bn100728095 BXA Auto Runs GBM + LAT

Model	α	β	E_{peak} (keV)	A_1	kT (keV)	A_2	Γ	A_3	$\log(\mathcal{L})$ / BIC / $\mathcal{Z}$	Flux $\times 10^{-7}$ (erg s^{-1}cm^{-2})	Fluence $\times 10^{-4}$ (erg cm^{-2})	E_{iso} $\times 10^{53}$ (erg)
S	-0.882	-2.716	258.4	-1.955	...	...	...	...	-190.29/404.23/-211.65	8.567	1.417	9.183
	$^{+0.020}_{-0.019}$	$^{+0.051}_{-0.150}$	$^{+5.5}_{-6.9}$	$^{+0.005}_{-0.005}$	...	...	...	...		$^{+0.119}_{-0.335}$	$^{+0.020}_{-0.055}$	$^{+0.128}_{-0.359}$
S+B	-0.852	-2.767	232.4	-1.955	161.1	-0.036	...	...	-189.15/413.78/-211.70	8.504	1.406	9.116
	$^{+0.010}_{-0.050}$	$^{+0.107}_{-0.099}$	$^{+31.5}_{-18.3}$	$^{+0.004}_{-0.006}$	$^{+10.4}_{-125.7}$	$^{+2.733}_{-11.842}$	...	...		$^{+0.177}_{-0.272}$	$^{+0.029}_{-0.045}$	$^{+0.190}_{-0.291}$
G+B	-0.699	-2.790	299.0	-1.775	36.9	-1.144	...	...	-192.47/420.41/-211.75	8.408	1.391	9.013
	$^{+0.015}_{-0.035}$	$^{+0.053}_{-4.924}$	$^{+20.4}_{-1.7}$	$^{+0.010}_{-0.016}$	$^{+132.4}_{-3.4}$	$^{+2.069}_{-10.881}$	...	...		$^{+0.022}_{-0.951}$	$^{+0.004}_{-0.157}$	$^{+0.023}_{-1.019}$
S+L	-0.886	-2.729	258.1	-1.957	...	...	-0.196	-11.129	-189.27/414.02/-212.18	8.507	1.407	9.119
	$^{+0.024}_{-0.015}$	$^{+0.064}_{-0.130}$	$^{+5.9}_{-6.7}$	$^{+0.006}_{-0.004}$	...	...	$^{+0.479}_{-3.156}$	$^{+3.930}_{-2.562}$		$^{+0.182}_{-0.269}$	$^{+0.030}_{-0.045}$	$^{+0.195}_{-0.288}$
S+B+L	-0.889	-2.921	250.5	-1.960	188.6	-0.266	-0.664	-8.851	-188.94/425.18/-212.21	8.350	1.381	8.951
	$^{+0.028}_{-0.010}$	$^{+0.254}_{-0.068}$	$^{+12.9}_{-0.0}$	$^{+0.009}_{-0.000}$	$^{+17.8}_{-153.1}$	$^{+2.280}_{-11.602}$	$^{+0.010}_{-2.643}$	$^{+1.452}_{-4.942}$		$^{+0.332}_{-0.101}$	$^{+0.055}_{-0.017}$	$^{+0.355}_{-0.108}$
C+B	-0.932	...	411.1	-1.958	41.9	0.012	...	...	-188.34/406.25/-212.96	7.992	1.322	8.567
	$^{+0.210}_{-0.020}$	...	$^{+17.5}_{-95.1}$	$^{+0.173}_{-0.017}$	$^{+51.2}_{-2.9}$	$^{+0.048}_{-7.142}$	...	...		$^{+0.151}_{-0.508}$	$^{+0.025}_{-0.084}$	$^{+0.162}_{-0.545}$
C+B+L	-0.802	...	343.3	-1.864	42.6	-0.221	-1.390	-11.783	-191.10/423.60/-213.58	7.577	1.253	8.122
	$^{+0.105}_{-0.062}$	...	$^{+19.6}_{-35.8}$	$^{+0.089}_{-0.069}$	$^{+124.7}_{-7.9}$	$^{+3.125}_{-11.686}$	$^{+0.618}_{-1.985}$	$^{+4.871}_{-1.672}$		$^{+0.039}_{-0.212}$	$^{+0.006}_{-0.035}$	$^{+0.041}_{-0.228}$
C	-0.716	...	314.1	-1.783	...	...	...	...	-195.86/409.46/-214.36	7.467	1.235	8.003
	$^{+0.020}_{-0.025}$	...	$^{+10.0}_{-7.5}$	$^{+0.010}_{-0.012}$	...	...	...	...		$^{+0.153}_{-0.118}$	$^{+0.025}_{-0.019}$	$^{+0.164}_{-0.126}$
C+L	-0.723	...	318.7	-1.787	...	...	-0.851	-8.097	-194.48/418.53/-214.82	7.549	1.248	8.092
	$^{+0.028}_{-0.017}$	...	$^{+5.3}_{-12.2}$	$^{+0.014}_{-0.008}$	...	...	$^{+0.154}_{-2.482}$	$^{+1.209}_{-5.480}$		$^{+0.072}_{-0.201}$	$^{+0.012}_{-0.033}$	$^{+0.078}_{-0.216}$
G	-0.694	-2.812	298.8	-1.769	...	...	...	...	-192.92/409.49/-215.68	8.401	1.389	9.005
	$^{+0.012}_{-0.039}$	$^{+0.010}_{-4.519}$	$^{+20.0}_{-2.9}$	$^{+0.006}_{-0.021}$	...	...	...	...		$^{+0.007}_{-0.934}$	$^{+0.001}_{-0.154}$	$^{+0.007}_{-1.001}$
G+L	-0.690	-2.922	299.8	-1.768	...	...	-0.350	-10.430	-191.78/419.05/-215.96	8.252	1.365	8.846
	$^{+0.015}_{-0.040}$	$^{+0.110}_{-3.926}$	$^{+18.5}_{-5.3}$	$^{+0.007}_{-0.021}$	...	...	$^{+0.348}_{-3.008}$	$^{+3.946}_{-3.133}$		$^{+0.158}_{-0.756}$	$^{+0.026}_{-0.125}$	$^{+0.170}_{-0.810}$
G+B+L	-0.711	-2.771	301.2	-1.774	32.2	-7.626	0.166	-13.041	-192.21/431.74/-219.12	8.506	1.407	9.118
	$^{+0.018}_{-0.024}$	$^{+0.124}_{-2.750}$	$^{+19.5}_{-0.0}$	$^{+0.004}_{-0.019}$	$^{+83.4}_{-8.2}$	$^{+3.872}_{-3.236}$	$^{+1.869}_{-3.590}$	$^{+5.415}_{-0.091}$		$^{+0.170}_{-0.969}$	$^{+0.028}_{-0.160}$	$^{+0.182}_{-1.038}$

TABLE 1. BXA Auto Runs fit results for bn100728095 using GBM + LAT data.

bn100728095 BXA Original Runs GBM + LAT

Model	α	β	E_{peak} (keV)	A_1	kT (keV)	A_2	Γ	A_3	$\log(\mathcal{L})$ / BIC / $\mathcal{Z}$	Flux $\times 10^{-7}$ (erg s^{-1}cm^{-2})	Fluence $\times 10^{-4}$ (erg cm^{-2})	E_{iso} $\times 10^{53}$ (erg)
S+B	-0.881	-2.728	248.8	-1.960	171.1	-0.282	...	...	-189.51/414.50/-211.82	8.612	1.424	9.231
	$^{+0.019}_{-0.021}$	$^{+0.062}_{-0.140}$	$^{+15.2}_{-2.3}$	$^{+0.009}_{-0.001}$	$^{+0.8}_{-136.2}$	$^{+2.557}_{-11.918}$	...	...		$^{+0.071}_{-0.373}$	$^{+0.012}_{-0.062}$	$^{+0.076}_{-0.400}$
S+B+L	-0.887	-2.783	241.5	-1.959	170.8	-0.118	-2.105	-7.427	-189.07/425.45/-212.06	8.523	1.410	9.136
	$^{+0.025}_{-0.013}$	$^{+0.114}_{-0.079}$	$^{+22.4}_{-9.3}$	$^{+0.008}_{-0.002}$	$^{+1.4}_{-136.5}$	$^{+2.858}_{-11.748}$	$^{+1.404}_{-1.242}$	$^{+0.073}_{-6.263}$		$^{+0.156}_{-0.287}$	$^{+0.026}_{-0.048}$	$^{+0.167}_{-0.308}$
S	-0.880	-2.734	256.5	-1.954	...	...	...	...	-190.29/404.23/-212.67	8.497	1.405	9.108
	$^{+0.019}_{-0.022}$	$^{+0.075}_{-0.128}$	$^{+7.7}_{-5.0}$	$^{+0.003}_{-0.006}$	...	...	...	...		$^{+0.194}_{-0.264}$	$^{+0.032}_{-0.044}$	$^{+0.208}_{-0.283}$
S+L	-0.881	-2.694	257.3	-1.955	...	...	0.557	-14.972	-189.34/414.16/-213.55	8.580	1.419	9.197
	$^{+0.020}_{-0.020}$	$^{+0.030}_{-0.166}$	$^{+6.7}_{-6.0}$	$^{+0.004}_{-0.005}$	...	...	$^{+1.154}_{-3.901}$	$^{+7.737}_{-1.250}$		$^{+0.101}_{-0.340}$	$^{+0.017}_{-0.056}$	$^{+0.108}_{-0.364}$
C	-0.717	...	314.4	-1.784	...	...	...	...	-195.87/409.47/-214.37	7.464	1.234	8.000
	$^{+0.020}_{-0.025}$	...	$^{+10.0}_{-7.1}$	$^{+0.010}_{-0.012}$	...	...	...	...		$^{+0.155}_{-0.107}$	$^{+0.026}_{-0.018}$	$^{+0.166}_{-0.115}$
C+B	-0.739	...	327.7	-1.807	41.2	-0.836	...	...	-194.62/418.81/-214.74	7.623	1.261	8.171
	$^{+0.043}_{-0.000}$	...	$^{+4.0}_{-21.4}$	$^{+0.034}_{-0.012}$	$^{+128.4}_{-8.7}$	$^{+2.379}_{-11.337}$	...	...		$^{+0.009}_{-0.278}$	$^{+0.002}_{-0.046}$	$^{+0.010}_{-0.298}$
C+L	-0.714	...	312.2	-1.781	...	...	-1.034	-7.408	-194.42/418.40/-214.88	7.434	1.229	7.968
	$^{+0.020}_{-0.027}$	...	$^{+11.8}_{-5.4}$	$^{+0.008}_{-0.014}$	...	...	$^{+0.434}_{-2.323}$	$^{+0.539}_{-6.316}$		$^{+0.184}_{-0.083}$	$^{+0.030}_{-0.014}$	$^{+0.197}_{-0.089}$
C+B+L	-0.710	...	311.6	-1.780	63.0	-3.331	-1.178	-6.756	-194.49/430.38/-215.29	7.430	1.229	7.964
	$^{+0.013}_{-0.029}$	...	$^{+12.3}_{-4.7}$	$^{+0.006}_{-0.015}$	$^{+104.2}_{-24.2}$	$^{+0.015}_{-8.614}$	$^{+0.507}_{-2.124}$	$^{+0.157}_{-6.785}$		$^{+0.186}_{-0.073}$	$^{+0.031}_{-0.012}$	$^{+0.199}_{-0.078}$
G	-0.692	-2.836	298.2	-1.768	...	...	...	...	-192.91/409.47/-215.69	8.356	1.382	8.957
	$^{+0.012}_{-0.041}$	$^{+0.029}_{-4.253}$	$^{+20.5}_{-2.9}$	$^{+0.005}_{-0.022}$	...	...	...	...		$^{+0.063}_{-0.877}$	$^{+0.010}_{-0.145}$	$^{+0.067}_{-0.940}$
G+B (v1)	-0.863	-4.387	365.8	-1.917	46.7	0.019	...	...	-192.74/420.96/-215.96	7.798	1.290	8.359
	$^{+0.181}_{-0.131}$	$^{+1.570}_{-2.969}$	$^{+47.3}_{-70.0}$	$^{+0.153}_{-0.126}$	$^{+120.0}_{-13.8}$	$^{+3.135}_{-11.987}$	...	...		$^{+0.617}_{-0.333}$	$^{+0.102}_{-0.055}$	$^{+0.662}_{-0.356}$
G+B (v2)	-0.711	-2.979	309.6	-1.787	41.0	-0.962	...	...	-192.79/421.06/-216.07	8.278	1.369	8.874
	$^{+0.023}_{-0.022}$	$^{+0.132}_{-4.463}$	$^{+9.3}_{-11.3}$	$^{+0.019}_{-0.004}$	$^{+121.6}_{-5.6}$	$^{+2.341}_{-11.003}$	...	...		$^{+0.113}_{-0.806}$	$^{+0.019}_{-0.133}$	$^{+0.121}_{-0.864}$
G+L	-0.643	-2.769	288.1	-1.754	...	...	-2.711	-4.423	-191.78/419.05/-216.21	8.390	1.387	8.993
	$^{+0.036}_{-0.086}$	$^{+0.037}_{-4.350}$	$^{+29.9}_{-6.9}$	$^{+0.008}_{-0.035}$	...	...	$^{+1.996}_{-0.664}$	$^{+2.322}_{-9.235}$		$^{+0.033}_{-0.919}$	$^{+0.005}_{-0.152}$	$^{+0.035}_{-0.985}$
G+B+L	-0.687	-2.804	295.2	-1.766	135.8	-7.877	-0.091	-11.843	-191.87/431.05/-216.66	8.347	1.380	8.947
	$^{+0.004}_{-0.045}$	$^{+0.027}_{-4.531}$	$^{+23.4}_{-1.1}$	$^{+0.001}_{-0.024}$	$^{+29.1}_{-98.3}$	$^{+4.486}_{-3.877}$	$^{+0.685}_{-3.223}$	$^{+4.788}_{-1.697}$		$^{+0.061}_{-0.868}$	$^{+0.010}_{-0.144}$	$^{+0.065}_{-0.930}$

TABLE 2. BXA Original Runs fit results for bn100728095 using GBM + LAT data.

bn100728095 XSPEC/Error Command GBM + LAT

Model	α	β	E_{peak} (keV)	A_1	kT (keV)	A_2	Γ	A_3	C-Stat / $\log(\mathcal{L})$ / AIC / BIC	Flux $\times 10^{-7}$ (erg $s^{-1}cm^{-2}$)	Fluence $\times 10^{-4}$ (erg cm^{-2})	E_{iso} $\times 10^{53}$ (erg)
S	-0.879	-2.723	257.1	-1.955	...	...	...	...	380.52/-190.26/388.52/404.17	8.526	1.410	9.139
	+0.020	+0.079	+28.0	+0.005						+0.241	+0.040	+0.258
	−0.020	−0.103	−25.4	−0.005	...	...	...	...		−0.241	−0.040	−0.258
C+B	-0.923	...	409.5	-1.954	41.8	0.004	...	...	376.52/-188.26/386.52/406.09	8.005	1.324	8.580
	+0.056		+88.3	+0.040	+2.8	+0.096				+0.244	+0.040	+0.261
	−0.056	...	−69.4	−0.041	−2.8	−0.127	...	...		−0.244	−0.040	−0.261
G	-0.693	-2.815	298.1	-1.768	...	...	...	...	385.79/-192.89/393.79/409.44	8.395	1.388	8.999
	+0.026	+0.127	+21.7	+0.013						+0.279	+0.046	+0.299
	−0.025	−0.230	−19.9	−0.013	...	...	...	...		−0.279	−0.046	−0.299
C	-0.718	...	314.8	-1.784	...	...	...	...	391.71/-195.86/397.71/409.45	7.477	1.236	8.014
	+0.023		+19.8	+0.009						+0.132	+0.022	+0.142
	−0.022	...	−18.4	−0.009	...	...	...	...		−0.132	−0.022	−0.142
S+B	-1.040	-3.051	346.0	-2.074	35.2	-0.059	...	...	375.44/-187.72/387.44/410.92	8.446	1.397	9.053
	+0.067	+0.260	+156.0	+0.047	+2.6	+0.129				+0.378	+0.062	+0.405
	−0.056	−0.534	−110.3	−0.039	−3.3	−0.223	...	...		−0.378	−0.062	−0.405
G+B (v2)	-0.911	-3.178	396.4	-1.944	41.9	-0.012	...	...	375.78/-187.89/387.78/411.27	8.360	1.383	8.961
	+0.062	+0.392	+90.0	+0.048	+3.0	+0.101				+0.434	+0.072	+0.466
	−0.057	$-NA$	−74.1	−0.044	−2.9	−0.139	...	...		−0.434	−0.072	−0.466
S+L	-0.880	-2.737	257.1	-1.955	...	...	-0.568	-9.526	378.14/-189.07/390.14/413.62	8.497	1.405	9.108
	$+NA$	$+NA$	$+NA$	$+NA$			$+NA$	$+NA$		+0.261	+0.043	+0.279
	$-NA$	$-NA$	$-NA$	$-NA$	...	...	$-NA$	$-NA$		−0.261	−0.043	−0.279
C+B+L	-0.923	...	409.5	-1.954	41.8	0.004	-0.863	-8.096	373.45/-186.72/387.45/414.84	8.005	1.324	8.580
	+0.056		+88.3	+0.040	+2.8	+0.096	+0.392	+2.773		+0.244	+0.040	+0.261
	−0.056	...	−69.4	−0.041	−2.8	−0.127	−0.686	$-NA$		−0.244	−0.040	−0.261
G+B (v1)	-0.586	-2.746	280.7	-1.737	4.3	-1.150	...	...	380.23/-190.11/392.23/415.71	8.355	1.382	8.956
	+0.061	+0.101	+36.1	+0.021	+1.0	+0.164				$+NA$	$+NA$	$+NA$
	−0.056	−0.153	−31.9	−0.020	−1.0	−0.239	...	...		$-NA$	$-NA$	$-NA$
G+L	-0.592	-2.776	285.5	-1.749	...	...	-2.210	-3.782	382.56/-191.28/394.56/418.04	8.383	1.386	8.986
	+0.064	+0.113	+39.7	+0.018			+0.329	+0.271		+0.352	+0.058	+0.378
	−0.069	−0.221	−34.0	−0.019	...	...	−1.085	−1.250		−0.352	−0.058	−0.378
C+L	-0.718	...	314.8	-1.784	...	...	-0.454	-10.000	388.84/-194.42/398.84/418.41	7.477	1.236	8.014
	+0.001		+3.3	+0.000			+0.065	+5.204		+0.132	+0.022	+0.142
	−0.001	...	−3.3	−0.000	...	...	−0.111	$-NA$		−0.132	−0.022	−0.142
S+B+L	-1.045	-3.120	349.8	-2.078	35.3	-0.046	-0.891	-7.988	372.54/-186.27/388.54/419.85	8.389	1.387	8.992
	+0.065	+0.241	+110.9	+0.046	+2.6	+0.123	+0.327	+2.424		+0.413	+0.068	+0.443
	−0.054	−0.529	−116.5	−0.037	−3.2	−0.211	−0.600	$-NA$		−0.413	−0.068	−0.443
G+B+L	-0.911	-3.285	397.5	-1.945	41.9	-0.011	-0.865	-8.105	372.79/-186.40/388.79/420.10	8.300	1.373	8.897
	+0.060	+0.437	+90.6	+0.047	+2.9	+0.101	+0.385	+2.667		+0.403	+0.067	+0.432
	−0.058	$-NA$	−71.4	−0.044	−2.9	−0.137	−0.655	$-NA$		−0.403	−0.067	−0.432

TABLE 3. XSPEC fit results for bn100728095 using GBM + LAT data and errors from the Error command.