

- SOLVED AND SCRAMBLED
1. A transmission line operating at $\omega = 10^8 \text{ rad/s}$ has these parameter values: $R = 0.1 \Omega/\text{m}$, $L = 0.2 \mu\text{H}/\text{m}$, $C = 10 \mu\text{F}/\text{m}$. Find:
 (i) α (ii) β (iii) γ (iv) v (v) Z_0

solution:

Sohit :-

$$R = 0.1 \Omega/\text{m}, L = 0.2 \mu\text{H}/\text{m}, h = 10 \mu\text{mho}/\text{m}$$

$$C = 100 \mu\text{F}/\text{m}, \omega = 10^8 \text{ rad/s}$$

$$\gamma = \sqrt{(R + j\omega L)(h + j\omega C)} \quad \text{[12]}$$

$$= \left\{ (0.1 + j \times 10^8 \times 0.2 \times 10^{-6}) (10 \times 10^{-4} + j \times 10^8 \times 100 \times 10^{-12}) \right\}$$

$$((20 \angle 89.71^\circ) (0.01 \angle 89.94^\circ))^{1/2}$$

$$= 0.447 \angle 89.825^\circ$$

$$\gamma = 1.365 \times 10^{-3} + j 0.4469 \text{ m}^{-1}$$

$$\gamma = \alpha + j\beta$$

$$\alpha = 1.356 \times 10^{-3} \text{ rad/m}, \beta = 0.4469 \text{ rad/m}$$

$$v = \lambda f = \frac{2\pi}{\beta} \times \frac{\omega}{2\pi} = \frac{\omega}{\beta} = \frac{10^8}{0.4469} = \frac{10^8}{0.4469}$$

$$= 2.22 \times 10^8 \text{ m/s}$$

$$Z_0 = \sqrt{\frac{R + j\omega L}{h + j\omega C}} =$$

$$= \left(\frac{20 \angle 89.71^\circ}{0.01 \angle 89.94^\circ} \right) \text{ZL} = 44.72 \angle -0.12^\circ$$

$$= 44.71 - j \times 0.092 \Omega$$

A certain transmission line has a characteristic impedance of $75 + j0.01 \Omega$ and is terminated in a load impedance of $70 + j50 \Omega$. Compute: (a) The reflection coefficient (b) The transmission coefficient.

$\delta \text{V} \text{in } \div$

$$Z_0 = 75 + j0.01 \Omega$$

$$Z_L = 70 + j50 \Omega$$

$$(a) \Gamma = \frac{Z_L - Z_0}{Z_L + Z_0}$$

$$= \frac{70 + j50 - 75 - j0.01 \Omega}{70 + j50 + 75 + j0.01 \Omega}$$

$$= 0.33 \angle 76.7^\circ$$

$$= 0.08 + j0.32$$

$$(b) \tau = \frac{2 \times Z_L}{Z_L + Z_0} = \frac{2 \times (70 + j50)}{70 + j50 + 75 + j0.01}$$

$$= 1.12 \angle 16.5^\circ = 1.08 + j0.32$$

A distortionless line has $Z_0 = 60 \Omega$, $\alpha = 20 \text{ mNp/m}$, $v = 0.6 c$, λ at 100 MHz.

Solution:

SOLN :-

distortionless line

$$Z_0 = 60\Omega, \alpha = 20 \text{ mNp/m}, v = 0.6c, f = 100 \text{ Hz}$$

$$\frac{R}{L} = \frac{\alpha}{C} \quad \text{--- (i)}$$

$$\gamma = \sqrt{R\alpha} + j\omega\sqrt{LC}$$

$$\alpha = \sqrt{R\alpha}, \beta = \omega\sqrt{LC}$$

$$Z_0 = \sqrt{\frac{L}{C}} + j0$$

$$R_0 = \sqrt{\frac{L}{C}}, x_0 = 0$$

$$V = \lambda \times f = \frac{2\pi}{\lambda} \times \frac{\omega}{2\pi} = \frac{\omega}{\beta} = \frac{\omega}{\omega\sqrt{LC}} = \frac{1}{\sqrt{LC}} \quad \text{--- (a)}$$

$$\alpha = \sqrt{R\alpha} = \left(R \times \frac{RC}{L} \right)^{1/2} \quad \text{from (i)}$$

$$= R \sqrt{\frac{C}{L}} = \frac{R}{Z_0}$$

$$* R = 2Z_0 = 20 \times 10^{-3} \times 60 \\ = 1.2 \text{ ohm}$$

$$\omega = \sqrt{R\mu}$$

$$* h = \frac{\omega^2}{R} = \frac{(20 \times 10^{-3})^2}{1.2} = 333 \times 10^{-6} \text{ m} \\ = 333 \times 10^{-6} \text{ m}$$

$$Z_0 = \sqrt{\frac{L}{C}} \quad , \quad V = \frac{1}{\sqrt{LC}}$$

$$* \frac{Z_0}{V} = \sqrt{\frac{L^2 C}{C}}$$

$$* \frac{Z_0}{V} = L$$

$$* \frac{C_0}{0.6} = L$$

$$* \therefore L = \frac{60}{0.6 \times 3 \times 10^8} = 333 \text{ nH/m}$$

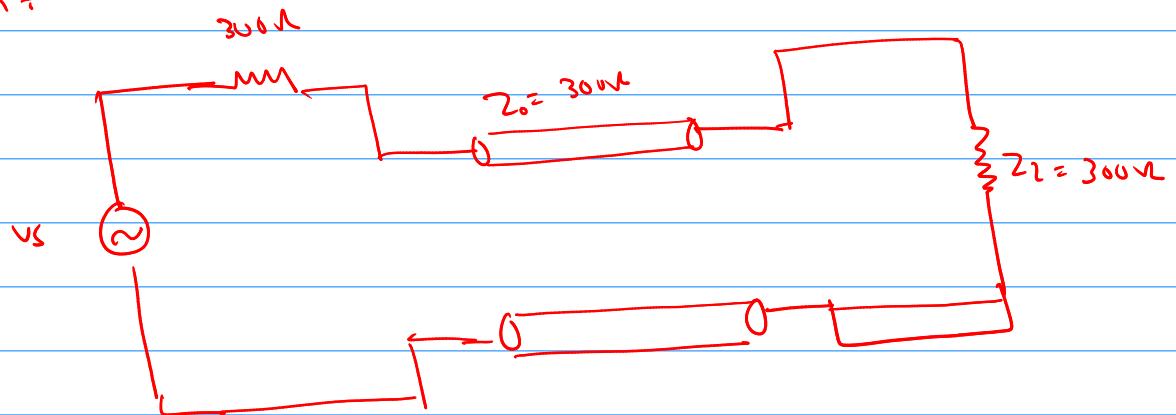
$$* \frac{R}{L} = \frac{h}{C}$$

$$* C = \frac{h \times L}{R} = \frac{333 \times 10^{-1} \times 333 \times 10^{-9}}{12} \\ = 92.40 \text{ pF/m}$$

$$\Rightarrow \lambda = \frac{V}{f} = \frac{0.6 \times 3 \times 10^8}{100 \times 10^6} = 1.8 \text{ m}$$

Numerical example-4 :-
 Assume a two wire 300Ω lossless line ($Z_0 = 300\Omega$) such as the lead in wire from the antenna to the TV. Suppose the length of the line is 2m. & the value of $L \perp C$ is such that the velocity on the line is $2.5 \times 10^8 \text{ m/s}$. The line is terminated at with a receiver having the input resistance of 300Ω . The antenna is represented by the thevenin's equivalent $Z = 300\Omega$ in series with the voltage source (V_s) = 60V at 100MHz. Determine the load voltage, load current & power delivered to the load by the line.

SOL:



$$T = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{300 - 300}{300 + 300} = 0$$

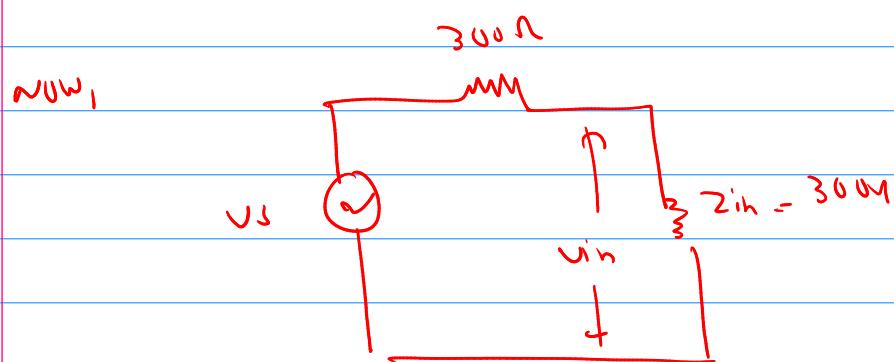
$$V_s = 60 \cos(2\pi \times 10^8 t) \text{ V}$$

$$\beta f = \frac{2\pi}{\lambda} \times 2\pi = \frac{4\pi f}{V} = \frac{4\pi \times 10^9}{2.5 \times 10^3} = 1.6\pi$$

$$Z_{in} = Z_0 \cdot \left[\frac{Z_L + jZ_0 \tan \phi}{Z_0 + jZ_L \tan \phi} \right]$$

$$= 300 \left[\frac{300 + j \times 300 \times \tan 1.6\pi^c}{300 + j \times 300 \times \tan 1.6\pi^c} \right]$$

$$= 300 \Omega$$



$$V_{in} = V_S \times \frac{Z_{in}}{Z_{in} + 300} = V_S \times \frac{300}{300 + 300}$$

$$\begin{aligned} V_{in} &= 60 \cos(2\pi \times 10^8 t) \times \frac{1}{2} \\ &= 30 \cos(2\pi \times 10^8 t) \text{ V} \end{aligned}$$

$$T = 0$$

$$\begin{aligned} V_L &= 30 \cos(2\pi \times 10^8 t - \beta \ell) \\ &= 30 \cos(2\pi \times 10^8 t - 1.6\pi^c) \end{aligned}$$

$$\begin{aligned} \text{Input current } (I_{in}) &= \frac{V_{in}}{Z_{in}} = \frac{30 \cos(2\pi \times 10^8 t)}{300} \\ &= 0.1 \cos(2\pi \times 10^8 t) \end{aligned}$$

$$I_L = \frac{V_L}{Z_L} = \frac{30 \text{ V}_\text{os}}{300} (2\pi \times 10^8 t - 1.6\pi) \text{ A}$$

$$= 0.1 \cos (2\pi \times 10^8 t - 1.6\pi) \text{ A}$$

$P_{in} = P_2 = V_{in} (\text{rms}) \times I_{in} (\text{rms})$

(losses)

$$\approx \frac{30}{\sqrt{2}} \times \frac{0.1}{\sqrt{2}} = 1.5 \text{ W}$$

3. A standard air filled rectangular waveguide with dimension $a = 8.636$, $b = 4.318$ cm is fed by a 4 GHz from a coaxial cable. Determine whether a TE_{10} mode will be propagated. If so, calculate the phase velocity and the group velocity.

Solution:

so let's

$$(at off frequency), f_c = \frac{c}{2} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2}$$

$\text{TE}_{10} \quad (m=1, n=0)$

For TE_{10} , we have $m=1, n=0$

since the waveguide is air filled, $v = c = 3 \times 10^8 \text{ m/s}$

$$f_c = \frac{3 \times 10^8}{2} \sqrt{\left(\frac{1}{8.636 \times 10^{-2}}\right)^2 + \left(\frac{0}{4.318 \times 10^{-2}}\right)^2}$$

$$\Rightarrow f_c = 1.737 \times 10^9 \text{ Hz} = 1.737 \text{ GHz}$$

As 4 GHz is greater than f_c , the TE_{10} will propagate.

Phase velocity, $v_p = \frac{c}{\sqrt{1 - \left(\frac{f_c}{f}\right)^2}}$

$$= \frac{3 \times 10^8}{\sqrt{1 - \left(\frac{1.737}{4}\right)^2}} \rightarrow \text{both in Hz}$$

$$= 3.33 \times 10^8 \text{ m/s}$$

$$\text{Group velocity, } v_g = \frac{v_p^2}{v_p} = \frac{(3 \times 10^8)^2}{3.33 \times 10^8} = 2.7 \times 10^8 \text{ m/s}$$

4. A 6 GHz signal is to be propagated in TE_{10} mode in rectangular waveguide. If its group velocity is 90 percent of free space velocity, what must be the breadth of the waveguide.

Given:

$$v_g = 0.9 c$$

$$v_g = \frac{c}{n}$$

$$\text{or} \quad 0.9c = \frac{\sqrt{f}}{\sqrt{1 - \left(\frac{fc}{f}\right)^2}}$$

$$\text{or} \quad 0.9c = \sqrt{1 - \left(\frac{fc}{f}\right)^2}$$

But when $f = c$

$$\text{or} \quad 0.9 = \sqrt{1 - \frac{fc^2}{g^2}}$$

$$\text{or} \quad 0.81 = 1 - \frac{fc^2}{g^2}$$

$$\therefore \frac{fc^2}{g^2} = 0.19 \quad \text{--- (i)}$$

$$\text{Also, } fc = \frac{v}{2} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{h}{b}\right)^2}$$

$$\text{For TE}_{10} \quad m=1, n=0$$

$$\text{or} \quad fc = \frac{c}{2} \sqrt{\left(\frac{1}{a}\right)^2}$$

$$\therefore fc = \frac{c}{2a} \quad \text{--- (ii)}$$

Q1

$$\frac{\left(\frac{C}{2a}\right)^2}{(\beta)^2} = 0.19$$

Q2

$$\frac{\left(\frac{3 \times 10^8}{2}\right)^2 \times \frac{1}{a^2}}{(6 \times 10^9)^2} = 0.19$$

Q3

$$a^2 = \frac{\left(\frac{3 \times 10^8}{2}\right)^2}{(6 \times 10^9)^2 \times 0.19} \quad \therefore a = 0.05735 \text{ m}$$

5. Consider a rectangular waveguide with $\epsilon_r = 2$, $\mu = \mu_0$ with dimensions $a = 1.07 \text{ cm}$, $b = 0.43 \text{ cm}$. Find the cutoff frequency for TM₁₁ mode and the dominant mode.

[2074 Chaitra]

Sohit

$$f_c = \frac{v}{2} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2}$$

$$\text{where, } v = \frac{1}{\sqrt{\mu \epsilon}} = \frac{1}{\sqrt{\mu_0 \epsilon_0 \epsilon_r}} = \frac{1}{\sqrt{2 \mu_0 \epsilon_0}} = 2.1213 \times 10^8 \text{ m/s}$$

For TM₁₁, $m=1$, $n=1$

$$f_c = \frac{2.1213 \times 10^8}{2} \sqrt{\left(\frac{1}{1.07 \times 10^{-2}}\right)^2 + \left(\frac{1}{0.43 \times 10^{-2}}\right)^2}$$

$$\therefore f_c = 26.58 \text{ GHz}$$

For rectangular waveguide, the dominant mode is TE_{10}
 $m=1, n=0$

$$f_c = \frac{v}{2} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2}$$

$$= \frac{2.1213 \times 10^8}{2} \sqrt{\left(\frac{1}{1.07 \times 10^{-2}}\right)^2 + 0} = 9.9126 \text{ GHz}$$

An air-filled rectangular waveguide of inside dimensions $7 \times 3.5 \text{ cm}$ operates in the dominant TE_{10} mode. (a) Find the cutoff frequency (b) Determine the phase velocity of the wave in the guide at a frequency of 3.5 GHz . (c) Determine the guide wavelength at the same frequency.

Soln :-

$$\textcircled{a} \quad f_c = \frac{v}{2} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2} \quad \text{For } \text{TE}_{10} \quad m=1, n=0$$

Air filled

$$f_c = \frac{c}{2} \sqrt{\left(\frac{1}{a}\right)^2 + 0} = \frac{c}{2a} = \frac{3 \times 10^8}{2 \times 7 \times 3.5 \times 10^{-2}} = 2.1428 \text{ GHz}$$

$$\textcircled{b} \quad V_p = \frac{V}{\sqrt{1 - \left(\frac{4c}{f}\right)^2}} = \frac{c}{\sqrt{1 - \left(\frac{4c}{f}\right)^2}}$$

$$= \frac{3 \times 10^8}{\sqrt{1 - \left(\frac{2.1428 \times 10^9}{3.5 \times 10^9}\right)^2}} = 3.794 \times 10^8 \text{ m/s}$$

$$\textcircled{c} \quad \lambda_{\text{guide}} = \frac{\lambda}{\sqrt{1 - \left(\frac{4c}{f}\right)^2}} = \frac{c/f}{\sqrt{1 - \left(\frac{4c}{f}\right)^2}}$$

$$= \frac{(3 \times 10^8) (3.5 \times 10^9)}{\left(1 - \left(\frac{2.1428 \times 10^9}{3.5 \times 10^9}\right)^2\right)^{1/2}} = 10.84 \text{ cm}$$

7. Standard air-filled waveguides have been designed for the radar bands. One type, designated WG-16, is suitable for X-band applications. Its dimensions are: $a = 2.29 \text{ cm}$ and $b = 1.02 \text{ cm}$. If it is desired that a WG-16 waveguide operate only in the dominant TE_{10} mode and that the operating frequency be at least 25% above the cutoff frequency of the TE_{10} mode but no higher than 95% of the next higher cutoff frequency, what is the allowable operating-frequency range?
-

Soln :-

For $a = 2.29 \times 10^{-2} \text{ m}$, $b = 1.02 \times 10^{-2} \text{ m}$, the two modes having the lowest cut off frequencies are TE_{10} and TE_{20} .

$$f_c = \frac{\nu}{2} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2}$$

For air filled $\nu = c$, corresponding to TE_{10} and TE_{20} modes, we calculate

$$f_{c10} = \frac{c}{2a} = \frac{3 \times 10^8}{2 \times 2.29 \times 10^{-2}} = 6.55 \times 10^9 \text{ Hz}$$

$$f_{c20} = \frac{c}{a} = \frac{3 \times 10^8}{2.29 \times 10^{-2}} = 13.10 \times 10^9 \text{ Hz}$$

Thus, the allowable operating frequency range under the specified conditions is :-

$$1.25 f_{c10} \leq f \leq 0.95 f_{c20}$$

$$\text{or, } 8.19 \times 10^9 \text{ Hz} \leq f \leq 12.45 \times 10^9 \text{ Hz}$$

An air line characteristic impedance of 70Ω and phase constant of 3 rad/m at 100 MHz . Calculate the inductance per meter and the capacitance per meter of the line.

Solution:

$$80 \Omega \text{ h}^{-\frac{1}{2}}$$

Air line can be regarded as lossless line

$$R = G = h$$

$$Y = \sqrt{(R + j\omega L)(G + j\omega C)}$$

$$\text{For } R = G = \delta$$

$$V = j\omega \sqrt{LC}$$

$$\omega \text{ rad} \quad \omega + j\beta = j\omega \sqrt{LC}$$

$$Q = 0, \quad \beta = \omega \sqrt{LC} \quad \text{--- (i)}$$

$$Z_0 \text{ (characteristic impedance)} = \sqrt{\frac{R + j\omega L}{G + j\omega C}}$$

$$Z_0 = \sqrt{\frac{L}{C}}$$

$$\text{or} \quad R_0 + jX_0 = \sqrt{\frac{L}{C}} + j0$$

$$\therefore Z_0 = R_0 = \sqrt{\frac{L}{C}}, \quad X_0 = 0 \quad \text{--- (ii)}$$

Dividing (i) by (ii)

$$\frac{\beta}{R_0} = \frac{\omega \sqrt{LC}}{\sqrt{\frac{L}{C}}} = \omega C$$

or $C = \frac{\beta}{\omega R_0} = \frac{\beta}{\omega Z_0} = \frac{3}{2\pi \times 100 \times 10^6 \times 70} = 68.2 \mu F/m$

From part (i)

$$R_0 = \sqrt{\frac{L}{C}}$$

or $L = R_0^2 C = Z_0^2 C = (70)^2 \times (68.2 \times 10^{-12})$
 $= 334.4 \text{ nH/m}$

$\therefore C = 68.2 \mu F/m, L = 334.4 \text{ nH/m}$

11. A telephone line has $R = 30 \Omega/\text{km}$, $L = 100 \text{ mH/km}$, $G = 0$, and $C = 20 \mu\text{F/km}$. At $f = 1 \text{ kHz}$, obtain: (a) the characteristic impedance of the line (b) the propagation constant (c) the phase velocity.

Solution:

Given:

$$R = 30 \Omega/\text{km} = 30 \times 10^{-3} \text{ V/m}$$

$$L = 100 \text{ mH/km} = 100 \times 10^{-6} \text{ H/m}$$

$$G = 0, C = 20 \times 10^{-6} \times 10^{-3} \text{ F/m} = 20 \times 10^{-9} \text{ F/m}$$

$$f = 1 \text{ kHz}$$

$$\omega = 2\pi f = 2\pi \times 10^3 = 6283.1853 \text{ rad/s}$$

$$\begin{aligned}
 @) \quad Z_0 &= \sqrt{\frac{R+j\omega L}{G+j\omega C}} \\
 &= \left(\frac{30 \times 10^3 + j 6283 \cdot 1853 \times 100 \times 10^{-9}}{0 + j 6283 \cdot 1853 \times 20 \times 10^{-9}} \right)^{1/2} \\
 &= \left(\frac{0.629 \angle 87.266^\circ}{1.2566 \times 10^{-4} \angle 90^\circ} \right)^{1/2} \\
 &\approx \sqrt{5005.5705} \angle -2.734^\circ \\
 &\approx \sqrt{5005.5705} \angle \frac{-2.734}{2} \\
 &\approx 70.75 \angle -1.367^\circ \approx
 \end{aligned}$$

$$\begin{aligned}
 b) \quad Y &= \sqrt{(R+j\omega L)(G+j\omega C)} \\
 &= \sqrt{(0.629 \angle 87.266^\circ)(1.2566 \times 10^{-4} \angle 90^\circ)} \\
 &= \sqrt{7.9040 \times 10^{-5} \angle 177.266^\circ} \\
 &\approx \sqrt{7.9040 \times 10^{-5}} \angle \frac{177.266^\circ}{2} \\
 &\approx 8.890 \times 10^{-3} \angle 88.633^\circ
 \end{aligned}$$

$$c) \quad V = \frac{\omega}{\rho}$$

$$\omega = 6283.1853 \text{ rad/s}$$

$$Y = (2.1208 \times 10^{-4} + j 8.8874 \times 10^{-3}) \text{ m}^{-1}$$

$$f = 8.8874 \times 10^{-3} \text{ rad/m}$$

$$V = \frac{6283.1853}{8.8874 \times 10^{-3}} = 7.069 \times 10^5 \text{ m/s}$$

12. A transmission line operating at 500 MHz has $Z_0 = 80 \Omega$, $\alpha = 0.04 \text{ Np/m}$, $\beta = 1.5 \text{ rad/m}$. Find the line parameters R , L , G , and C .

solve:

$$Z_0 = 80\Omega, \alpha = 0.04 \text{ Np/m}, \beta = 1.5 \text{ rad/m}$$

$$f = 500 \text{ MHz}$$

$$Y = \alpha + j\beta = \sqrt{(R+j\omega L)(G+j\omega C)}$$

$$\text{or } Y^2 = (R+j\omega L)(G+j\omega C) \quad \text{---(i)}$$

$$Z_0 = \sqrt{\frac{R+j\omega L}{G+j\omega C}}$$

$$\text{or } Z_0^2 = \frac{R+j\omega L}{G+j\omega C} \quad \text{---(ii)}$$

From (i) and (ii)

$$Y^2 = Z_0^2 (h+j\omega c) (h+j\omega c)$$

$$\text{or } \frac{Y^2}{Z_0^2} = (h+j\omega c)^2$$

$$\text{or } \frac{1}{Z_0^2} [(Z^2 - \beta^2)] = (h+j\omega c)^2$$

$$\text{or } \frac{1}{Z_0^2} [(Z^2 - \beta^2) + j2Z\beta] = [(h^2 - \omega^2 c^2) + j(2hc\omega)]$$

Evaluating real and imaginary parts

$$\frac{1}{Z_0^2} (Z^2 - \beta^2) = h^2 - \omega^2 c^2$$

$$\text{or } \frac{1}{(80)^2} (0.04^2 - 1.5^2) = h^2 - (2\pi \times 500 \times 10^6)^2 c^2$$

$$\text{or } h^2 - 9.8695 \times 10^{18} c^2 = -3.5131 \times 10^{-4} \quad \text{--- (iii)}$$

$$\frac{1}{Z_0^2} (2Z\beta) = 2hc\omega$$

$$\text{or } hc = 2.9840 \times 10^{-15} \quad \text{--- (iv)}$$

From eqn (iii) & (iv)

$$\left(\frac{2.9840 \times 10^{-15}}{c} \right)^2 - 9.8695 \times 10^{18} c^2 = -3.5131 \times 10^{-4}$$

$$0V \quad 8.9042 \times 10^{-30} - 9.8695 \times 10^{18} C^4 + 3.5131 \times 10^{-4} C^2 = 0$$

$$0V \quad 9.8695 \times 10^{18} C^4 - 3.5131 \times 10^{-4} C^2 - 8.9042 \times 10^{-30} = 0$$

which is in form of $ax^2 + bx + c = 0$

$$C^2 = 3.5620 \times 10^{-23} \Rightarrow C = 5.9682 \times 10^{-12} \text{ F/m}$$
$$= 5.9682 \text{ pF/m}$$

From (iv)

$$R = \frac{2.9840 \times 10^{-15}}{C} = \frac{2.9840 \times 10^{-15}}{5.9682 \times 10^{-12}} = 5 \times 10^{-4} \text{ S/m}$$

using part (i)

$$Z_0^2 (R + j\omega C) = (R + j\omega L)$$

$$0V \quad R = Z_0^2 C = (80)^2 \times (5 \times 10^{-4}) = 3.2 \text{ Ohm}$$

$$L = Z_0^2 C = 80^2 \times (5.9682 \times 10^{-12})$$
$$= 3.196 \times 10^{-8} \text{ H/m}$$
$$= 38.196 \text{ nH/m}$$

Hence, $R = 3.2 \text{ Ohm}$, $L = 38.196 \text{ nH/m}$,

$$C = 5 \times 10^{-4} \text{ S/m}, \quad R = 5.9682 \text{ pF/m}$$

16. A lossless transmission line with $Z_0 = 60 \Omega$ is 400 m long. It is terminated with load $Z_L = 40 + j80 \Omega$ and is operated with frequency of 1 MHz. Let $v=0.8c$. Find:
- The reflection coefficient (Γ)
 - The standing wave ratio (s or SWR)
 - Input Impedance (Z_{in})

Solution:

[2063 Kartik]

So h:

$$\textcircled{1} \quad \Gamma = \frac{Z_L - Z_0}{Z_L + Z_0}$$

$$= \frac{(40 + j80) - (60 + j0)}{(40 + j80) + (60 + j0)} = 0.6439 < 65.4^\circ$$

$$\textcircled{2} \quad \text{SWR} = \frac{1 + |\Gamma|}{1 - |\Gamma|} = \frac{1 + 0.6439}{1 - 0.6439} = 4.62$$

$$\textcircled{3} \quad Z_{in} = Z_0 \left[\frac{Z_L + jZ_0 \tan \beta l}{Z_0 + jZ_L \tan \beta l} \right]$$

$$\beta l = \frac{2\pi}{\lambda} l = \frac{2\pi f l}{v} = \frac{2\pi \times 10^6 \times 400}{0.8 \times 3 \times 10^8} = \frac{10\pi^2}{3}$$

$$Z_{in} = 60 \angle 0^\circ \left[\frac{40 + j80 + j60 \angle 0^\circ \tan \frac{10\pi^2}{3}}{60 \angle 0^\circ + j(40 + j80) \tan \frac{10\pi^2}{3}} \right]$$

$$= 108 \angle -60.9^\circ \Omega$$

$$[104.7876 \angle 138.598^\circ] = 108 \angle -60.9^\circ \Omega$$

17: A certain transmission line 2 m long operating at $\omega = 10^6$ rad/s has $\alpha = 8 \text{ dB/m}$, $\beta = 1 \text{ rad/m}$, and $Z_0 = 60 + j40 \Omega$. If the line is connected to a source of $10 \angle 0^\circ \text{ V}$, $Z_g = 40 \Omega$ and terminated by a load of $20 + j50 \Omega$, determine the input impedance.

SOLN :-

$$\textcircled{a} \quad Q = \gamma d \beta \text{Im} = \frac{8}{8 \cdot 686} N \text{pIm} = 0.921 N \text{pIm}$$

$$\begin{aligned} \beta &= 1 \text{ rad Im}, \quad r = Q + j\beta \\ &= 0.921 + j \times 1 \text{ m}^{-1} \end{aligned}$$

$$V_L = 2(0.921 + j) = 1.842 + j2$$

$$\tanh rL = \tanh h(1.842 + j2)$$

$$= \frac{\sinh(2 \times 1.842)}{\cosh 2 \times 1.842 + (\alpha 2 \times 2)} + j \frac{\sinh 2 \times 2}{\cosh 2 \times 1.842 + \cos 2 \times 2}$$

$$\sinh 3.68 = \frac{e^{3.68} - e^{-3.68}}{2} = 19.8105$$

$$\cosh 3.68 = \frac{e^{3.68} + e^{-3.68}}{2} = 19.8858$$

$$\begin{aligned} \tanh rL &= \frac{19.8105}{19.8858 + \cos 4} + j \frac{\sin 4}{19.8858 + \cos 4} \\ &= 1.0327 - j 0.0394 \end{aligned}$$

$$Z_{in} = Z_0 \left[\frac{Z_L + Z_0 \tanh \gamma L}{Z_0 + Z_L \tanh \gamma L} \right]$$

$$= (60 + j40) \left[\frac{(20 + 50j) + (60 + j40)(1.0327 - j0.0329)}{(60 + 40j) + (20 + j50)(1.0327 - j0.0329)} \right]$$

$$= 71.7817 \angle 0.573^\circ$$

$$\therefore Z_{in} = 60.322 + j38.9706 \Omega \quad \#$$

19. Calculate the cut-off frequencies of the first four propagating modes for an air-filled copper wave guide with dimension $a = 2.5 \text{ cm}$, $b = 1.2 \text{ cm}$. [2073 Shrawan]

Solution:

Soln:

$$f_{c \min} = \frac{\pi}{2} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2}$$

air filled

$$f_{c \min} = \frac{c}{2} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2}$$

Dominant mode of rectangular wave is TE₁₀

$$f_{c10} = \frac{c}{2a} = \frac{3 \times 10^8}{2 \times 2.5 \times 10^{-2}} = 6 \times 10^9 \text{ Hz} \approx 6 \text{ GHz}$$

Now,

$$f_{c01} = \frac{c}{2} \sqrt{\left(\frac{0}{a}\right)^2 + \left(\frac{1}{1.2 \times 10^{-2}}\right)^2}$$
$$= 12.5 \text{ GHz} > 6 \text{ GHz}$$

TE₀₁ mode will propagate

$$f_{c11} = \frac{c}{2} \sqrt{\left(\frac{1}{a}\right)^2 + \left(\frac{1}{b}\right)^2} = 13.865 \text{ GHz} > 6 \text{ GHz}$$

TE₁₁ will propagate

$$f_{c21} = \frac{c}{2} \sqrt{\left(\frac{2}{a}\right)^2 + \left(\frac{1}{b}\right)^2} = 17.327 \text{ GHz} > 6 \text{ GHz}$$

So, TE₂₁ mode will propagate

$$f_{c20} = \frac{c}{2} \sqrt{\left(\frac{2}{a}\right)^2 + \left(\frac{0}{b}\right)^2} = 12 \text{ GHz} > 6 \text{ GHz}$$

So, TE₂₀ mode will propagate.

Hence, the cut-off frequencies of the first four propagating modes are 12 GHz, 12.5 GHz, 13.865 GHz, 17.327 GHz.

22. If a transmission line having characteristics impedance $Z_0 = 200 \Omega$ is operating at frequency 15 MHz with propagation constant $\gamma = j0.5 \text{ m}^{-1}$, then determine
- Velocity of propagation
 - Wavelength
 - Inductance
 - Capacitance

Solution:

[2068 Shrawan]

$$\text{Velocity } (v) = f\lambda = f \times \frac{2\pi}{\beta} = \frac{15 \times 10^6 \times 2\pi}{0.5} = 1.8849 \times 10^8 \text{ m/s}$$

We have, $\gamma = \alpha + j\beta = j0.5 \text{ m}^{-1}$

$\alpha = 0$ So, it is a lossless transmission line.

$$\beta = 0.5 \text{ m}^{-1}$$

$$\gamma = \sqrt{(R + j\omega L)(G + j\omega C)}$$

As $\alpha = 0$, we have $R = 0, G = 0$.

$$\text{So, } \beta = \omega \sqrt{LC}$$

$$\text{or, } \omega \sqrt{LC} = 0.5$$

$$\text{or, } \sqrt{LC} = \frac{0.5}{\omega} = \frac{0.5}{2\pi f}$$

$$LC = \left(\frac{0.5}{2\pi f}\right)^2 \quad \text{(i)}$$

Characteristics impedance is given as

$$Z_0 = \sqrt{\frac{R + j\omega L}{G + j\omega C}} = \sqrt{\frac{0 + j\omega L}{0 + j\omega C}} = \sqrt{\frac{L}{C}}$$

$$\frac{L}{C} = Z_0^2 = (200)^2$$

$$\therefore L = (200)^2 C \quad \text{(ii)}$$

From equations (i) and (ii),

$$(200)^2 C^2 = \left(\frac{0.5}{2\pi f}\right)^2$$

$$\therefore C = \frac{0.5}{2\pi f} \times \frac{1}{200}$$

$$= \frac{0.5}{2\pi \times 15 \times 10^6 \times 200} = 2.653 \times 10^{-11} = 26.533 \text{ pF}$$

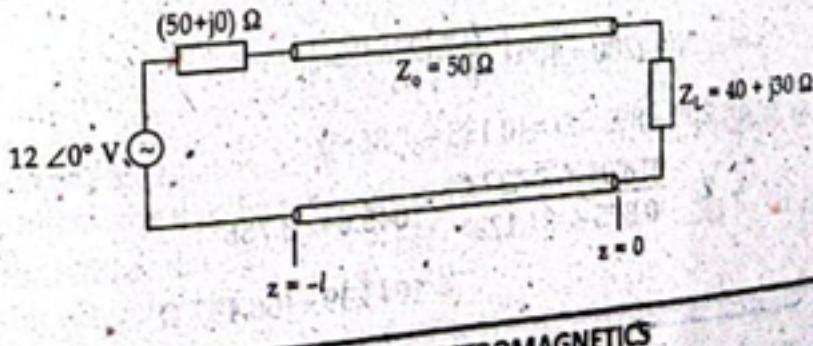
From equation (ii),

$$L = (200)^2 \times (2.653 \times 10^{-11}) = 1.0612 \times 10^{-6} \text{ H} = 1.0612 \text{ mH}$$

$$\text{Wavelength } (\lambda) = \frac{2\pi}{\beta} = 12.56 \text{ m}$$

24. A 50Ω lossless line has a length of 0.4λ . The operating frequency is 300 MHz. A load $Z_L = 40 + j30 \Omega$ is connected at $z = 0$, and the Thevenin equivalent source at $z = -l$ is $12\angle0^\circ$ in series with $Z_{Th} = 50 + j0 \Omega$. Find: (a) The reflection coefficient (Γ) (b) The voltage standing wave ratio (VSWR) [2072 Kartik] (c) The input impedance (Z_{in}).

Solution:



$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{(40 + j30) - 50}{(40 + j30) + 50} = 0.333\angle90^\circ$$

$$\text{VSWR} = \frac{1 + |\Gamma|}{1 - |\Gamma|} = \frac{1 + 0.333}{1 - 0.333} = 1.998$$

For lossless line,

$$Z_{in} = Z_0 \frac{(Z_L + jZ_0 \tan \beta l)}{(Z_0 + jZ_L \tan \beta l)}$$

$$\beta l = \frac{2\pi}{\lambda} \times 0.4\lambda = 2.513^\circ$$

$$\therefore Z_{in} = 26.1428\angle13.048^\circ \Omega$$

25. A lossless line having

25. A lossless line having an air dielectric has a characteristics impedance of 400Ω . The line is operating at 200 MHz and $Z_{in} = 200 - j200 \Omega$. Find: (a) SWR (b) Z_L if the line is 1 m long. (c) the distance from the load to the nearest voltage maximum.

[2074 Ashwin]

Solution:

We have,

$$Z_{in} = Z_0 \left(\frac{Z_L + jZ_0 \tan\beta l}{Z_0 + jZ_L \tan\beta l} \right) \quad \text{(i)}$$

$$Z_0 = 400 \Omega, Z_{in} = 200 - j200 \Omega$$

$$\text{Let, } v = c = 3 \times 10^8 \text{ m/s}$$

$$\beta = \frac{2\pi}{\lambda} = \frac{2\pi f}{v} = \frac{2\pi \times 200 \times 10^6}{3 \times 10^8} = \frac{4\pi}{3} \text{ rad/m}$$

$$\beta l = \frac{4\pi}{3} \times 1 = \left(\frac{4\pi}{3}\right)^c$$

So, from equation (i),

$$200 - j200 = 400 \left[\frac{Z_L + j400 \tan\left(\frac{4\pi}{3}\right)^c}{400 + jZ_L \tan\left(\frac{4\pi}{3}\right)^c} \right]$$

$$\text{or, } 200 - j200 = 400 \left(\frac{Z_L + j1692.82}{400 + jZ_L \cdot 1.73} \right)$$

$$\text{or, } 200 - 892.82j = (0.135 - j0.865)Z_L$$

$$\therefore Z_L = \frac{914.94 \angle -77.373^\circ}{0.875 \angle -81.129^\circ} = 1045.64 \angle 3.756^\circ$$

$$= 1043.39 + j68.497 \Omega$$

$$\text{Using, } \text{SWR} = \frac{1 + |\Gamma|}{1 - |\Gamma|}$$

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0}$$

$$= \frac{1043.39 + j68.497 - 400}{1043.39 + j68.497 + 400} = \frac{647.025 \angle 6.076^\circ}{1445.014 \angle 2.716^\circ} = 0.447 \angle 3.36^\circ$$

$$\text{So, } \text{SWR} = \frac{1 + 0.447}{1 - 0.447} = 2.616$$

For finding the distance to the nearest voltage maximum,
 $z_{max} = -\frac{1}{2\beta} (\phi + 2n\pi); n = 0, \pm 1, \pm 2,$

Taking $n = 0$,

$$z_{max} = -\frac{\phi}{2\beta}$$

$$\text{As } \Gamma = 0.447 \angle 3.36^\circ = |\Gamma| \angle \phi, \phi = 3.36^\circ$$

$$\text{So, } z_{max} = \frac{-3.36^\circ}{2 \left(\frac{4\pi}{3}\right)^c} = \frac{-3.36^\circ}{\left(2 \times \frac{4\pi}{3} \times \frac{180}{\pi}\right)} = -7 \times 10^{-3} \text{ m}$$

26. An air-filled rectangular waveguide has dimensions $a = 2$ cm, $b = 1$ cm. Determine the range of frequencies over which the guide will operate single mode (TE_{10}). [2016 Ashwin]

Solution:

$$f_{cmn} = \frac{v}{2} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2}$$

$$f_{c10} = \frac{v}{2} \times \frac{1}{a}$$

As waveguide is air filled, $v = c = 3 \times 10^8$ m/s

$$\therefore f_{c10} = \frac{3 \times 10^8}{2} \times \frac{1}{2 \times 10^{-2}} = 7.5 \times 10^9 \text{ Hz} = 7.5 \text{ GHz}$$

The next higher mode will be either TE_{20} or TE_{01} , as

$$f_{c20} = \frac{v}{2} \times \frac{2}{a} = \frac{3 \times 10^8}{2} \times \frac{2}{2 \times 10^{-2}} = 15 \times 10^9 \text{ Hz} = 15 \text{ GHz}$$

$$f_{c01} = \frac{v}{2} \times \frac{1}{b} = \frac{3 \times 10^8}{2} \times \frac{1}{1 \times 10^{-2}} = 15 \times 10^9 \text{ Hz} = 15 \text{ GHz}$$

Note: Students are advised to find out f_c for other modes too to confirm the next higher mode will be TE_{20} or TE_{01} .
Therefore, the operating range over which the guide will be single mode is $7.5 \text{ GHz} < f < 15 \text{ GHz}$

ELECTROMAGNETICS

