# Predictive Model for Automotive Fan Performance using Thin Airfoil Theory: Update Meeting

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## **Challenges**

- Implementation of body forces in new CFD packages
- Need to account for losses through fan to predict flow rate accurately simple loss model must be added to Hall et al. approach
- Model may need modification for low blade counts typically found in automotive fans

# Focus of Last Meeting: 2D Basic Body Force in OpenFOAM

Major Activity	Mo 1	Mo 2	Mo 3	N	o 4	Mo 5	Mo 6	Mo 7	Mo 8	Mo 9
Build simple grids for testing body force model (OpenFOAM)										
Implement body force model into OpenFOAM, including debugging for simple flat plate blades where solution can be analytically estimated										
Build model of fan test facility with fan of interest (body force model – OpenFOAM; model with fan blades – OpenFOAM and StarCCM+)										
Implement simple loss model for fan based on local deviation (body force)										
Verify model performance in OpenFOAM by comparing results for fans previously modelled within the applicant's research group using other software										
Carry out simulations for fan of interest (body force model + model with fan blades) and compare to existing experimental data (OpenFOAM and StarCCM+)										

# OF Impl. Completed & Validated, Fan Test Model Ready

				Past •			Future		
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# BF + Bladed CFD Starting Soon, Loss Model Work Moved Back

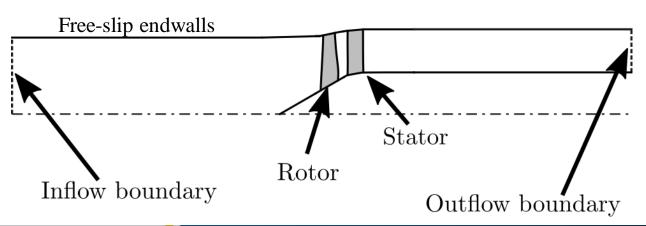
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## Key Messages

- Implementation of body force model for 3D applications in OpenFOAM complete
- Model validated with results from Ansys CFX
- Computational domain for the Pacifica fan test complete ready to move on to body force and bladed CFD

## Whittle Fan - Test Case to Assess 3D Model Implementation

- Same low-speed fan modelled by Hall et al. (2017), Defoe et al. (2018)
- Experimental facility at the Whittle Lab, U. of Cambridge relevant publications 2014-2017
- Ansys CFX results available for design flow coefficier  $\ \phi = \frac{m}{\bar{\rho}^M A_1 U_{mid}} = 0.50$



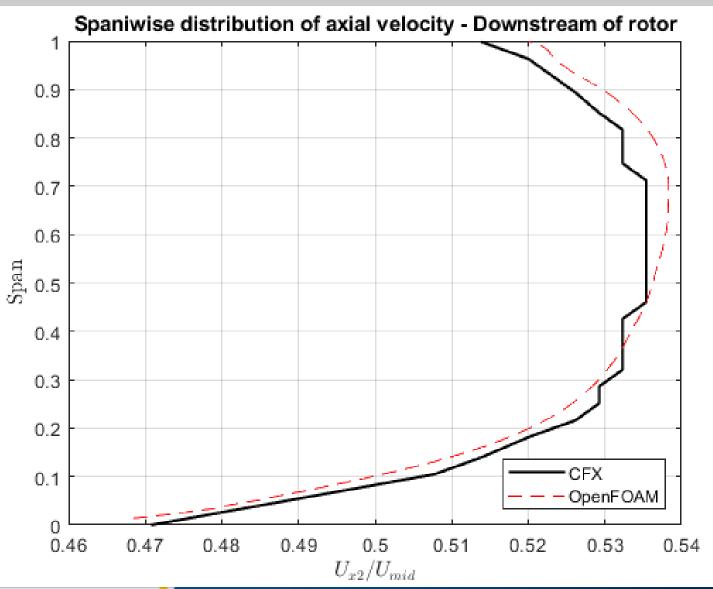
## CFD Cases Similar but not Identical

- CFX: compressible (but Mach<0.3 everywhere)</li>
  - Inlet: total pressure/temperature/velocity direction
  - Outlet: static pressure set to yield desired mass flow rate
- OpenFOAM: incompressible
  - Inlet: velocity inlet (sets volume flow)
  - Outlet: static pressure (sets total pressure level)

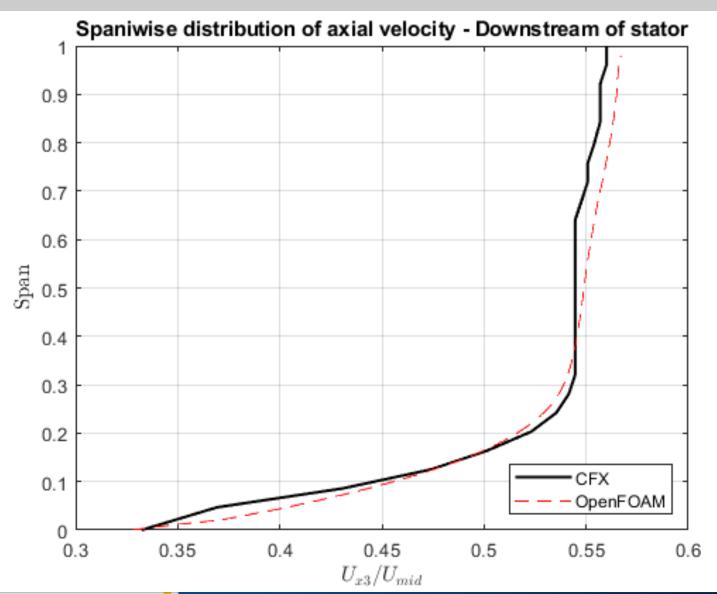
## CFD Solvers Work Differently – Leads to Differing Grids

- CFX is a node-centered code: data is stored at the corners of cells
- OpenFOAM is a cell-centered code: data is stored at cell centres
- Means that grid-independent solutions may not be the same, and may occur on different grids
- CFX results confirmed to be grid-independent for OVERALL STAGE performance
- OpenFOAM results checked for convergence of radial profiles
- Led to a grid 9X finer than that used in CFX

## Mass Flow Distributions Similar at Rotor Exit

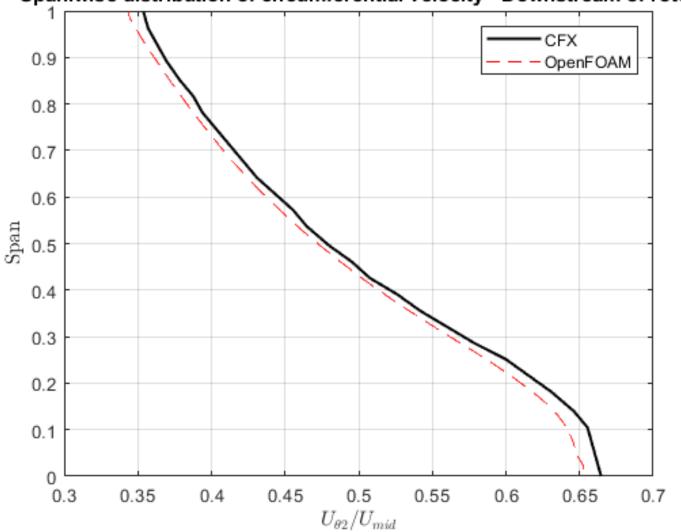


## Mass Flow Distributions Similar at Stator Exit



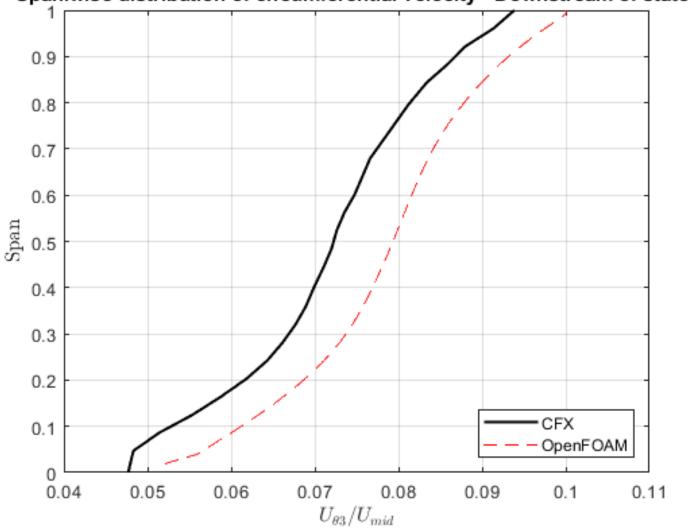
## OF Predicts Slightly Lower Flow Turning at Rotor Exit





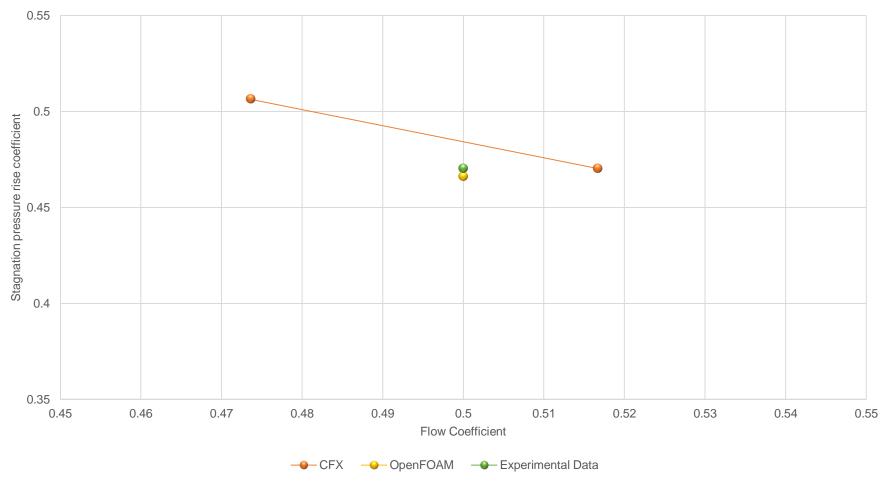
# OF Stator Again Eliminates Less Swirl than CFX



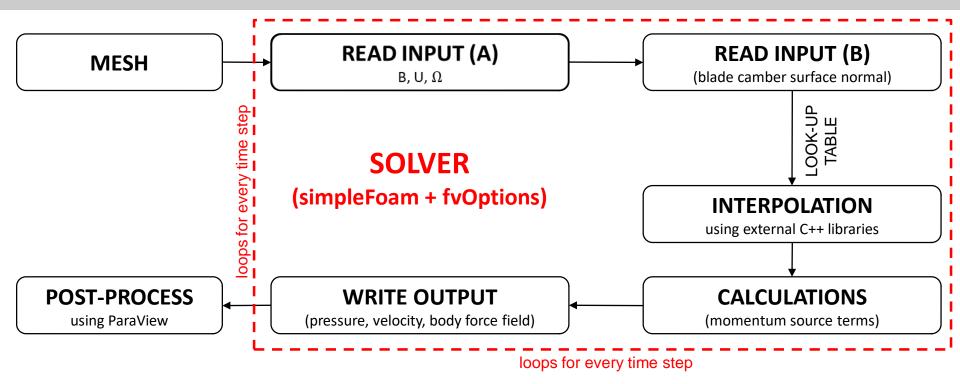


## OF Yields a More Accurate Total Pressure Rise Coefficient





## Challenges with Previous BF Implementation



#### Three biggest challenges:

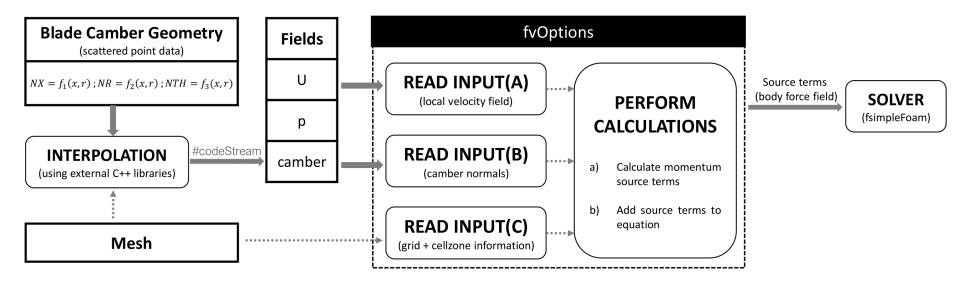
- 1. Distinguishing b/w cell zones with & without turbomachinery
- 2. Moving NX, NR, NTH interpolation code out of fvOptions, but within the OpenFOAM framework
- 3. Minimizing memory use & redundant calculations



## Improved OF BF Impl. Speeds up Calculation ~100X

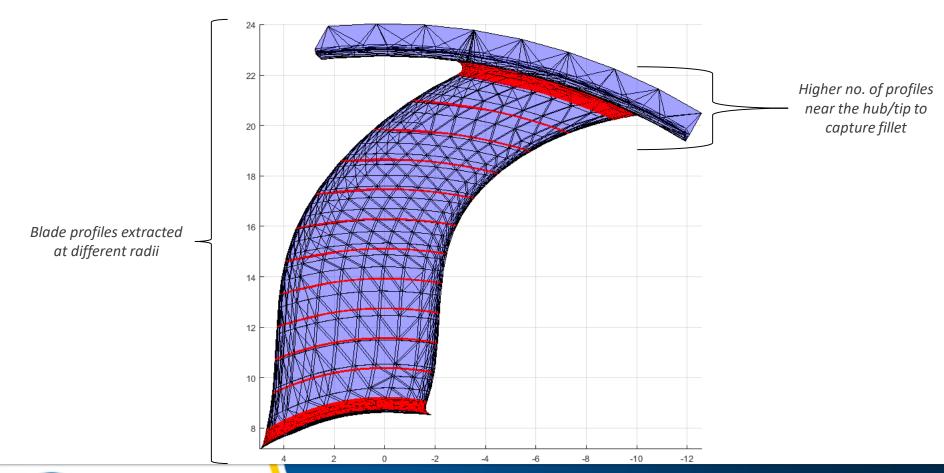
#### **New features:**

- 1. BF calculations for specific cellZones only
- 2. Separate camber field defined requires solver recompilation (fsimpleFoam)
- 3. Interpolation performed only once, defined as initial field setting for camber

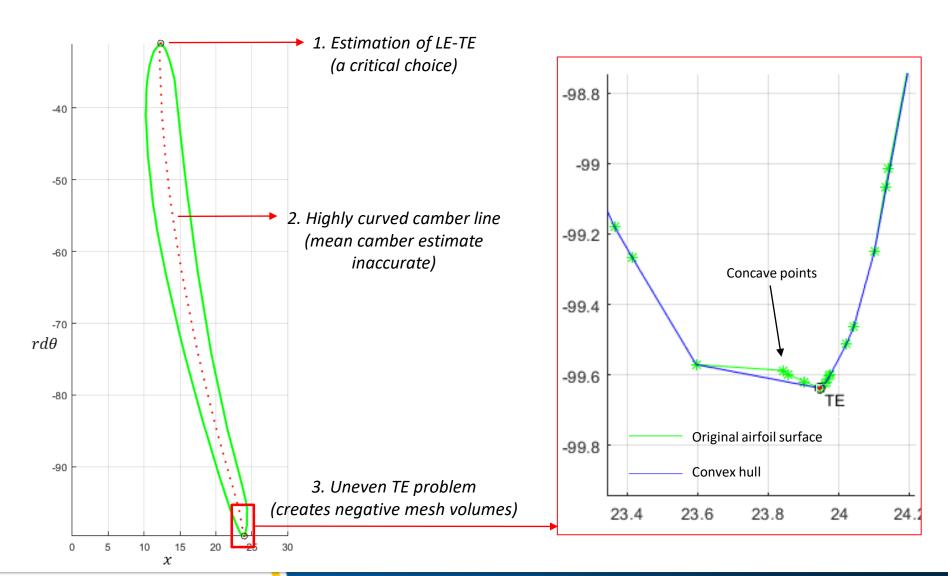


# Extracting Pacifica Blade Geometry – Very Time-consuming

- Challenge: Accurately capture complex blade shape with twist and fillets
- Solution: Extract a high no. of profiles from .stl file, makes manual cleanup difficult



# Generating Clean Airfoil Profiles for TurboGrid – Challenges



## Profiles Cleaned - Keeping Accuracy and Efficiency in Mind

#### Estimation of LE/TE:

- By definition, the two most distant points on an airfoil profile
- Generated using rotating calipers algorithm

## Extracting camber line:

- Mean camber line is first approximation
- Iteratively find a line with equal perpendicular distances from suction and pressure surfaces.

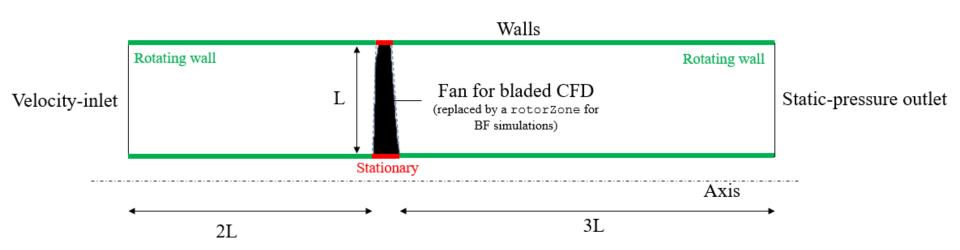
## Uneven TE problem:

TE neighboring region replaced by a convex hull

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## Pacifica Computational Domain & Boundary Conditions

- Different grids to be created for bladed and BF simulations
- Boundary conditions:
  - Inlet: velocity inlet (set to achieve target mass flow rate)
  - Outlet: static pressure (sets total pressure level)



# CFD Simulations To Assess Accuracy of Blade Loading Model

SOLVER TYPE OF SIMULATION	OpenFOAM	Star-CCM+
Single blade, single passage model	<ol> <li>Free-slip blade walls</li> <li>No-slip blade walls         <ul> <li>(compared to experimental data)</li> </ul> </li> </ol>	<ol> <li>Free-slip blade walls</li> <li>No-slip blade walls         <ul> <li>(compared to OF simulations for solver validation)</li> </ul> </li> </ol>
Body force model	<ol> <li>W/o loss model         (compared to free-slip bladed CFD to assess model accuracy)</li> <li>W/ loss model         (implemented if needed)</li> </ol>	For later

## Resources needed from FCA

- StarCCM+ for CFD of fan test facility model with blades, simulated in StarCCM+
- Spend time on-site with ARDC staff to help Palak set up computations in Star-CCM+
- Post-processing Information needed about measurement plane locations for pressure rise for provided experimental data

## Back To Key Messages

- Activities re-shuffled but project timeline essentially on schedule
- Body force model completely implemented, optimized and validated
- Pacifica computational domain for bladed CFD ready in TurboGrid