bn090510016 BXA Auto Runs GBM + LAT

Model	α	β	E_{peak} (keV)	A_1	kT (keV)	A_2	Γ	A_3	$\log(\mathcal{L})$ / BIC / $\mathcal{Z}$	Flux $\times 10^{-5}$ (erg s^{-1}cm^{-2})	Fluence $\times 10^{-5}$ (erg cm^{-2})	E_{iso} $\times 10^{52}$ (erg)
S+B+L	-0.808	-3.052	3071.2	-1.705	33.0	-0.234	-1.469	-2.866	-163.43/376.35/-185.89	1.869	1.794	3.961
	$^{+0.008}_{-0.078}$	$^{+0.048}_{-0.373}$	$^{+517.6}_{-179.0}$	$^{+0.053}_{-0.010}$	$^{+135.3}_{-0.3}$	$^{+1.719}_{-11.522}$	$^{+0.090}_{-0.063}$	$^{+0.242}_{-0.369}$		$^{+0.105}_{-0.097}$	$^{+0.101}_{-0.094}$	$^{+0.223}_{-0.207}$
S+L	-0.851	-3.103	3167.0	-1.668	...	...	-1.452	-2.950	-164.06/365.24/-186.66	1.867	1.792	3.957
	$^{+0.050}_{-0.037}$	$^{+0.104}_{-0.318}$	$^{+426.5}_{-275.9}$	$^{+0.018}_{-0.044}$	...	...	$^{+0.076}_{-0.078}$	$^{+0.323}_{-0.286}$		$^{+0.108}_{-0.105}$	$^{+0.104}_{-0.101}$	$^{+0.230}_{-0.223}$
G+B+L	-0.571	-3.447	3694.6	-1.806	23.1	0.234	-1.560	-2.480	-163.48/376.45/-189.07	1.849	1.775	3.918
	$^{+0.117}_{-0.228}$	$^{+0.418}_{-0.097}$	$^{+675.2}_{-153.3}$	$^{+0.170}_{-0.101}$	$^{+144.1}_{-11.1}$	$^{+2.534}_{-11.980}$	$^{+0.153}_{-0.011}$	$^{+0.074}_{-0.635}$		$^{+0.002}_{-0.170}$	$^{+0.002}_{-0.164}$	$^{+0.005}_{-0.361}$
G+L	-0.760	-3.292	4027.3	-1.669	...	...	-1.515	-2.696	-164.49/366.10/-189.57	1.743	1.673	3.693
	$^{+0.072}_{-0.044}$	$^{+0.268}_{-0.279}$	$^{+372.8}_{-493.2}$	$^{+0.035}_{-0.036}$	...	...	$^{+0.114}_{-0.037}$	$^{+0.162}_{-0.437}$		$^{+0.109}_{-0.071}$	$^{+0.105}_{-0.068}$	$^{+0.232}_{-0.150}$
C+L	-0.682	...	4104.2	-1.735	...	...	-1.560	-2.401	-170.90/372.74/-192.01	1.845	1.771	3.910
	$^{+0.033}_{-0.110}$	...	$^{+938.1}_{-282.0}$	$^{+0.058}_{-0.018}$	...	...	$^{+0.052}_{-0.019}$	$^{+0.055}_{-0.195}$		$^{+0.075}_{-0.096}$	$^{+0.072}_{-0.092}$	$^{+0.159}_{-0.203}$
C+B+L	-0.584	...	3780.1	-1.807	50.7	0.255	-1.581	-2.309	-169.85/383.00/-192.10	1.861	1.786	3.943
	$^{+0.061}_{-0.206}$	...	$^{+1240.4}_{-54.1}$	$^{+0.127}_{-0.052}$	$^{+118.4}_{-14.6}$	$^{+2.069}_{-12.040}$	$^{+0.071}_{-0.003}$	$^{+0.037}_{-0.276}$		$^{+0.057}_{-0.114}$	$^{+0.055}_{-0.110}$	$^{+0.121}_{-0.242}$
S	-0.816	-2.314	1881.0	-1.625	...	...	...	...	-200.36/425.46/-217.27	1.300	1.248	2.754
	$^{+0.055}_{-0.035}$	$^{+0.051}_{-0.049}$	$^{+239.9}_{-203.1}$	$^{+0.013}_{-0.023}$	...	...	...	...		$^{+0.105}_{-0.090}$	$^{+0.101}_{-0.087}$	$^{+0.222}_{-0.191}$
S+B	-0.803	-2.327	1984.4	-1.654	31.9	-0.059	...	...	-199.92/436.95/-217.45	1.315	1.262	2.786
	$^{+0.043}_{-0.047}$	$^{+0.064}_{-0.036}$	$^{+152.5}_{-300.8}$	$^{+0.043}_{-0.004}$	$^{+137.0}_{-1.3}$	$^{+1.932}_{-11.584}$	...	...		$^{+0.094}_{-0.103}$	$^{+0.090}_{-0.099}$	$^{+0.199}_{-0.217}$
G+B	-0.652	-2.306	1998.6	-1.613	23.7	-0.144	...	...	-199.64/436.41/-219.73	1.311	1.259	2.779
	$^{+0.006}_{-0.113}$	$^{+0.051}_{-0.052}$	$^{+436.4}_{-220.0}$	$^{+0.042}_{-0.002}$	$^{+143.5}_{-8.9}$	$^{+2.013}_{-11.668}$	...	...		$^{+0.083}_{-0.116}$	$^{+0.080}_{-0.111}$	$^{+0.176}_{-0.246}$
G	-0.709	-2.306	2092.4	-1.590	...	...	...	...	-200.14/425.02/-219.75	1.308	1.256	2.772
	$^{+0.051}_{-0.056}$	$^{+0.049}_{-0.051}$	$^{+350.3}_{-289.4}$	$^{+0.019}_{-0.021}$	...	...	...	...		$^{+0.086}_{-0.103}$	$^{+0.083}_{-0.099}$	$^{+0.183}_{-0.218}$
C+B	-1.029	...	9284.9	-1.693	199.5	1.394	...	...	-494.10/1019.14/-511.83	1.415	1.359	2.999
	$^{+0.091}_{-0.012}$	...	$^{+80.6}_{-1280.4}$	$^{+0.080}_{-0.004}$	$^{+6.5}_{-120.4}$	$^{+0.087}_{-9.840}$	...	...		$^{+0.304}_{-0.006}$	$^{+0.292}_{-0.006}$	$^{+0.644}_{-0.013}$
C	-0.949	...	8068.9	-1.615	...	...	...	...	-500.12/1018.80/-512.90	1.704	1.636	3.611
	$^{+0.025}_{-0.024}$	...	$^{+336.8}_{-276.4}$	$^{+0.013}_{-0.019}$	...	...	...	...		$^{+0.069}_{-0.075}$	$^{+0.066}_{-0.072}$	$^{+0.146}_{-0.159}$

TABLE 1. BXA Auto Runs fit results for bn090510016 using GBM + LAT data.

bn090510016 BXA Original Runs GBM + LAT

Model	α	β	E_{peak} (keV)	A_1	kT (keV)	A_2	Γ	A_3	$\log(\mathcal{L})$ / BIC / $\mathcal{Z}$	Flux $\times 10^{-5}$ (erg s^{-1}cm^{-2})	Fluence $\times 10^{-5}$ (erg cm^{-2})	E_{iso} $\times 10^{52}$ (erg)
S+B+L	-0.709	-3.017	2926.5	-1.789	34.2	0.341	-1.521	-2.776	-163.04/375.58/-186.99	1.896	1.821	4.019
	$^{+0.089}_{-0.176}$	$^{+0.010}_{-0.414}$	$^{+673.1}_{-12.2}$	$^{+0.136}_{-0.074}$	$^{+136.7}_{-0.1}$	$^{+2.208}_{-12.924}$	$^{+0.141}_{-0.011}$	$^{+0.160}_{-0.446}$		$^{+0.081}_{-0.123}$	$^{+0.078}_{-0.118}$	$^{+0.172}_{-0.261}$
S+L	-0.828	-3.134	3186.9	-1.691	...	...	-1.490	-2.801	-164.16/365.44/-187.09	1.895	1.819	4.015
	$^{+0.027}_{-0.059}$	$^{+0.135}_{-0.295}$	$^{+399.9}_{-284.6}$	$^{+0.040}_{-0.022}$	...	...	$^{+0.114}_{-0.042}$	$^{+0.177}_{-0.450}$		$^{+0.083}_{-0.128}$	$^{+0.080}_{-0.123}$	$^{+0.176}_{-0.270}$
G+B+L	-0.743	-3.284	3917.1	-1.669	194.4	-2.544	-1.523	-2.652	-164.40/378.29/-188.53	1.779	1.708	3.771
	$^{+0.048}_{-0.057}$	$^{+0.254}_{-0.290}$	$^{+464.6}_{-356.0}$	$^{+0.034}_{-0.033}$	$^{+26.0}_{-158.8}$	$^{+0.241}_{-9.920}$	$^{+0.114}_{-0.025}$	$^{+0.101}_{-0.459}$		$^{+0.068}_{-0.100}$	$^{+0.065}_{-0.096}$	$^{+0.144}_{-0.213}$
G+L	-0.744	-3.205	3895.1	-1.660	...	...	-1.468	-2.878	-164.47/366.06/-188.91	1.787	1.716	3.787
	$^{+0.056}_{-0.058}$	$^{+0.176}_{-0.396}$	$^{+526.9}_{-368.4}$	$^{+0.025}_{-0.045}$	...	...	$^{+0.060}_{-0.084}$	$^{+0.340}_{-0.238}$		$^{+0.066}_{-0.111}$	$^{+0.063}_{-0.106}$	$^{+0.139}_{-0.235}$
C+L	-0.671	...	4012.7	-1.737	...	...	-1.564	-2.382	-170.91/372.76/-192.03	1.854	1.780	3.930
	$^{+0.027}_{-0.120}$	...	$^{+1052.8}_{-213.7}$	$^{+0.058}_{-0.019}$	...	...	$^{+0.056}_{-0.016}$	$^{+0.041}_{-0.210}$		$^{+0.068}_{-0.106}$	$^{+0.065}_{-0.102}$	$^{+0.144}_{-0.225}$
C+B+L	-0.661	...	4344.7	-1.768	31.0	-0.074	-1.549	-2.422	-169.65/382.61/-192.13	1.875	1.800	3.973
	$^{+0.014}_{-0.131}$	...	$^{+699.5}_{-511.5}$	$^{+0.091}_{-0.012}$	$^{+136.9}_{-2.8}$	$^{+2.091}_{-12.539}$	$^{+0.040}_{-0.032}$	$^{+0.079}_{-0.168}$		$^{+0.043}_{-0.126}$	$^{+0.042}_{-0.121}$	$^{+0.092}_{-0.268}$
S+B	-0.752	-2.297	1863.9	-1.670	35.4	0.114	...	...	-199.99/437.09/-217.85	1.301	1.249	2.758
	$^{+0.008}_{-0.096}$	$^{+0.035}_{-0.066}$	$^{+259.5}_{-192.2}$	$^{+0.059}_{-0.020}$	$^{+134.4}_{-1.1}$	$^{+2.349}_{-12.679}$	...	...		$^{+0.104}_{-0.096}$	$^{+0.100}_{-0.093}$	$^{+0.220}_{-0.204}$
S	-0.812	-2.310	1860.4	-1.624	...	...	...	...	-200.35/425.44/-218.42	1.297	1.245	2.748
	$^{+0.052}_{-0.039}$	$^{+0.046}_{-0.054}$	$^{+280.5}_{-183.3}$	$^{+0.013}_{-0.025}$	...	...	...	...		$^{+0.108}_{-0.088}$	$^{+0.104}_{-0.085}$	$^{+0.229}_{-0.187}$
G	-0.694	-2.294	1998.2	-1.590	...	...	...	...	-200.15/425.04/-219.58	1.283	1.231	2.718
	$^{+0.038}_{-0.069}$	$^{+0.037}_{-0.062}$	$^{+421.4}_{-196.1}$	$^{+0.018}_{-0.020}$	...	...	...	...		$^{+0.106}_{-0.081}$	$^{+0.102}_{-0.078}$	$^{+0.226}_{-0.172}$
G+B	-0.676	-2.282	1926.6	-1.603	21.1	-0.216	...	...	-199.78/436.67/-219.96	1.246	1.196	2.641
	$^{+0.020}_{-0.087}$	$^{+0.025}_{-0.074}$	$^{+502.7}_{-139.2}$	$^{+0.031}_{-0.008}$	$^{+149.6}_{-13.6}$	$^{+2.097}_{-12.492}$	...	...		$^{+0.142}_{-0.044}$	$^{+0.137}_{-0.042}$	$^{+0.302}_{-0.092}$

TABLE 2. BXA Original Runs fit results for bn090510016 using GBM + LAT data.

bn090510016 XSPEC/Error Command GBM + LAT

Model	α	β	E_{peak} (keV)	A_1	kT (keV)	A_2	Γ	A_3	C-Stat / $\log(\mathcal{L})$ / AIC / BIC	Flux $\times 10^{-5}$ (erg $s^{-1}cm^{-2}$)	Fluence $\times 10^{-5}$ (erg cm^{-2})	E_{iso} $\times 10^{52}$ (erg)
S+L	-0.845	-3.179	3214.4	-1.679	...	...	-1.475	-2.844	327.86/-163.93/339.86/364.97	1.876	1.801	3.976
	$^{+0.049}_{-0.041}$	$^{+0.185}_{-0.222}$	$^{+803.1}_{-659.0}$	$^{+0.029}_{-0.037}$	...	...	$^{+0.089}_{-0.065}$	$^{+0.249}_{-0.357}$		$^{+0.108}_{-0.108}$	$^{+0.103}_{-0.103}$	$^{+0.228}_{-0.228}$
G+L	-0.739	-3.221	3866.1	-1.670	...	...	-1.506	-2.725	328.45/-164.23/340.45/365.57	1.769	1.698	3.749
	$^{+0.069}_{-0.056}$	$^{+0.207}_{-0.267}$	$^{+816.4}_{-674.7}$	$^{+0.035}_{-0.044}$	...	...	$^{+0.089}_{-0.059}$	$^{+0.225}_{-0.356}$		$^{+0.087}_{-0.087}$	$^{+0.083}_{-0.083}$	$^{+0.184}_{-0.184}$
S+B+L	-0.673	-3.244	3052.6	-1.845	35.5	0.440	-1.540	-2.593	322.83/-161.42/338.83/372.32	1.936	1.858	4.102
	$^{+0.178}_{-0.118}$	$^{+0.189}_{-0.229}$	$^{+932.8}_{-723.6}$	$^{+0.104}_{-0.156}$	$^{+9.5}_{-8.2}$	$^{+0.217}_{-0.305}$	$^{+0.088}_{-0.054}$	$^{+0.200}_{-0.347}$		$^{+0.134}_{-0.134}$	$^{+0.129}_{-0.129}$	$^{+0.284}_{-0.284}$
G+B+L	-0.419	-3.272	3465.5	-1.914	33.6	0.506	-1.574	-2.460	322.86/-161.43/338.86/372.35	1.913	1.837	4.054
	$^{+0.245}_{-0.192}$	$^{+0.193}_{-0.252}$	$^{+1571.4}_{-1079.4}$	$^{+0.133}_{-0.184}$	$^{+7.9}_{-8.1}$	$^{+0.202}_{-0.297}$	$^{+0.066}_{-0.039}$	$^{+0.136}_{-0.258}$		$^{+0.132}_{-0.132}$	$^{+0.127}_{-0.127}$	$^{+0.280}_{-0.280}$
C+L	-0.701	...	4210.6	-1.723	...	...	-1.556	-2.417	341.64/-170.82/351.64/372.57	1.848	1.775	3.917
	$^{+0.077}_{-0.073}$	...	$^{+1198.6}_{-868.7}$	$^{+0.034}_{-0.038}$	...	...	$^{+0.037}_{-0.030}$	$^{+0.103}_{-0.131}$		$^{+0.099}_{-0.099}$	$^{+0.095}_{-0.095}$	$^{+0.209}_{-0.209}$
C+B+L	-0.397	...	3689.4	-1.961	38.2	0.538	-1.584	-2.311	335.30/-167.65/349.30/378.60	1.957	1.878	4.146
	$^{+0.202}_{-0.170}$	...	$^{+1504.3}_{-968.2}$	$^{+0.122}_{-0.154}$	$^{+8.4}_{-7.5}$	$^{+0.167}_{-0.252}$	$^{+0.030}_{-0.024}$	$^{+0.077}_{-0.100}$		$^{+0.130}_{-0.130}$	$^{+0.124}_{-0.124}$	$^{+0.275}_{-0.275}$
G	-0.708	-2.299	2052.3	-1.589	...	...	...	...	400.23/-200.12/408.23/424.98	1.288	1.237	2.730
	$^{+0.057}_{-0.053}$	$^{+0.047}_{-0.052}$	$^{+520.2}_{-418.7}$	$^{+0.019}_{-0.020}$	...	...	...	...		$^{+0.090}_{-0.090}$	$^{+0.086}_{-0.086}$	$^{+0.190}_{-0.190}$
S	-0.806	-2.307	1866.2	-1.628	...	...	...	...	400.59/-200.30/408.59/425.34	1.299	1.247	2.752
	$^{+0.047}_{-0.043}$	$^{+0.048}_{-0.052}$	$^{+517.2}_{-402.9}$	$^{+0.018}_{-0.019}$	...	...	...	...		$^{+0.089}_{-0.089}$	$^{+0.086}_{-0.086}$	$^{+0.189}_{-0.189}$
G+B	-0.527	-2.300	1851.3	-1.667	17.1	0.118	...	...	397.29/-198.65/409.29/434.41	1.321	1.268	2.800
	$^{+0.167}_{-0.130}$	$^{+0.049}_{-0.052}$	$^{+772.0}_{-553.9}$	$^{+0.054}_{-0.070}$	$^{+6.3}_{-4.6}$	$^{+0.235}_{-0.404}$	...	...		$^{+0.094}_{-0.094}$	$^{+0.090}_{-0.090}$	$^{+0.198}_{-0.198}$
S+B	-0.690	-2.311	1802.1	-1.701	21.3	0.110	...	...	398.32/-199.16/410.32/435.44	1.321	1.268	2.799
	$^{+0.133}_{-0.100}$	$^{+0.050}_{-0.052}$	$^{+594.0}_{-443.9}$	$^{+0.055}_{-0.071}$	$^{+12.6}_{-6.8}$	$^{+0.253}_{-0.493}$	...	...		$^{+0.091}_{-0.091}$	$^{+0.087}_{-0.087}$	$^{+0.193}_{-0.193}$
C	-0.949	...	8088.7	-1.617	...	...	...	...	1000.23/-500.12/1006.23/1018.79	1.702	1.634	3.606
	$^{+0.025}_{-0.025}$	...	$^{+649.4}_{-601.8}$	$^{+0.011}_{-0.012}$	...	...	...	...		$^{+0.072}_{-0.072}$	$^{+0.069}_{-0.069}$	$^{+0.153}_{-0.153}$

TABLE 3. XSPEC fit results for bn090510016 using GBM + LAT data and errors from the Error command.