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Investigation of the Hydraulic Flip Phenomenon for Diesel Fuel Cavitation in a Planar Injection Nozzle

Thomas Frank (*), Tim Wittmann, Daniel Langmeyer

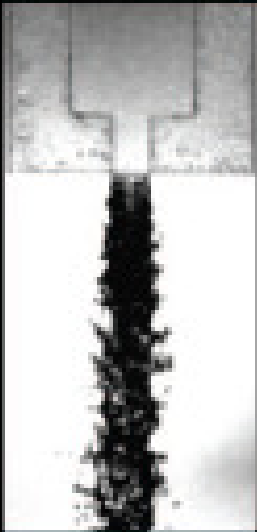
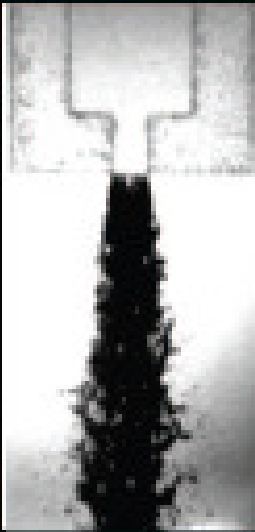

(*) ANSYS Fluid Solver Validation Manager

MFBU, ANSYS Germany, Otterfing









Outline

- The Injector Experiment
- Objectives of the CFD Investigation
- Geometry, Mesh and CFD Setup
- Preliminary Investigations, Observations, Hysteresis Effects
- Target Flow Characteristics and the Hydraulic Flip
- Results with **ANSYS CFX 16.0** and **ANSYS Fluent 16.0**
- Solver Comparison & Conclusions

Turbulent flow		Hydraulic flip
0.13	0.19	0.40
5.2	9.2	14.4
		
4.6217	1.4765	0.6027

Motivation

- Injector systems in ICE (internal combustion engines)
- Usual fuel spray flow pattern is a symmetric conical jet/spray
- Under certain circumstances the fuel injection leads to the so-called “hydraulic flip”, i.a. flow attachment to one side of the injector wall or combustion chamber
 - non-symmetric fuel jet/spray
 - adverse effects on mixture formation and ICE engine performance

	Turbulent flow		Beginning point of cavitation	Growth of cavitation		Hydraulic flip
Injection pressure(P_{inj} , MPa)	0.13	0.19	0.20	0.21	0.35	0.40
Flow rate (Q, L/min)	5.2	9.2	9.7	10.0	14.6	14.4
Internal and External images						
Cavitation number(K)	4.6217	1.4765	1.3282	1.2497	0.5863	0.6027

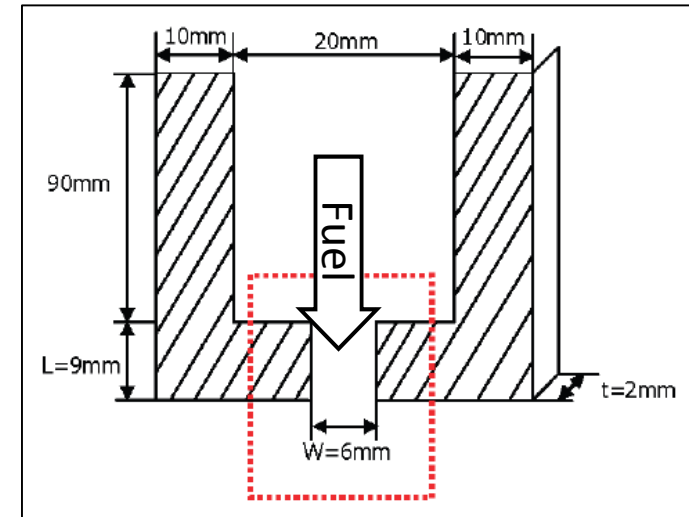
The Injector Experiment

S.H. Park, H.K. Suh, Ch.S. Lee: “Effect of Cavitating Flow on the Flow and Fuel Atomization Characteristics of Biodiesel and Diesel Fuels”, *Energy & Fuels*, **2008**, Vol. 22, pp. 605-613

Fuel injection pressure: 130 - 450 kPa
 Ambient pressure: 100 kPa
 Ambient temperature: 293 K

4 different flow patterns in dependence on inlet pressure:

- Turbulent flow
- Beginning point of cavitation
- Growth of cavitation
- Hydraulic flip



	Turbulent flow		Beginning point of cavitation	Growth of cavitation		Hydraulic flip
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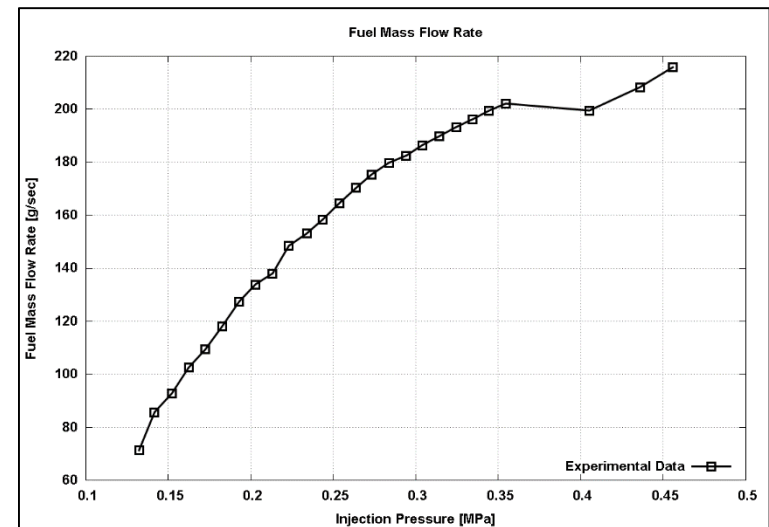
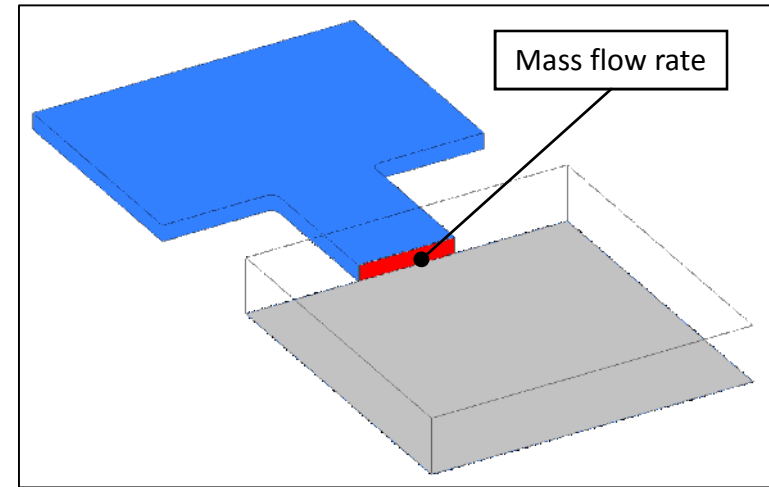
Objectives of the CFD Investigation

Experimental information:

- Injector mass flow rate
- Flow patterns from flow visualization

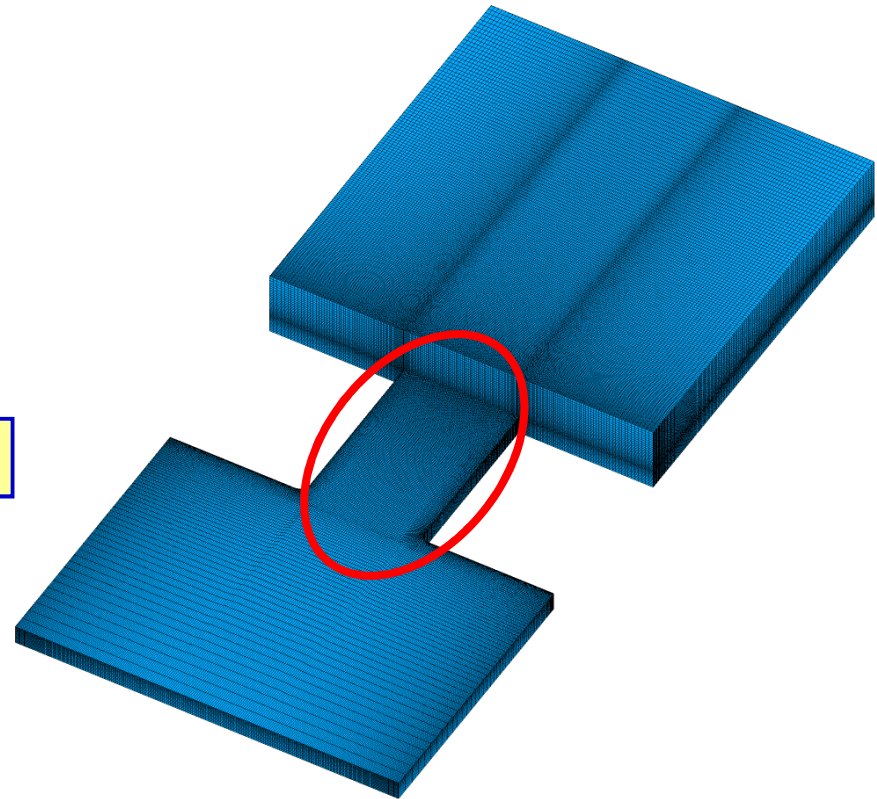
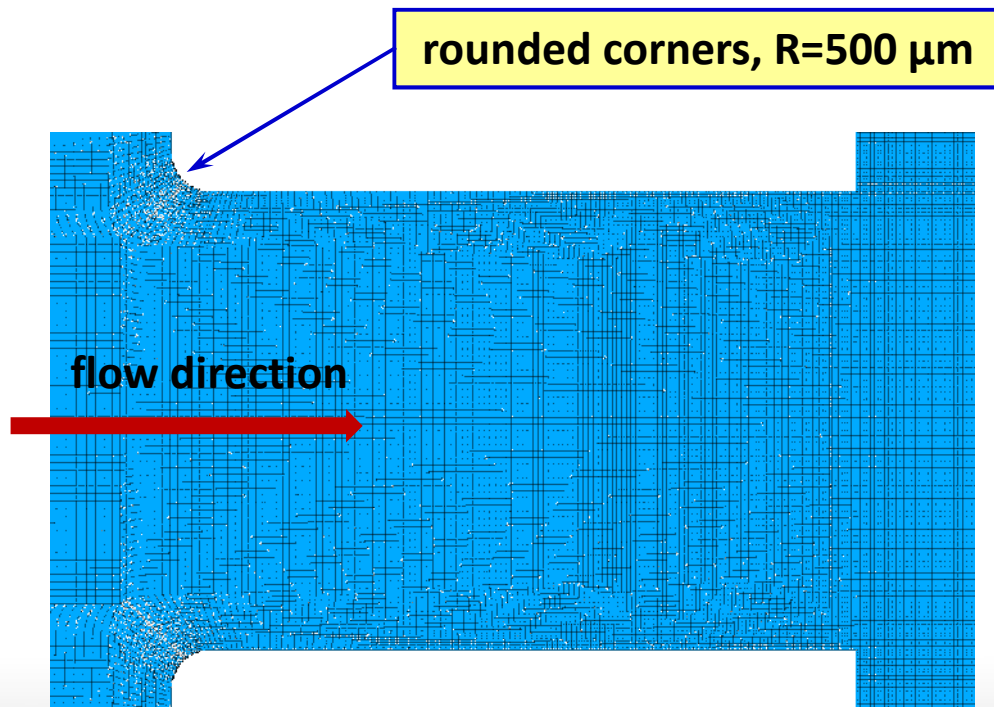
Questions to be addressed:

- Can CFD predict and forecast the occurrence of a hydraulic flip?
- Can CFD predict the occurring injector mass flow limitation under the conditions of injector cavitation and hydraulic flip?
- Identification of a stable and reproducible CFD work flow



Geometry and Computational Mesh

Elements	2 007 585
Nodes	2 095 488
Max. Aspect Ratio	17.4
Min. Angle	54.6



Boundary Conditions

Inlet:

- Total pressure = **125 - 450 kPa**
- Turbulent intensity = 1%
- Hydraulic diameter = 3.5 mm
- Diesel Volume Fraction = 1

Outlet:

- Static pressure = 100 kPa
- Backflow turbulent intensity = 1%
- Backflow hydraulic diameter = 13.5 mm
- Air Backflow Volume Fraction = 1

Upstream & Downstream Chamber Walls:

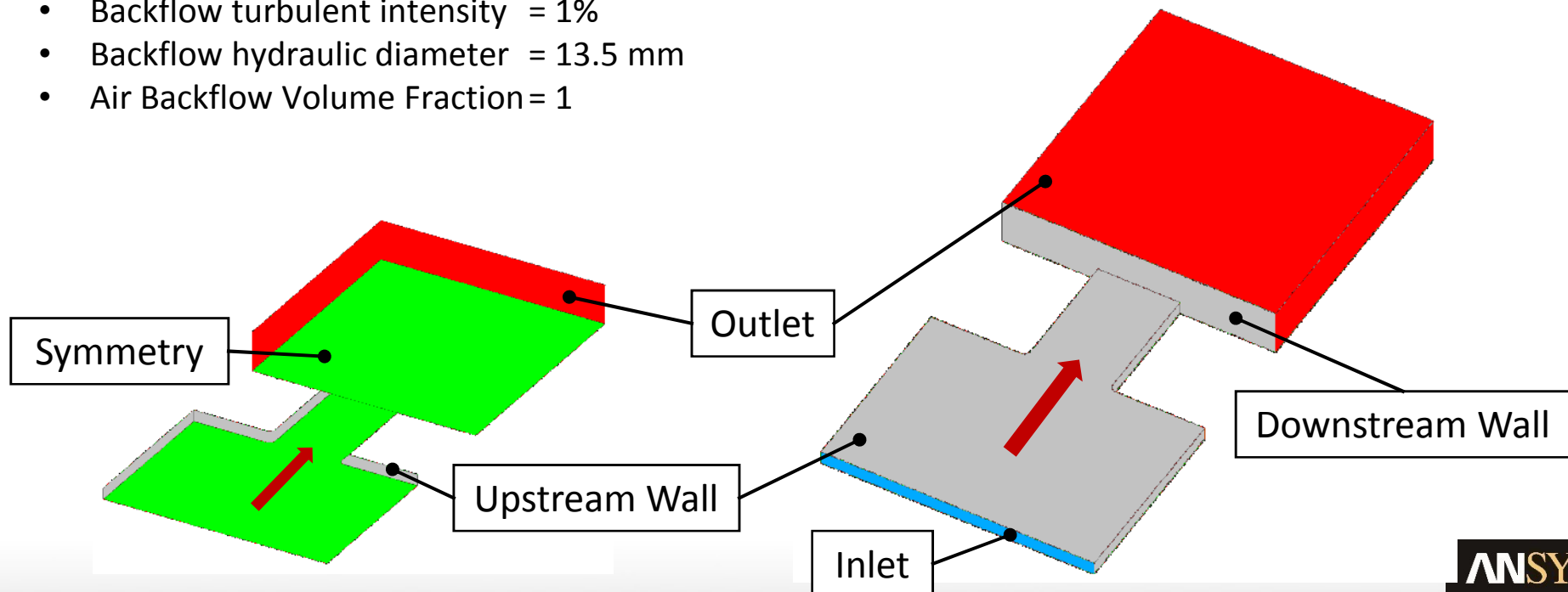
- No Slip Wall

Symmetry Plane

- Taking advantage of symmetry in z-direction

Fluid:

- Operating pressure = 100000 Pa



CFD Setup & Fluid Material Properties

- 3-phase flow: Diesel liquid - Diesel vapor - Air
- ANSYS CFX : Homogenous Eulerian multiphase flow with cavitation
ANSYS Fluent: 3-phase VOF with cavitation (homog. Eulerian mixture)
- Phase transition due to cavitation:
 - Diesel liquid – Diesel vapor: Zwart-Gerber-Belamri cavitation model
- Phase pairs without mass transfer:
 - Diesel liquid – air
 - Diesel vapor – air

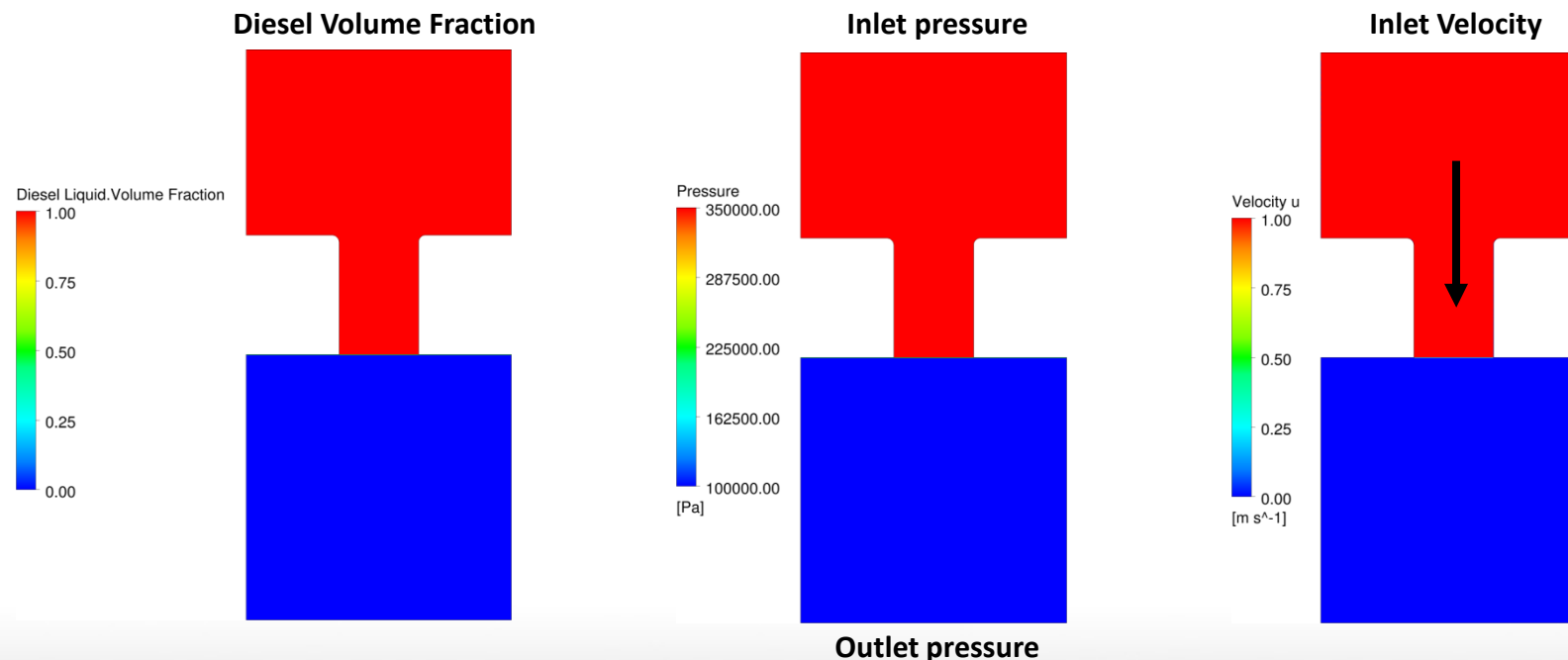
	Air	Diesel liquid	Diesel vapor
Density (kg/m³)	1.225	830	1
Viscosity (kg/m s)	$1.7894 \cdot 10^{-6}$	0.00223	$7 \cdot 10^{-6}$

	Diesel liquid / Air	Air / Diesel vapor	Diesel liquid / Diesel vapor
Surface tension (N/m)	0.026	0	0.026

Flow Initialization

Steady-state vs. Transient Flow Patterns

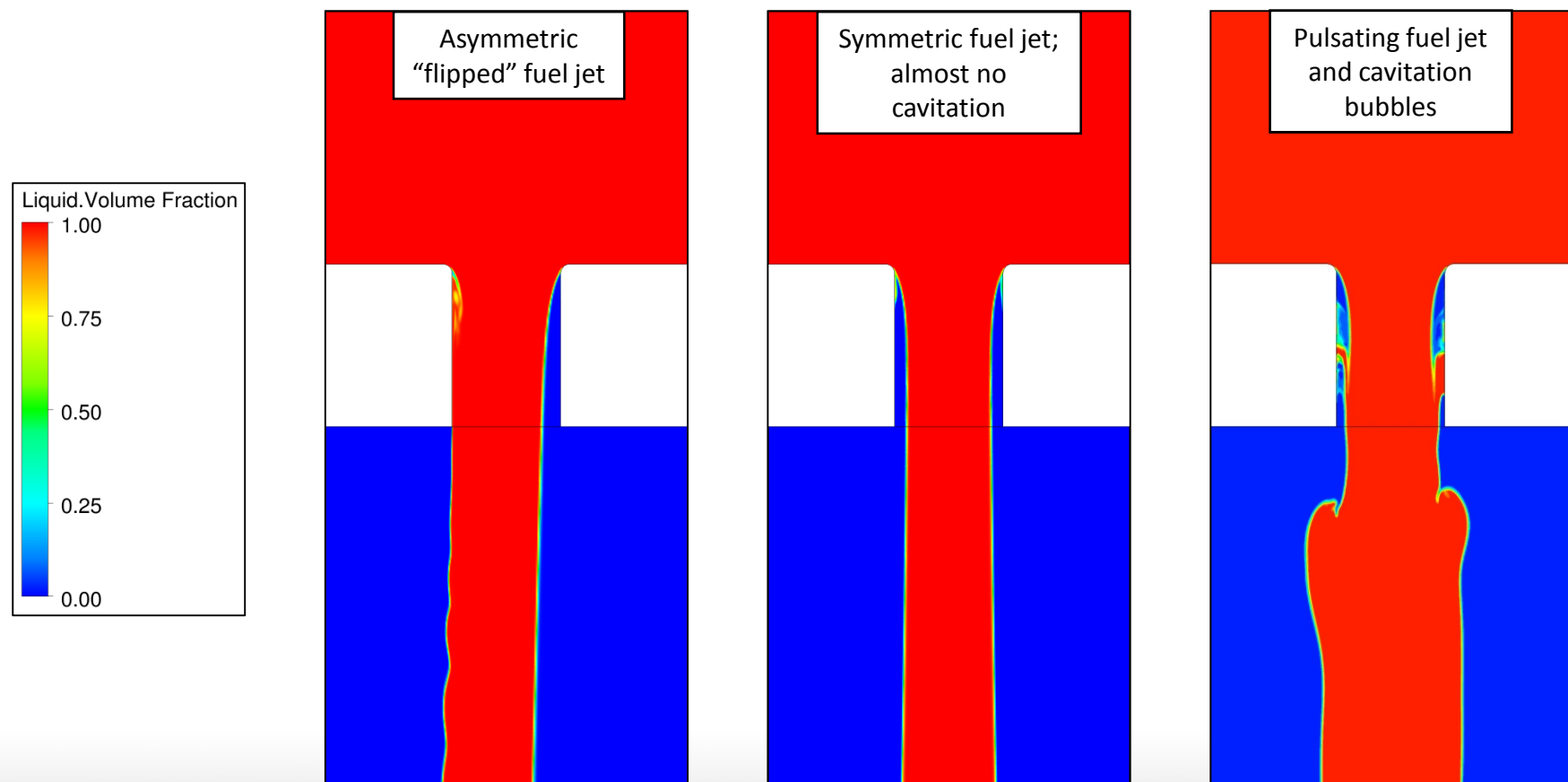
- Preliminary investigations used a symmetric initialization:
 - Applied for not or slightly cavitating flow regimes ($P_{\text{Inlet}}=125 \text{ kPa}, \dots, 350 \text{ kPa}$)
 - To save computational effort for flow development in the injector, most CFD simulations have been initialized from a fully developed flow pattern corresponding to inlet pressure $P_{\text{Inlet}} \in [125 \text{ kPa}, \dots, 200 \text{ kPa}]$
 - Observation of **steady-state flow patterns** for $P_{\text{Inlet}} \in [125 \text{ kPa}, \dots, 350 \text{ kPa}]$
 - Observation of strong **flow instability** for $P_{\text{Inlet}} \in [350 \text{ kPa}, \dots, 450 \text{ kPa}] \rightarrow$ **transient**



1st Preliminary CFD Results

Flow Patterns, Flow Instability & The Hydraulic Flip

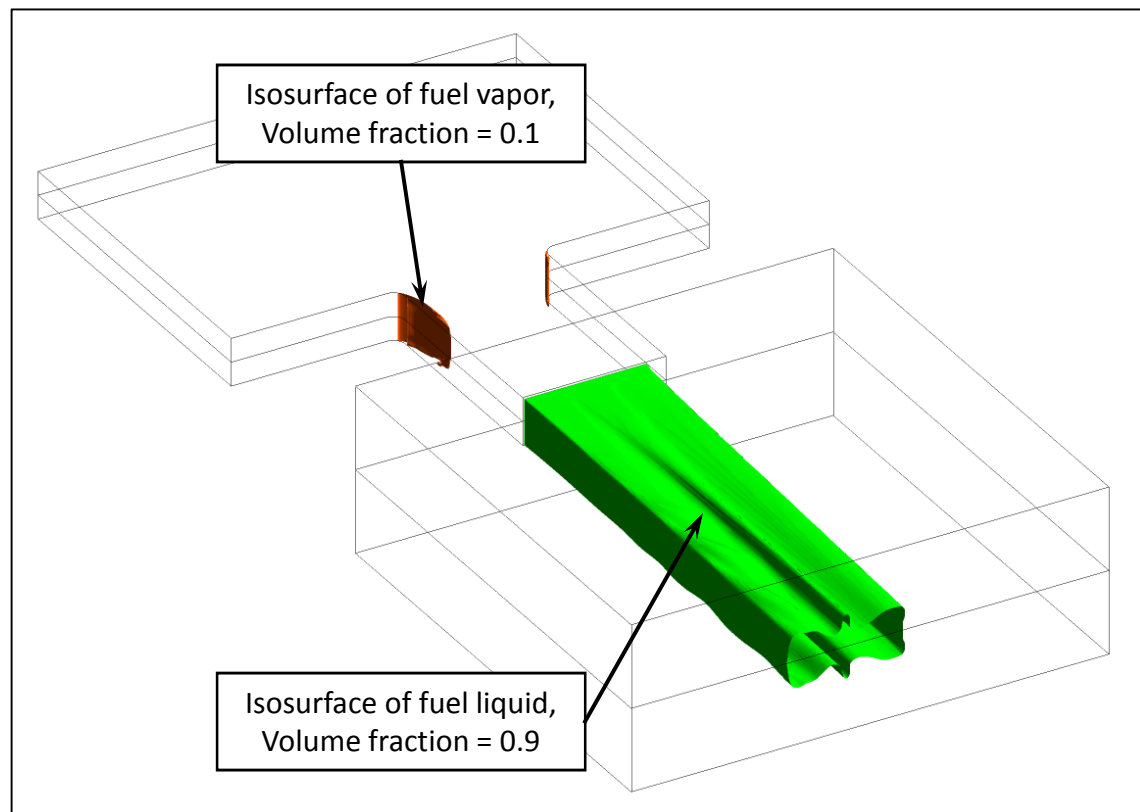
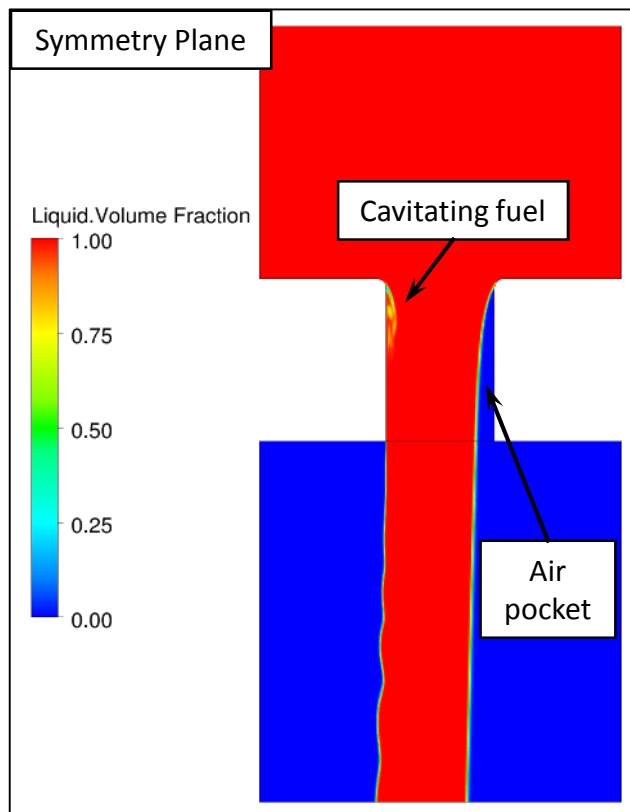
- The researchers Park et al. (2007) observed occurrence of hydraulic flip starting from $P_{\text{Inlet}}=400$ kPa
- Occurrence in CFD simulations so far depends on small flow disturbances, e.g. induced by certain solver, BC settings and flow initialization.
- In general there were three observed characteristic flow patterns for applied higher inlet pressure:



1st Preliminary CFD Results

The Hydraulic Flip – Diesel Volume Fraction

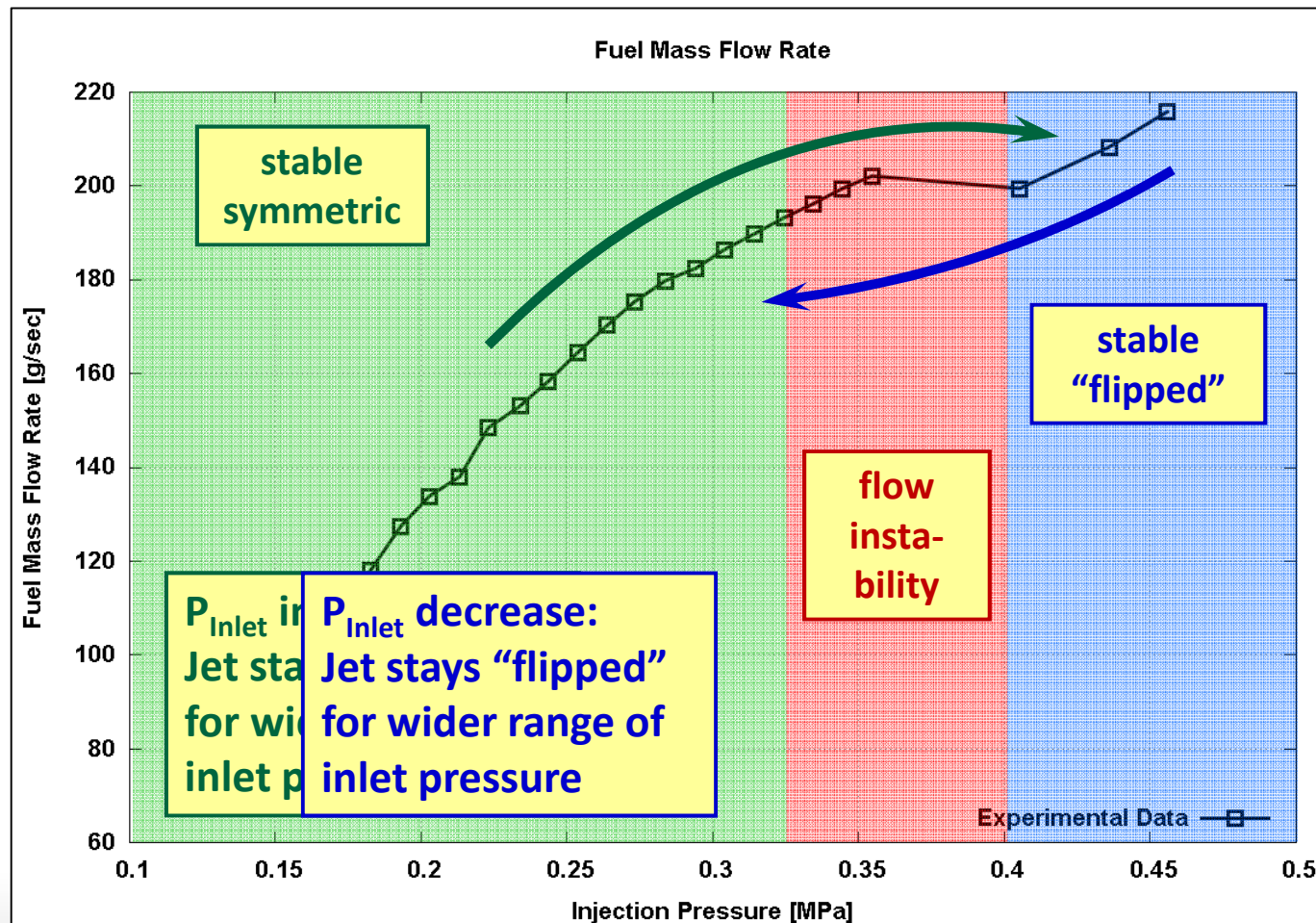
- Once the hydraulic flip occurred, it appeared to be very stable
→ almost quasi steady-state
- Images show the Diesel volume fraction distribution for a transient calculation with occurrence of the hydraulic flip and $P_{\text{inlet}}=450$ kPa.



1st Preliminary CFD Results

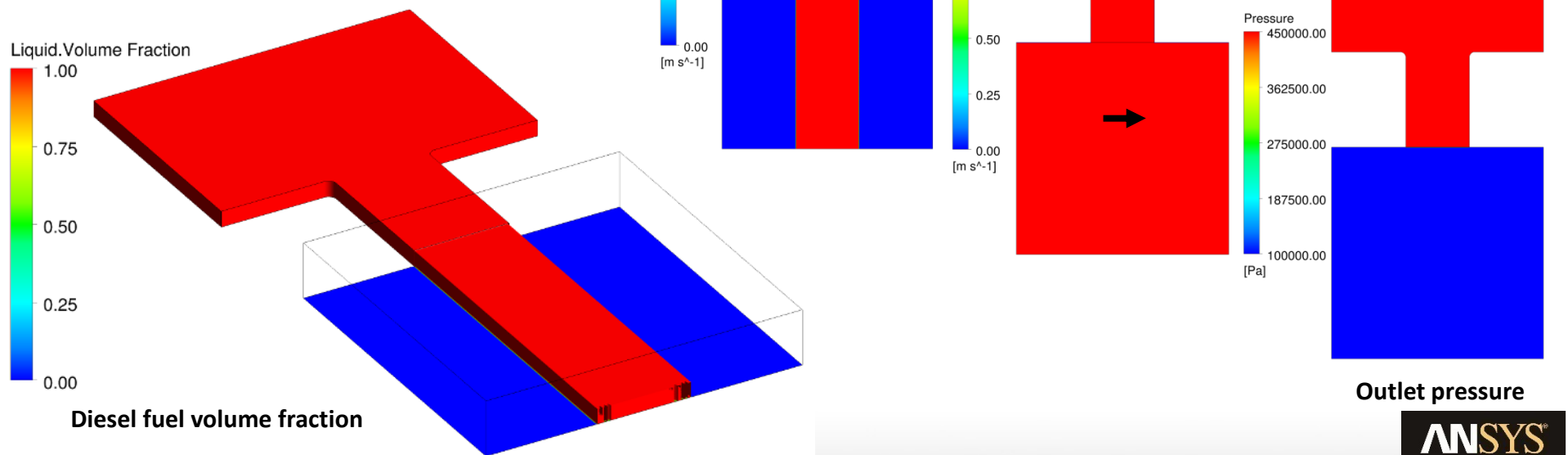
Hysteresis Effects by Variation of P_{Inlet}

- Observed strong hysteresis effects in flow regime transitions from a stable symmetric fuel jet/spray to a stable hydraulic flip with inclined fuel jet/spray

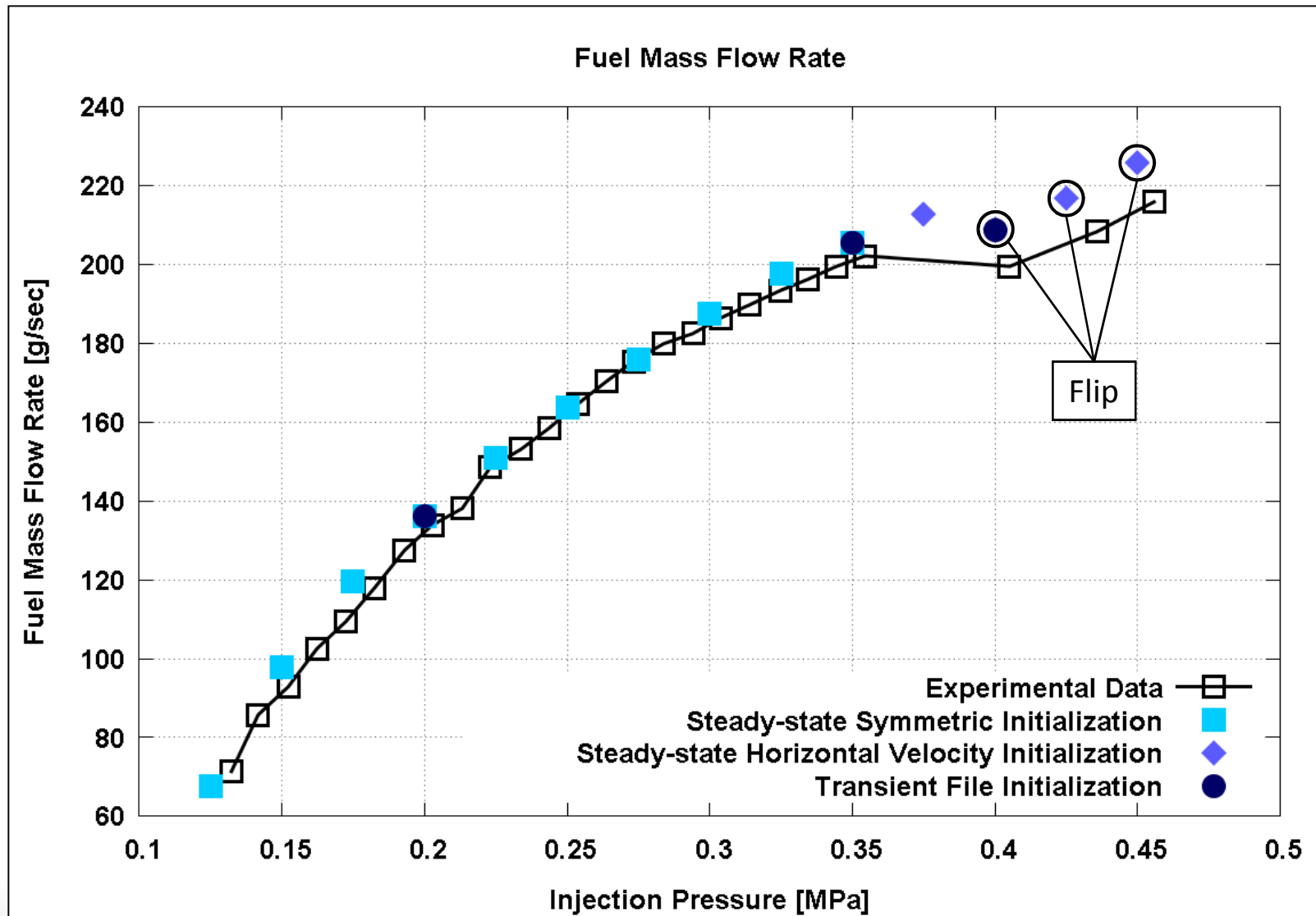


Change in Flow Initialization

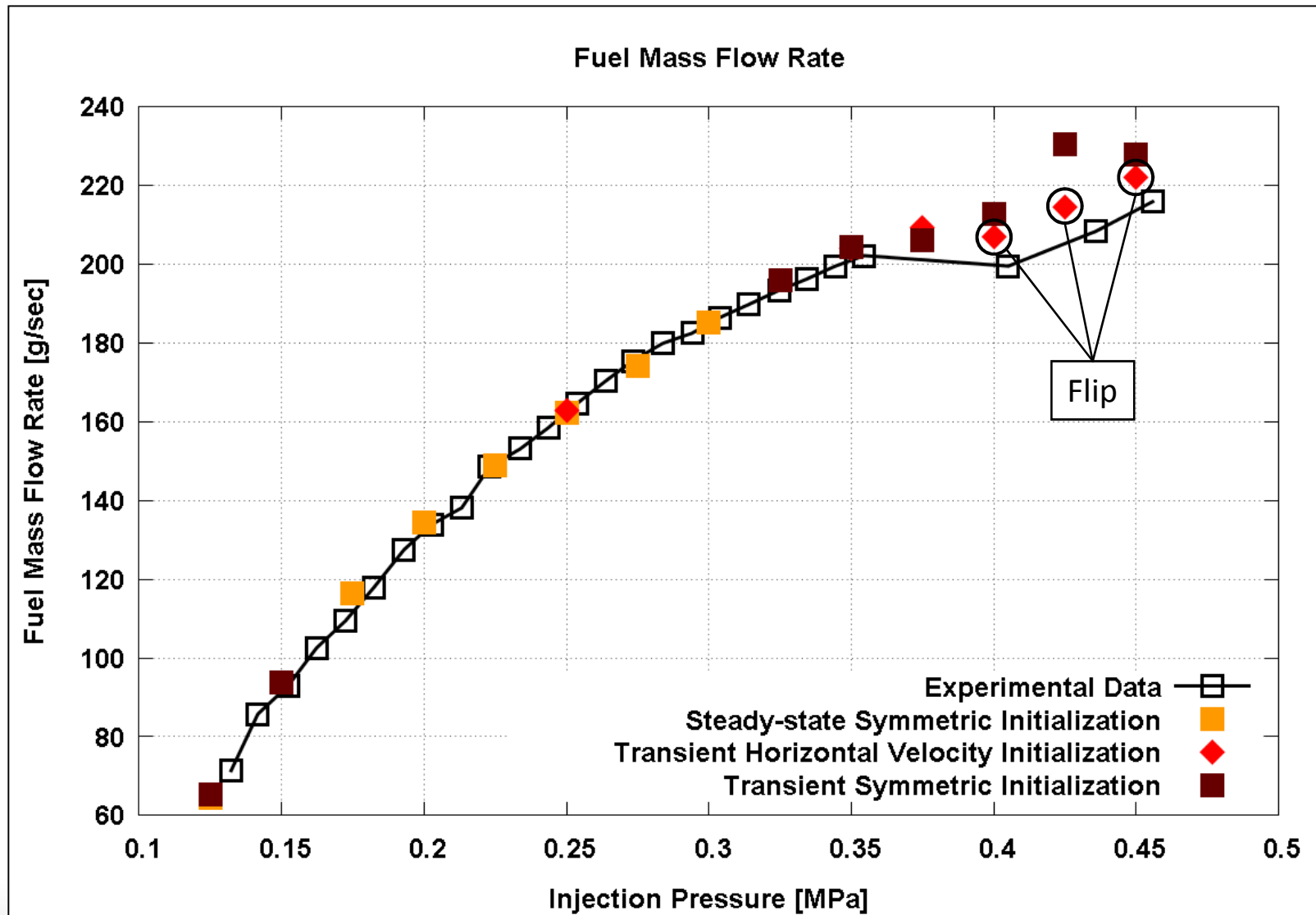
- Attempt to avoid this kind of hysteresis and unstable CFD prediction
- Using domain initialization with a horizontal velocity component
 - Reproducible hydraulic flip
 - Occurs only for inlet pressures which show the hydraulic flip in experiment as well
 - CFD simulations became reproducible and independent from numerics



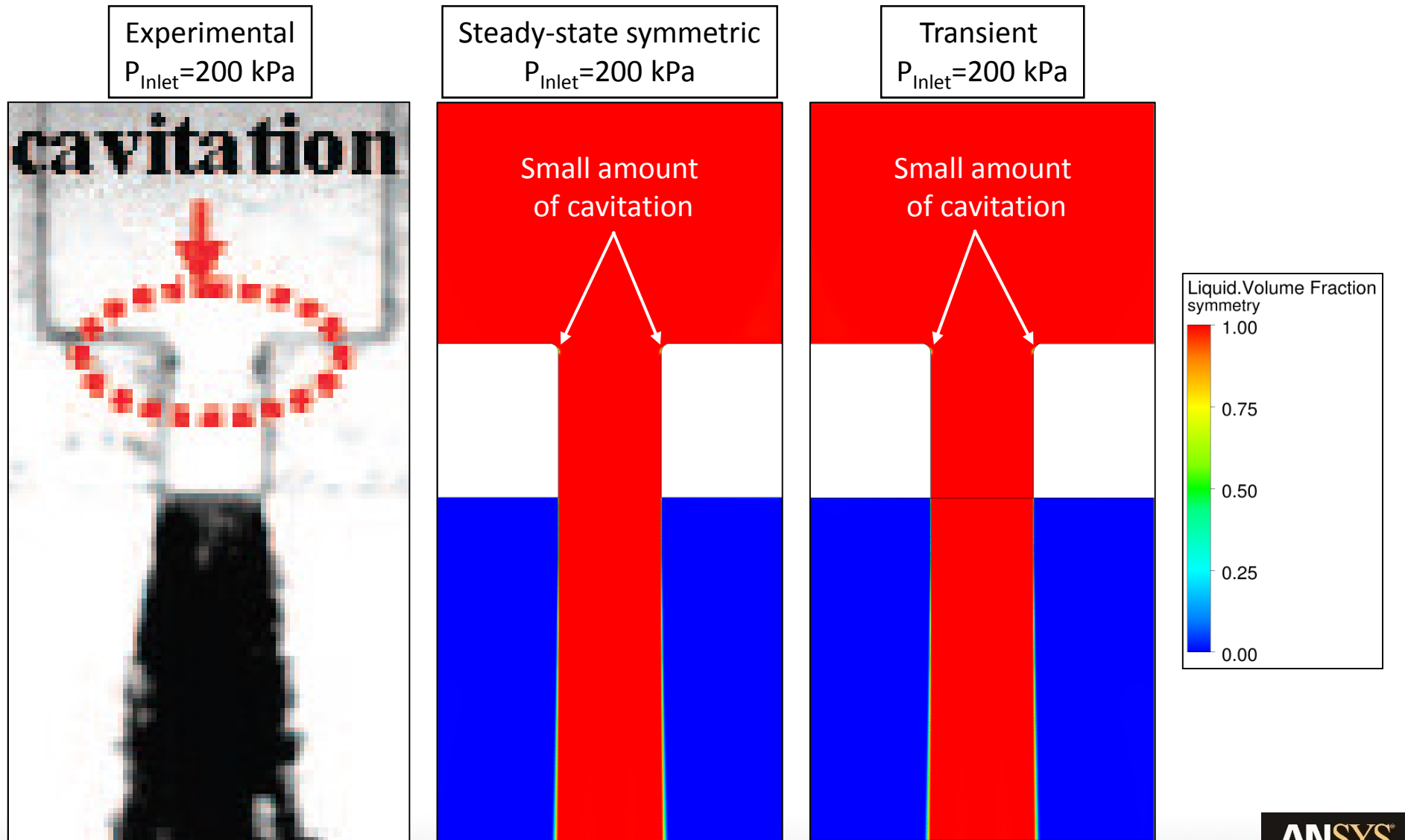
ANSYS CFX Results – Fuel Mass Flow Rate



ANSYS Fluent Results – Fuel Mass Flow Rate



Results – Flow Pattern Visualization

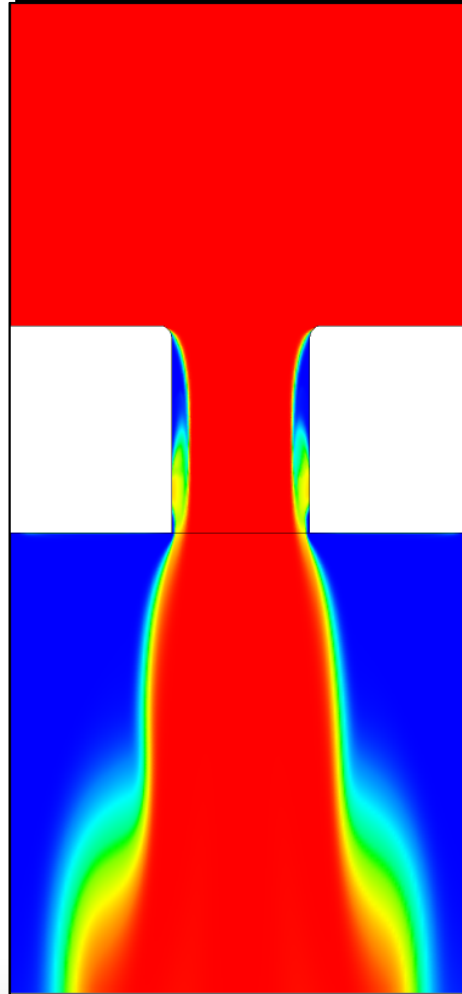


Results – Flow Pattern Visualization

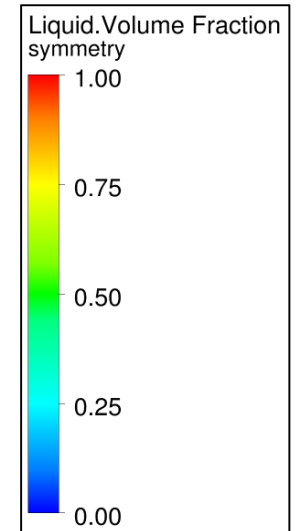
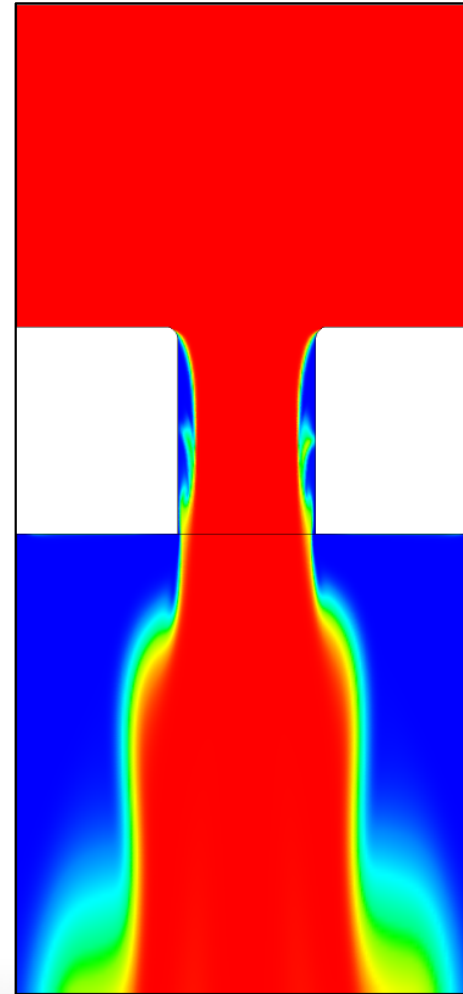
Experiment
 $P_{\text{Inlet}}=350 \text{ kPa}$



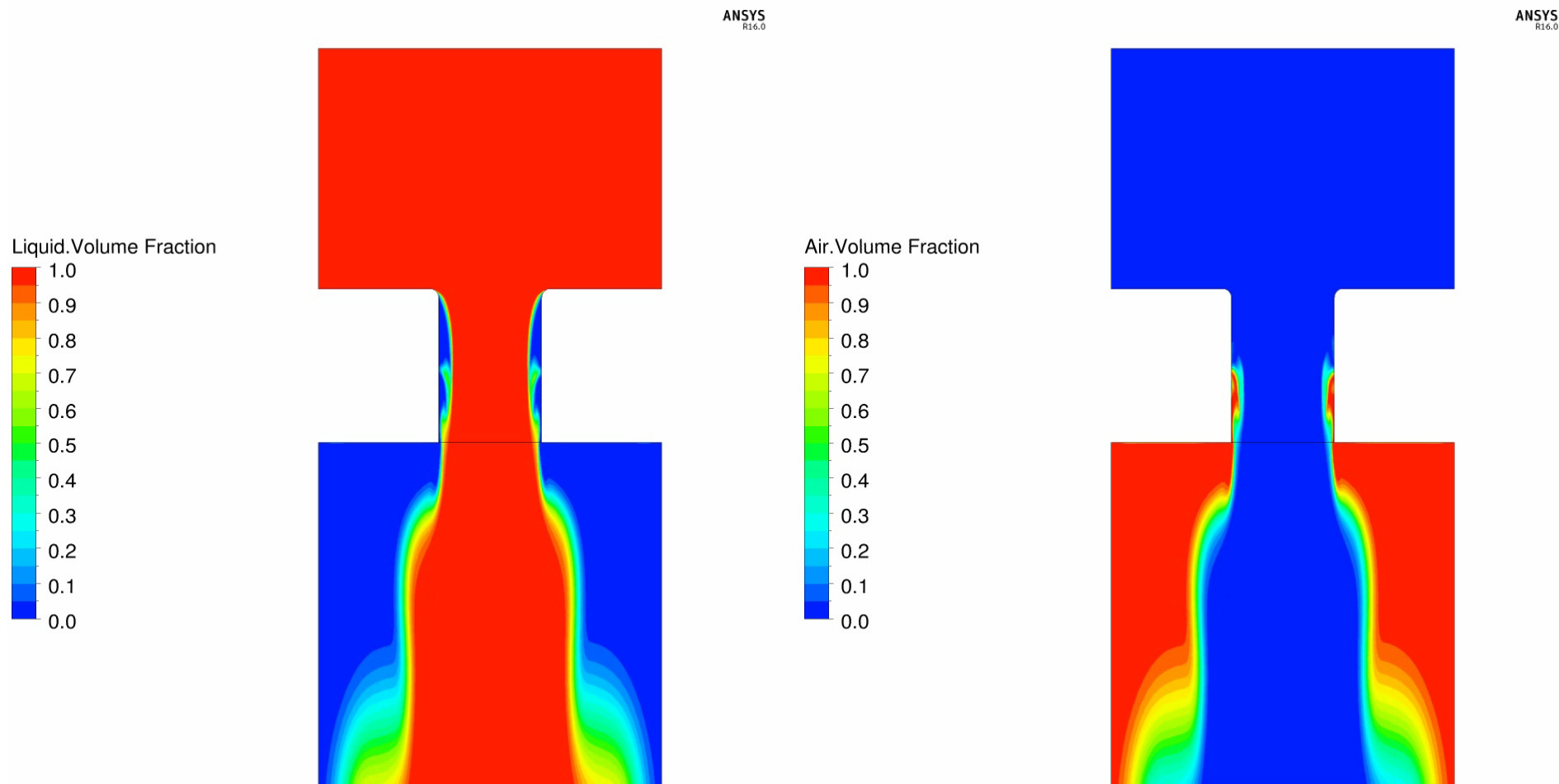
Steady-state symmetric
 $P_{\text{Inlet}}=350 \text{ kPa}$



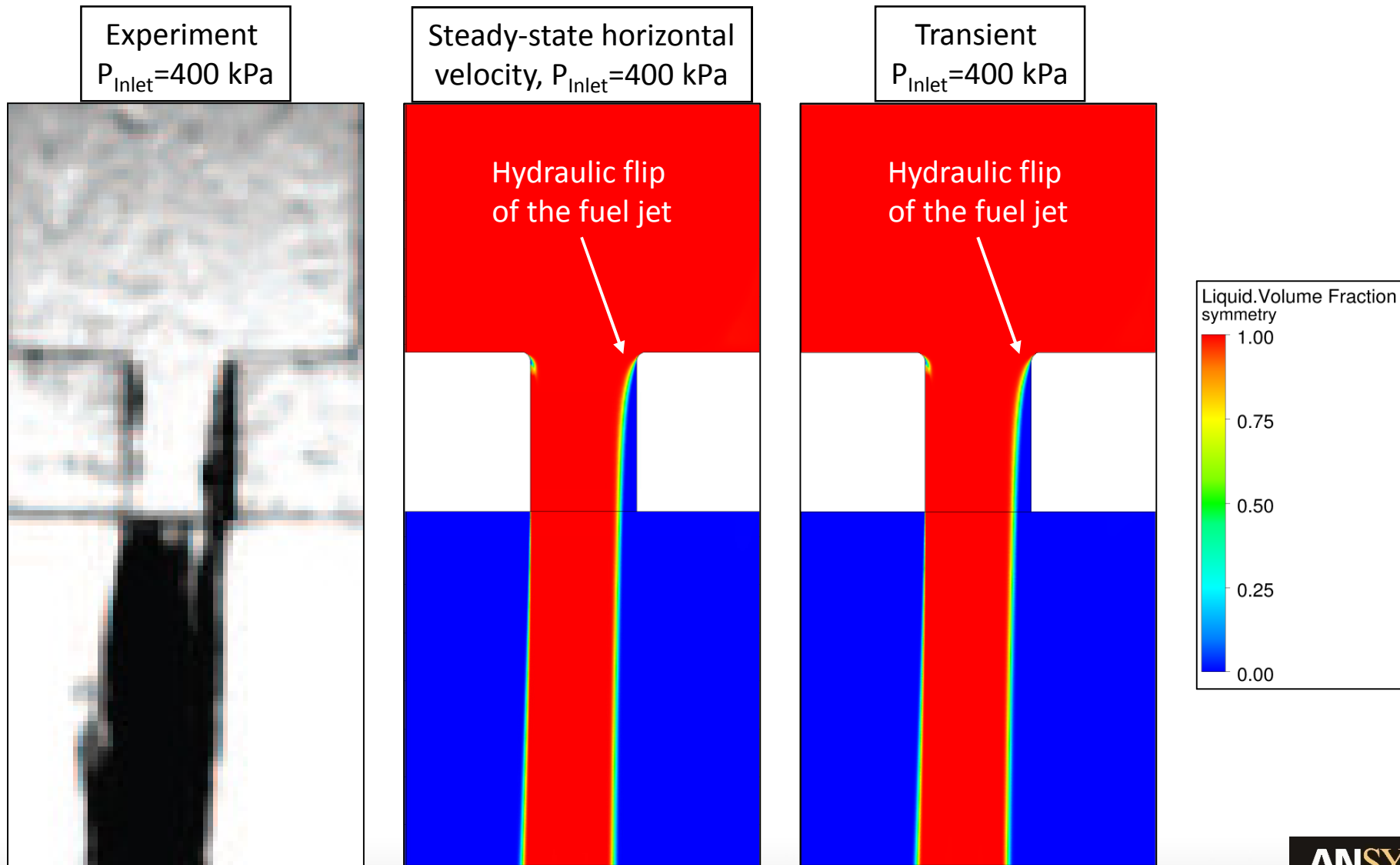
Transient
 $P_{\text{Inlet}}=350 \text{ kPa}$



Results – Pulsating Flow, $P_{\text{Inlet}} = 350$ kPa Initialization from Stable Symmetric Jet



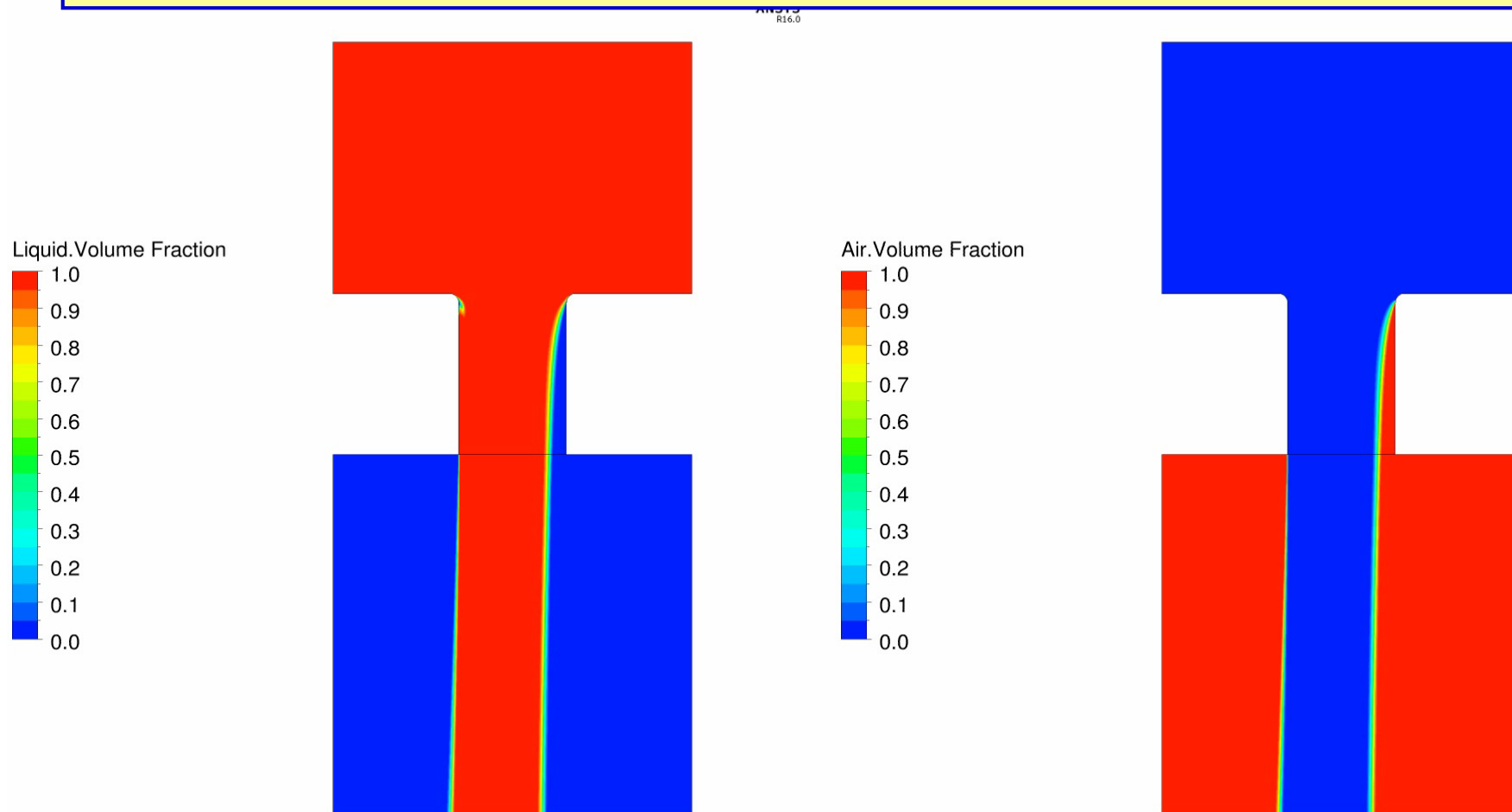
Results – Flow Pattern Visualization



Results – Video from Hydraulic Flip Simulation

$P_{\text{Inlet}} = 400 \text{ kPa}$

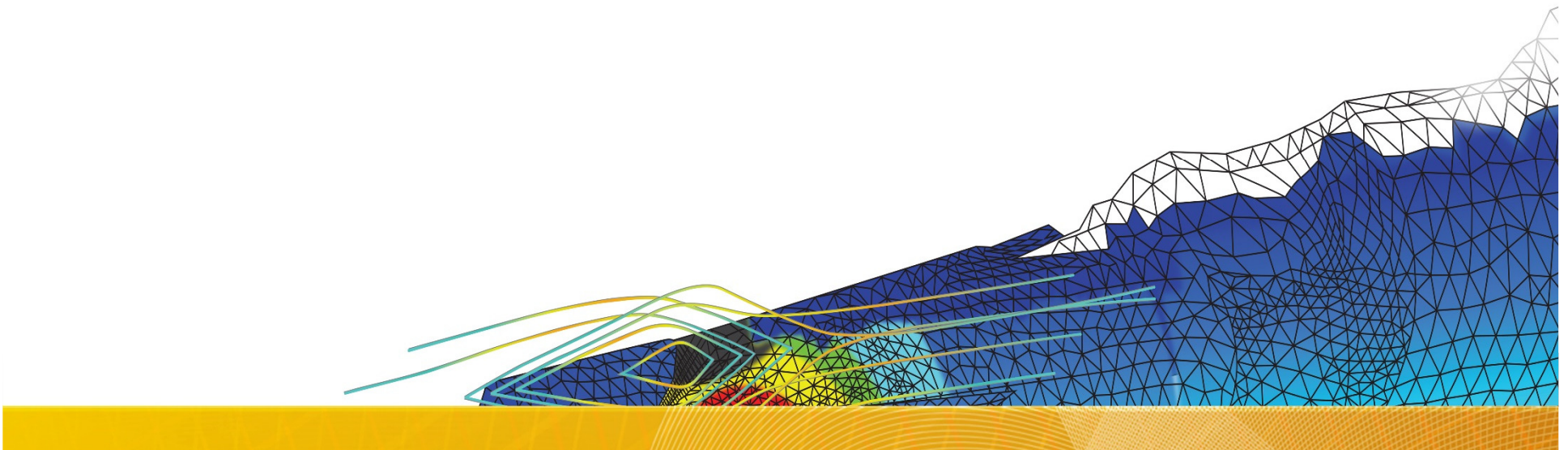
The hydraulic flip of the injected jet becomes very stable and almost steady



Realize Your Product Promise®

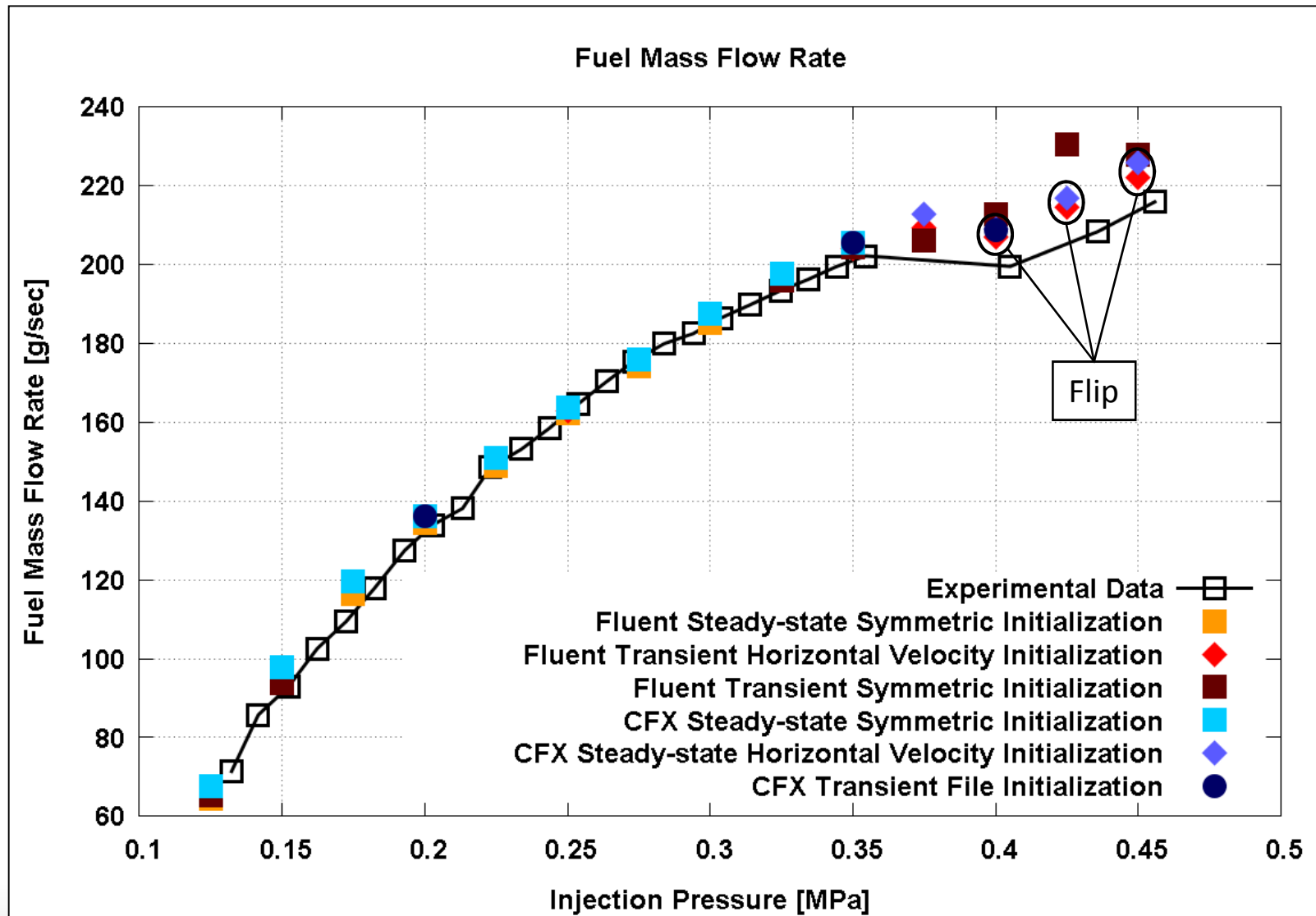


ANSYS CFD Solver Comparison



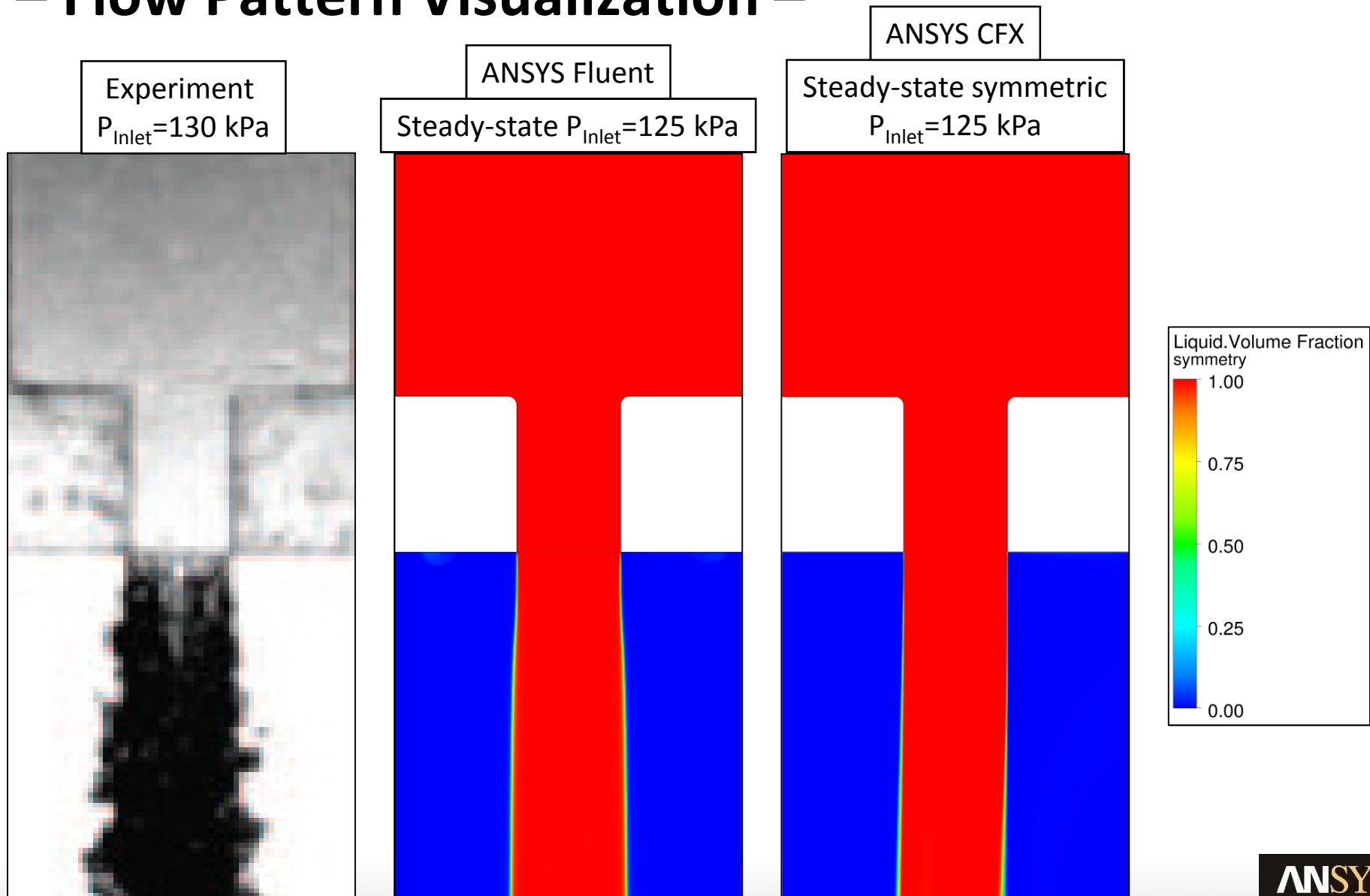
ANSYS CFD Solver Comparison

– Fuel Mass Flow Rate –



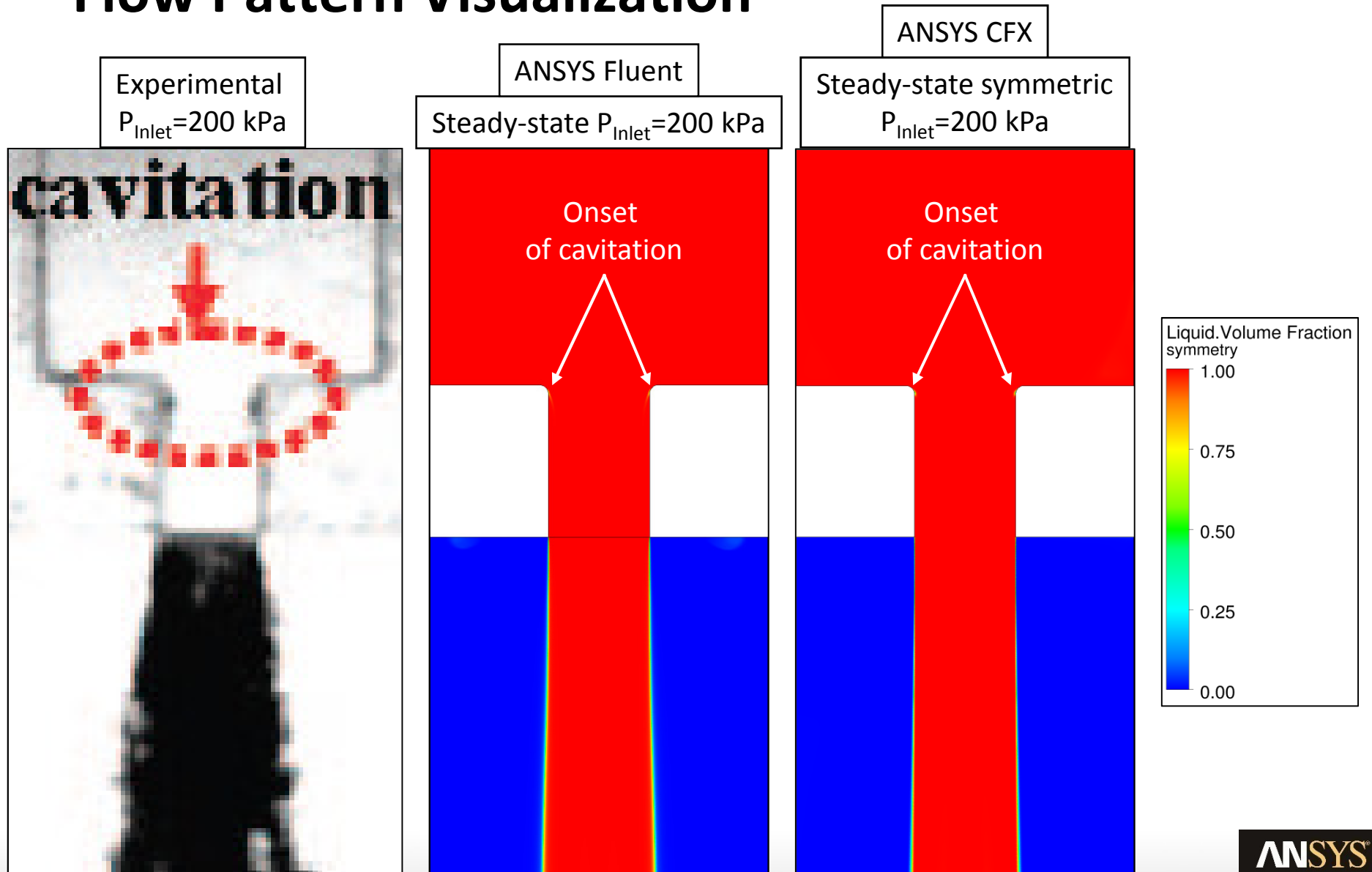
ANSYS CFD Solver Comparison

– Flow Pattern Visualization –



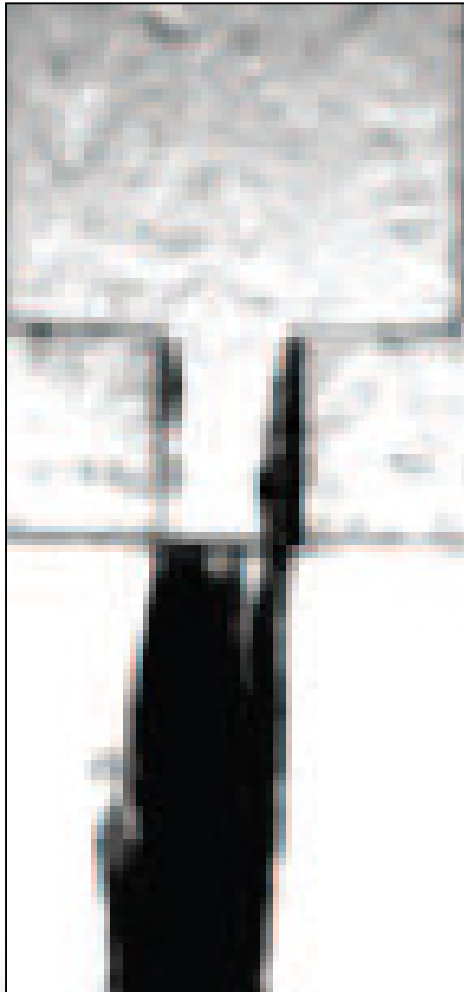
ANSYS CFD Solver Comparison

– Flow Pattern Visualization –



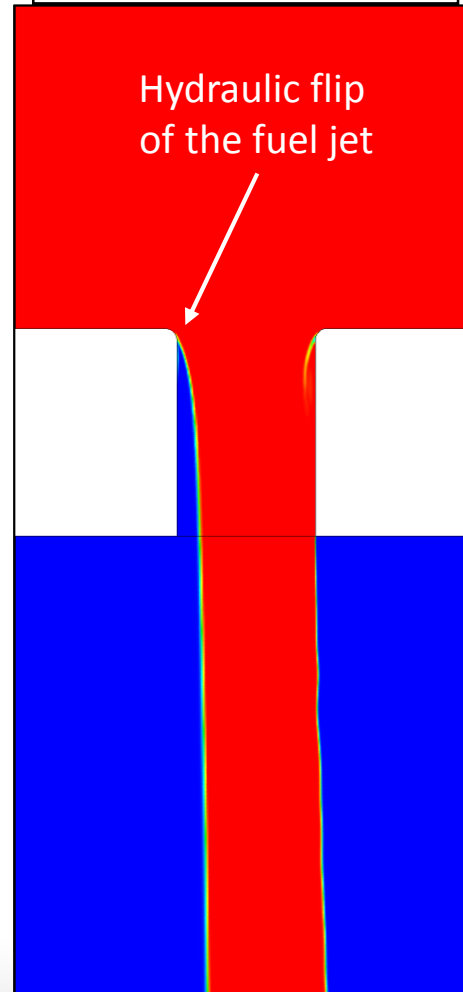
ANSYS CFD Solver Comparison – Hydraulic Flip

Experiment
 $P_{\text{Inlet}}=400 \text{ kPa}$



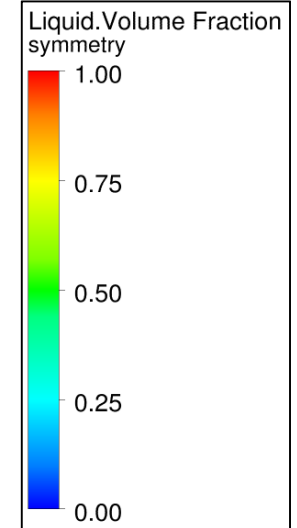
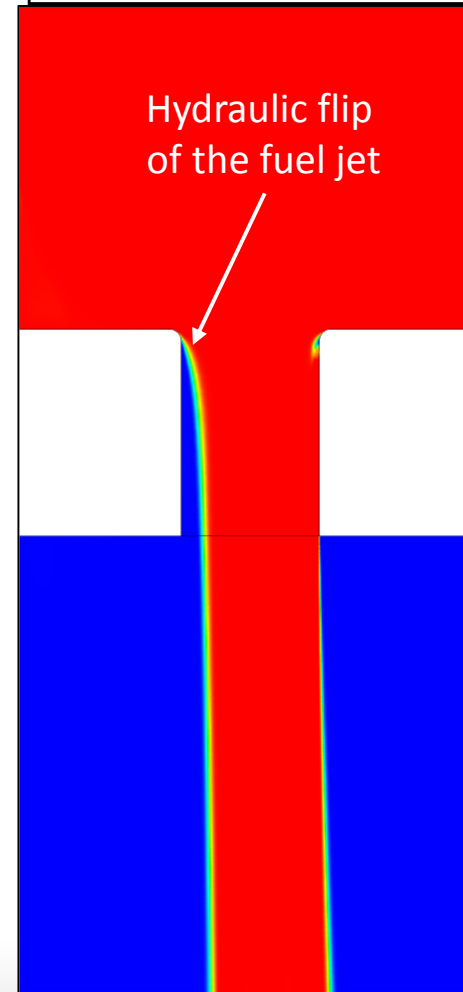
ANSYS Fluent

Transient horizontal
velocity, $P_{\text{Inlet}}=400 \text{ kPa}$



ANSYS CFX

Steady-state horizontal
velocity, $P_{\text{Inlet}}=400 \text{ kPa}$



ANSYS

Final Conclusions

- A CFD methodology was derived for both ANSYS CFD solvers [ANSYS CFX](#) and [ANSYS Fluent](#) to reliably and accurately predict the phenomenon of the hydraulic flip in fuel injectors.
- The liquid fuel mass flow rate in dependence of varying P_{inlet} is very well predicted for low and medium inlet pressure. The results for ANSYS CFX and ANSYS Fluent are almost identical and in very good agreement to experimental data.
- The mass flow rate limitation due to the occurrence of the hydraulic flip for high inlet pressure is predicted in good agreement to data. Results of ANSYS Fluent are slightly closer to the experiment.
- The flow regime change for varying P_{inlet} as predicted by CFD is in good agreement with experimental flow pattern visualization. The resolution of the spray breakup in the air filled chamber was not the focus of this investigation and would require a LES-like simulation approach.



Thank you!

