtering in the second op amp, and instead make it do only amplifying. If the powerline noise do come in effect in the future, we may place it back.

Another thing I did not noticed in the past is that the upper limit of the amplified signal is not 5V, but 3.5V instead. So the 3.5V output I was seeing is generated by saturation of the component. I should have noticed that by the clipping in the peaks. Nevertheless, here are the new calculations:

$$G_1 = 50 = 34\text{dB}$$

$$F_L = \frac{1}{2\pi R_{IN}C_{IN}} = 0.16\text{Hz}$$

$$F_H = \frac{1}{2\pi R_F C_F} = 18.83\text{Hz}$$

$$G_2 = 20 = 26\text{dB}$$

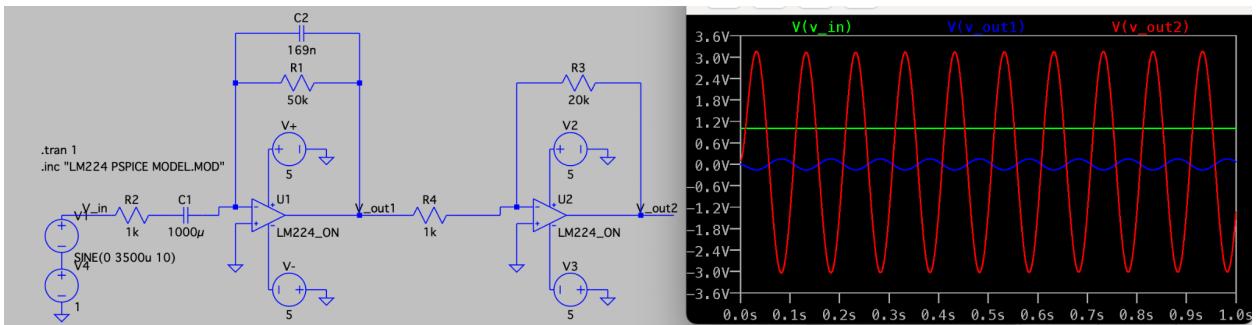
$$\text{Total gain} = 1000 = 60\text{dB}$$

$$V_i = 3500 \mu\text{V}$$

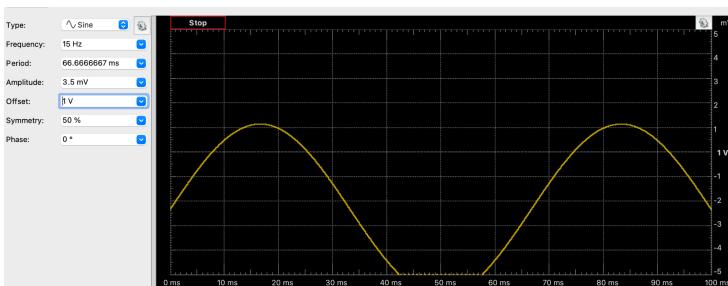
$$V_o = 3.5\text{V (simulation)} 1.5\text{V (actual)}$$

Interestingly, [the actual voltage is way lower than simulation](#). I don't really know why. I may need to bring it up for consultation.

Simulation



Test signal : sine wave 15Hz, 3.5mV, offset(drift) of 1V

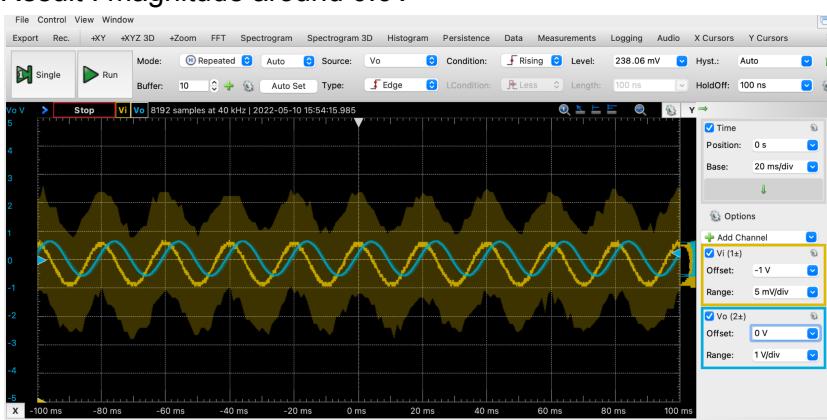


Result : The drift is successfully removed, but the magnitude is 1.5V instead



Test with 50Hz sine (powerline)

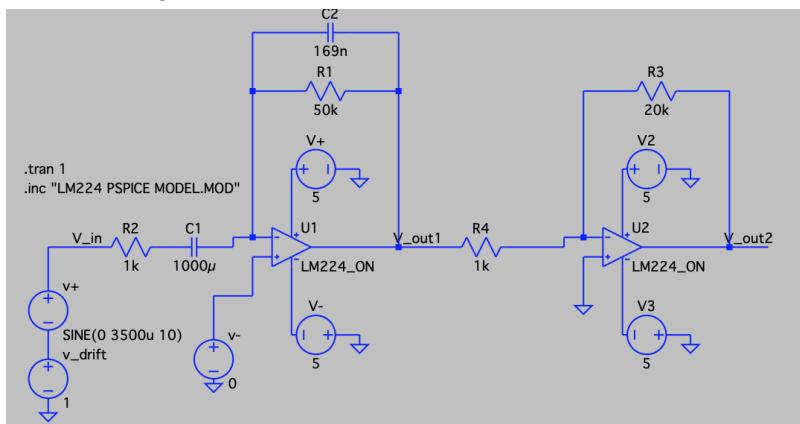
Result : magnitude around 0.6V



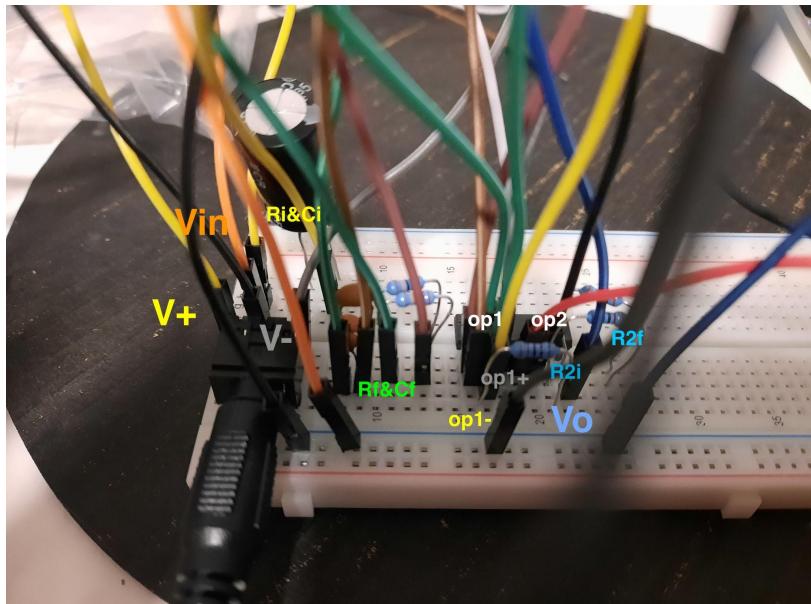
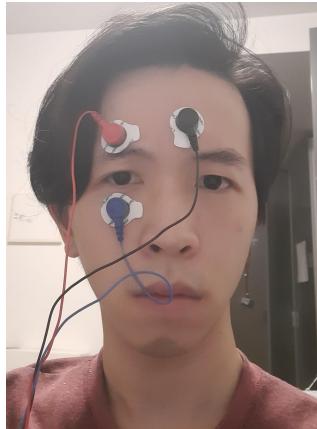
Testing with eog sensor

With the audio jack, I connected the middle pin(sleeve/ ground) to the ground, right most pin(tip/V+) to V_{in}, and left most pin (ring/ V-) to the + end of the first opamp.

The resulting circuit is as follows:



The result shows that there are no differences between V_i and the gaze angle. I may have not connected the audio jack correctly, or I may have not considered certain noises generated by the jack.





Gazing up

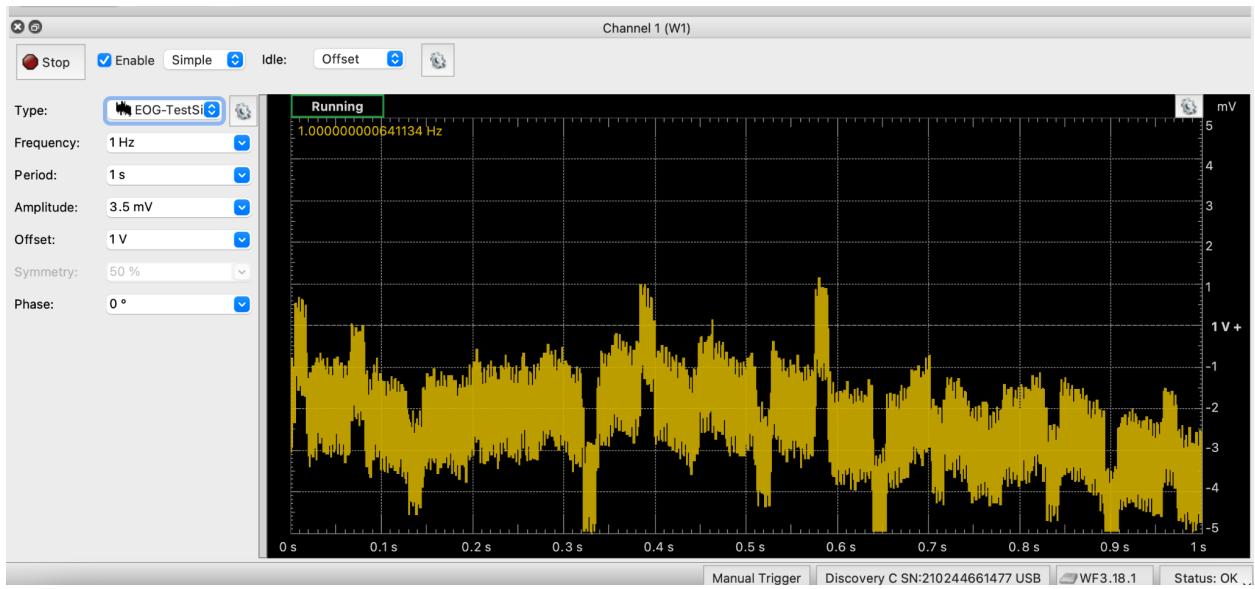


Gazing down



Gazing middle

Testing with workshop's dataset



Result: 1V drift successfully removed, signal amplified to 1V magnitude.



Future plans:

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