bn080916009 BXA Auto Runs GBM + LAT

Model	α	β	E_{peak} (keV)	A_1	kT (keV)	A_2	Γ	A_3	$\log(\mathcal{L})$ / BIC / $\mathcal{Z}$	Flux $\times 10^{-6}$ (erg s^{-1}cm^{-2})	Fluence $\times 10^{-5}$ (erg cm^{-2})	E_{iso} $\times 10^{54}$ (erg)
S+B	-1.273	-2.231	809.5	-1.955	44.2	0.203	...	...	-140.25/316.13/-169.26	1.525	9.603	3.601
	$^{+0.028}_{-0.040}$	$^{+0.024}_{-0.022}$	$^{+169.7}_{-104.8}$	$^{+0.019}_{-0.029}$	$^{+4.3}_{-1.2}$	$^{+0.114}_{-0.071}$	...	...		$^{+0.032}_{-0.043}$	$^{+0.203}_{-0.268}$	$^{+0.076}_{-0.101}$
G+B	-1.240	-2.230	993.9	-1.922	48.8	0.257	...	...	-141.27/318.18/-172.32	1.516	9.545	3.579
	$^{+0.036}_{-0.034}$	$^{+0.021}_{-0.028}$	$^{+210.5}_{-141.5}$	$^{+0.026}_{-0.026}$	$^{+2.7}_{-3.0}$	$^{+0.075}_{-0.079}$	...	...		$^{+0.046}_{-0.032}$	$^{+0.288}_{-0.204}$	$^{+0.108}_{-0.076}$
S+L	-0.927	-2.176	401.8	-1.847	...	...	-2.147	-3.176	-144.95/325.55/-172.80	1.461	9.199	3.450
	$^{+0.082}_{-0.189}$	$^{+0.002}_{-0.024}$	$^{+69.3}_{-15.0}$	$^{+0.016}_{-0.004}$	...	...	$^{+0.989}_{-1.210}$	$^{+0.521}_{-9.546}$		$^{+0.049}_{-0.006}$	$^{+0.306}_{-0.037}$	$^{+0.115}_{-0.014}$
S+B+L	-0.975	-2.177	412.8	-1.841	191.2	-9.724	-2.326	-3.436	-145.16/337.85/-172.93	1.465	9.227	3.460
	$^{+0.053}_{-0.143}$	$^{+0.001}_{-0.023}$	$^{+59.6}_{-7.0}$	$^{+0.011}_{-0.001}$	$^{+23.6}_{-154.7}$	$^{+6.851}_{-2.175}$	$^{+1.377}_{-1.059}$	$^{+0.515}_{-9.510}$		$^{+0.043}_{-0.010}$	$^{+0.272}_{-0.063}$	$^{+0.102}_{-0.024}$
S	-1.107	-2.191	454.1	-1.835	...	...	...	...	-149.87/323.49/-173.04	1.474	9.286	3.482
	$^{+0.013}_{-0.016}$	$^{+0.009}_{-0.012}$	$^{+24.4}_{-15.3}$	$^{+0.004}_{-0.006}$	...	...	...	...		$^{+0.030}_{-0.022}$	$^{+0.191}_{-0.136}$	$^{+0.072}_{-0.051}$
G+B+L	-1.231	-2.230	958.9	-1.916	47.5	0.242	-0.531	-9.606	-139.39/326.31/-174.88	1.516	9.546	3.580
	$^{+0.063}_{-0.008}$	$^{+0.027}_{-0.005}$	$^{+30.1}_{-208.8}$	$^{+0.049}_{-0.006}$	$^{+3.7}_{-1.7}$	$^{+0.000}_{-0.161}$	$^{+0.326}_{-2.702}$	$^{+3.418}_{-2.805}$		$^{+0.032}_{-0.029}$	$^{+0.199}_{-0.183}$	$^{+0.074}_{-0.068}$
G+L	-0.763	-2.182	392.6	-1.730	...	...	-2.036	-2.982	-147.65/330.94/-178.60	1.464	9.222	3.458
	$^{+0.017}_{-0.209}$	$^{+0.010}_{-0.016}$	$^{+85.8}_{-6.5}$	$^{+0.019}_{-0.021}$	...	...	$^{+0.046}_{-1.060}$	$^{+0.142}_{-1.677}$		$^{+0.067}_{-0.004}$	$^{+0.425}_{-0.025}$	$^{+0.159}_{-0.009}$
G	-1.027	-2.198	507.5	-1.755	...	...	...	...	-155.66/335.08/-180.79	1.504	9.470	3.552
	$^{+0.016}_{-0.025}$	$^{+0.010}_{-0.014}$	$^{+43.7}_{-27.1}$	$^{+0.009}_{-0.014}$	...	...	...	...		$^{+0.034}_{-0.026}$	$^{+0.213}_{-0.166}$	$^{+0.080}_{-0.062}$
C+B+L	-1.302	...	5074.0	-2.180	48.8	0.511	-1.778	-2.729	-209.40/460.38/-243.15	1.521	9.576	3.591
	$^{+0.042}_{-0.034}$	...	$^{+308.4}_{-312.6}$	$^{+0.020}_{-0.039}$	$^{+2.1}_{-1.5}$	$^{+0.042}_{-0.022}$	$^{+0.015}_{-0.018}$	$^{+0.064}_{-0.058}$		$^{+0.038}_{-0.046}$	$^{+0.237}_{-0.290}$	$^{+0.089}_{-0.109}$
C+L	-0.516	...	383.2	-1.765	...	...	-1.806	-2.535	-234.39/498.48/-262.81	1.307	8.229	3.086
	$^{+0.066}_{-0.073}$	...	$^{+27.1}_{-15.9}$	$^{+0.015}_{-0.020}$	...	...	$^{+0.010}_{-0.007}$	$^{+0.018}_{-0.029}$		$^{+0.046}_{-0.028}$	$^{+0.287}_{-0.178}$	$^{+0.108}_{-0.067}$
C+B	-1.369	...	6305.5	-2.029	47.1	0.416	...	...	-923.53/1876.76/-951.41	1.603	10.095	3.786
	$^{+0.007}_{-0.006}$	...	$^{+50.4}_{-85.0}$	$^{+0.009}_{-0.005}$	$^{+1.6}_{-1.8}$	$^{+0.024}_{-0.023}$	...	...		$^{+0.028}_{-0.014}$	$^{+0.177}_{-0.086}$	$^{+0.066}_{-0.032}$
C	-1.314	...	5727.9	-1.908	...	...	...	...	-1162.90/2343.63/-1177.91	1.949	12.273	4.603
	$^{+0.006}_{-0.007}$	...	$^{+117.9}_{-98.8}$	$^{+0.003}_{-0.004}$	...	...	...	...		$^{+0.022}_{-0.025}$	$^{+0.141}_{-0.159}$	$^{+0.053}_{-0.060}$

TABLE 1. BXA Auto Runs fit results for bn080916009 using GBM + LAT data.

bn080916009 BXA Original Runs GBM + LAT

Model	α	β	E_{peak} (keV)	A_1	kT (keV)	A_2	Γ	A_3	$\log(\mathcal{L})$ / BIC / $\mathcal{Z}$	Flux $\times 10^{-6}$ (erg s^{-1}cm^{-2})	Fluence $\times 10^{-5}$ (erg cm^{-2})	E_{iso} $\times 10^{54}$ (erg)
S+B (v2)	-1.287	-2.224	827.5	-1.963	46.5	0.255	...	...	-140.24/316.11/-169.35	1.514	9.537	3.577
	$^{+0.044}_{-0.025}$	$^{+0.019}_{-0.029}$	$^{+153.9}_{-128.7}$	$^{+0.028}_{-0.021}$	$^{+2.1}_{-3.8}$	$^{+0.059}_{-0.132}$	...	...		$^{+0.045}_{-0.033}$	$^{+0.286}_{-0.211}$	$^{+0.107}_{-0.079}$
S+B (v1)	-1.295	-2.237	887.3	-1.968	46.0	0.267	...	...	-140.25/316.15/-169.52	1.535	9.664	3.624
	$^{+0.050}_{-0.019}$	$^{+0.031}_{-0.016}$	$^{+91.5}_{-183.3}$	$^{+0.031}_{-0.016}$	$^{+2.5}_{-3.2}$	$^{+0.054}_{-0.135}$	...	...		$^{+0.022}_{-0.054}$	$^{+0.136}_{-0.338}$	$^{+0.051}_{-0.127}$
S+B+L	-1.283	-2.241	851.2	-1.963	43.9	0.232	-0.584	-9.211	-138.31/324.15/-170.81	1.532	9.647	3.618
	$^{+0.178}_{-0.010}$	$^{+0.051}_{-0.007}$	$^{+14.0}_{-395.9}$	$^{+0.125}_{-0.007}$	$^{+42.7}_{-1.2}$	$^{+0.044}_{-7.195}$	$^{+0.861}_{-2.882}$	$^{+3.428}_{-3.602}$		$^{+0.005}_{-0.061}$	$^{+0.030}_{-0.382}$	$^{+0.011}_{-0.143}$
G+B (v2)	-1.231	-2.227	961.8	-1.918	47.9	0.242	...	...	-141.26/318.16/-172.39	1.513	9.529	3.574
	$^{+0.026}_{-0.045}$	$^{+0.018}_{-0.031}$	$^{+247.7}_{-113.8}$	$^{+0.022}_{-0.032}$	$^{+3.9}_{-1.8}$	$^{+0.096}_{-0.065}$	...	...		$^{+0.047}_{-0.031}$	$^{+0.296}_{-0.193}$	$^{+0.111}_{-0.072}$
G+B (v1)	-1.235	-2.227	972.1	-1.917	48.4	0.250	...	...	-141.24/318.11/-173.04	1.521	9.579	3.592
	$^{+0.042}_{-0.025}$	$^{+0.010}_{-0.037}$	$^{+232.2}_{-132.6}$	$^{+0.030}_{-0.021}$	$^{+2.3}_{-2.8}$	$^{+0.039}_{-0.111}$	...	...		$^{+0.056}_{-0.010}$	$^{+0.352}_{-0.064}$	$^{+0.132}_{-0.024}$
G+B+L	-1.244	-2.234	1028.6	-1.927	49.7	0.288	0.031	-12.827	-139.58/326.69/-173.20	1.528	9.621	3.608
	$^{+0.047}_{-0.015}$	$^{+0.027}_{-0.015}$	$^{+74.6}_{-204.1}$	$^{+0.036}_{-0.010}$	$^{+1.7}_{-3.6}$	$^{+0.023}_{-0.119}$	$^{+0.648}_{-3.282}$	$^{+5.607}_{-0.685}$		$^{+0.026}_{-0.043}$	$^{+0.163}_{-0.272}$	$^{+0.061}_{-0.102}$
S+L	-0.942	-2.182	413.5	-1.852	...	...	-2.098	-3.160	-145.14/325.92/-173.85	1.471	9.263	3.474
	$^{+0.059}_{-0.174}$	$^{+0.005}_{-0.017}$	$^{+55.4}_{-1.0}$	$^{+0.021}_{-0.009}$	...	...	$^{+0.860}_{-1.254}$	$^{+0.464}_{-9.313}$		$^{+0.038}_{-0.018}$	$^{+0.236}_{-0.112}$	$^{+0.089}_{-0.042}$
S	-1.109	-2.191	460.7	-1.836	...	...	...	...	-149.90/323.56/-174.09	1.483	9.337	3.502
	$^{+0.017}_{-0.014}$	$^{+0.010}_{-0.011}$	$^{+18.6}_{-21.7}$	$^{+0.005}_{-0.005}$	...	...	...	...		$^{+0.022}_{-0.029}$	$^{+0.140}_{-0.181}$	$^{+0.053}_{-0.068}$
G+L	-0.735	-2.174	374.4	-1.716	...	...	-2.094	-3.008	-147.77/331.18/-178.74	1.449	9.125	3.422
	$^{+0.035}_{-0.233}$	$^{+0.003}_{-0.023}$	$^{+100.7}_{-8.6}$	$^{+0.007}_{-0.034}$	...	...	$^{+0.027}_{-0.987}$	$^{+0.087}_{-1.657}$		$^{+0.083}_{-0.010}$	$^{+0.521}_{-0.061}$	$^{+0.195}_{-0.023}$
G	-1.026	-2.196	505.7	-1.755	...	...	...	...	-155.67/335.10/-180.80	1.502	9.456	3.546
	$^{+0.015}_{-0.025}$	$^{+0.009}_{-0.016}$	$^{+46.4}_{-25.6}$	$^{+0.009}_{-0.014}$	...	...	...	...		$^{+0.038}_{-0.024}$	$^{+0.236}_{-0.151}$	$^{+0.089}_{-0.057}$
C+B+L	-1.287	...	4910.0	-2.183	48.8	0.510	-1.780	-2.718	-209.41/460.41/-242.99	1.536	9.673	3.628
	$^{+0.031}_{-0.043}$	...	$^{+381.6}_{-181.5}$	$^{+0.024}_{-0.026}$	$^{+1.6}_{-1.7}$	$^{+0.029}_{-0.026}$	$^{+0.016}_{-0.013}$	$^{+0.048}_{-0.067}$		$^{+0.026}_{-0.049}$	$^{+0.163}_{-0.308}$	$^{+0.061}_{-0.115}$
C+L	-0.513	...	389.4	-1.770	...	...	-1.807	-2.533	-234.38/498.46/-262.75	1.321	8.317	3.119
	$^{+0.064}_{-0.075}$	...	$^{+21.1}_{-22.8}$	$^{+0.021}_{-0.016}$	...	...	$^{+0.010}_{-0.007}$	$^{+0.017}_{-0.031}$		$^{+0.031}_{-0.044}$	$^{+0.194}_{-0.279}$	$^{+0.073}_{-0.105}$

TABLE 2. BXA Original Runs fit results for bn080916009 using GBM + LAT data.

bn080916009 XSPEC/Error Command GBM + LAT

Model	α	β	E_{peak} (keV)	A_1	kT (keV)	A_2	Γ	A_3	C-Stat / log($\mathcal{L}$) / AIC / BIC	Flux $\times 10^{-6}$ (erg s^{-1}cm^{-2})	Fluence $\times 10^{-5}$ (erg cm^{-2})	E_{iso} $\times 10^{54}$ (erg)
S+B (v2)	-1.286	-2.230	849.4	-1.965	45.4	0.250	...	...	280.10/-140.05/292.10/315.74	1.521	9.579	3.592
	+0.032	+0.021	+225.4	+0.023	+2.6	+0.074				+0.039	+0.246	+0.092
	−0.029	−0.023	−177.0	−0.021	−2.7	−0.092	...	...		−0.039	−0.246	−0.092
G+B (v2)	-1.240	-2.231	1007.5	-1.924	48.6	0.265	...	...	282.27/-141.14/294.27/317.91	1.521	9.580	3.593
	+0.036	+0.023	+296.4	+0.027	+2.9	+0.070				+0.040	+0.250	+0.094
	−0.033	−0.025	−227.7	−0.025	−2.8	−0.084	...	...		−0.040	−0.250	−0.094
S+B (v1)	-0.961	-2.176	394.6	-1.826	4.2	-0.703	...	...	287.18/-143.59/299.18/322.82	1.433	9.026	3.385
	+0.057	+0.010	+52.0	+0.007	+0.5	+0.115				+0.025	+0.155	+0.058
	−0.052	−0.010	−44.4	−0.006	−0.5	−0.152	...	...		−0.025	−0.155	−0.058
S	-1.107	-2.191	456.2	-1.836	...	...	...	...	299.71/-149.86/307.71/323.47	1.477	9.299	3.487
	+0.015	+0.010	+41.3	+0.005						+0.026	+0.162	+0.061
	−0.015	−0.011	−36.8	−0.005	...	...	...	...		−0.026	−0.162	−0.061
S+L	-0.907	-2.182	400.5	-1.856	...	...	-2.058	-3.048	289.57/-144.78/301.57/325.21	1.459	9.189	3.446
	+0.083	+0.013	+58.5	+0.020			+0.118	+0.183		+0.027	+0.169	+0.063
	−0.087	−0.023	−55.3	−0.015	...	...	−0.410	−0.542		−0.027	−0.169	−0.063
S+B+L	-1.252	-2.279	880.7	-1.996	43.9	0.258	-1.830	-3.298	277.88/-138.94/293.88/325.40	1.551	9.766	3.662
	$+NA$	$+NA$	$+NA$	$+NA$	$+NA$	$+NA$	$+NA$	$+NA$		+0.093	+0.583	+0.219
	$-NA$	$-NA$	$-NA$	$-NA$	$-NA$	$-NA$	$-NA$	$-NA$		−0.093	−0.583	−0.219
G+B+L	-1.132	-2.279	963.0	-1.961	44.5	0.234	-1.887	-3.042	279.02/-139.51/295.02/326.54	1.558	9.813	3.680
	$+NA$	$+NA$	$+NA$	$+NA$	$+NA$	$+NA$	$+NA$	$+NA$		+0.073	+0.460	+0.173
	$-NA$	$-NA$	$-NA$	$-NA$	$-NA$	$-NA$	$-NA$	$-NA$		−0.073	−0.460	−0.173
G+B (v1)	-0.811	-2.172	378.2	-1.693	4.0	-0.625	...	...	291.43/-145.71/303.43/327.07	1.433	9.025	3.384
	+0.071	+0.011	+82.9	+0.025	+0.4	+0.093				+0.026	+0.164	+0.061
	−0.064	−0.012	−67.2	−0.022	−0.4	−0.114	...	...		−0.026	−0.164	−0.061
G+L	-0.743	-2.178	384.0	-1.721	...	...	-2.077	-3.003	295.01/-147.51/307.01/330.65	1.464	9.222	3.458
	+0.110	+0.014	+106.5	+0.024			+0.128	+0.183		+0.031	+0.197	+0.074
	−0.100	−0.025	−85.6	−0.022	...	...	−0.355	−0.445		−0.031	−0.197	−0.074
G	-1.030	-2.198	510.6	-1.756	...	...	...	...	311.29/-155.65/319.29/335.06	1.505	9.476	3.554
	+0.020	+0.012	+57.6	+0.012						+0.030	+0.192	+0.072
	−0.019	−0.012	−50.7	−0.011	...	...	...	...		−0.030	−0.192	−0.072
C+B+L	-0.556	...	710.3	-2.113	36.2	0.259	-1.826	-2.471	427.48/-213.74/441.48/469.06	1.551	9.768	3.663
	+0.156		+283.9	+0.005	+2.5	+0.065	+0.009	+0.022		+0.060	+0.379	+0.142
	−0.130	...	−187.1	−0.018	−2.4	−0.075	−0.008	−0.025		−0.060	−0.379	−0.142
C+L	-0.515	...	385.4	-1.767	...	...	-1.805	-2.538	468.57/-234.29/478.57/498.27	1.310	8.252	3.095
	+0.071		+59.9	+0.011			+0.008	+0.022		+0.032	+0.199	+0.075
	−0.067	...	−51.1	−0.014	...	...	−0.008	−0.025		−0.032	−0.199	−0.075

TABLE 3. XSPEC fit results for bn080916009 using GBM + LAT data and errors from the Error command.

bn080916009 XSPEC/Fakeit Command GBM + LAT

Model	α	β	E_{peak} (keV)	A_1	kT (keV)	A_2	Γ	A_3	C-Stat / $\log(\mathcal{L})$ / AIC / BIC	Flux $\times 10^{-6}$ (erg $s^{-1}cm^{-2}$)	Fluence $\times 10^{-5}$ (erg cm^{-2})	E_{iso} $\times 10^{54}$ (erg)
S+B (v2)	-1.286	-2.230	849.4	-1.965	45.4	0.250	...	...	280.10/-140.05/292.10/315.74	1.521	9.579	3.592
	+0.035	+0.023	+160.0	+0.025	+2.8	+0.079				+0.037	+0.235	+0.088
	−0.032	−0.027	−129.9	−0.023	−2.7	−0.101	...	...		−0.041	−0.255	−0.096
G+B (v2)	-1.240	-2.231	1007.5	-1.924	48.6	0.265	...	...	282.27/-141.14/294.27/317.91	1.521	9.580	3.593
	+0.039	+0.025	+223.6	+0.030	+3.0	+0.074				+0.039	+0.243	+0.091
	−0.036	−0.029	−178.1	−0.028	−2.8	−0.086	...	...		−0.042	−0.262	−0.098
S+B (v1)	-0.961	-2.176	394.6	-1.826	4.2	-0.703	...	...	287.18/-143.59/299.18/322.82	1.433	9.026	3.385
	+0.056	+0.010	+19.7	+0.006	+0.5	+0.121				+0.025	+0.160	+0.060
	−0.044	−0.010	−19.2	−0.006	−0.5	−0.119	...	...		−0.024	−0.154	−0.058
S	-1.107	-2.191	456.2	-1.836	...	...	...	...	299.71/-149.86/307.71/323.47	1.477	9.299	3.487
	+0.015	+0.010	+20.2	+0.005						+0.026	+0.164	+0.062
	−0.014	−0.011	−19.0	−0.005	...	...	...	...		−0.025	−0.158	−0.059
S+L	-0.907	-2.182	400.5	-1.856	...	...	-2.058	-3.048	289.57/-144.78/301.57/325.21	1.459	9.189	3.446
	+0.065	+0.009	+19.2	+0.017			+0.144	+0.185		+0.028	+0.174	+0.065
	−0.076	−0.032	−21.8	−0.016	...	...	−0.324	−0.406		−0.022	−0.137	−0.051
S+B+L	-1.252	-2.279	880.7	-1.996	43.9	0.258	-1.830	-3.298	277.88/-138.94/293.88/325.40	1.551	9.766	3.662
	+0.054	+0.042	+150.0	+0.028	+2.5	+0.064	+0.100	+0.209		+0.046	+0.290	+0.109
	−0.040	−0.043	−126.5	−0.025	−3.2	−0.086	−0.119	−0.617		−0.041	−0.259	−0.097
G+B+L	-1.132	-2.279	963.0	-1.961	44.5	0.234	-1.887	-3.042	279.02/-139.51/295.02/326.54	1.558	9.813	3.680
	+0.063	+0.043	+197.9	+0.035	+3.1	+0.069	+0.063	+0.120		+0.046	+0.288	+0.108
	−0.062	−0.052	−149.7	−0.030	−3.2	−0.076	−0.106	−0.238		−0.044	−0.277	−0.104
G+B (v1)	-0.811	-2.172	378.2	-1.693	4.0	-0.625	...	...	291.43/-145.71/303.43/327.07	1.433	9.025	3.384
	+0.063	+0.010	+28.6	+0.022	+0.4	+0.090				+0.028	+0.176	+0.066
	−0.054	−0.011	−27.4	−0.019	−0.4	−0.090	...	...		−0.027	−0.168	−0.063
G+L	-0.743	-2.178	384.0	-1.721	...	...	-2.077	-3.003	295.01/-147.51/307.01/330.65	1.464	9.222	3.458
	+0.075	+0.009	+32.8	+0.020			+0.150	+0.178		+0.031	+0.194	+0.073
	−0.087	−0.035	−23.8	−0.021	...	...	−0.320	−0.370		−0.023	−0.143	−0.054
G	-1.030	-2.198	510.6	-1.756	...	...	...	...	311.29/-155.65/319.29/335.06	1.505	9.476	3.554
	+0.019	+0.012	+36.5	+0.011						+0.032	+0.202	+0.076
	−0.019	−0.013	−32.3	−0.011	...	...	...	...		−0.030	−0.187	−0.070
C+B+L	-0.556	...	710.3	-2.113	36.2	0.259	-1.826	-2.471	427.48/-213.74/441.48/469.06	1.551	9.768	3.663
	+0.131		+105.5	+0.052	+2.2	+0.065	+0.008	+0.020		+0.059	+0.369	+0.138
	−0.103	...	−81.3	−0.060	−2.2	−0.066	−0.007	−0.024		−0.057	−0.362	−0.136
C+L	-0.515	...	385.4	-1.767	...	...	-1.805	-2.538	468.57/-234.29/478.57/498.27	1.310	8.252	3.095
	+0.076		+18.4	+0.017			+0.009	+0.025		+0.031	+0.197	+0.074
	−0.062	...	−18.5	−0.015	...	...	−0.009	−0.026		−0.033	−0.205	−0.077

TABLE 4. XSPEC fit results for bn080916009 using GBM + LAT data and errors from Fakeit runs.