

Electrostatics

by Tony Shing

Overview:

- Basic problems: Find \vec{E} and V by Coulomb's law with integration
- Gauss law, electric flux, divergence & divergence theorem
- Electrical potential & Poisson equation
- Image charge method

In electromagnetism, theoretically every problem can be solved through a set of PDEs called the **Maxwell Equations**.

$$\begin{aligned} \longrightarrow \quad \vec{\nabla} \cdot \vec{E} &= \frac{\rho}{\epsilon_0} & \vec{\nabla} \cdot \vec{B} &= 0 \\ \vec{\nabla} \times \vec{E} &= -\frac{\partial \vec{B}}{\partial t} & \vec{\nabla} \times \vec{B} &= \mu_0 \vec{J} + \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t} \end{aligned}$$

However, a *system of PDEs* is too complicated to be solved. So we need to learn different "tricks" to avoid them, which are enough for some simple scenarios.

Electrostatics only concerns the 1st equation of the set - Gauss's law.

1 Basic Skill: Coulomb's Law with Integration

Promoting point charge to a distribution of charge is straightforward by

$$\left(\begin{array}{c} \text{Point} \\ \text{charge} \end{array} \right) = Q \quad \Longrightarrow \quad \int_{\text{whole space}} dQ \quad \sim \quad \sum_{\text{everywhere}} \left(\begin{array}{c} \text{Infinitesimal} \\ \text{charge units} \end{array} \right)$$

Coulomb's law is then a sum of all E-field contribution from every infinitesimal charge:

$$\vec{E} = \frac{1}{4\pi\epsilon_0} \frac{Q}{r^2} \hat{r} \quad \Longrightarrow \quad \int d\vec{E} = \int_{\text{whole space}} \frac{1}{4\pi\epsilon_0} \frac{dQ}{r^2} \hat{r}$$

And the formula for electrical potential follows:

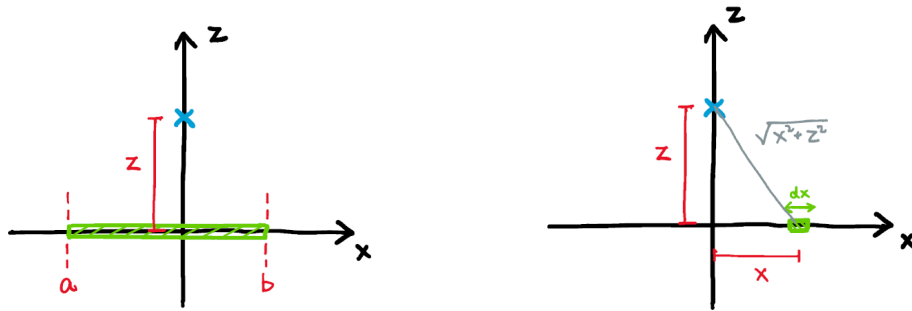
$$V = \frac{1}{4\pi\epsilon_0} \frac{Q}{r} \quad \Longrightarrow \quad \int dV = \int_{\text{whole space}} \frac{1}{4\pi\epsilon_0} \frac{dQ}{r}$$

Notations:

We often use these symbols to represent charge density at different dimension:

- Charge per volume = $\rho \Rightarrow dQ = \rho d\tau = \left(\frac{\text{Charge}}{\text{per volume}}\right) \left(\frac{\text{Unit}}{\text{volume}}\right)$
- Charge per area = $\sigma \Rightarrow dQ = \sigma ds = \left(\frac{\text{Charge}}{\text{per area}}\right) \left(\frac{\text{Unit}}{\text{area}}\right)$
- Charge per length = $\lambda \Rightarrow dQ = \lambda dl = \left(\frac{\text{Charge}}{\text{per length}}\right) \left(\frac{\text{Unit}}{\text{length}}\right)$

Example 1.1. Suppose there is a rod lying on the x-axis, with its ends at $x = a$ and $x = b$. Let the total charge it carries be Q . What is the E-field / electric potential on an arbitrary point on the z axis?



We can analyze by dividing the rod into infinitesimal pieces:

- Each segment has a length dx
- Charge on each segment is thus $\lambda dx = \frac{Q}{L} dx$, where $L = b - a$.
- For the segment at position x , its distance from the targeted point is $\sqrt{z^2 + x^2}$.

Thus we can calculate V and \vec{E} :

1. Electrical potential does not concern directions. So we can directly write

$$V = \frac{1}{4\pi\epsilon_0} \int_a^b \frac{\frac{Q}{L} dx}{\sqrt{z^2 + x^2}}$$

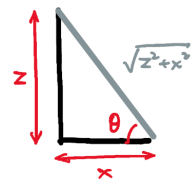
2. Electric field concerns directions. So we need to resolve the direction's component from the segment to the target point.

- The E-field's vertical component (z) should be integrated as:

$$E_z = \frac{1}{4\pi\epsilon_0} \int_a^b \frac{\frac{Q}{L} dx}{z^2 + x^2} \sin \theta = \frac{1}{4\pi\epsilon_0} \int_a^b \frac{\frac{Q}{L} dx}{z^2 + x^2} \frac{z}{\sqrt{z^2 + x^2}}$$

- Similarly for the horizontal component (x):

$$E_x = \frac{1}{4\pi\epsilon_0} \int_a^b \frac{\frac{Q}{L} dx}{z^2 + x^2} \cos \theta = \frac{1}{4\pi\epsilon_0} \int_a^b \frac{\frac{Q}{L} dx}{z^2 + x^2} \frac{x}{\sqrt{z^2 + x^2}}$$



2 Gauss's Law

The Gauss's Law has two different expressions:

$$\oiint \vec{E} \cdot d\vec{s} = \frac{Q}{\epsilon_0} \quad (\text{Integral form})$$

$$\vec{\nabla} \cdot \vec{E} = \frac{\rho}{\epsilon_0} \quad (\text{Differential form})$$

It is easier to study the physical meaning and visualize by the integral form. After that we can generalize to the differential form by introducing an operator called **divergence**.

2.1 Flux

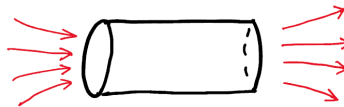
The literal description in Gauss's law integral form is

$$\left(\begin{array}{c} \text{Flux of electric field} \\ \text{on a closed surface} \end{array} \right) = \oiint \vec{E} \cdot d\vec{s} = \frac{Q}{\epsilon_0} = \frac{(\text{Charge enclosed})}{(\text{Constant})}$$

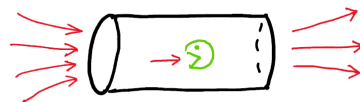
We first need to understand what **flux** is, and what that weird integral sign even means.

2.1.1 An Analogy: A Water Pipe

To begin with, we can make an analogy using a water pipe. Along a normal pipe, we expect that the amount of water flowing in should equal to the amount of water flowing out.



- If we somehow find that the (amount of water flowing in) > (amount flowing out), we know there is something absorbing water in the pipe!



There is a "sink"
in the pipe!

- If we somehow find that the (amount of water flowing in) < (amount flowing out), we know there is something producing water in the pipe!



There is a "source"
in the pipe!

How can we quantitatively tell if there is a source / sink in the pipe? We can measure by the volume flowing in / out within a short time interval Δt :

- Volume flowing in = $v_{\text{in}} \cdot \Delta t \cdot A_{\text{in}} = \left(\begin{array}{c} \text{Velocity at} \\ \text{entrance} \end{array} \right) \cdot \Delta t \cdot \left(\begin{array}{c} \text{Area of} \\ \text{entrance opening} \end{array} \right)$
- Volume flowing out = $v_{\text{out}} \cdot \Delta t \cdot A_{\text{out}} = \left(\begin{array}{c} \text{Velocity at} \\ \text{exit} \end{array} \right) \cdot \Delta t \cdot \left(\begin{array}{c} \text{Area of} \\ \text{exit opening} \end{array} \right)$

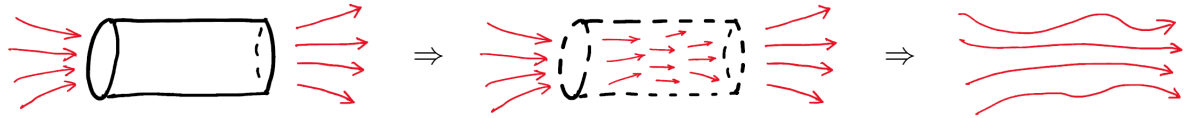
Then we can define a measure $\Phi = (v_{\text{out}} A_{\text{out}} - v_{\text{in}} A_{\text{in}})$ such that

$$\begin{cases} \text{if } \Phi > 0 & \Rightarrow \text{There is a source} \\ \text{if } \Phi < 0 & \Rightarrow \text{There is a sink} \end{cases}$$

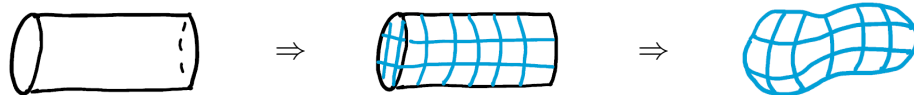
2.1.2 Generalizing to Field

Now use your imagination to extend idea:

1. The flow of water should be continuous - We can describe the flow of water by a continuous vector field $\vec{F}(\vec{r})$.



2. Our water pipe may be of any irregular shape - We can "twist" the pipe into an arbitrary closed surface.



Note: A "closed" surface needs to be well-distinguished between its "inner surface" and "outer surface".

Under these circumstances, in/out-flow are not restricted just flowing through the entrance / exit opening, but can appear on anywhere on the surface - each of the small grid on the surface can have a different field vector poking through it.

- Out-flow = Poking from inner to outer surface
- In-flow = Poking from outer to inner surface

How can the flow direction be described mathematically? We can first define a normal vector \vec{s} for each grid. By convention, this \vec{s}

- has a magnitude equal to the surface's area of the grid.
- points outward of the surface (from inner to outer).

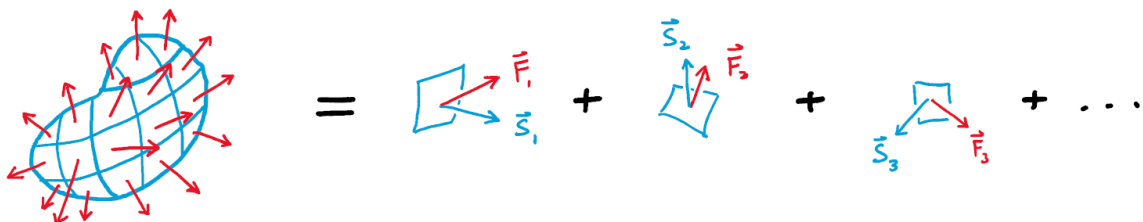
Then we can take the dot product between the field vector \vec{F} and the surface normal vector \vec{s} :

- If $\vec{F} \cdot \vec{s} > 0$, they are more or less in similar direction $\Rightarrow \vec{F}$ is pointing outward!
- If $\vec{F} \cdot \vec{s} < 0$, they are more or less in opposite direction $\Rightarrow \vec{F}$ is pointing inward!

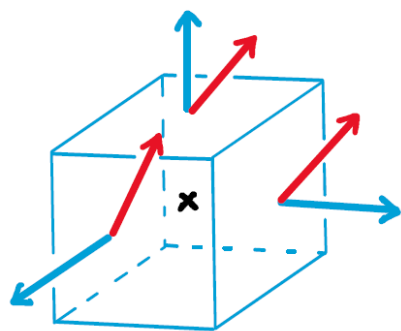
Finally, we define "flux" Φ over the closed surface:

$$\Phi = \sum_{\substack{\text{All small grids } i \\ \text{on the closed surface}}} \vec{F}_i \cdot \vec{s}_i \longrightarrow \oint \vec{F}(\vec{r}) \cdot d\vec{s}$$

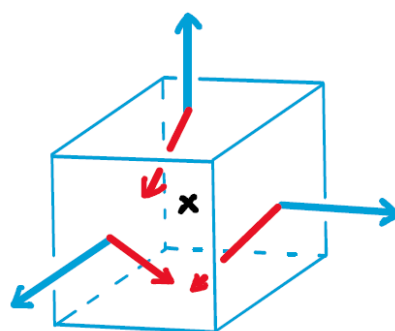
A circle on double integral
= The surface integral is over a closed surface



We can use the sign of Φ to tell if there are more in-flow (or out-flow) of field lines through the surface, thus telling if there are sources (or sinks) enclosed by the surface.



If flux > 0 , the surface likely contains a **diverging point** (source) of the field.



If flux < 0 , the surface likely contains a **converging point** (sink) of the field.

2.1.3 Calculation Example

Recall that in line integral, we have to parametrize the line before we can actually do the integral. In calculation of flux, it is even more painful - it is an area integral and we have to parametrize a surface, which is generally an impossible task without very advanced calculus.

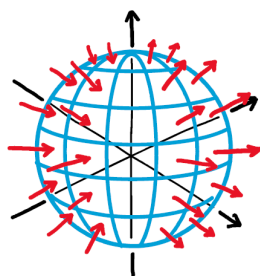
Because this is just a physics course, here only introduces some surfaces with simple parametrization. **And in most cases we do not to calculate them when using Gauss's law.**

Example 2.1. (Flux over a spherical surface)

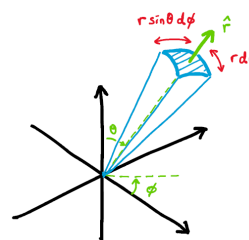
An easy parametrization is making use of the spherical coordinate. Positions on the surface can be located by the 2 angular variables (θ, ϕ) :

$$\begin{pmatrix} x \\ y \\ z \end{pmatrix} = \begin{pmatrix} x_0 \\ y_0 \\ z_0 \end{pmatrix} + \begin{pmatrix} r \sin \theta \cos \phi \\ r \sin \theta \sin \phi \\ r \cos \theta \end{pmatrix}$$

where (x_0, y_0, z_0) indicates the center of the sphere and r is the radius of the sphere.



with unit area as



The infinitesimal area is then $(r d\theta) \times (r \sin \theta d\phi)$ and normal in \hat{r} direction.

$$d\vec{s} = \hat{r} r^2 \sin \theta d\theta d\phi$$

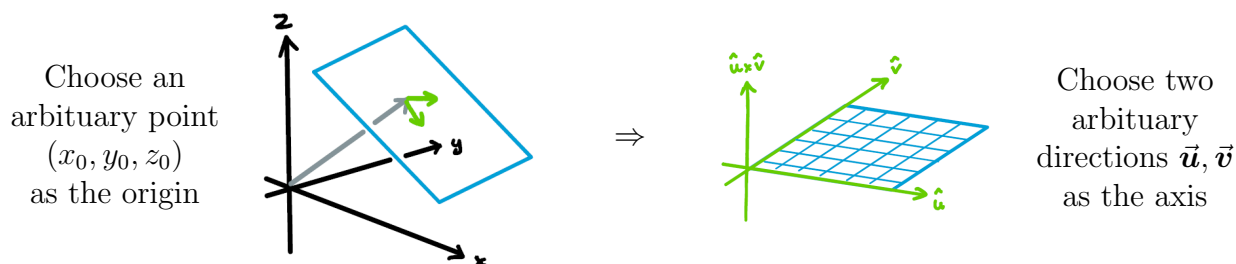
So the flux is simply a double integral over the whole sphere surface.

$$\Phi = \oiint \vec{F} \cdot d\vec{s} = \int_{\theta=0}^{\theta=\pi} \int_{\phi=0}^{\phi=2\pi} \vec{F}(x, y, z) \cdot \hat{r} r^2 \sin \theta d\theta d\phi$$

Example 2.2. (Flux over a plane)

We are free to choose any two perpendicular unit vectors $\hat{\mathbf{u}}, \hat{\mathbf{v}}$ to form a 2D coordinate system on the plane, expressing a position using 2 length quantities (u, v) :

$$\begin{pmatrix} x \\ y \\ z \end{pmatrix} = \begin{pmatrix} x_0 \\ y_0 \\ z_0 \end{pmatrix} + u \underbrace{\begin{pmatrix} u_x \\ u_y \\ u_z \end{pmatrix}}_{\hat{\mathbf{u}}} + v \underbrace{\begin{pmatrix} v_x \\ v_y \\ v_z \end{pmatrix}}_{\hat{\mathbf{v}}}$$

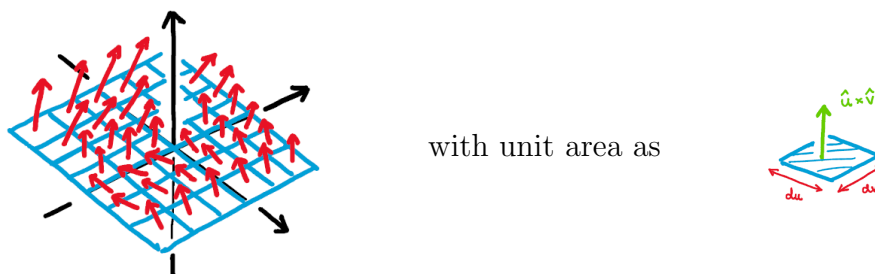


The infinitesimal area is then $(du) \times (dv)$ and normal must be in $(\hat{\mathbf{u}} \times \hat{\mathbf{v}})$ direction.

$$d\vec{s} = (\hat{\mathbf{u}} \times \hat{\mathbf{v}}) du dv$$

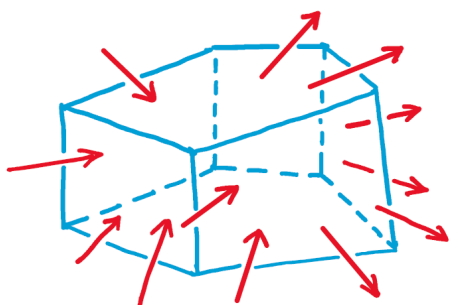
So the flux is simply a double integral over a region on the plane.

$$\Phi = \oiint \vec{\mathbf{F}} \cdot d\vec{s} = \int_{v=c}^{v=d} \int_{u=a}^{u=b} \vec{\mathbf{F}}(x, y, z) \cdot (\hat{\mathbf{u}} \times \hat{\mathbf{v}}) du dv$$



2.2 Divergence

However there is a problem in using flux - if we choose the surface too arbitrarily, the calculated flux is no longer meaningful.



E.g. If we choose a very big surface and calculate the flux ≈ 0 , Does it tells us where the diverging/converging points are?

To tackle this problem, we need to introduce the **divergence** operator:

$$\underbrace{\vec{\nabla} \cdot}_{\substack{\text{Like gradient operator} \\ \text{but with a dot}}} \bullet \stackrel{\text{def}}{=} \frac{\partial \bullet}{\partial x} + \frac{\partial \bullet}{\partial y} + \frac{\partial \bullet}{\partial z} \stackrel{\text{def}}{=} \underbrace{\text{div}}_{\substack{\text{Sometimes we} \\ \text{just write "div"}}} \bullet$$

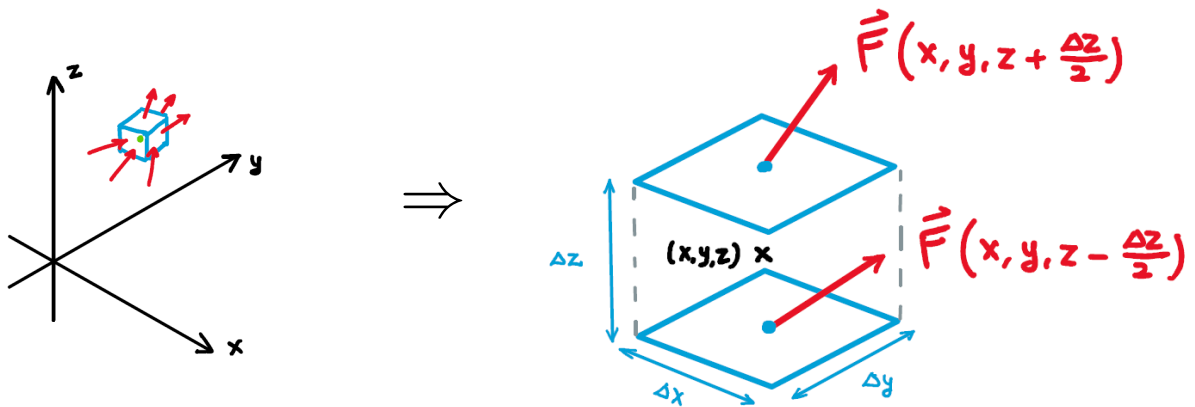
The divergence operator can be applied on a vector function, and it returns a scalar (number) function.

$$\begin{aligned} \vec{\nabla} \cdot \vec{F} &= \begin{pmatrix} \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \end{pmatrix} \begin{pmatrix} F_x \\ F_y \\ F_z \end{pmatrix} \\ &= \frac{\partial F_x}{\partial x} + \frac{\partial F_y}{\partial y} + \frac{\partial F_z}{\partial z} \\ &= (\text{A number}) \end{aligned}$$

The divergence of a vector field is related to its **total flux through an infinitesimally small but closed surface**.

2.2.1 Geometrical Interpretation

To visualize, we can draw an infinitesimal small cube around a point (x, y, z) . Although a cube has 6 faces, because of symmetry in all 3 directions, it suffices to just analyze by the 2 faces that are parallel to the x - y plane.



- Normal direction of these 2 faces = \hat{z} \Rightarrow The surface normal vector = $(\Delta x \Delta y) \hat{z}$.
- Center point of top surface = $(x, y, z + \frac{\Delta z}{2})$ \Rightarrow The field pokes through it = $\vec{F}(x, y, z + \frac{\Delta z}{2})$.
- Center point of bottom surface = $(x, y, z - \frac{\Delta z}{2})$ \Rightarrow The field pokes through it = $\vec{F}(x, y, z - \frac{\Delta z}{2})$.

Therefore the total flux through the 2 planes is

$$\begin{aligned}
 \left(\begin{array}{c} \text{Total Out-flux through} \\ \text{surfaces // x-y plane} \end{array} \right) &= \left(\begin{array}{c} \text{Out-flux through} \\ \text{top face} \end{array} \right) - \left(\begin{array}{c} \text{In-flux through} \\ \text{bottom face} \end{array} \right) \\
 d\Phi_{xy} &= \vec{F}(x, y, z + \frac{\Delta z}{2}) \cdot \hat{z}(\Delta x \Delta y) - \vec{F}(x, y, z - \frac{\Delta z}{2}) \cdot \hat{z}(\Delta x \Delta y) \\
 &= \left(\frac{\vec{F}(x, y, z + \frac{\Delta z}{2}) - \vec{F}(x, y, z - \frac{\Delta z}{2})}{\Delta z} \right) \cdot \hat{z}(\Delta x \Delta y \Delta z) \\
 &= \left(\frac{\vec{F}(x, y, z + \frac{\Delta z}{2}) - \vec{F}(x, y, z - \frac{\Delta z}{2})}{\Delta z} \right) \cdot \hat{z}(\Delta x \Delta y \Delta z) \\
 &\quad \text{This is exactly partial } z \\
 &= \frac{\partial}{\partial z} \vec{F}(x, y, z) \cdot \hat{z}(\Delta x \Delta y \Delta z) \\
 &\quad \swarrow \text{Dot product to } \hat{z} = \text{Only take } z \text{ component} \\
 &= \frac{\partial}{\partial z} F_z(x, y, z) (\Delta x \Delta y \Delta z) \\
 &= \left(\begin{array}{c} \text{Divergence's} \\ z \text{ term} \end{array} \right) \left(\begin{array}{c} \text{Unit} \\ \text{volume} \end{array} \right)
 \end{aligned}$$

We can expect the similar results in the other 2 directions. Gather them together:

$$\begin{aligned}
 \left(\begin{array}{c} \text{Total flux through} \\ \text{the volume} \end{array} \right) &= \left(\begin{array}{c} \text{Total flux through} \\ \text{surfaces // y-z plane} \end{array} \right) + \left(\begin{array}{c} \text{Total flux through} \\ \text{surfaces // x-z plane} \end{array} \right) + \left(\begin{array}{c} \text{Total flux through} \\ \text{surfaces // x-y plane} \end{array} \right) \\
 &= \left[\left(\begin{array}{c} \text{Divergence's} \\ x \text{ term} \end{array} \right) + \left(\begin{array}{c} \text{Divergence's} \\ y \text{ term} \end{array} \right) + \left(\begin{array}{c} \text{Divergence's} \\ z \text{ term} \end{array} \right) \right] \left(\begin{array}{c} \text{Unit} \\ \text{volume} \end{array} \right) \\
 d\Phi &= \left[\frac{\partial F_x}{\partial x} + \frac{\partial F_y}{\partial y} + \frac{\partial F_z}{\partial z} \right] (dx dy dz) \\
 &= (\vec{\nabla} \cdot \vec{F})(dx dy dz)
 \end{aligned}$$

Therefore we can geometrically interpret divergence as

$$\boxed{(\text{Divergence}) = \vec{\nabla} \cdot \vec{F} \sim \frac{d\Phi}{dx dy dz} = \frac{(\text{Flux through a closed surface})}{(\text{Volume enclosed by the surface})} \sim (\text{Flux density})}$$

↑
This density
is by volume

2.2.2 Divergence Theorem

With the geometrical interpretation, we can directly state (without proof) a convenient formula related to divergence - the **divergence theorem**:

$$\boxed{\oint \vec{F} \cdot d\vec{s} = \iiint (\vec{\nabla} \cdot \vec{F}) d\tau}$$

which can be literally interpret as

$$\left(\begin{matrix} \text{Total} \\ \text{Flux} \end{matrix} \right) \sim \sum_{\text{All volumes}} \left(\begin{matrix} \text{Flux} \\ \text{per volume} \end{matrix} \right) \times (\text{Volume})$$

2.3 Gauss's Law - Explanation

The Gauss's law is purely an observation about the relation between E-field and charges:

Total flux of E-field on a closed surface $\neq 0$	\Leftrightarrow	There are charges inside the surface
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The two forms of Gauss's law are describing this same observation:

– Integral form:

$$(\vec{E}'\text{'s flux}) \sim \oiint \vec{E} \cdot d\vec{s} = \frac{Q}{\epsilon_0} \sim (\text{Charge})$$

– Differential form:

$$\left(\begin{matrix} \vec{E}'\text{'s flux} \\ \text{density} \end{matrix} \right) \sim \vec{\nabla} \cdot \vec{E} = \frac{\rho}{\epsilon_0} \sim \left(\begin{matrix} \text{Charge} \\ \text{density} \end{matrix} \right)$$

And the two form can be inter-converted by divergence theorem.

$$\begin{array}{ccc} \oiint \vec{E} \cdot d\vec{s} & = & \frac{Q}{\epsilon_0} \\ \text{Divergence Theorem} \downarrow & & \downarrow \text{Charge to Charge density} \\ \iiint (\vec{\nabla} \cdot \vec{E}) d\tau & = & \frac{1}{\epsilon_0} \iiint \rho d\tau \end{array}$$

2.4 Applying Gauss's Law Integral Form

In beginner electromagnetism, there is only one type of problem related to Gauss's law :

*Given the charge distribution, find the E-field everywhere by Gauss's law integral form
in some very symmetrical scenarios.*

which is basically asking you to *revert* the flux calculation:

$$\oiint \vec{E} \cdot d\vec{s} = \frac{Q}{\epsilon_0} \quad \Rightarrow \quad \vec{E} = \text{Some function of } Q$$

If Q has a very ugly distribution, there is nothing we can do other than solving some PDEs. But **if Q distributes very symmetrically, \vec{E} should also be symmetrical**, such that the flux integral can be broken into multiplications.

In these cases, we can choose a "Gaussian" surface to to be integrated where

1. \vec{E} has constant magnitude everywhere on the surface.
2. \vec{E} forms the same angle with the surface normal vector everywhere on the surface

Only then, the flux integral can be broken down as

$$\begin{aligned}
 \oiint \vec{E} \cdot d\vec{s} &= \oiint |\vec{E}| |d\vec{s}| \cos \theta \quad \leftarrow \text{Just dot product } \vec{a} \cdot \vec{b} = |\vec{a}| |\vec{b}| \cos \theta \\
 &= |\vec{E}| \cos \theta \oiint |d\vec{s}| \\
 &= |\vec{E}| \cos \theta (\text{Total surface area})
 \end{aligned}$$

Same magnitude everywhere
Can move out of integral!
Form same angle everywhere
Can move out of integral!


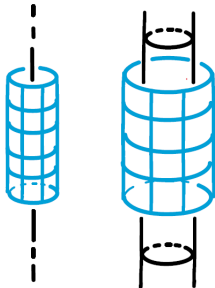
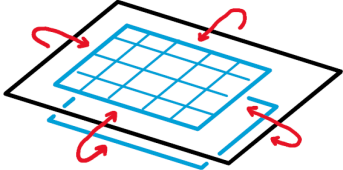
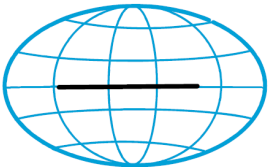
such that we can find the magnitude of \vec{E} with simple division

$$|\vec{E}| = \frac{(\text{Total flux})}{(\text{Total surface area}) \cos \theta} = \frac{Q/\epsilon_0}{(\text{Total surface area}) \cos \theta}$$

In fact, there are not many of these "very symmetrical" cases. These examples below, with their respective Gaussian surfaces, are basically all the variations you can find in textbooks.

Charge configuration
(Assuming uniform density)

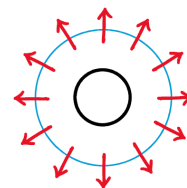
Good Gaussian surface

Sphere		Spherical shell
Infinitely long rod / cylinder		Curved face of cylinder
Infinitely large plane		Infinitely large planes wrapping it around
Finite long rod		Ellipsoid with foci = end points of the rod

P.S. In electrostatics (no moving charges), all good Gaussian surfaces are equipotential surfaces.

Example 2.3. Given a solid sphere with uniform charge density ρ and radius R . By spherical symmetry, the E-field must satisfy:

- Only point in radial direction.
- Magnitude does not depend on angular directions θ, ϕ .



Therefore we can choose the Gaussian surface to be a sphere of radius r to find the magnitude of E-field at distance r from the sphere center.

$$\begin{aligned}
 |\vec{E}| &= \frac{Q/\epsilon_0}{(\text{Total surface area}) \cos \theta} \\
 &= \frac{Q}{\epsilon_0} \cdot \frac{1}{(4\pi r^2)} \cdot \frac{1}{\cos 0^\circ} \quad \leftarrow \begin{array}{l} \text{E-field = radial} \\ \therefore \text{Normal to surface} \end{array} \\
 &= \frac{Q}{4\pi\epsilon_0 r^2} \\
 \Rightarrow \quad \vec{E} &= \frac{Q}{4\pi\epsilon_0 r^2} \hat{r} \quad \leftarrow \text{You have to manually add the unit vector}
 \end{aligned}$$

1. For radial distance $r < R$, the total charge enclosed in the gaussian surface is only the core of the sphere, up to radius r . So we should take $Q = \frac{4}{3}\pi r^3 \rho$.

$$\vec{E} = \frac{(\frac{4}{3}\pi r^3 \rho)}{4\pi\epsilon_0 r^2} \hat{r} = \frac{\rho r}{3\epsilon_0} \hat{r}$$



2. For radial distance $r > R$ the total charge enclosed in the gaussian surface is the whole sphere, So we should take $Q = \frac{4}{3}\pi R^3 \rho$.

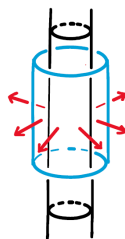
$$\vec{E} = \frac{(\frac{4}{3}\pi R^3 \rho)}{4\pi\epsilon_0 r^2} \hat{r} = \frac{\rho R^3}{3\epsilon_0 r^2} \hat{r}$$



Example 2.4. Given an infinitely long hollow cylinder with inner radius = a and outer radius = b , and its charge density is proportional to distance from center r , i.e. $\rho(\vec{r}) = kr$.

For cylinder, we can claim by cylindrical symmetry that the E-field must satisfy:

- Only point in r direction.
- Magnitude does not depend on θ or z .

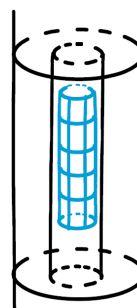


Therefore we can choose the Gaussian surface to be a cylindrical sheet radius r and an arbitrary length L (which will be cancelled later) to find the magnitude of E-field at distance r from the rotation axis.

$$\begin{aligned}
 |\vec{E}| &= \frac{Q/\epsilon_0}{(\text{Total surface area}) \cos \theta} \\
 &= \frac{Q}{\epsilon_0} \cdot \frac{1}{(2\pi r L)} \cdot \frac{1}{\cos 0^\circ} \quad \leftarrow \begin{array}{l} \text{E-field = radial} \\ \therefore \text{Normal to curved surface} \end{array} \\
 &= \frac{Q}{2\pi\epsilon_0 r L} \quad \leftarrow \begin{array}{l} \text{E-field = radial} \\ \therefore \text{Only go through the curved surface} \\ \text{Top/bottom surface has no flux} \end{array} \\
 \Rightarrow \vec{E} &= \frac{Q}{2\pi\epsilon_0 r L} \hat{r} \quad \leftarrow \text{You have to manually add the unit vector}
 \end{aligned}$$

This time the charge density depends on position, so the total charge enclosed by the surface needs to be computed by integration.

1. For radial distance $r < a$, there is no charge enclosed because the cylinder is hollow. So $Q = 0$ implying $\vec{E} = 0$.

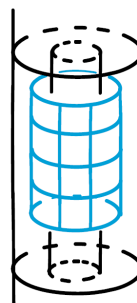


2. For radial distance $a < r < b$, total enclosed charge are distributed from radius = a to radius = r , which calculates as

$$Q = \int_a^r \rho \cdot 2\pi r L \, dr = 2\pi k L \int_a^r r^2 \, dr = \frac{2\pi k L}{3} (r^3 - a^3)$$

So the E-field is

$$\vec{E} = \frac{Q}{2\pi\epsilon_0 r L} \hat{r} = \frac{k}{3\epsilon_0} \left(r^2 - \frac{a^3}{r} \right) \hat{r}$$

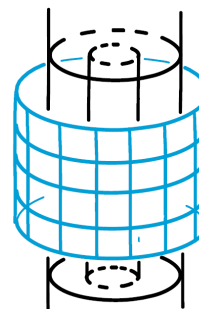


3. For radial distance $r > b$, total enclosed charge are distributed from radius = a to radius = b , which calculates as

$$Q = \int_a^b \rho \cdot 2\pi r L \, dr = 2\pi k L \int_a^b r^2 \, dr = \frac{2\pi k L}{3} (b^3 - a^3)$$

So the E-field is

$$\vec{E} = \frac{Q}{2\pi\epsilon_0 r L} \hat{r} = \frac{k}{3\epsilon_0 r} (b^3 - a^3) \hat{r}$$



3 Electric Potential

3.1 Mathematical Origin

The reason to create a electrical potential function $V(\vec{r})$ is rather mathematical:

- Observation: E-field by static charge never forms loops. \Rightarrow Static E-field is conservative.
- Mathematical fact: Any conservative field can be expressed as the gradient of some scalar function (i.e. potential).

Therefore we can define a scalar function $V(\vec{r})$ such that

$$\boxed{\vec{E}(\vec{r}) = -\vec{\nabla}V(\vec{r})}$$

And the reverse can be calculated by

$$\boxed{V(\vec{r}_0) = - \int_{\text{any path from } \infty \text{ to } \vec{r}_0} \vec{E}(\vec{r}) \cdot d\vec{r} = - \int_{\infty}^{\vec{r}_0} \vec{E}(\vec{r}) d\vec{r}}$$

3.2 Poisson Equation

If we substitute $\vec{E} = -\vec{\nabla}V$ into the Gauss's law, we arrive at a new equation:

$$\begin{aligned} \frac{\rho}{\epsilon_0} &= \vec{\nabla} \cdot \vec{E} \\ &= \vec{\nabla} \cdot (-\vec{\nabla}V) \\ &= -\vec{\nabla} \cdot \left(\frac{\partial V}{\partial x} \hat{x} + \frac{\partial V}{\partial y} \hat{y} + \frac{\partial V}{\partial z} \hat{z} \right) \\ &= - \left(\frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2} \right) \stackrel{\text{def}}{=} -\nabla^2 V \end{aligned}$$

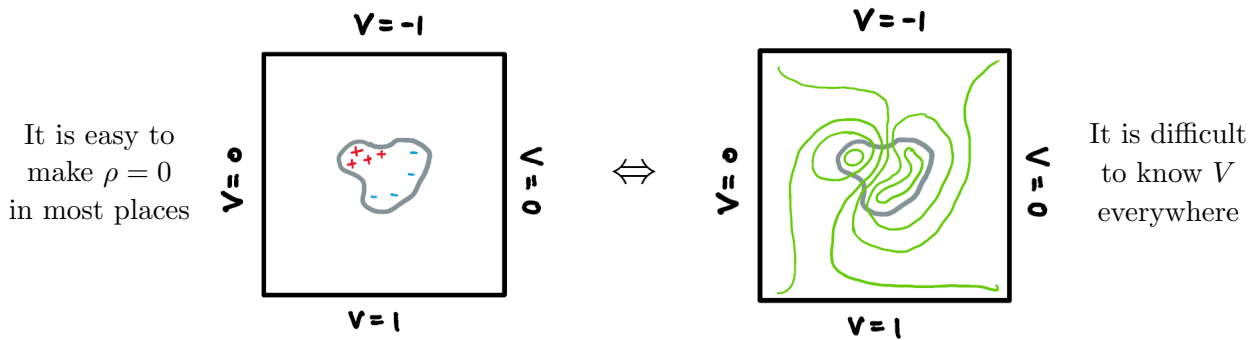
This is called
Laplacian Operator

$$\boxed{\nabla^2 V(\vec{r}) = -\frac{\rho(\vec{r})}{\epsilon_0}}$$

This equation belongs to a class of PDE called **Poisson equation**, which is one of the earliest studied PDEs in history. It is the most fundamental relation between potential and charge. Given any configurations of charge or potential, ideally we can find the other using this PDE.

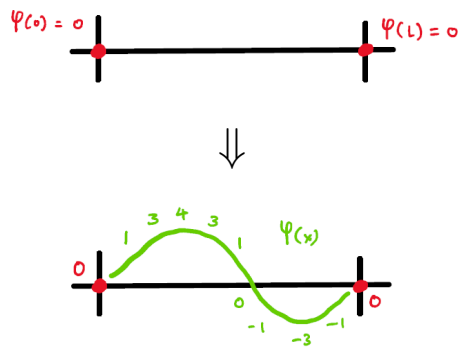
- $V(\vec{r})$ to $\rho(\vec{r})$: Computing ∇^2 is just a sum of 2nd order derivatives. (Easy!)
- $\rho(\vec{r})$ to $V(\vec{r})$: Need to solve the Laplacian equation, which is a 2nd order non-homogeneous linear PDE. (Awful!)

Unfortunately in realistic problems, it is more frequent to ask for $V(\vec{r})$ (or $\vec{E}(\vec{r})$) from $\rho(\vec{r})$, because we can usually confine the charge distribution in a small region by using very small test objects; but for potential and E-field, they are always everywhere.

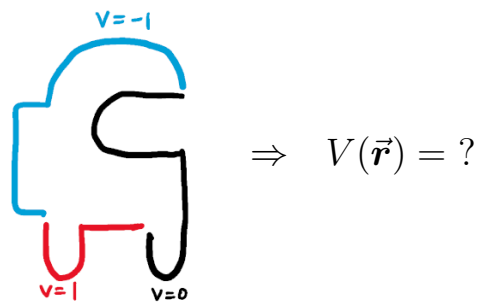


We are not going to discuss how to solve the Poisson equation here - it can take several book chapters to analyze the solution forms at different boundary conditions. (And in many cases, we need to resort to numerical methods.) Those shall be left to the future you if you are determined to study physics.

In 1D wave equation, boundary conditions are only about the 2 end points. Obtaining the general solutions is relatively easy.



In Poisson equation, boundary conditions are about the line/face at the edge of the region. There can be too many variations.



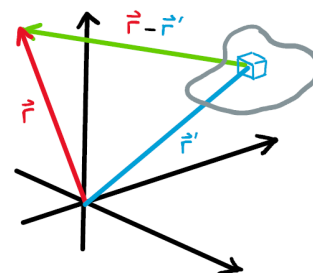
Even though, we have already seen the solution in one very special case - When the region of interest is infinitely large AND potential is chosen to be 0 at infinity far, i.e. $V(\vec{r} = \infty) = 0$, the solution is exactly the Coulomb's law.

$$V(\vec{r}) = \frac{1}{4\pi\epsilon_0} \iiint_{\text{infinitely large space}} \frac{\rho(\vec{r}')}{|\vec{r} - \vec{r}'|} d^3\vec{r}'$$

$$\sim \frac{1}{4\pi\epsilon_0} \sum_{\text{everywhere}} \frac{(\text{charge})}{(\text{distance})}$$

$$\equiv \text{Coulomb's law for electric potential}$$

(But written in a fancier vector form)



3.3 Finding \vec{E} from Q

On the other hand, Poisson equation provides an alternative to calculate E-field distribution from charge distribution. If we compare the Gauss's law and Poisson equation:

- Poisson equation :

$V(\vec{r})$ is a scalar function. Only 1 function $V(\vec{r})$ to be solved.

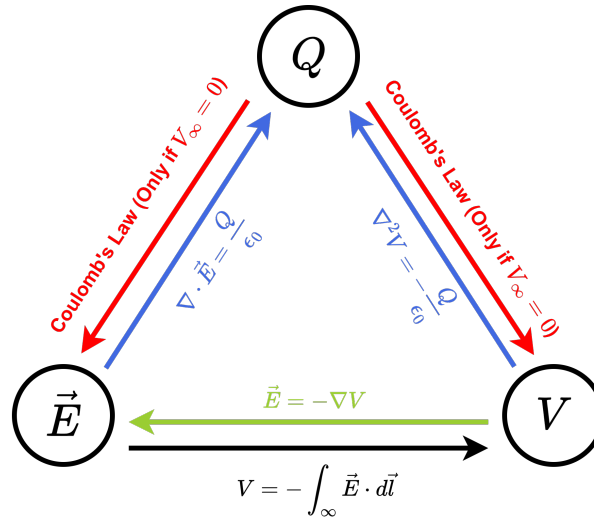
$$\nabla^2 V = -\frac{\rho}{\epsilon_0} \quad \Leftrightarrow \quad \underbrace{\frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2}}_{\text{All about } V} = -\frac{\rho}{\epsilon_0}$$

- Gauss's law :

$\vec{E}(\vec{r})$ is a vector function with 3 components $E_x(\vec{r})$, $E_y(\vec{r})$, $E_z(\vec{r})$, which are 3 inter-dependent functions to be solved.

$$\vec{\nabla} \cdot \vec{E} = \frac{\rho}{\epsilon_0} \quad \Leftrightarrow \quad \underbrace{\frac{\partial E_x}{\partial x} + \frac{\partial E_y}{\partial y} + \frac{\partial E_z}{\partial z}}_{\text{Involve different components}} = \frac{\rho}{\epsilon_0}$$

Obviously, there is no reason to try to directly solve the more difficult PDE of \vec{E} if we can alternatively solve the easier PDE of V , and then take gradient to get \vec{E} (i.e. via $\vec{E} = -\vec{\nabla}V$).



In this way, we can tell the solution of Gauss's law as a PDE, which is as expected, the Coulomb's law for \vec{E} .

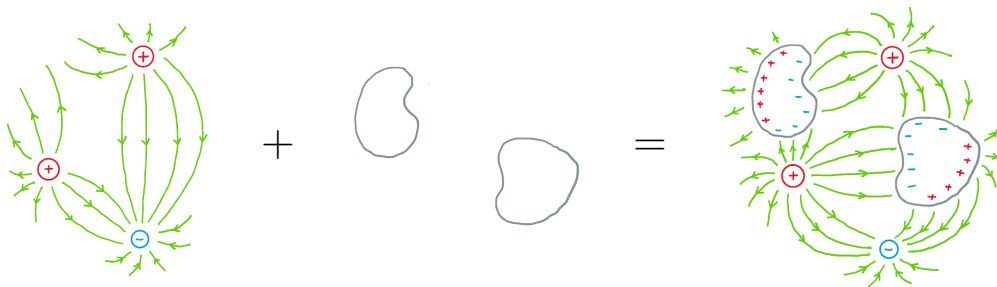
$$\begin{aligned} \vec{E}(\vec{r}) &= -\vec{\nabla}V(\vec{r}) = \frac{1}{4\pi\epsilon_0} \iiint_{\text{infinitely large space}} \frac{\rho(\vec{r}')}{|\vec{r} - \vec{r}'|^2} \left[\frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|} \right] d^3\vec{r}' \\ &\sim \frac{1}{4\pi\epsilon_0} \sum_{\text{everywhere}} \frac{(\text{charge})}{(\text{distance})^2} (\text{unit}_{\text{vector}}) \\ &\equiv \text{Coulomb's law for electric field} \\ &\quad (\text{But written in a fancier vector form}) \end{aligned}$$

4 Image Charge Method

4.1 Induced Charge & Equipotential on Conductors

Suppose we want to solve an electrostatics problem with conductors present. Because charges can freely flow in conductors, the presence of external charge sources can *induce* new charge in the conductors.

- The induced charge's distribution completely depends on the positions of external charge, and also the shape of the conductor.
- **Measuring the induced charge distribution is impossible**, because any charge probe will disturb it.



In previous sections, we are solving for \vec{E} and V where the charge distribution ρ is known everywhere. But this time we do not know the exact distribution of induced charge! Luckily, if the induced charges are distributed on conductors, there is one property that the induced charges need to satisfy:

Charges on conductor must distribute themselves such that the whole conductor is of equi-potential.

This is intuitive - because charges are allowed to move freely, they will spontaneously distribute themselves until net electric force on them is 0, i.e. the electric potential will be the same everywhere on the conductor.

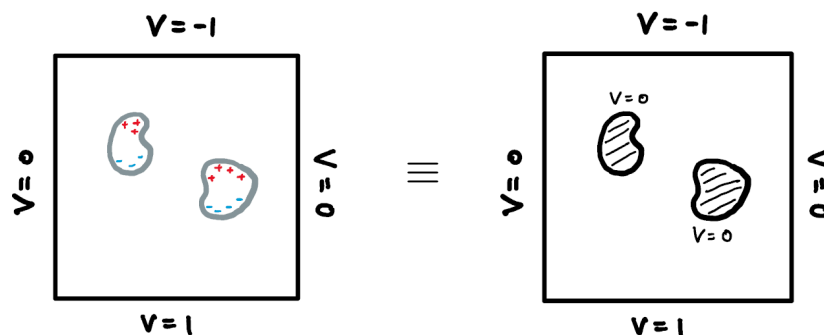
This charge feels greater repulsion from the right than from the left.



Now the force is balanced.

4.2 Image charges

In the perspective of solving PDE, requiring "conductor = equipotential" only means an additional boundary condition of V over the conductor's surface.



From mathematical studies of Poisson equation, there is the **uniqueness theorem of Poisson equation** (proof on [wiki](#)) that if the boundary conditions of V is fixed,

- Any solutions of the Poisson equation can only be different by a constant function.

$$\nabla^2 V = -\frac{\rho}{\epsilon_0} \quad \xrightarrow{\text{Solve}} \quad V = V(\vec{r}) + (\text{Any constant } C)$$

- So E-field, the gradient of V , is uniquely determined by the boundary conditions of V .

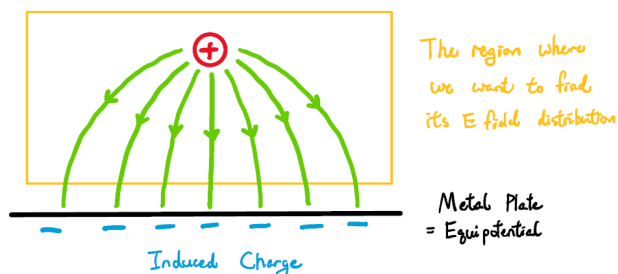
$$\vec{E} = -\vec{\nabla}(V(\vec{r}) + C) = -\vec{\nabla}V(\vec{r}) + 0 = (\text{Same for any } C)$$

This theorem allows us to skip calculating where the induced charge are - **we may find another charge configurations that creates the same potential boundary condition but easier to calculate.** By the uniqueness theorem, the E-field in these two configurations must be the same.

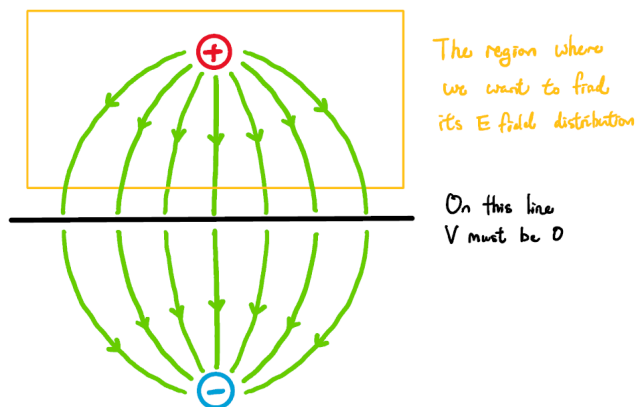
This approach is called the **image charge method**, and the charges that we used to create the alternative configuration are called **image charge**. They are called so because the alternative configurations usually look like a "reflection" of the external charge sources through the conductor surface.

Example 4.1. ("Reflection" by plane)

Consider a point charge q at distance d from an infinitely large metal surface which is maintained at $V = 0$. We expect an induced charge distribution forming on the surface and contribute to the potential/E-field on top of the surface.



But we already know another similar configuration that creates a flat equipotential surface of $V = 0$ and satisfy $V(\infty = 0)$ - when there is an additional charge of $-q$ at distance d under the metal surface.



The principle of image charge method tells us that the potential and E-field (on top of the metal surface) in both cases must be identical because they satisfy the same boundary condition of V . Therefore the potential is

$$V_{\text{(top half)}}(x, y, z) = \left(\text{Contribution by original charge } q \right) + \left(\text{Contribution by image charge } -q \right)$$

$$= \frac{q}{4\pi\epsilon_0} \frac{1}{\sqrt{x^2 + y^2 + (z-d)^2}} - \frac{q}{4\pi\epsilon_0} \frac{1}{\sqrt{x^2 + y^2 + (z+d)^2}}$$

and the E-field is

$$\vec{E}_{\text{(top half)}}(x, y, z) = -\vec{\nabla} V_{\text{(top half)}}(x, y, z)$$

$$= -\vec{\nabla} \left(\frac{q}{4\pi\epsilon_0} \left[\frac{1}{\sqrt{x^2 + y^2 + (z-d)^2}} - \frac{1}{\sqrt{x^2 + y^2 + (z+d)^2}} \right] \right)$$

$$= \frac{q}{4\pi\epsilon_0} \left(\frac{x\hat{x} + y\hat{y} + (z-d)\hat{z}}{(x^2 + y^2 + (z-d)^2)^{\frac{3}{2}}} - \frac{x\hat{x} + y\hat{y} + (z+d)\hat{z}}{(x^2 + y^2 + (z+d)^2)^{\frac{3}{2}}} \right)$$

While the V and \vec{E} on the bottom half must be 0 because it is in the metal.

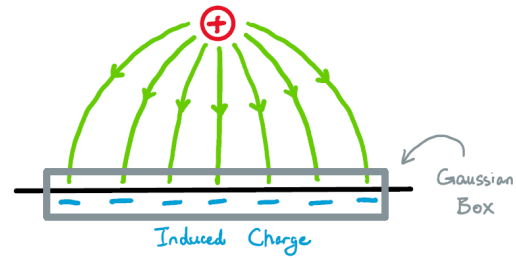
After getting \vec{E} , we can also find the induced charge distribution using Gauss's law. By drawing a Gaussian box with area A on the surface at position $(x, y, 0)$,

$$\left(\text{Total flux} \right) = \left(\text{Flux through top surface} \right)$$

$$= \vec{E}_{\text{(top half)}}(x, y, 0) \cdot A\hat{z}$$

$$= \frac{qA}{4\pi\epsilon_0} \frac{-2d}{(x^2 + y^2 + d^2)^{\frac{3}{2}}}$$

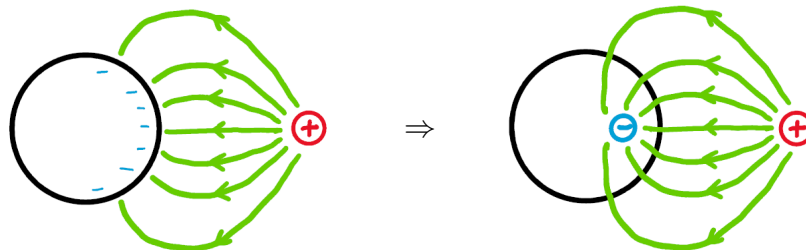
$$\equiv \frac{Q_{\text{induced}}}{\epsilon}$$



$$\Rightarrow \left(\text{Induced charge surface density} \right) = \sigma_{\text{induced}} \equiv \frac{Q_{\text{induced}}}{A} = -\frac{q}{2\pi} \frac{d}{(x^2 + y^2 + d^2)^{\frac{3}{2}}}$$

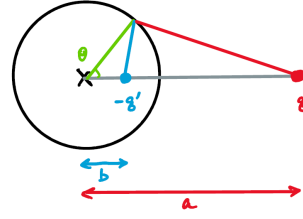
Example 4.2. ("Reflection" by Sphere)

Consider a point charge q at distance a from the center of a metal sphere of radius R which is maintained at $V = 0$. We expect an induced charge distribution forming on the surface and contribute to the potential/E-field on top of the surface.



In the spherical case, we can substitute the induced charge by a single point charge $-q'$ at distance b from the sphere's center, which can be calculated by

$$\begin{cases} b = \frac{R^2}{a} \\ q' = -\frac{R}{a}q \end{cases}$$



Proof

Choose the origin to be the center of the sphere and direction to q to be $\theta = 0$. Since it requires the potential on the sphere to be $V(r = R) = 0$, we can write the total V as

$$\begin{aligned} V(R, \theta, \phi) = 0 &= \left(\text{Contribution by} \right) + \left(\text{Contribution by} \right) \\ &= \frac{q}{4\pi\epsilon_0} \frac{1}{\sqrt{R^2 + a^2 - 2Ra \cos \theta}} - \frac{q'}{4\pi\epsilon_0} \frac{1}{\sqrt{R^2 + b^2 - 2Rb \cos \theta}} \\ \Rightarrow \left(\frac{-q'}{q} \right) &= \frac{R^2 + b^2 - 2Rb \cos \theta}{R^2 + a^2 - 2Ra \cos \theta} \\ 0 &= \underbrace{\left[1 - \left(\frac{q'}{q} \right)^2 \right] R^2 + \left[b^2 - \left(\frac{q'}{q} \right)^2 a^2 \right]}_{\text{This part is independent of } \theta} - \underbrace{2R \left[b - \left(\frac{q'}{q} \right)^2 a \right]}_{\text{Coefficient of } \cos \theta} \cos \theta \end{aligned}$$

This relation should hold for any θ .

1. Therefore the coefficient of $\cos \theta$ must be 0.

$$\begin{aligned} 0 &= 2R \left[b - \left(\frac{q'}{q} \right)^2 a \right] \\ \Rightarrow \frac{b}{a} &= \left(\frac{q'}{q} \right)^2 \end{aligned}$$

2. Then the remaining term must also become 0.

$$\begin{aligned} 0 &= \left[1 - \left(\frac{q'}{q} \right)^2 \right] R^2 + \left[b^2 - \left(\frac{q'}{q} \right)^2 a^2 \right] \\ &= \left(1 - \frac{b}{a} \right) R^2 + \left(b^2 - a^2 \cdot \frac{b}{a} \right) \\ &= \left(1 - \frac{b}{a} \right) R^2 + ab \left(\frac{b}{a} - 1 \right) \\ &= \left(1 - \frac{b}{a} \right) (R^2 - ab) \\ \Rightarrow \text{Either } b &= a_{\text{(reject)}} \quad \text{or} \quad \underline{b = \frac{R^2}{a}} \end{aligned}$$

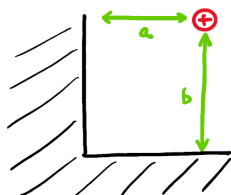
Finally substitute back into $\frac{b}{a} = \left(\frac{q'}{q}\right)^2$ to get

$$q' = \pm \sqrt{\frac{b}{a}} q = -\frac{R}{a} q$$

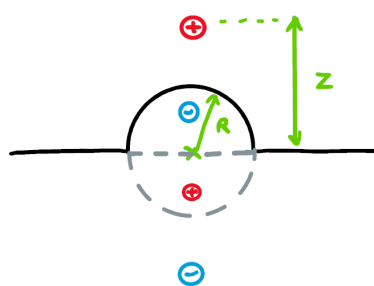
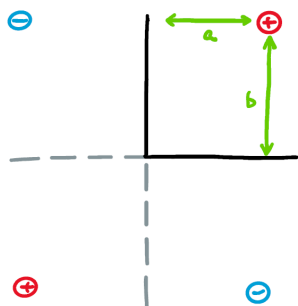
The image charge must be negative to be physical

□

Exercise 4.1. How do you add image charges in these situations, such that the potential on the metal surface satisfy $V = 0$?



Solutions:



Here we shall summarize the methods of solving electrostatics problems:

1. Very symmetric configurations \Rightarrow Gauss's law integral form. No calculus required.
 2. Not so symmetric but satisfies $V(\vec{r} = \infty) = 0 \Rightarrow$ Multiple integral with Coulomb's law.
 3. $V(\vec{r}) = 0$ on some nice surfaces with induced charge \Rightarrow Try image charge method.
 4. All the above do not apply \Rightarrow Solve Poisson equation of $V(\vec{r})$ explicitly. PDE hell.
-

— The End —