bn131108862 BXA Auto Runs GBM + LAT

Model	α	β	E_{peak} (keV)	A_1	kT (keV)	A_2	Γ	A_3	$\log(\mathcal{L})$ / BIC / $\mathcal{Z}$	Flux $\times 10^{-6}$ (erg s^{-1}cm^{-2})	Fluence $\times 10^{-5}$ (erg cm^{-2})	E_{iso} $\times 10^{53}$ (erg)
S+B	-1.039	-2.181	314.6	-1.638	80.4	0.293	...	...	-172.64/382.40/-196.89	2.246	4.155	5.834
	$^{+0.070}_{-0.025}$	$^{+0.008}_{-0.032}$	$^{+33.4}_{-7.9}$	$^{+0.037}_{-0.025}$	$^{+86.8}_{-46.1}$	$^{+2.589}_{-12.151}$	...	...		$^{+0.140}_{-0.070}$	$^{+0.260}_{-0.130}$	$^{+0.365}_{-0.182}$
S	-0.992	-2.202	337.2	-1.607	...	...	...	...	-174.39/373.53/-197.33	2.360	4.365	6.129
	$^{+0.023}_{-0.022}$	$^{+0.012}_{-0.012}$	$^{+10.9}_{-13.3}$	$^{+0.006}_{-0.006}$	...	...	...	...		$^{+0.027}_{-0.042}$	$^{+0.050}_{-0.078}$	$^{+0.070}_{-0.110}$
S+L	-0.975	-2.205	327.6	-1.608	...	...	-1.834	-3.747	-174.11/385.33/-197.62	2.338	4.324	6.071
	$^{+0.007}_{-0.037}$	$^{+0.015}_{-0.008}$	$^{+20.3}_{-3.3}$	$^{+0.006}_{-0.005}$	...	...	$^{+1.080}_{-1.567}$	$^{+2.836}_{-9.945}$		$^{+0.049}_{-0.018}$	$^{+0.090}_{-0.033}$	$^{+0.127}_{-0.047}$
S+B+L	-1.001	-2.165	313.9	-1.627	92.3	0.278	-3.445	-11.339	-172.43/394.35/-198.04	2.287	4.230	5.939
	$^{+0.034}_{-0.013}$	$^{+0.024}_{-0.048}$	$^{+33.8}_{-9.5}$	$^{+0.026}_{-0.015}$	$^{+74.3}_{-56.8}$	$^{+2.933}_{-12.114}$	$^{+2.760}_{-0.118}$	$^{+4.914}_{-2.324}$		$^{+0.101}_{-0.030}$	$^{+0.186}_{-0.056}$	$^{+0.261}_{-0.079}$
G+B	-1.042	-2.176	416.5	-1.603	48.7	0.365	...	...	-172.48/382.08/-201.67	2.255	4.171	5.857
	$^{+0.209}_{-0.123}$	$^{+0.002}_{-0.030}$	$^{+59.0}_{-101.0}$	$^{+0.154}_{-0.103}$	$^{+110.3}_{-8.0}$	$^{+0.240}_{-11.574}$	...	...		$^{+0.115}_{-0.023}$	$^{+0.212}_{-0.043}$	$^{+0.298}_{-0.061}$
G	-0.859	-2.195	331.1	-1.462	...	...	...	...	-176.74/378.22/-202.04	2.333	4.316	6.059
	$^{+0.030}_{-0.026}$	$^{+0.011}_{-0.013}$	$^{+17.3}_{-15.2}$	$^{+0.015}_{-0.014}$	...	...	...	...		$^{+0.042}_{-0.032}$	$^{+0.078}_{-0.059}$	$^{+0.110}_{-0.082}$
G+L	-0.710	-2.192	302.2	-1.433	...	...	-2.370	-3.299	-174.19/385.50/-202.27	2.318	4.288	6.020
	$^{+0.104}_{-0.173}$	$^{+0.008}_{-0.014}$	$^{+44.8}_{-10.6}$	$^{+0.009}_{-0.042}$	...	...	$^{+1.481}_{-1.033}$	$^{+1.500}_{-10.088}$		$^{+0.057}_{-0.013}$	$^{+0.106}_{-0.025}$	$^{+0.149}_{-0.034}$
G+B+L	-0.778	-2.193	308.3	-1.440	97.1	-0.614	-2.575	-3.790	-174.35/398.18/-202.40	2.323	4.297	6.033
	$^{+0.050}_{-0.107}$	$^{+0.008}_{-0.014}$	$^{+39.0}_{-8.6}$	$^{+0.007}_{-0.035}$	$^{+70.0}_{-60.1}$	$^{+2.445}_{-11.217}$	$^{+1.744}_{-0.779}$	$^{+2.109}_{-9.704}$		$^{+0.049}_{-0.017}$	$^{+0.091}_{-0.031}$	$^{+0.128}_{-0.044}$
C+L	-0.551	...	322.6	-1.477	...	...	-1.786	-2.494	-193.35/417.63/-220.97	1.887	3.490	4.901
	$^{+0.038}_{-0.098}$	...	$^{+20.1}_{-7.9}$	$^{+0.012}_{-0.021}$	...	...	$^{+0.023}_{-0.010}$	$^{+0.031}_{-0.069}$		$^{+0.059}_{-0.023}$	$^{+0.110}_{-0.043}$	$^{+0.154}_{-0.061}$
C+B+L	-0.569	...	326.1	-1.480	44.7	-12.050	-1.784	-2.499	-193.28/429.86/-221.10	1.903	3.520	4.942
	$^{+0.059}_{-0.080}$	...	$^{+17.7}_{-11.0}$	$^{+0.014}_{-0.020}$	$^{+123.4}_{-10.6}$	$^{+9.192}_{-0.191}$	$^{+0.022}_{-0.012}$	$^{+0.037}_{-0.066}$		$^{+0.045}_{-0.035}$	$^{+0.083}_{-0.064}$	$^{+0.116}_{-0.090}$
C+B	-1.350	...	6500.2	-1.869	41.6	0.656	...	...	-868.56/1768.06/-896.67	3.028	5.600	7.862
	$^{+0.010}_{-0.008}$	...	$^{+88.7}_{-99.3}$	$^{+0.010}_{-0.007}$	$^{+1.3}_{-1.2}$	$^{+0.022}_{-0.017}$	...	...		$^{+0.067}_{-0.036}$	$^{+0.124}_{-0.067}$	$^{+0.174}_{-0.094}$
C	-1.351	...	6484.4	-1.713	...	...	...	...	-1173.98/2366.51/-1192.34	3.784	6.998	9.825
	$^{+0.007}_{-0.004}$	...	$^{+44.0}_{-68.3}$	$^{+0.003}_{-0.004}$	...	...	...	...		$^{+0.049}_{-0.037}$	$^{+0.090}_{-0.069}$	$^{+0.127}_{-0.097}$

TABLE 1. BXA Auto Runs fit results for bn131108862 using GBM + LAT data.

bn131108862 BXA Original Runs GBM + LAT

Model	α	β	E_{peak} (keV)	A_1	kT (keV)	A_2	Γ	A_3	$\log(\mathcal{L})$ / BIC / $\mathcal{Z}$	Flux $\times 10^{-6}$ (erg s^{-1}cm^{-2})	Fluence $\times 10^{-5}$ (erg cm^{-2})	E_{iso} $\times 10^{53}$ (erg)
S+B (v1)	-1.004 $^{+0.034}_{-0.013}$	-2.149 $^{+0.038}_{-0.064}$	294.2 $^{+54.5}_{-27.6}$	-1.640 $^{+0.039}_{-0.025}$	81.5 $^{+84.6}_{-43.6}$	0.438 $^{+2.161}_{-12.294}$	... ...	... ...	-171.66/380.43/-197.68	2.214 $^{+0.173}_{-0.096}$	4.094 $^{+0.321}_{-0.177}$	5.748 $^{+0.450}_{-0.248}$
S+B (v2)	-1.029 $^{+0.061}_{-0.015}$	-2.180 $^{+0.010}_{-0.034}$	326.4 $^{+21.6}_{-2.7}$	-1.630 $^{+0.029}_{-0.017}$	97.0 $^{+73.1}_{-62.8}$	0.163 $^{+2.788}_{-12.245}$	... ...	... ...	-174.12/385.35/-197.76	2.294 $^{+0.093}_{-0.023}$	4.243 $^{+0.173}_{-0.043}$	5.958 $^{+0.243}_{-0.060}$
S	-0.990 $^{+0.022}_{-0.022}$	-2.205 $^{+0.015}_{-0.009}$	334.7 $^{+13.4}_{-11.2}$	-1.606 $^{+0.005}_{-0.006}$	... ...	... ...	... ...	... ...	-174.42/373.59/-198.36	2.353 $^{+0.036}_{-0.036}$	4.352 $^{+0.066}_{-0.067}$	6.110 $^{+0.093}_{-0.094}$
S+B+L	-0.967 $^{+0.000}_{-0.046}$	-2.197 $^{+0.007}_{-0.016}$	327.8 $^{+19.9}_{-4.2}$	-1.607 $^{+0.005}_{-0.006}$	79.0 $^{+90.2}_{-40.8}$	-1.079 $^{+1.487}_{-10.941}$	-3.133 $^{+2.360}_{-0.243}$	-4.772 $^{+1.663}_{-8.935}$	-173.82/397.13/-198.50	2.341 $^{+0.048}_{-0.022}$	4.329 $^{+0.089}_{-0.041}$	6.079 $^{+0.126}_{-0.057}$
S+L	-0.946 $^{+0.022}_{-0.067}$	-2.198 $^{+0.007}_{-0.016}$	326.1 $^{+22.5}_{-2.6}$	-1.605 $^{+0.005}_{-0.007}$	... ...	... ...	-2.793 $^{+2.080}_{-0.558}$	-4.187 $^{+2.253}_{-9.567}$	-173.74/384.59/-199.06	2.347 $^{+0.041}_{-0.029}$	4.340 $^{+0.077}_{-0.053}$	6.094 $^{+0.107}_{-0.075}$
G+B (v2)	-0.977 $^{+0.144}_{-0.077}$	-2.167 $^{+0.011}_{-0.039}$	344.1 $^{+4.0}_{-29.8}$	-1.541 $^{+0.094}_{-0.057}$	59.1 $^{+103.3}_{-18.9}$	0.321 $^{+0.922}_{-11.864}$	... ...	... ...	-172.80/382.71/-201.79	2.226 $^{+0.146}_{-0.059}$	4.117 $^{+0.270}_{-0.110}$	5.780 $^{+0.380}_{-0.154}$
G	-0.860 $^{+0.028}_{-0.026}$	-2.195 $^{+0.010}_{-0.013}$	330.8 $^{+18.2}_{-14.0}$	-1.460 $^{+0.013}_{-0.016}$	... ...	... ...	... ...	... ...	-176.75/378.25/-202.00	2.338 $^{+0.039}_{-0.035}$	4.325 $^{+0.072}_{-0.065}$	6.072 $^{+0.101}_{-0.092}$
G+B (v1)	-0.977 $^{+0.146}_{-0.085}$	-2.163 $^{+0.019}_{-0.043}$	342.7 $^{+7.9}_{-27.6}$	-1.541 $^{+0.094}_{-0.060}$	57.1 $^{+108.3}_{-21.4}$	0.328 $^{+1.938}_{-12.021}$	... ...	... ...	-173.04/383.20/-202.14	2.230 $^{+0.146}_{-0.068}$	4.124 $^{+0.270}_{-0.125}$	5.790 $^{+0.379}_{-0.176}$
G+B+L	-0.888 $^{+0.062}_{-0.003}$	-2.141 $^{+0.043}_{-0.067}$	288.6 $^{+59.4}_{-26.5}$	-1.478 $^{+0.032}_{-0.002}$	77.9 $^{+88.7}_{-43.9}$	0.348 $^{+3.143}_{-12.196}$	-2.039 $^{+1.207}_{-1.348}$	-12.095 $^{+6.308}_{-1.506}$	-174.41/398.31/-202.57	2.226 $^{+0.149}_{-0.077}$	4.117 $^{+0.276}_{-0.143}$	5.781 $^{+0.388}_{-0.200}$
G+L	-0.716 $^{+0.095}_{-0.167}$	-2.191 $^{+0.008}_{-0.017}$	308.5 $^{+39.1}_{-2.3}$	-1.440 $^{+0.001}_{-0.035}$	... ...	... ...	-2.232 $^{+1.303}_{-1.176}$	-3.231 $^{+1.450}_{-10.158}$	-173.92/384.96/-202.58	2.334 $^{+0.042}_{-0.033}$	4.317 $^{+0.078}_{-0.060}$	6.061 $^{+0.109}_{-0.084}$
C+L	-0.589 $^{+0.083}_{-0.055}$	... ...	330.6 $^{+12.0}_{-15.7}$	-1.485 $^{+0.019}_{-0.014}$	... ...	... ...	-1.777 $^{+0.014}_{-0.020}$	-2.518 $^{+0.058}_{-0.044}$	-193.35/417.64/-220.97	1.909 $^{+0.039}_{-0.044}$	3.531 $^{+0.072}_{-0.082}$	4.957 $^{+0.101}_{-0.115}$
C+B+L	-0.578 $^{+0.068}_{-0.073}$	... ...	330.2 $^{+13.6}_{-15.2}$	-1.490 $^{+0.024}_{-0.009}$	27.4 $^{+144.1}_{-7.7}$	-0.890 $^{+1.862}_{-11.153}$	-1.777 $^{+0.014}_{-0.020}$	-2.503 $^{+0.042}_{-0.062}$	-192.77/428.84/-221.07	1.907 $^{+0.042}_{-0.039}$	3.527 $^{+0.077}_{-0.073}$	4.952 $^{+0.109}_{-0.102}$

TABLE 2. BXA Original Runs fit results for bn131108862 using GBM + LAT data.

bn131108862 XSPEC/Error Command GBM + LAT

Model	α	β	E_{peak} (keV)	A_1	kT (keV)	A_2	Γ	A_3	C-Stat / log($\mathcal{L}$) / AIC / BIC	Flux $\times 10^{-6}$ (erg s^{-1}cm^{-2})	Fluence $\times 10^{-5}$ (erg cm^{-2})	E_{iso} $\times 10^{53}$ (erg)
S	-0.991	-2.201	335.0	-1.606	...	...	...	...	348.72/-174.36/356.72/373.46	2.351	4.349	6.106
	+0.023	+0.011	+27.3	+0.006						+0.036	+0.066	+0.092
	−0.022	−0.012	−24.7	−0.006	...	...	...	...		−0.036	−0.066	−0.092
G	-0.856	-2.195	330.4	-1.460	...	...	...	...	353.44/-176.72/361.44/378.19	2.336	4.321	6.067
	+0.029	+0.012	+33.5	+0.015						+0.038	+0.070	+0.099
	−0.028	−0.012	−29.8	−0.015	...	...	...	...		−0.038	−0.070	−0.099
S+B (v2)	-1.032	-2.141	292.7	-1.654	82.9	0.527	...	...	342.08/-171.04/354.08/379.20	2.196	4.061	5.702
	+0.034	+0.026	+76.3	+0.020	+9.8	+0.137				+0.074	+0.137	+0.192
	−0.035	−0.028	−57.9	−0.022	−10.6	−0.231	...	...		−0.074	−0.137	−0.192
S+B (v1)	-0.856	-2.194	311.1	-1.600	5.3	-0.570	...	...	344.46/-172.23/356.46/381.57	2.318	4.288	6.020
	+0.087	+0.012	+41.9	+0.007	+1.1	+0.190				+0.037	+0.068	+0.096
	−0.075	−0.012	−36.1	−0.007	−1.1	−0.302	...	...		−0.037	−0.068	−0.096
G+B (v2)	-1.022	-2.178	403.3	-1.585	49.8	0.327	...	...	344.46/-172.23/356.46/381.57	2.274	4.206	5.906
	+0.074	+0.020	+142.5	+0.059	+12.6	+0.118				+0.059	+0.109	+0.153
	−0.066	−0.018	−111.9	−0.052	−5.7	−0.170	...	...		−0.059	−0.109	−0.153
G+B (v1)	-0.665	-2.186	287.0	-1.403	4.7	-0.505	...	...	344.63/-172.32/356.63/381.75	2.291	4.237	5.949
	+0.087	+0.012	+59.6	+0.031	+0.8	+0.133				+0.038	+0.070	+0.098
	−0.080	−0.012	−48.6	−0.028	−0.8	−0.187	...	...		−0.038	−0.070	−0.098
S+L	-0.859	-2.239	309.5	-1.628	...	...	-1.871	-2.869	345.73/-172.87/357.73/382.85	2.322	4.296	6.031
	+0.097	+0.044	+60.0	+0.008			+0.087	+0.175		+0.042	+0.077	+0.108
	−0.090	−0.045	−47.7	−0.013	...	...	−0.290	−0.357		−0.042	−0.077	−0.108
G+L	-0.620	-2.233	295.7	-1.437	...	...	-1.897	-2.746	346.22/-173.11/358.22/383.34	2.300	4.255	5.973
	+0.107	+0.048	+67.3	+0.028			+0.062	+0.125		+0.043	+0.079	+0.111
	−0.097	−0.051	−55.0	−0.023	...	...	−0.281	−0.351		−0.043	−0.079	−0.111
S+B+L	-0.720	-2.220	296.2	-1.622	7.0	-0.568	-1.897	-2.919	343.36/-171.68/359.36/392.85	2.306	4.265	5.988
	$+NA$	$+NA$	$+NA$	$+NA$	$+NA$	$+NA$	$+NA$	$+NA$		+0.096	+0.178	+0.250
	$-NA$	$-NA$	$-NA$	$-NA$	$-NA$	$-NA$	$-NA$	$-NA$		−0.096	−0.178	−0.250
G+B+L	-0.595	-2.214	284.9	-1.409	5.5	-0.652	-1.876	-3.002	343.81/-171.90/359.81/393.30	2.287	4.230	5.939
	$+NA$	$+NA$	$+NA$	$+NA$	$+NA$	$+NA$	$+NA$	$+NA$		+0.121	+0.224	+0.314
	$-NA$	$-NA$	$-NA$	$-NA$	$-NA$	$-NA$	$-NA$	$-NA$		−0.121	−0.224	−0.314
C+L	-0.570	...	326.7	-1.481	...	...	-1.783	-2.501	386.50/-193.25/396.50/417.44	1.902	3.517	4.939
	+0.073		+47.8	+0.009			+0.018	+0.046		+0.043	+0.080	+0.113
	−0.068	...	−41.2	−0.012	...	...	−0.016	−0.054		−0.043	−0.080	−0.113
C+B+L	-0.551	...	394.5	-1.621	30.9	0.130	-1.808	-2.425	377.59/-188.80/391.59/420.90	2.003	3.704	5.201
	+0.163		+124.7	+0.014	+2.5	+0.141	+0.018	+0.051		+0.065	+0.121	+0.170
	−0.123	...	−88.5	−0.001	−4.5	−0.195	−0.017	−0.055		−0.065	−0.121	−0.170
C+B	-1.046	...	480.2	-1.607	45.3	0.287	...	...	2386.48/-1193.24/2396.48/2417.41	2.047	3.786	5.315
	+0.061		+143.4	+0.043	+5.3	+0.133				+0.087	+0.160	+0.225
	−0.060	...	−102.6	−0.044	−4.6	−0.199	...	...		−0.087	−0.160	−0.225

TABLE 3. XSPEC fit results for bn131108862 using GBM + LAT data and errors from the Error command.