Multistate histogram-free reweighting for vapor-liquid coexistence calculations of non-simulated force field parameters

Richard A. Messerly,*,† Mohammad S. Barhaghi,‡ Jeffrey J. Potoff,‡ and Michael R. Shirts¶

†Thermodynamics Research Center, National Institute of Standards and Technology, Boulder, Colorado, 80305, United States

‡Department of Chemical Engineering and Materials Science, Wayne State University, Detroit, Michigan 48202, United States

¶Department of Chemical and Biological Engineering, University of Colorado, Boulder, Colorado, 80309, United States

E-mail: richard.messerly@nist.gov

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Abstract

1 Introduction

A key use of molecular simulation is the ability to accurately and efficiently estimate vapor-liquid coexistence properties, i.e., saturated liquid density ($\rho_{\rm liq}^{\rm sat}$), saturated vapor density ($\rho_{\rm vap}^{\rm sat}$), saturated vapor pressures ($P_{\rm vap}^{\rm sat}$), and enthalpy of vaporization ($\Delta H_{\rm v}$). The accuracy of coexistence estimates depends on the underlying molecular model (a.k.a., force field, potential model, or Hamiltonian) while the computational efficiency depends primarily on the simulation methods, software, and hardware. Due to the abundance of experimental vapor-liquid coexistence data and the sensitivity of such properties to both short- and long-range non-bonded interactions, numerous force fields have been parameterized using $\rho_{\rm liq}^{\rm sat}$, $P_{\rm vap}^{\rm sat}$, and $\Delta H_{\rm v}$. Although the development of accurate force fields has been greatly enabled by the improved efficiency of simulation methods, parameterization of non-bonded interactions with vapor-liquid coexistence calculations remains an arduous and time-consuming task. ¹⁻³

Several methods exist for computing vapor-liquid coexistence properties. These include Gibbs Ensemble Monte Carlo (GEMC), two phase molecular dynamics (2ϕ MD), isothermal-isochoric integration (ITIC), and Grand Canonical Monte Carlo coupled with histogram reweighting (GCMC-HR). Advantages and disadvantages exist for each method. For example, GEMC and GCMC require insertion moves that are computationally inefficient for complex molecular structures with high density liquid phases. Several advanced simulation techniques are available to overcome this challenge, 4 which has enabled GEMC and GCMC-HR to be the primary methods of choice for vapor-liquid coexistence calculations.

Some clear advantages and disadvantages exist for GCMC-HR compared with GEMC.

For example, one advantage of GCMC-HR is the higher precision. Furthermore, coexistence properties can be computed at temperatures that are not simulated directly. However, GEMC is arguably more straightforward in that simulations are performed only at the desired saturation temperatures ($T^{\rm sat}$). By contrast, GCMC-HR requires a series of GCMC simulations for a single $T^{\rm sat}$. This set includes a near-critical simulation that "bridges" the vapor and liquid phases. Obtaining the appropriate chemical potential (μ) for this bridge simulation is a cumbersome and, typically, iterative process (although more advanced methods exist to obtain a good initial estimate for μ^6).

Another disadvantage of GCMC-HR compared to GEMC is that GCMC-HR requires more post-processing (i.e., histogram reweighting), while simple block averaging is typically sufficient for GEMC. Histogram reweighting (and more generally, configuration reweighting) is an important tool in many fields of molecular simulation. In fact, it has long since been known that it is possible to estimate properties for state j by reweighting configurations that were sampled with state i. For example, umbrella sampling simulations are often processed using the weighted histogram analysis method (WHAM) to compute free energy differences between states. A popular alternative to WHAM is the Multistate Bennett Acceptance Ratio (MBAR), 11,12 which is readily available in the *pymbar* package.

In this study, we substitute HR with MBAR for the GCMC-HR approach of computing vapor-liquid coexistence properties. Section 2.3 demonstrates that MBAR and HR are mathematically equivalent (in the limit of zero bin width) while Section 3 shows that they are also numerically equivalent (to within statistical uncertainties). Note that, as Boulougouris et al. demonstrate how to combine HR with GEMC (GEMC-HR) to estimate saturation properties at non-simulated temperatures, ¹³ MBAR could alternatively be applied to GEMC simulations.

Substituting the standard HR approach with MBAR is not the primary purpose of this

study. Rather, we demonstrate how GCMC-MBAR can also estimate coexistence properties for non-simulated parameter sets, which can greatly accelerate force field parameterization. In a similar study, Messerly et al. demonstrate how to combine MBAR with ITIC (MBAR-ITIC) to optimize Mie λ -6 (generalized Lennard-Jones) potentials. ^{14,15} For MBAR-ITIC, a series of NVT simulations along an isotherm and isochores are performed with a "reference" force field ($\theta_{\rm ref}$). MBAR computes the internal energy (U) and pressure (P) (or compressibility factor, Z) for each $T-\rho$ state point with a non-simulated ("rerun") force field ($\theta_{\rm rr}$). ITIC then converts the U and P values into vapor-liquid coexistence properties. ^{16,17}

The results from Messerly et al. demonstrate that MBAR-ITIC is most reliable in the local domain, i.e., for parameter sets near the "reference" parameter set from which configurations are sampled. He furthermore, MBAR-ITIC performs best for changes in the non-bonded well-depth parameter (ϵ) while it performs significantly worse for large changes in the non-bonded size and repulsive parameters $(\sigma$ and λ , respectively). This is typically referred to as poor "overlap" and can be quantified by the "number of effective samples" $(N_{\rm eff})$, which is essentially the number of non-negligible samples that contribute to the estimated ensemble averages. Poor overlap (low $N_{\rm eff}$) is especially problematic for ITIC as a large number of snapshots is needed to obtain precise estimates of P in the liquid phase, which are essential to obtain reasonable values of $\rho_{\rm liq}^{\rm sat}$.

Our initial hypothesis was that GCMC-MBAR should have better overlap over the non-bonded parameter space than what was observed for MBAR-ITIC. There are two main reasons for this hypothesis/aspiration. First, as opposed to the fixed density NVT simulations, the fluctuating density of a GCMC simulation produces a wider range of configurations and energies. Second, ITIC requires accurate calculations of U and P in the vapor phase, which necessitate larger box sizes (and, thereby, more molecules) than those typically utilized with GCMC. By utilizing fewer molecules, GCMC simulations

experience larger energy fluctuations (on a percent basis) which improves the overlap between states. We also hypothesized that the impact of poor overlap would be less severe compared to ITIC, where poor overlap leads to sporadic and nonsensical coexistence estimates.

The method outlined in this study is similar in spirit to "Hamiltonian scaling" (HS), which has been applied to both GEMC 18 and GCMC simulations. $^{10,19-21}$ The HS approach samples from multiple force fields (Hamiltonians) in a single simulation according to a weighted sampling probability. Vapor-liquid coexistence curves for each force field are estimated post-simulation by reweighting the configurations accordingly. For the Grand Canonical Monte Carlo implementation of Hamiltonian scaling (HS-GCMC), μ and T are not stationary during the simulation, rather the current value of μ and T depends on which force field is being sampled. Despite HS-GCMC proving to be a powerful tool to optimize force field parameters, $^{10,19-21}$ it has yet to gain widespread popularity. This is likely due to the added complexity of both the simulation protocol and the histogram post-processing. Also, HS requires that a decision be made *a priori* regarding which force fields are to be tested. By contrast, MBAR does not require any modification of the simulation procedure, the post-processing is essentially unchanged, and the non-bonded parameter sets need not be selected prior to the simulations.

Recently, Weidler and Gross proposed "individualized," i.e., compound-specific, parameter sets for compounds which contain large amounts of experimental data. ²² To avoid overfitting, a one-dimensional optimization is employed which scales ϵ for all unitedatom sites while not adjusting σ or λ . MBAR is ideally suited for this " ϵ -scaling" approach for at least two reasons. First, as mentioned previously, MBAR is most reliable when extrapolating in ϵ rather than σ and/or λ . Second, the rate-limiting step for MBAR is recomputing the configurational energies for a different force field. Furthermore, storing millions of configuration "snapshots" is highly memory intensive. While basis functions

(see Section 2.4) alleviate the additional computational cost and reduce the memory load, ϵ -scaling does not require storing/recomputing configurations or basis functions. Instead, the energies for each snapshot are simply multiplied by the ϵ -scaling parameter.

The outline for this study is the following. Section 2 provides details regarding the force fields, simulation set-up, and post-simulation analysis with MBAR. Section 3 provides a comparison of GCMC-MBAR and GCMC-HR as well as various applications of GCMC-MBAR for force field parameterization. Section 4 discusses some limitations and provides recommendations for future work. Section 5 presents the primary conclusions.

2 Methods

2.1 Force fields

The force fields utilized in this study are Transferable Potentials for Phase Equilibria (TraPPE-UA, also referred to simply as TraPPE^{1,23,24}), Mie Potentials for Phase Equilibria (MiPPE), ^{3,25} and Nath, Escobedo, and de Pablo revised (NERD). Each force field adopts a united-atom (UA) representation, where non-polar hydrogens are not modeled explicitly. The non-bonded potential is of the generalized Lennard-Jones (Mie λ -6) form.

The bond lengths for the TraPPE, MiPPE, and NERD force fields are 0.154 nm for all compounds studied. The same angle and dihedral potentials are used for each force field. Angular bending interactions are evaluated using a harmonic potential:

$$u^{\text{bend}} = \frac{k_{\theta}}{2} \left(\theta - \theta_0\right)^2 \tag{1}$$

where $u^{\rm bend}$ is the bending energy, θ is the instantaneous bond angle, θ_0 is the equilibrium bond angle (see Table 1), and k_{θ} is the harmonic force constant with $k_{\theta}/k_{\rm B} = 62500 \, {\rm K/rad^2}$ for all bonding angles, where $k_{\rm B}$ is the Boltzmann constant.

Table 1: Equilibrium bond angles (θ_0) .²³ CH_i and CH_j represent CH₃, CH₂, CH, or C sites.

| Bending sites | θ_0 (degrees) |
|--------------------------|----------------------|
| CH_i - CH_2 - CH_j | 114.0 |
| CH_i - CH - CH_j | 112.0 |
| CH_i - C - CH_j | 109.5 |

Dihedral torsional interactions are determined using a cosine series:

$$u^{\text{tors}} = c_0 + c_1[1 + \cos\phi] + c_2[1 - \cos 2\phi] + c_3[1 + \cos 3\phi]$$
 (2)

where u^{tors} is the torsional energy, ϕ is the dihedral angle and c_n are the Fourier constants listed in Table 2.

Table 2: Fourier constants (c_n/k_B) in units of K.²³ CH_i and CH_j represent CH₃, CH₂, CH, or C sites.

| Torsion sites | $c_0/k_{\rm B}$ | $c_1/k_{ m B}$ | $c_2/k_{ m B}$ | $c_3/k_{\rm B}$ |
|--|-----------------|----------------|----------------|-----------------|
| CH _i -CH ₂ -CH ₂ -CH _j | 0.0 | 355.03 | -68.19 | 791.32 |
| CH_i - CH_2 - CH - CH_j | -251.06 | 428.73 | -111.85 | 441.27 |
| CH_i - CH_2 - C - CH_j | 0.0 | 0.0 | 0.0 | 461.29 |
| CH_i - CH - CH - CH_j | -251.06 | 428.73 | -111.85 | 441.27 |

Non-bonded interactions between sites located in two different molecules or separated by more than three bonds within the same molecule are calculated using a Mie λ -6 potential (of which the Lennard-Jones, LJ, 12-6 is a subclass):

$$u^{\rm nb}(\epsilon, \sigma, \lambda; r) = \left(\frac{\lambda}{\lambda - 6}\right) \left(\frac{\lambda}{6}\right)^{\frac{6}{\lambda - 6}} \epsilon \left[\left(\frac{\sigma}{r}\right)^{\lambda} - \left(\frac{\sigma}{r}\right)^{6}\right] \tag{3}$$

where $u^{\rm nb}$ is the van der Waals interaction, σ is the distance (r) where $u^{\rm nb}=0$, $-\epsilon$ is the energy of the potential at the minimum (i.e., $u^{\rm nb}=-\epsilon$ and $\frac{\partial u^{\rm nb}}{\partial r}=0$ for $r=r_{\rm min}$), and λ is

the repulsive exponent.

The non-bonded Mie λ -6 force field parameters for TraPPE, MiPPE, and NERD are provided in Table 3. MiPPE reports a "generalized" (MiPPE-gen) and "short/long" (MiPPE-SL) CH and C parameter set. The "short" and "long" parameters are implemented when the number of carbons in the backbone is ≤ 4 and > 4, respectively. Also note that the NERD force field has several different parameter sets for CH₃ sites.

Table 3: Non-bonded (intermolecular) parameters for TraPPE, 1,23 MiPPE, 3,25 and NERD. 26

| United-atom | $\epsilon/k_{ m B}$ (K) | σ (nm) | λ | | | | |
|---------------------------------------|-------------------------|---------------|-----------|--|--|--|--|
| TraPPE | | | | | | | |
| CH ₃ | 98 (134.5) | 0.375 (0.352) | 12 | | | | |
| CH_2 | 46 | 0.395 | 12 | | | | |
| СН | 10 | 0.468 | 12 | | | | |
| C | 0.5 | 0.640 | 12 | | | | |
| MiPPE | | | | | | | |
| CH ₃ | 121.25 | 0.3783 | 16 | | | | |
| CH_2 | 61 | 0.399 | 16 | | | | |
| CH, gen. | 15 | 0.46 | 16 | | | | |
| C, gen. | 1.2 | 0.61 | 16 | | | | |
| CH, short | 15 | 0.47 | 16 | | | | |
| C, short | 1.45 | 0.61 | 16 | | | | |
| CH, long | 14 | 0.47 | 16 | | | | |
| C, long | 1.2 | 0.62 | 16 | | | | |
| NERD | | | | | | | |
| CH_3 | 104.00 | 0.3910 | 12 | | | | |
| CH_3 (2-methylpropane) | 78.23 | 0.3880 | 12 | | | | |
| CH ₃ (2,2-dimethylpropane) | 74.50 | 0.3910 | 12 | | | | |
| CH_2 | 45.80 | 0.3930 | 12 | | | | |
| СН | 39.70 | 0.3850 | 12 | | | | |
| С | 17.00 | 0.3910 | 12 | | | | |

Non-bonded parameters between two different site types (i.e., cross-interactions) are determined using Lorentz-Berthelot combining rules 27 for ϵ and σ and an arithmetic mean

for the repulsive exponent λ (as recommended in Reference 3):

$$\epsilon_{ij} = \sqrt{\epsilon_{ii}\epsilon_{jj}} \tag{4}$$

$$\sigma_{ij} = \frac{\sigma_{ii} + \sigma_{jj}}{2} \tag{5}$$

$$\lambda_{ij} = \frac{\lambda_{ii} + \lambda_{jj}}{2} \tag{6}$$

where the ij subscript refers to cross-interactions and the subscripts ii and jj refer to same-site interactions.

2.2 Simulation set-up

The majority of results presented in Section 3 are obtained by reprocessing simulation output that were analyzed in previous studies utilizing histogram reweighting. ^{25,28} New simulation results are provided for n-hexane, 2-methylpropane, 2,2-dimethylpropane, 2,2,4-trimethylhexane, 2,3-dimethylbutane, 2,3,4-trimethylpentane, 2,2,3,3-tetramethylbutane, and cyclohexane. All simulations are performed using GPU optimized Monte Carlo (GOMC) with Grand Canonical Monte Carlo (GCMC), where the chemical potential (μ), volume (V), and temperature (T) are constant.

A series of nine simulations are performed, two in the vapor phase, six in the liquid phase, and one near critical which acts as the "bridge" between the vapor and liquid phases. A low-density (less than twenty molecules) initial configuration is utilized for the vapor phase simulations, while the bridge and liquid phase simulations are initialized with a high-density (around 200 molecules) configuration. The system volume is the same for each simulation, but varies somewhat between compounds. The prescribed chemical potentials and temperatures for the branched alkanes are the same as those utilized in Mick et al. 25 The $\mu-T$ values for n-hexane and cyclohexane are determined in this study.

All state points are reported in Supporting Information.

The equilibration stage for each GCMC simulation consists of 2×10^7 Monte Carlo steps (MCS). The production stage is 4×10^7 MCS for vapor simulations and 2.5×10^7 MCS for the liquid and "bridge" simulations. Snapshots (i.e., number of molecules, internal energy, and optionally the xyz coordinates) are stored every 200 MCS to reduce the correlation between sequential configurations. Thus, the total number of snapshots $(N_{\rm snaps})$ is 2×10^5 for vapor simulations and 1.25×10^5 for liquid and "bridge" simulations. The type of Monte Carlo move implemented for each step is selected randomly with a 20%, 10%, and 70% probability of performing a displacement, rotation, and particle swap move, respectively. The move probabilities are slightly different for cyclohexane, namely, 30%, 10%, 40%, and 20% for displacement, rotation, particle swap, and crank-shaft moves, respectively.

Four different applications for MBAR are demonstrated in this study, where slightly different types of simulation output are required. First, we demonstrate how MBAR yields consistent results to those previously reported using histogram reweighting. The standard simulation output is used in this application, namely, a $2xN_{\rm snaps}$ array containing the number of molecules and the internal energy for all $N_{\rm snaps}$ snapshots. Second, we demonstrate how these same data can be used with MBAR to predict VLE properties when performing ϵ -scaling. Third, we investigate how well MBAR can predict VLE for force field "j" from sampled states of force field "i." In this case, a $3xN_{\rm snaps}$ array is required, where the additional column is the internal energy computed with force field "j" for the configurations sampled with force field "i." Fourth, we demonstrate how storing basis functions is a computationally efficient method for predicting VLE for multiple force fields that are unknown at runtime.

2.3 Multistate Bennett Acceptance Ratio

The GCMC approach for estimating phase coexistence requires significant post-processing. Before demonstrating how we implement MBAR for this purpose, we review the traditional histogram reweighting (HR) approach. We also discuss the steps of this procedure that are the same for both HR and MBAR. We refer the interested reader to the literature for derivations and more detailed discussion of the GCMC-HR equations (cf. 10).

The HR equation to compute the ensemble average for a given observable (O) is

$$\langle O(\mu, \beta) \rangle = \sum_{U} \sum_{N} O \times Pr(N, U; \mu, \beta)$$
 (7)

where $\langle \dots \rangle$ denotes an ensemble average and $Pr(N,U;\mu,\beta)$ is the probability of observing N particles with internal energy U for a given chemical potential (μ) and inverse temperature $(\beta \equiv \frac{1}{k_{\rm B}T}$, where $k_{\rm B}$ is the Boltzmann constant). The probability is obtained with HR using

$$Pr(N, U; \mu, \beta) = \frac{\sum_{i=1}^{R} Pr_i(N, U) \exp(-\beta U + \beta \mu N)}{\sum_{i=1}^{R} K_i \exp(-\beta_i U + \beta_i \mu_i N + C_i)}$$
(8)

where $Pr_i(N,U)$ is the probability of occurrence N particles in the simulation cell with total configurational energy in the vicinity of U, R is the number of runs (where the ith run corresponds to β_i and μ_i), K_i is the total number of observations ("snapshots") for run i (i.e., $K_i = \sum_{N,U} Pr_i(N,U)$), and C_i are "constants" that are calculated with the relationship

$$C(\mu, \beta) = -\ln \sum_{U} \sum_{N} \frac{\sum_{i=1}^{R} Pr_i(N, U) \exp(-\beta U + \beta \mu N)}{\sum_{i=1}^{R} K_i \exp(-\beta_i U + \beta_i \mu_i N + C_i)}$$
(9)

where $C_i = C(\mu_i, \beta_i)$.

Equations 7, 8, and 9 only allow for reweighting simulations at a different β and μ . By contrast, MBAR can also be applied to reweight simulations for different force field parameters (θ). The analogous MBAR equation to Equation 7 is

$$\langle O(\theta, \mu, \beta) \rangle = \sum_{n=1}^{K_{\text{snaps}}^{\text{tot}}} O(\boldsymbol{x}_n, N_n; \theta, \mu, \beta) \times W_n(\theta, \mu, \beta)$$
(10)

where x_n , N_n are configurations sampled from $i=1\dots R$ simulations at inverse temperature (β_i) , chemical potential (μ_i) , and force field parameters (θ_i) . $W_n(\theta,\beta,\mu)$ is the weight of the n^{th} configuration in a simulation with arbitrary μ , β , and θ . W_n is computed with the following expression (analogous to Equation 8)

$$W_n(\theta, \beta, \mu) = \frac{\exp[\hat{f}(\theta, \beta, \mu) - u(\boldsymbol{x}_n, N_n; \theta, \beta, \mu)]}{\sum\limits_{i=1}^{R} K_i \exp[\hat{f}(\theta_i, \beta_i, \mu_i) - u(\boldsymbol{x}_n, N_n; \theta_i, \beta_i, \mu_i)]}$$
(11)

where $\hat{f}(\theta, \beta, \mu)$ is the reduced free energy, K_i are the total number of snapshots from the i^{th} run, and $u(\boldsymbol{x}_n, N_n; \theta, \beta, \mu)$ is the reduced potential energy evaluated with θ , β , and μ for configuration \boldsymbol{x}_n, N_n . For the grand canonical ensemble, $u(\boldsymbol{x}_n, N_n; \theta, \beta, \mu) = \beta U(\boldsymbol{x}_n; \theta) - \beta \mu N_n$. The reduced free energy is computed with an expression analgous to Equation 9

$$\hat{f}(\theta, \beta, \mu) = -\ln \sum_{n=1}^{K_{\text{snaps}}^{\text{tot}}} \frac{\exp[-u(\boldsymbol{x}_n, N_n; \theta, \beta, \mu)]}{\sum_{i=1}^{R} K_i \exp[\hat{f}(\theta_i, \beta_i, \mu_i) - u(\boldsymbol{x}_n, N_n; \theta_i, \beta_i, \mu_i)]}$$
(12)

where $K_{\mathrm{snaps}}^{\mathrm{tot}} = \sum_{i} K_{i}$ is the total number of snapshots for all R runs.

Both HR and MBAR require solving a system of R-1 nonlinear equations for self-consistency (Equations 8 and 9 for HR and Equations 11 and 12 for MBAR). Specifically, initial guesses for C_i (HR) or \hat{f} (MBAR) are updated iteratively until convergence is achieved for the respective equations. There is provably only one solution, so as long as

certain criteria are met that will be discussed below. Thus, although a range of different solver methods exist, the only difference is efficiency and numerical stability.

These two sets of equations (HR: Equations 7, 8, and 9, MBAR: Equations 10, 11, and 12) can be seen as equivalent with the following assumptions. First, if all R simulations are performed using a single reference force field (θ_{ref}) and W_n and \hat{f} are computed with $\theta = \theta_i = \theta_{ref}$. Second, in the limit of infinitesimal histogram bin widths no histogram contains more than 1 sample. In that case, U and N for each histogram can be taken to be the $U(x_n)$ and N_n of the single observation in that histogram, and histograms with no particles can be omitted. We then observe that $Pr_i(N,U)$ is either 1 or 0, and the sum over all histograms becomes a sum over samples conducted in all R simulation runs. Eq. 9 reduces in this approximation to Eq. 12, and Eq. 8 reduces to Eq. 11.

However, a key advantage of MBAR over HR is that by changing from a sum over histograms to a sum over samples, we are free to perform simulations with other conditions besides μ and β . For example, we can carry out simulations at different force field parameters θ . In the histogram context, we cannot easily separate out samples in the same U histogram that were performed with different force field parameters. If we perform sums over samples, we can reevaluate the configuration with a range of different parameters for a relatively small expense.

For both HR and MBAR, the pressure equation is derived from $\ln \Xi = \beta PV$, where Ξ is the grand partition function. The HR expression is

$$C_1 - C_2 = \ln \frac{\Xi(\mu_2, V, \beta_2)}{\Xi(\mu_1, V, \beta_1)} = \beta_2 P_2 V - \beta_1 P_1 V$$
(13)

where P is the pressure, and runs 1 and 2 are performed with (μ_1, V, β_1) and (μ_2, V, β_2) ,

respectively. The analogous MBAR equation is

$$\hat{f}_1 - \hat{f}_2 = \ln \frac{\Xi(\theta_2, \mu_2, V, \beta_2)}{\Xi(\theta_1, \mu_1, V, \beta_1)} = \beta_2 P_2 V - \beta_1 P_1 V$$
(14)

where runs 1 and 2 can also be performed using different force field parameters, θ_1 and θ_2 , respectively. Computing the absolute pressure of P_1 with Equations 13 and 14 requires a reference pressure (P_2) , which is determined at a low-density where the ideal gas equation of state, $PV = Nk_{\rm B}T$, is assumed to be accurate.

The equilibrium chemical potential is determined by equating the pressures in the gas and liquid states. The gas and liquid states are integrated separately by dividing the configurations into low and high density phases.

After determining the saturation chemical potential $(\mu_{\rm sat})$, the vapor and liquid properties are computed with Equations 7 (HR) or 10 (MBAR) by separating the histograms or configurations into "vapor" and "liquid" phases. Typically this designation is based on U and/or N. For example, when computing $\rho_{\rm liq}^{\rm sat}$ and $U_{\rm liq}^{\rm sat}$ with HR, the double summation in Equation 7 is performed for $N > N_{\rm c}$, where $N_{\rm c}$ is an estimate for the critical number of molecules.

2.4 Basis functions

- 1. When applying MBAR to different parameter sets, $\theta \neq \theta_{ref}$, it is necessary to recompute energies
- 2. Basis functions accelerate the recompute energy step by storing the repulsive and attractive contributions that can be scaled by ϵ and σ
- 3. Basis functions are computed from GOMC using the recompute feature for different ϵ and σ and solving system of equations

3 Results

This section presents results from several different applications of GCMC-MBAR. First, we compute vapor-liquid coexistence properties in the case where the force field parameters do not change, i.e., $\theta_{\rm rr}=\theta_{\rm ref}$. Second, we perform a one-dimensional optimization in the ϵ -scaling parameter, ψ . This requires applying GCMC-MBAR with $\epsilon_{\rm rr}=\psi\times\epsilon_{\rm ref}$ while $\sigma_{\rm rr}=\sigma_{\rm ref}$ and $\lambda_{\rm rr}=\lambda_{\rm ref}$. Third, we determine the reliability of GCMC-MBAR when $\theta_{\rm rr}\neq\theta_{\rm ref}$ for different literature force fields. Fourth, we demonstrate how GCMC-MBAR can be applied to obtain new Mie λ -6 parameters for cyclohexane.

Section 2.3 demonstrated that MBAR and HR are mathematically equivalent in the limit of zero bin width and when $\theta_{\rm rr}=\theta_{\rm ref}$. Figure 1 provides numerical validation that GCMC-MBAR and GCMC-HR yield indistinguishable vapor-liquid coexistence properties. Note that the median percent deviation is approximately zero and that the largest deviations are within a few percent. The percent deviations shown in Figure 1 are averaged over the 31 branched alkanes studied by Mick et al. and the 11 alkynes studied by Barhaghi et al. The GCMC-HR values were not recomputed in this study but were taken from the literature. The GCMC-MBAR values were computed using the same raw simulation data as Mick et al. and Barhaghi et al. The only difference being that a single replicate was used to compute GCMC-MBAR values, whereas GCMC-HR used data from all five replicates.

Reference 22 proposed an ϵ -scaling approach for converting transferable parameters (TAMie) into compound-specific or individualized parameters (iTAMie). The philosophy being individualized parameters is that some compounds have sufficient reliable experimental data that a force field can be refined to improve the agreement. Refitting all non-bonded parameters simultaneously could lead to an overfit parameter set, which would likely perform poorly at state points outside of the training set. For this reason, Weidler

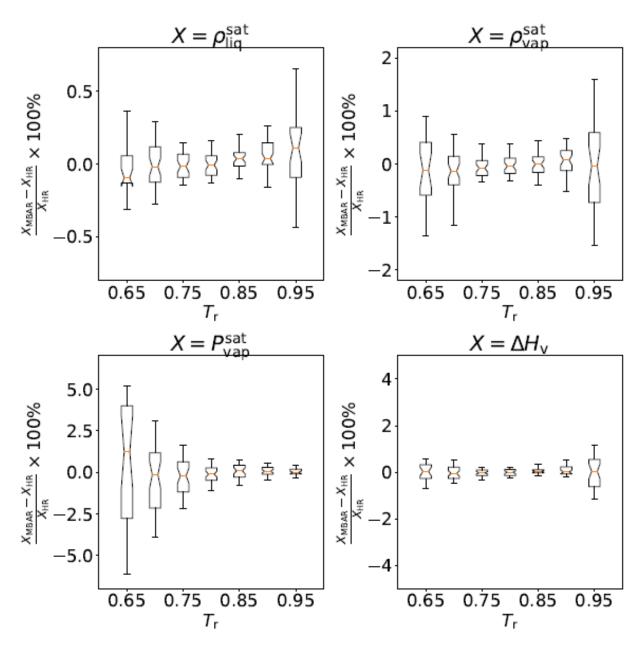


Figure 1: Percent deviations between coexistence properties computed using histogram reweighting (HR) and Multistate Bennett Acceptance Ratio (MBAR). Top-left, top-right, bottom-left, and bottom-right panels correspond to saturated liquid density, saturated vapor density, saturated vapor pressure, and enthalpy of vaporization, respectively. Boxes depict the first and third quartiles while whiskers represent the range that contains 95% of the data.

et al. optimize a single adjustable parameter (ψ) that scales all the ϵ values according to

$$\epsilon_{ii}^{\text{ind}} = \psi \epsilon_{ii}^{\text{tran}} \tag{15}$$

where $\epsilon_{ii}^{\rm ind}$ is the individualized ϵ value for united-atom ii and $\epsilon_{ii}^{\rm tran}$ is the corresponding transferable ϵ value. A truly transferable force field should have $\psi\approx 1$ for all compounds. Weigler et al. tend to characterize the individualization as being useful when the scaling is greater than 0.4% (i.e., $|1-\psi|>0.004$).

Figure 2 shows that the alkynes require a greater degree of scaling than the branched alkanes. The TAMie force field also found $\psi \approx 1$ for branched alkanes. Although ψ values for iTAMie were not reported for alkynes, the largest ψ value for olefins, ethers, and ketones was ≈ 1.01 . Therefore, the transferability of the MiPPE force field appears to be slightly poorer for 2-pentyne and 2-hexyne, which have an optimized $\psi > 1.01$. It is also interesting that only 3 out of 19 compounds require $\psi < 1$. By contrast, this trend was not observed in Reference 22.

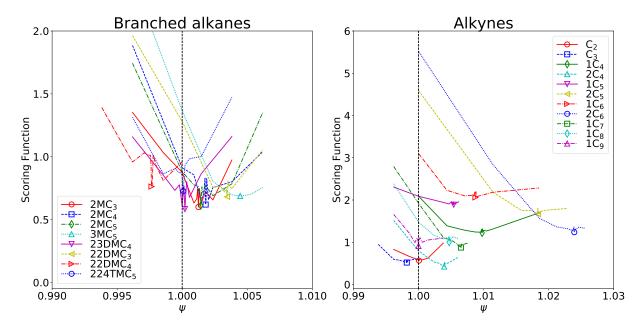


Figure 2: One dimensional optimization with ϵ -scaling (ϕ) of MiPPE-SL for select branched alkanes (left) and alkynes (right). Open symbols correspond to the original force field, i.e., $\phi=1$, while the filled stars are the optimal ϕ value for a given compound.

At least two reasons exist for why MBAR is ideally suited for ϵ -scaling. First, the energies in Equation ?? can be scaled by ϕ such that the configurations do not need to

be stored or recomputed. Second, MBAR is more reliable for changes in ϵ rather than changes in σ and/or λ . ¹⁴ A more demanding test of GCMC-MBAR is to vary several parameters simultaneously, including σ and λ . Because it is not possible to visualize a parameter space of greater than two dimensions, we perform this analysis of GCMC-MBAR using the TraPPE, NERD, MiPPE-gen, and MiPPE-SL force fields. Specifically, we use GCMC-MBAR to predict coexistence properties of the TraPPE force field by sampling configurations with MiPPE-gen, and vice versa (see Figure 4). We also predict coexistence properties for the NERD and MiPPE-SL force fields using configurations sampled from TraPPE and MiPPE-gen, respectively (see Figure 3).

Note that all three non-bonded parameters (ϵ , σ , and λ) for all four united-atom types (CH₃, CH₂, CH, and C) are different between the TraPPE and MiPPE-gen force fields. The TraPPE and NERD ϵ and σ values are different for all four united-atom types while $\lambda = 12$ for both force fields. The MiPPE-gen and MiPPE-SL force fields only differ in the ϵ and/or σ values for the CH and C sites . Specifically, the 2-methylpropane parameters are identical except for $\sigma_{\rm CH}$, the 2,2-dimethylpropane parameters are the same except for $\epsilon_{\rm C}$, and three parameters are different for 2,2,4-trimethylpentane ($\epsilon_{\rm CH}$, $\sigma_{\rm CH}$, and $\sigma_{\rm C}$). However, the difference in ϵ and σ values for MiPPE-gen and MiPPE-SL is significantly smaller than that between TraPPE and NERD.

Figures 3 and 4 compare the GCMC-MBAR predicted values for $\theta_{\rm rr} \neq \theta_{\rm ref}$ to those for $\theta_{\rm rr} = \theta_{\rm ref}$. Figure 3 contains $\lambda_{rmrr} = \lambda_{\rm ref}$ while Figure 4 corresponds to $\lambda_{rmrr} \neq \lambda_{\rm ref}$. Overall, MBAR is extremely reliable at predicting vapor phase properties ($\rho_{\rm vap}^{\rm sat}$ and $P_{\rm vap}^{\rm sat}$) while it is less reliable for liquid phase properties ($\rho_{\rm liq}^{\rm sat}$ and $\Delta H_{\rm v}$, which depends on both phases). In particular, note that the $\rho_{\rm liq}^{\rm sat}$ estimates in Figure 4 are sporadic and unreliable. This can be explained by the low number of effective samples in the liquid phase, which demonstrate that the repulsive exponent (λ) greatly impacts the configurational overlap in the liquid phase.

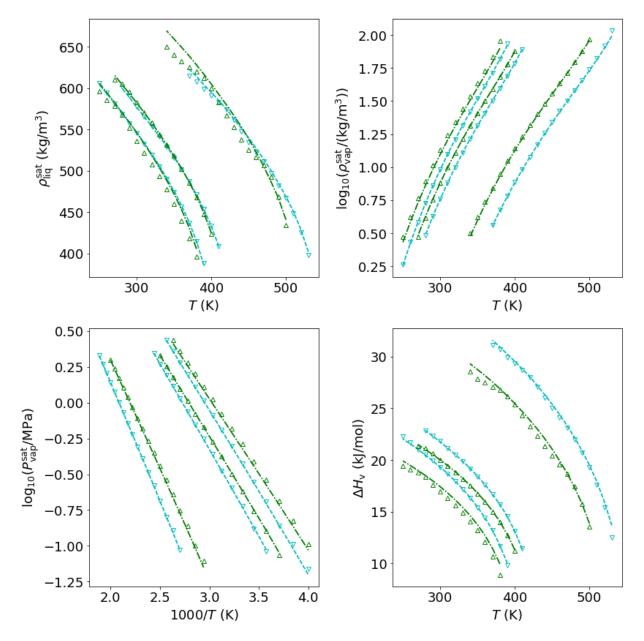


Figure 3: Comparison between MBAR-GCMC estimates (symbols) for $\theta_{\rm rr} \neq \theta_{\rm ref}$ and literature (MBAR-HR) values (lines) for $\theta_{\rm rr} = \theta_{\rm ref}$ with a constant repulsive exponent, i.e., $\lambda_{\rm rr} = \lambda_{\rm ref}$. MBAR-GCMC estimates for the NERD and MiPPE-SL force fields are computed using configurations sampled from TraPPE and MiPPE-gen, respectively. Top-left, top-right, bottom-left, and bottom-right panels correspond to saturated liquid density, saturated vapor density, saturated vapor pressure, and enthalpy of vaporization, respectively.

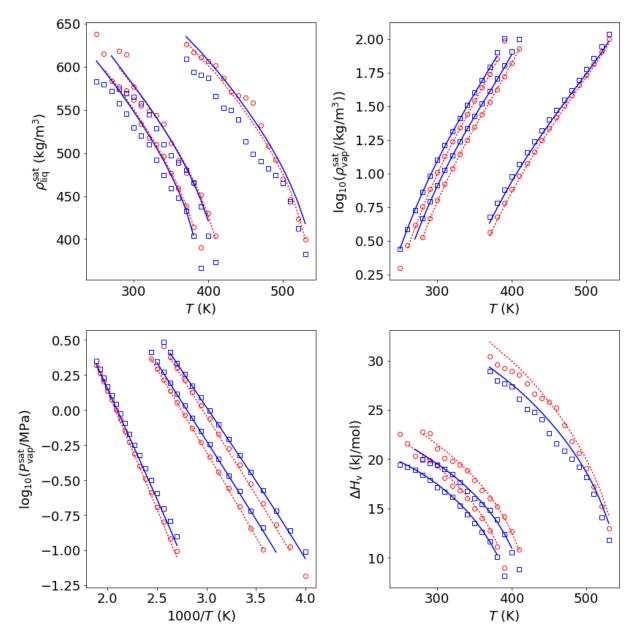


Figure 4: Comparison between MBAR-GCMC estimates (symbols) for $\theta_{\rm rr} \neq \theta_{\rm ref}$ and literature (MBAR-HR) values (lines) for $\theta_{\rm rr} = \theta_{\rm ref}$ with a non-constant repulsive exponent, i.e., $\lambda_{\rm rr} \neq \lambda_{\rm ref}$. MBAR-GCMC estimates for the TraPPE force field are computed using configurations sampled from MiPPE-gen, and vice versa. Top-left, top-right, bottom-left, and bottom-right panels correspond to saturated liquid density, saturated vapor density, saturated vapor pressure, and enthalpy of vaporization, respectively.

1. We validate that MBAR and HR are statistically indistinguishable with sufficient data by re-analyzing the simulation results of Mick et al. and Barhaghi et al. utiliz-

ing MBAR

- 2. Epsilon scaling for all the compounds that Mohammad has U and N values for (branched alkanes and alkynes) and which have good experimental data
- 3. We estimate MiPPE generalized and NERD VLE from TraPPE simulations, MiPPE S/L from MiPPE generalized, and TraPPE from MiPPE generalized
- 4. For $\lambda_{\rm ref}=12$ and $\lambda_{\rm rr}=16$, MBAR-GCMC predicts vapor density, vapor pressure, and heat of vaporization more accurately than liquid density
- 5. For $\lambda_{ref} = 12$ and $\lambda_{rr} = 12$, i.e., computing NERD from TraPPE simulations, MBAR-GCMC predicts all four properties accurately
- 6. We present how basis functions allow for rapid computation of wide range of parameter sets:
 - (a) *n*-hexane
 - (b) 2-methylpropane
 - (c) 2,2-dimethylpropane
 - (d) cyclopentane or cyclohexane
- 7. We provide supporting information with basis functions for several branched alkanes with TraPPE and MiPPE force fields

3.1 Figures

- 1. Percent deviation between MBAR and HR results for rholiq, rhovap, Psat, and DeltaHv
- 2. Comparison between MBAR bootstrapping and analytical uncertainties and HR uncertainties (?)

- 3. Scaling of epsilon post-simulation for branched alkanes and alkynes
- 4. Prediction of VLE for $\lambda_{ref} \neq \lambda_{rr}$
- 5. Prediction of VLE for $\lambda_{ref} = \lambda_{rr}$
- 6. Two-D scans of scoring functions for $\epsilon \sigma$ of CH3 (a) and CH2 (b) for *n*-hexane
- 7. Two-D scans of scoring functions for $\epsilon \sigma$ of CH3 (a) and CH (b) for 2-methylpropane
- 8. Two-D scans of scoring functions for $\epsilon \sigma$ of CH3 (a) and C (b) for 2,2-dimethylpropane
- 9. Two-D scans of scoring functions for $\epsilon-\sigma$ of CH2 for cyclopentane or cyclohexane (reference is TraPPE)

4 Discussion/Limitations/Future work

As ITIC is more reliable at near-triple-point conditions, MBAR-ITIC and MBAR-GCMC can be combined to cover most temperatures that span the vapor-liquid coexistence curve.

- 1. We recommend that future GCMC-VLE studies report the snapshots of N and U and/or basis functions to recompute U as this allows for future force field optimization
- 2. Improvements are possible with multiple θ or simulating a range of μ values

5 Conclusions

6 Acknowledgments

Mostafa and J. Richard Elliott provided valuable insights.

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7 Supporting Information

7.1 MBAR VLE estimates

Provide tables of MBAR estimates

7.2 Basis functions

1. Validation that basis functions give accurate energies

7.3 Raw data

1. Comparison of 2-D histograms for TraPPE and MiPPE. MBAR overlap, possible? Probably not without rerunning the simulations.