

Client Name

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Project Address

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Section

GARAGE CONVERSION

Stage

ARCHITECTURAL

Drawing Title

EXISTING PLANS

Drawing Status

FOR APPROVAL

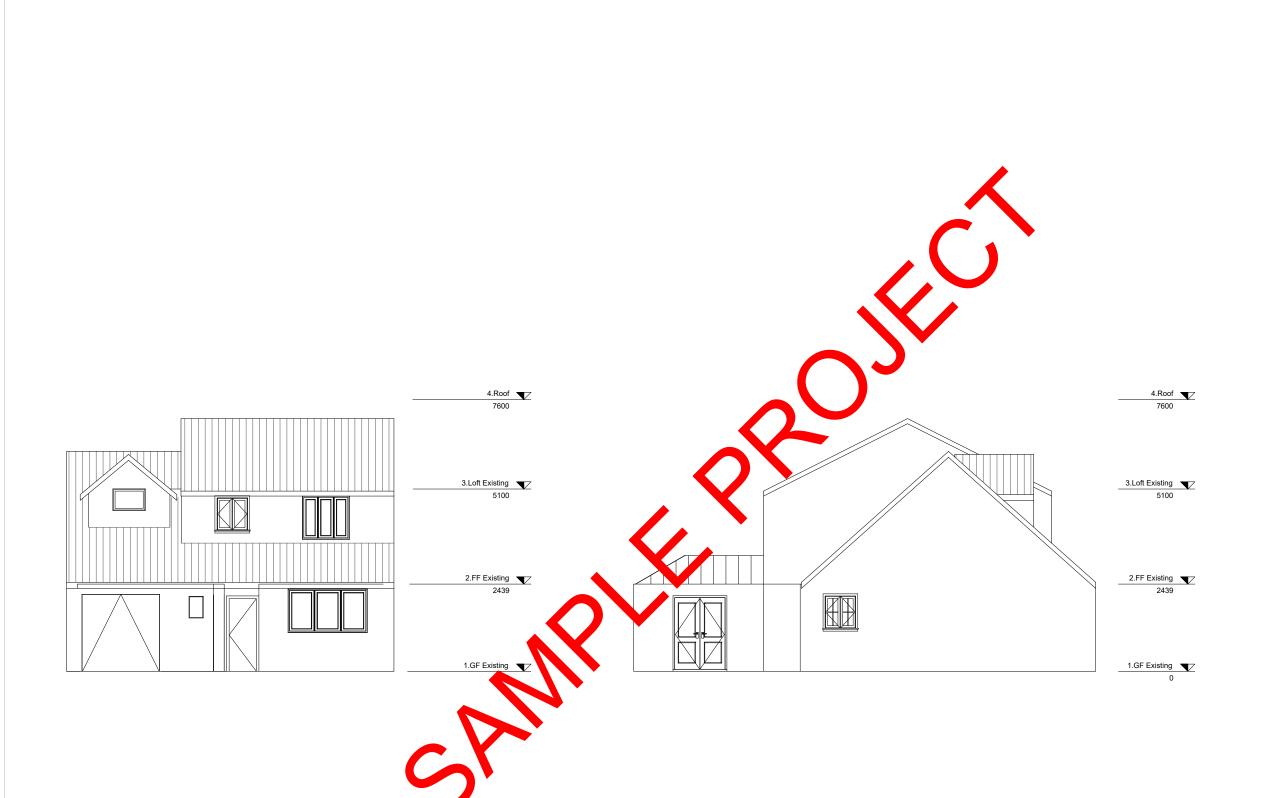
Revisions and Notes

Project No.	202	4-03-CR0 8	3XW
Drawing No.	PLA	NNING-002	<u> </u>
Revision		00	
Scale at A3		1:100	
Date		06-03-24	
Designed	MM	Checked	M٨
Drawn	MM	Approved	M٨



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Section

# GARAGE CONVERSION

Stage

# ARCHITECTURAL

Drawing Title

# EXISTING ELEVATIONS

Drawing Status

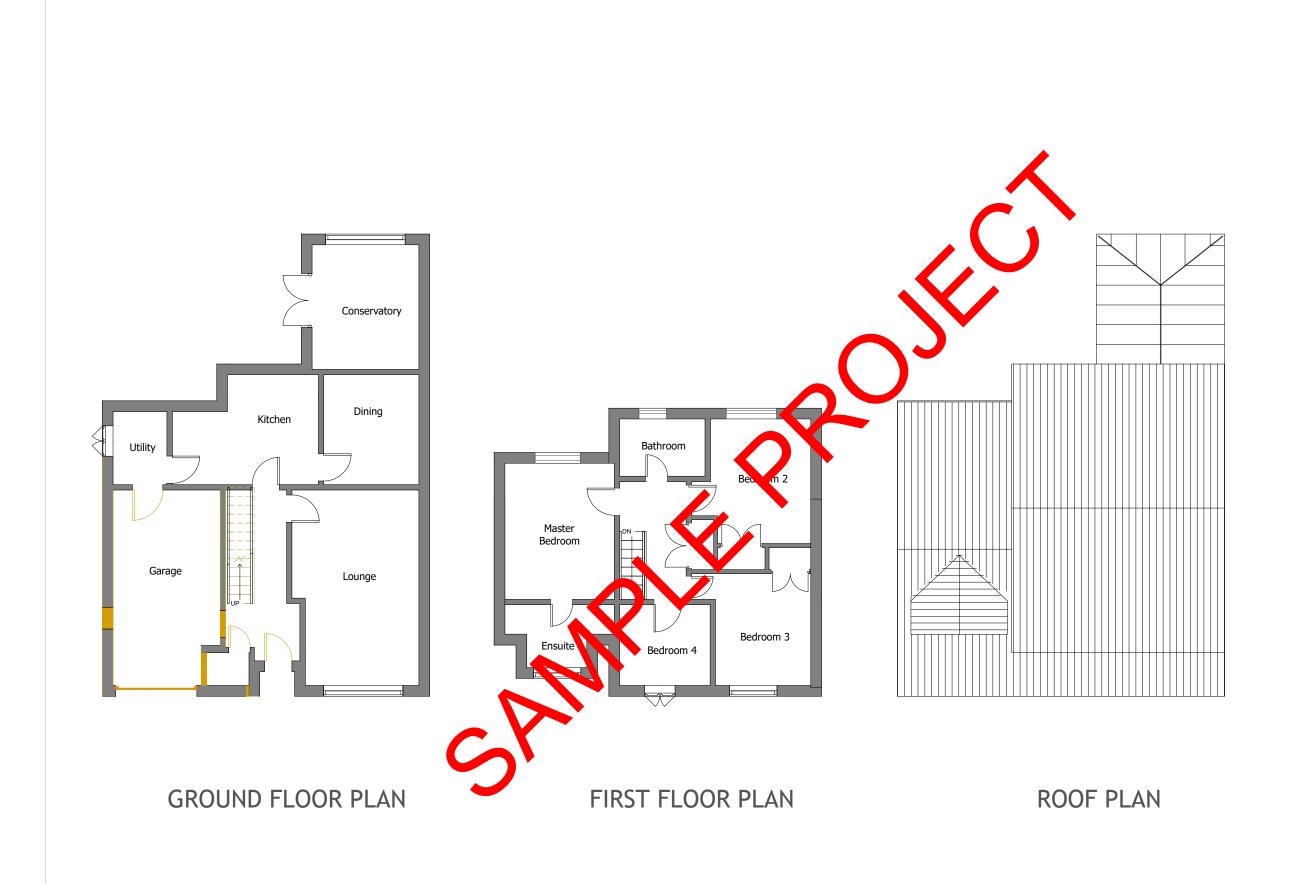
# FOR APPROVAL

Revisions and Notes

Project No.	202	4-03-CR0 8	XW
Drawing No.	PLA	NNING-003	3
Revision		00	
Scale at A3		1:100	
Date		06-03-24	
Designed	MM	Checked	M
Drawn	8888	Approved	٨٨/



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Section

GARAGE CONVERSION

Stage

ARCHITECTURAL

Drawing Title

DEMO PLANS

Drawing Status

FOR APPROVAL

Revisions and Notes

2024-03-CR0 8XW

 Drawing No.
 PLANNING-004

 Revision
 00

 Scale at A3
 1:100

Date 06-03-24

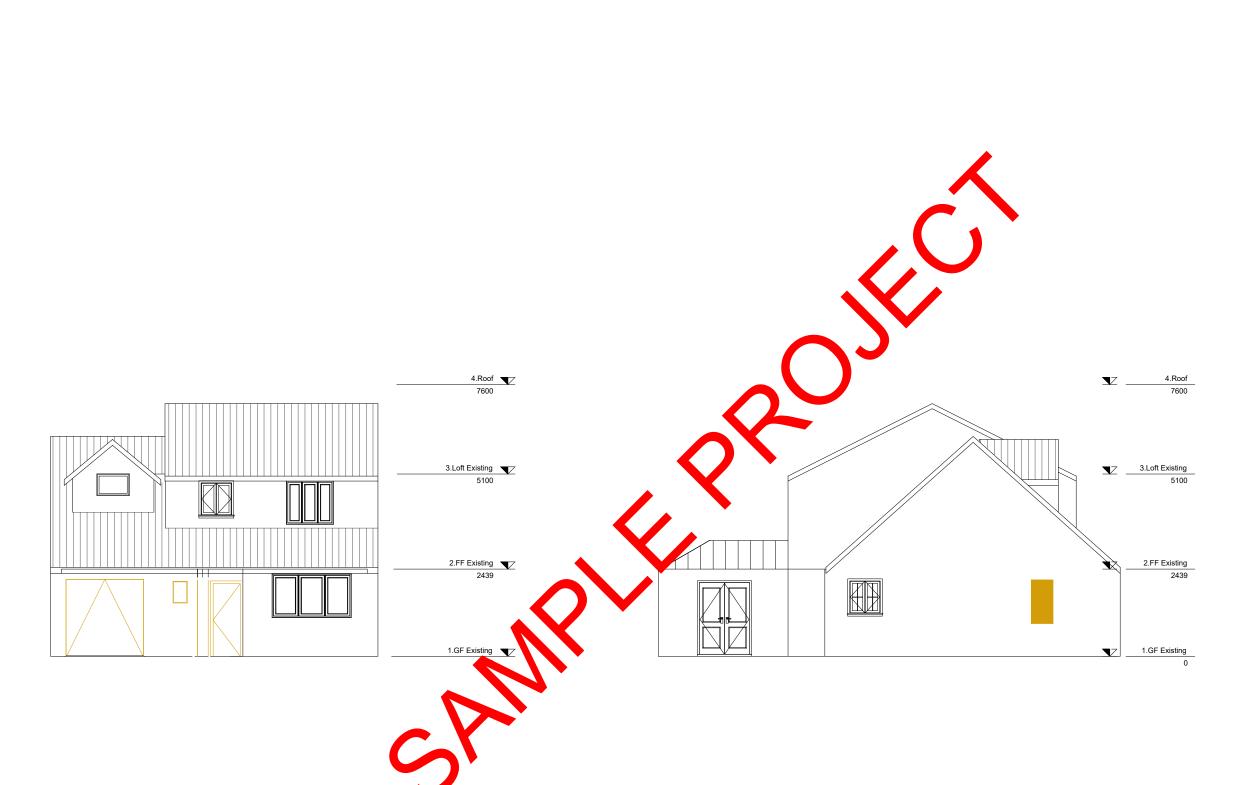
Designed MM Checked M
Drawn MM Approved M



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Client Name

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Section

# GARAGE CONVERSION

Stage

# ARCHITECTURAL

Drawing Title

# DEMO ELEVATIONS

Drawing Status

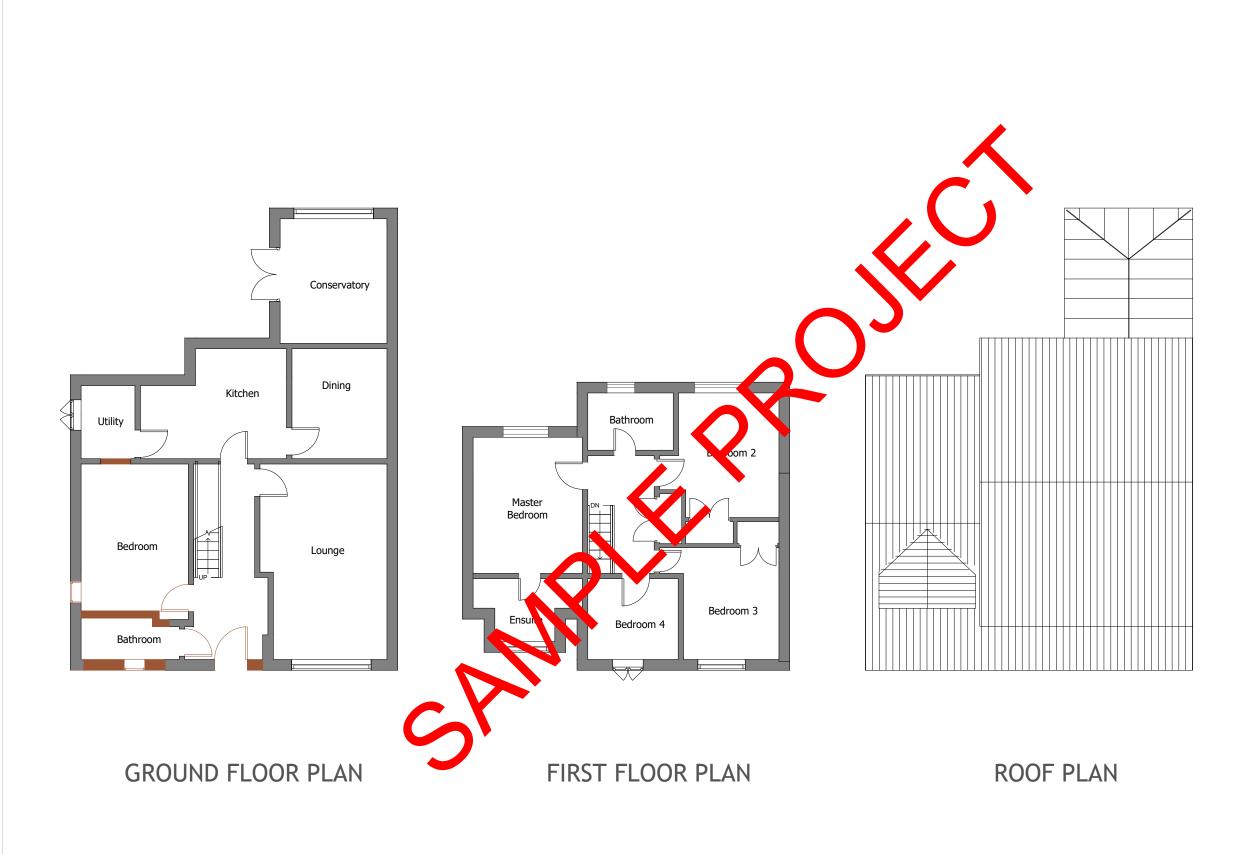
# FOR APPROVAL

Revisions and Notes

Project No.	202	4-03-CR0 8	3XW
Drawing No.	PLA	NNING-005	5
Revision		00	
Scale at A3		1:100	
Date		06-03-24	
Designed	MM	Checked	M٨
Descrip	***	Approved	888



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Client Name

ANIL WANGOO

Project Address

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Section

GARAGE CONVERSION

Stage

ARCHITECTURAL

Drawing Title

PROPOSED PLANS

Drawing Status FOR APPROVAL

Revisions and Notes

PLANNING-006 00 Revision

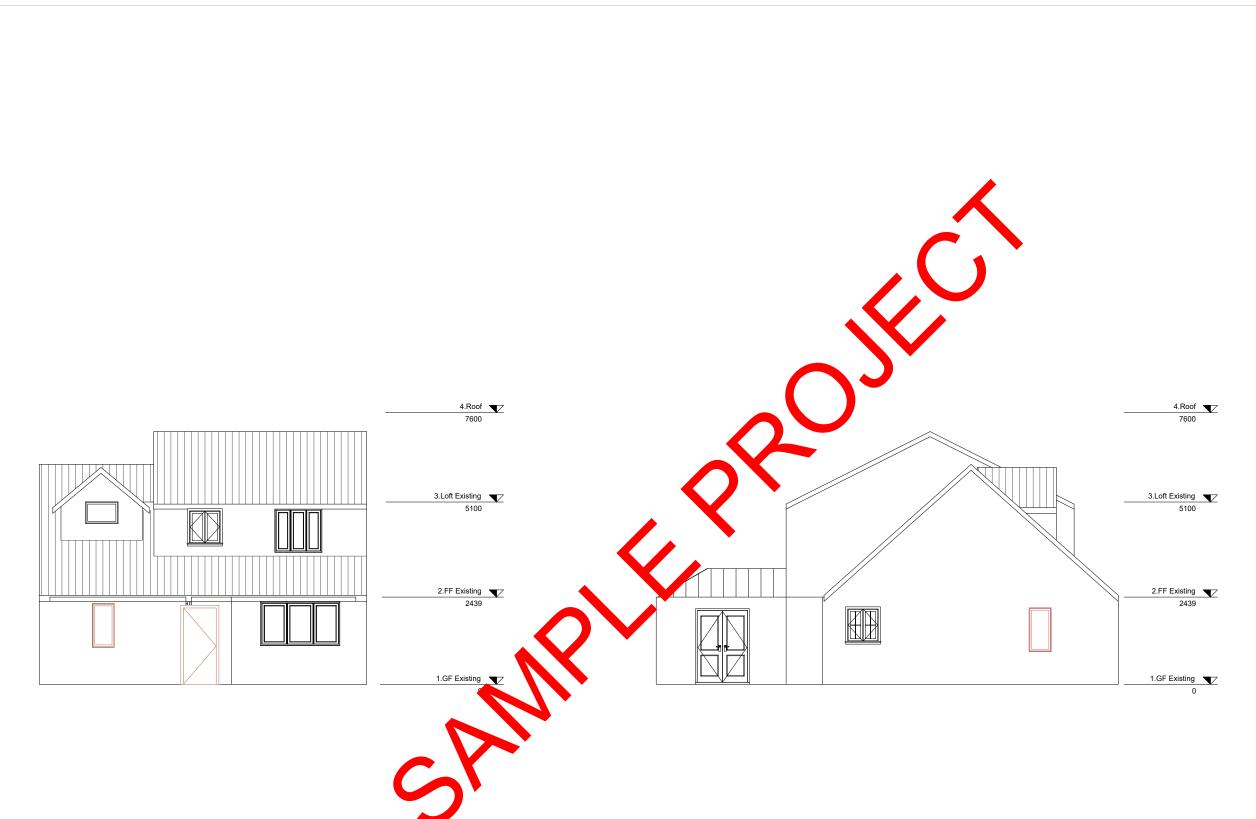
Scale at A3 1:100 06-03-24

MM Checked



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Client Name

Project Address

Section

GARAGE CONVERSION

Stage

ARCHITECTURAL

Drawing Title

# PROPOSED ELEVATIONS

Drawing Status

FOR APPROVAL

Revisions and Notes

Project No.	202	4-03-CR0 8	3XW
Drawing No.	PLA	NNING-007	7
Revision		00	
Scale at A3		1:100	
Date		06-03-24	
Designed	MM	Checked	M٨
Descrip	***	Approved	888



PEARL ENGINEERS PLANNERS & PROJECT MANAGERS

# **General Notes**

- 1. All drawings to be read in conjunction with all relevant specifications, architect's drawings and services engineer's drawings.
- 2. For setting out refer to architect's drawings.
- 3. All dimensions are in millimetres unless noted otherwise.
- 4. Do not scale from the drawings or the computer digital data. Only figured dimensions to be used
- 5. The contractor is to provide any temporary bracing necessary to maintain structural stability during construction.
- 6. The works have been designed and shall be constructed in accordance with the following codes. This list is not exhaustive and is only intended to list the 1. These notes are to be read in conjunction with relevant architect's and
- a) BS EN 1991-1-1:2002, BS EN 1991-1-7:2006: Code of practice for dead and imposed loads
- b) BS EN 1991-1-4:2005+A1:2010: Code of practice for wind loads.
- c) BS EN 1991-1-3:2003: Code of practice for imposed roof loads.
- d) BS EN 1997-1:2004: Code of practice for foundations.
- e) BS EN 1992-1-1:2004: Structural use of concrete.
- f) BS EN 1993-1-1:2005, BS EN 1993-1-5:2006, BS EN 1993-1-10:2005, BS EN 1993-5:2007, BS EN 1993-6:2007, BS EN 1993-1-8:2005: Structural use e) Timber to be carefully cut and planed to ensure tight fit and continuous of steelwork in buildings
- g) PD 6697:2010, BS EN 1996-3:2006, BS EN 1996-2:2006, BS EN 1996-1-1:2005+A1:2012: Structural use of un-reinforced masonry.
- h) BS EN 1995-1-1:2004+A1:2008: Structural use of timber.
- 7. The works have been designed for the finish state. The following superimposed loads have been used in the design: Floor loads - See structural engineer's calculations.
- Roof loads See structural engineer's calculations.
- 8. All works shall comply with the Building Regulations and other relevant statutory notices e.g. Health and Safety Bylaws, COSHH etc
- 9. The client / appointed contractor must take their own assurances on:
- a) Soil conditions on site and the gradient of land;
- b) Suitability / existing methods of storm water drainage;
- c) Trees (existing or removed) and their affect on foundations;
- d) Position and condition of main sewer.
- 10. Extensions/alterations to existing structures are subject to revision depending upon such being fully exposed. The client/thier contractor must take their own assurances that any structure designated for demolition/removal are not load bearing or that alternative methods of permanent support are put in place prior to removal. Existing walls, lintels and foundations that are intended to take additional loads, must first be fully exposed and checked for adequacy prior to the commencement of works.

# Foundations

- 1. The depth of the proposed foundations are subject to ground conditions and building control approval. These are to be minimum 1000mm deep subject to be founding in good ground of minimum 100kN/m2 bearing stratum (based on London Clay).
- 2. The excavations should be free from any mature tree roots. If there are

- large trees in the vicinity then the foundations depth is to be in accordance with NHBC standards guidelines for building near trees.
- 3. Where new foundations are to abut existing foundations, a soft joint of 75mm is to be formed using 'Claymaster' or similar approved unless noted 6. All vertical joints shall be completely filled. Bricks shall be laid frog up. The otherwise on the drawings.
- 4. Any foundations deeper than 1.5m should have suspended floors to avoid any heave. Where the foundations are cast within highly shrinkable soils, then anti-heave precautions such as compressible materials or void formers are to be applied to the foundations.

# Notes for Timber

- services engineer's drawings and specification.
- 2. All timber-work shall comply with BS EN 1995-1-1:2004+A1:2008.
- a) Roof joists shall be grade C24. Evidence of grading shall be provided before
- b) Blocking and battens shall be grade C24 softwood;
- c) The sizes shown on the drawings are finished sizes;
- d) In joint zones wanes, shakes and knots are not permitted;
- bearing against metalwork;
- f) All gaps between timber and metalwork to be resin-grouted, to the of the engineer.
- 4. All connectors, bolts, nails etc. shall be galvanised to BS 729.
- 5. Adhesive shall be to BS1204: Part 1: 1970, Type
- 6. All timber to be treated in accordance with the od Preservative itish \ and Damp-proofing Association Commodity Spe for 40 years cation desired service life

# Notes for Fire Resistance

- 1. These notes are to be re tion with relevant architect's services
- 2 All habitable do sure and the kitchen to be filled with
- enclosure, including glazing to doors, to be Any glaz
- . Mains interconnected smoke alarms to be provided to entrance all stairs landings
- ame spread to be provided to all new walls and ceilings.

#### Notes for Masonry

- 1. These notes are to be read in conjunction with relevant architect's services engineer's drawings and specifications.
- 2. All brickwork shall comply with PD 6697:2010, BS EN 1996-3:2006, BS EN 1996-2:2006. BS EN 1996-1-1:2005+A1:2012 .
- 3. All bricks shall have a minimum crushing strength of 20N/mm<sup>2</sup>.

- 4. Blockwork shall have a minimum crushing strength of 7N/mm<sup>2</sup>.
- 5. Mortar shall be a Class (ii) cement: lime putty: sand mix (1:1/2:4), unless indicated otherwise
- voids in perforated bricks shall be filled.
- 7. Fissured bricks or bricks with voids shall not be used.
- 8. Horizontal chases are prohibited. Vertical chases and builderswork holes shall be agreed with the architect.

#### Notes for Structural Steelwork

- 1. These notes are to be read in co services engineer's drawing and specifications
- 1-1:2005, BS EN 2. All steelwork shall composite S EN 1991 , BS EN 1993-5:2007, BS EN 1993-1-5:2006, B EN 1993-1 1993-6:2007, BS
- structural steelwork shall confirm to BS EN: Weldable st
- all steel shall be grade S355. Steel grade shall conform w
- herwise all butt welds shall be full penetration. ess noted
- otherwise all fillet welds shall be full profile with a minimum leg anath of 6mm
- 7. Unless noted otherwise all ordinary bolt assemblies shall be Grade 8.8.
- Unless noted otherwise all bolts shall be M16.
- 9. Unless noted otherwise all holding down bolts shall be M16 Grade 8.8 anchored a minimum of 200mm depth into the supporting concrete with a 100 x 100 x 8 thick washer plate at the embedded head of the bolt.
- 10. The clearance of base plates from supporting concrete shall be a minimum of 20mm and on completion of erection this shall be grouted solid under the full area of the base plate with 1:2 sand: cement grout.
- 11. Corrosion protection:
- a) Surface protection blast clean to SA 2.5 quality BS EN ISO 8501-1.
- b) Prefabricator primer epoxy zinc phosphate hb: 50 microns (DFT).
- c) Finishing coat see arch's spec.
- d) See arch's specification for details on colour and texture.
- 12. Fire protection
  - 30min One layer of plasterboard and skim coat or intumescent paint to manufacturer's specification.
  - 60min Two layers of plasterboard with joints staggered and skim coat or intumescent paint to manufacturer's specification.
- 13. Weather protection: Any steelwork exposed to external weather is either to be galvanized or stainless steel UNO.
- 14. All steel beams carrying load-bearing masonry walls wider than their flanges are to have 12mm thick top/bottom flange plates continuously welded along the length to suit the wall width UNO.

Note: The dimension deviation can be up to +/-75mm due to the tolerances and humar errors as the dimensions are recorded manually. All the dimensios must check on site by contractor and such dimensions to be

Client Name

Project Address

Section

**GARAGE CONVERSION** 

Stage

ARCHITECTURAL

Drawing Title **GENERAL NOTES** 

Drawing Status

FOR APPROVAL

Revisions and Notes

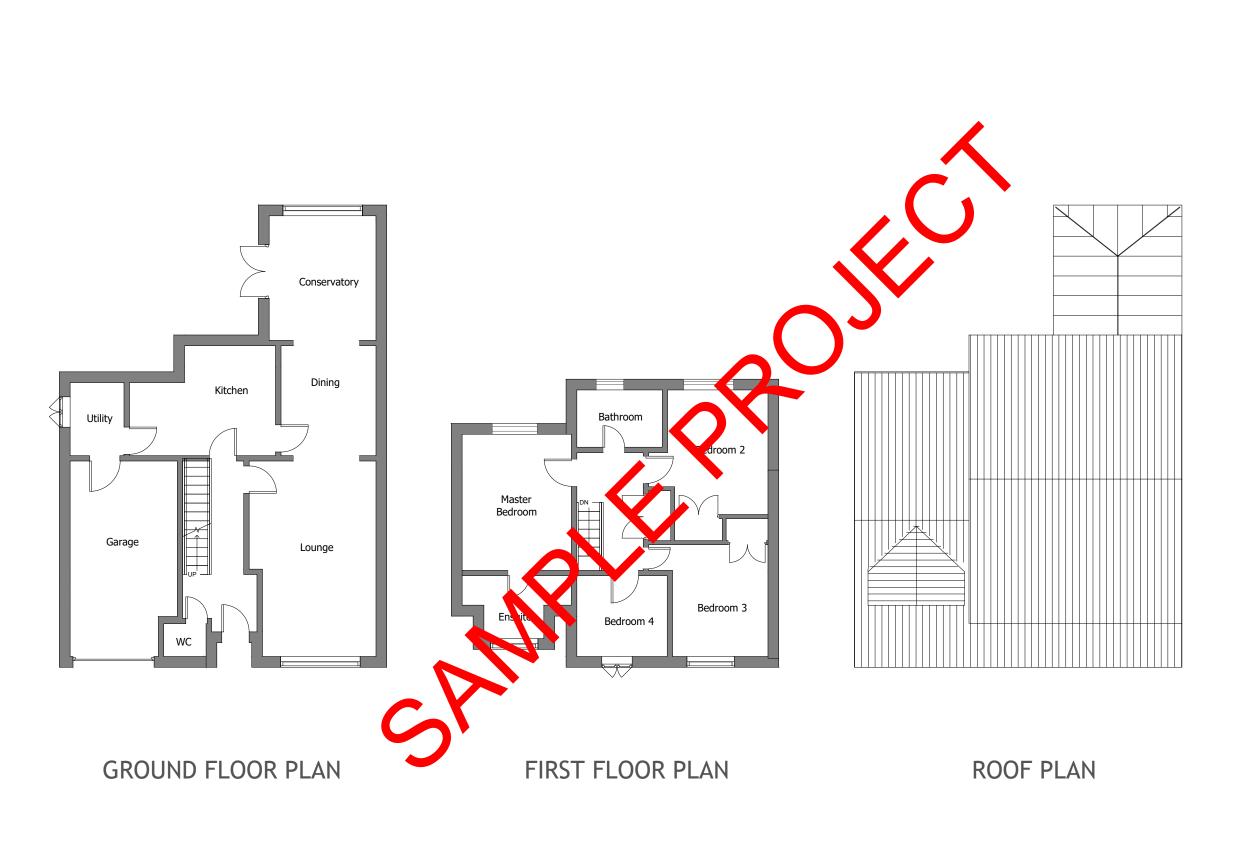
2024-03-CR0 8XW PLANNING-001 ററ Revision 1:100 Scale at A3 06-03-24

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Client Name

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GARAGE CONVERSION

Stage

ARCHITECTURAL

Drawing Title

EXISTING PLANS

Drawing Status

FOR APPROVAL

Revisions and Notes

 Project No.
 2024-03-CR0 8XW

 Drawing No.
 PLANNING-002

 Revision
 00

 Scale at A3
 1:100

 Date
 06-03-24

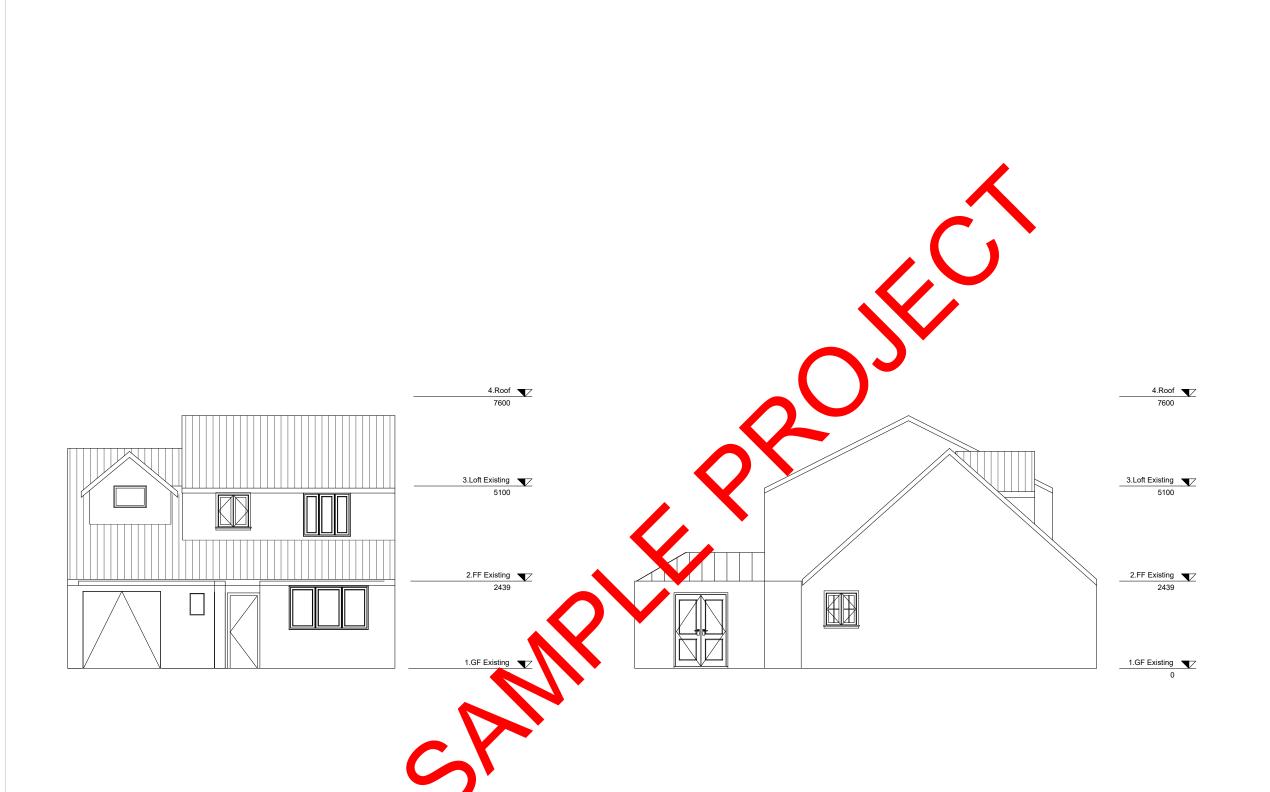
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 Drawn
 MM
 Approved
 MM



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Client Name

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GARAGE CONVERSION

Stage

ARCHITECTURAL

Drawing Title

EXISTING ELEVATIONS

Drawing Status

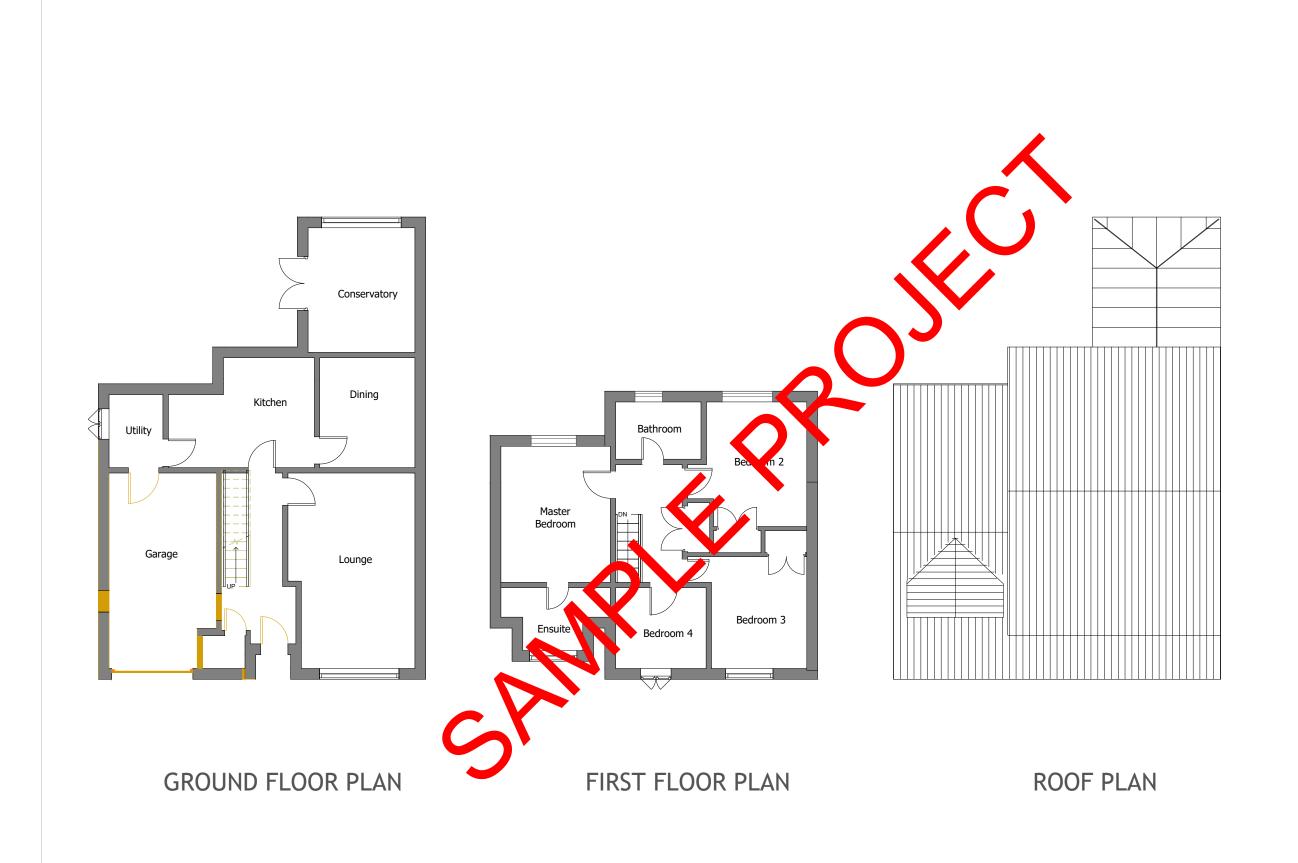
FOR APPROVAL

Revisions and Notes

Project No.	202	24-03-CR0 8	XW
Drawing No.	PLA	ANNING-003	3
Revision		00	
Scale at A3		1:100	
Date		06-03-24	
Designed	MM	Checked	M٨
Drawn	мм	Approved	٨٨٨



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Client Name

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GARAGE CONVERSION

Stage

ARCHITECTURAL

Drawing Title

DEMO PLANS

Drawing Status

FOR APPROVAL

Revisions and Notes

 Project No.
 2024-03-CR0 8XW

 Drawing No.
 PLANNING-004

 Revision
 00

 Scale at A3
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 Date
 06-03-24

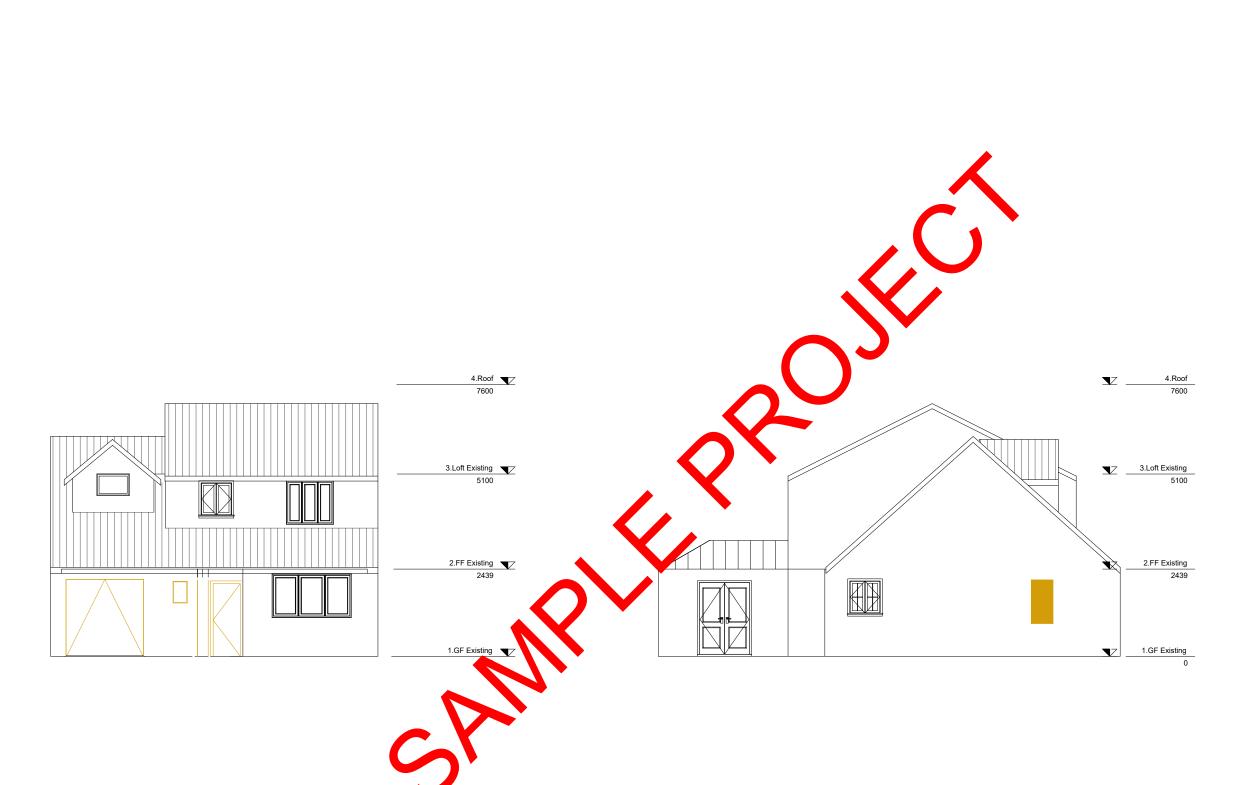
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Client Name

Project Address

Section

# GARAGE CONVERSION

Stage

# ARCHITECTURAL

Drawing Title

# DEMO ELEVATIONS

Drawing Status

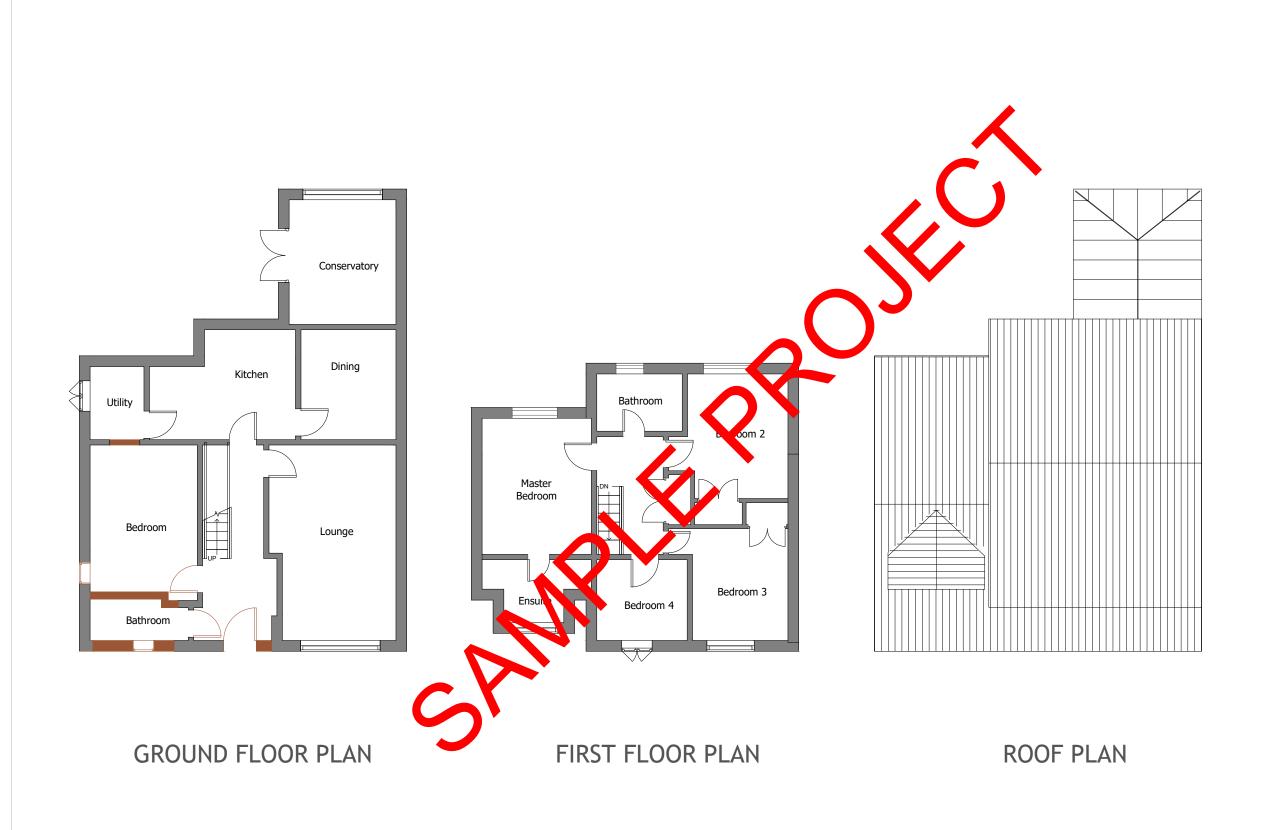
# FOR APPROVAL

Revisions and Notes

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Drawing No.	PLA	NNING-005	5
Revision		00	
Scale at A3		1:100	
Date		06-03-24	
Designed	MM	Checked	M٨
Descrip	***	Approved	888



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Stage

# ARCHITECTURAL

Drawing Title

# PROPOSED PLANS

Drawing Status

# FOR APPROVAL

Revisions and Notes

Project No. 2024-03-CR0 8XW

Drawing No. PLANNING-006

Revision 00

Scale at A3 1:100

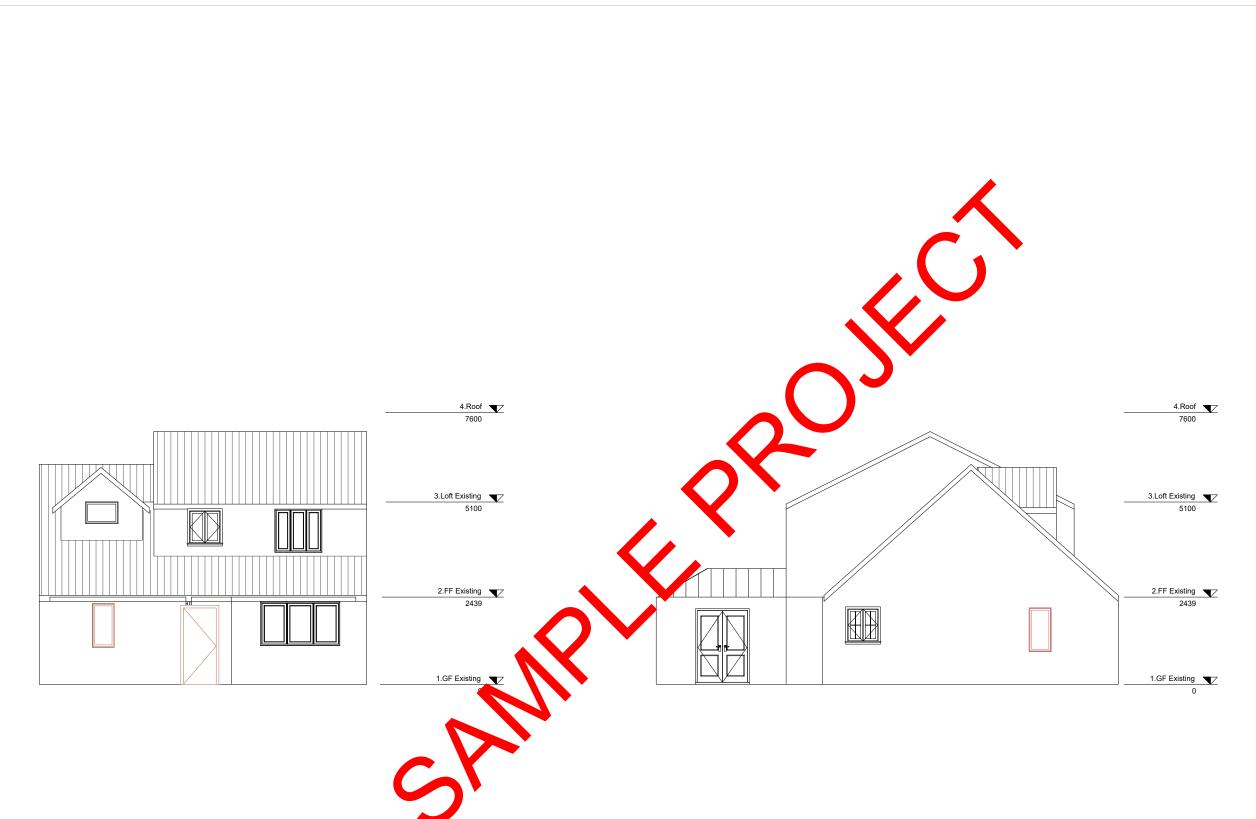
Date 06-03-24

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Client Name

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ARCHITECTURAL

Drawing Title

# PROPOSED ELEVATIONS

Drawing Status

FOR APPROVAL

Revisions and Notes

Project No.	202	4-03-CR0 8	3XW
Drawing No.	PLA	NNING-007	7
Revision		00	
Scale at A3		1:100	
Date		06-03-24	
Designed	MM	Checked	M٨
Descrip	***	Approved	888



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#### ELECTRICAL

ALL ELECTRICAL WORK REQUIRED TO MEET THE REQUIREMENTS OF PART P (ELECTRICAL SAFETY) MUST BE DESIGNED, INSTALLED, INSPECTED AND TESTED BY A COMPETENT PERSON REGISTERED UNDER A COMPETENT PERSON SELF CERTIFICATION SCHEME SUCH AS BRE CERTIFICATION LTD, BSI, NICEIC CERTIFICATION SERVICES OR ZURICH LTD. AN APPROPRIATE BS7671 ELECTRICAL INSTALLATION CERTIFICATE IS TO BE ISSUED FOR THE WORK BY A PERSON COMPETENT TO DO SO. A COPY OF A CERTIFICATE WILL BE GIVEN TO BUILDING CONTROL ON COMPLETION.

#### INTERNAL LIGHTING

INSTALL LOW ENERGY LIGHT FITTINGS THAT ONLY TAKE LAMPS HAVING A LUMINOUS EFFICIENCY BETTER THAN 80 LUMENS PER CIRCUIT WATT. ALL FIXED TO HAVE LIGHTING CAPACITY (LM) 185 X TOTAL FLOOR AREA, TO COMPLY WITH PART L OF THE CURRENT BUILDING REGULATIONS AND THE DOMESTIC BUILDING SERVICES COMPLIANCE GUIDE.

#### SMOKE DETECTERS:

L3 FIRE ALARM SYSTEM TO BS 5839 TO BE INSTALLED (PROTECTION OF ESCAPE ROUTES). MAINS POWERED SMOKE DETECTORS(SD), WITH BACKUP BATTREY, TO BE FITTED IN HALLWAY AND UPPER LANDINGS, ALL LINKED TO EACH OTHER AND ON AN INDEPENDANT CIRCUIT WITH A SEPERATE FUSE.

ALL SMOKE DETECTORS(SD) & ALARMS (TO BS 5446-1) TO BE MAINS POWERED, WITH BACKUP BATTERY AND TO BE FITTED IN THE CIRCULATION SPACE IN HALLWAY AND ALL UPPER LANDINGS, ALL LINKED TO EACH OTHER AND ON AN INDEPENDENT CIRCUIT WITH A SEPARATE FUSE. EXACT POSITIONS TO BE CONFIRMED ON SITE

#### FIRE DOORS

ALL DOORS TO HABITABLE ROOMS WITHIN STAIR ENCLOSURE TO BE FD30 DOORS FITTED WITH A PERKOMATIC SELF CLOSER. 25X38MM DOOR STOPS GLUED AND SCREWED TO FRAME. THIS IS NOT REQUIRED FOR A TWO STORY (GROUND+FIRST FLOOR) BUILDING BUT STRONGLY RECOMMENDED. DOORS TO BE FULL PANEL DOORS WITH NO GLAZING.

DETAILS ON CABLING FOR COMPUTERS AND NETWORKING, TELEPHONE, SECURITY SYSTEM, MUSIC SYSTEM, DOOR ENTRY AND CONTROL SYSTEM, ETC. TO BE AGREED SEPARATELY.

ALL ELECTRICAL WIRING & INSTALLATIONS TO CONFORM TO BS7671 "REQUIREMENTS FOR ELECTRICAL INSTALLATIONS" AND ANY OTHER REGULATIONS APPLICABLE TO SIMILAR RESIDENTIAL HOUSES.

THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL THE TEMPORARY WORKS, THE STABILITY OF THE EXISTING STRUCTURE, EARTHWORKS, EXCAVATIONS, ETC; THE CONTRACTOR WILL ENSURE THAT THE BUILDINGS WILL BE ADEQUATELY SUPPORTED AT ALL STAGES OF CONSTRUCTION, INCLUDING ANY EARTHWORK SUPPORTS MADE NECESSARY BY EXCAVATIONS AND GROUND CONDITIONS. THE SUPPORTS AND PROPS TO BE PROVIDED TILL THE FINAL RETAINING WALL IS IN PLACE.



#### NEW AND REPLACEMENT WINDOWS

NEW AND REPLACEMENT WE DOWS TO BE DOUBLE GLAZED WITH 16-20MM ARGON GAP AND SOFT COAT LOW-E GLASS. WINDOW ENERGY RATE OF TO BE BAND BOR BETTER AND TO ACHIEVE U-VALUE OF 1.4 W/M²K. THE POOR AND VINDOW OP LINGS SHOULD BE LIMITED TO 25% OF THE EXTENSION FLOOR AREA PLANT THE AREA OF THE ATTENSION OPENINGS COVERED BY THE EXTENSION. INSULATED TO STERRO AND TO BE USED IN REVEALS TO ABUT JAMBS AND TO BE CONSIDERED WITHIN DEVEAL OPENIS. FULLY ISULATED AND CONTINUOUS CAVITY CLOSERS TO BE USED AROUND IN YEALS.

WINDOWS AND DOOR WES TO BE TAPED TO SURROUNDING OPENINGS USING AIR SEALING TAPE.
WINDOWS TO BE TIED WITH TRICKLE VENTS TO PROVIDE ADEQUATE BACKGROUND VENTILATION
IN CORDANCE ITH APPROVED DOCUMENT F.

#### NEW AN REPLACEMENT DOORS

AND REPLACEMENT DOORS TO ACHIEVE A U-VALUE OF 1.4W/M<sup>2</sup>K. GLAZED AREAS TO BE DOUBLE GLAZED WITH 16-20MM ARGON GAP AND SOFT LOW-E GLASS. GLASS TO BE TOUGHENED OR LAMINATED SAFETY GLASS TO BS 6206, BS EN 14179 OR BS EN ISO 12543-1 AND PART K OF THE CURRENT BUILDING REGULATIONS.

INSULATED PLASTERBOARD TO BE USED IN REVEALS TO ABUT JAMBS AND TO BE CONSIDERED WITHIN REVEAL SOFFITS. FULLY INSULATED AND CONTINUOUS CAVITY CLOSERS TO BE USED AROUND REVEALS.

WINDOWS AND DOOR FRAMES TO BE TAPED TO SURROUNDING OPENINGS USING AIR SEALING TAPE. THERMAL RELIGING

CARE SHALL BE TAKEN TO LIMIT THE OCCURRENCE OF THERMAL BRIDGING IN THE INSULATION LAYERS CAUSED BY GAPS WITHIN THE THERMAL ELEMENT, (I.E. AROUND WINDOWS AND DOOR OPENINGS). REASONABLE PROVISION SHALL ALSO BE MADE TO ENSURE THE EXTENSION IS CONSTRUCTED TO MINIMIZE UNWANTED AIR LEAKAGE THROUGH THE NEW BUILDING FABRIC.

#### MATERIALS AND WORKMANSHIP

ALL WORK WILL COMPLY WITH THE THE CURRENT BUILDING REGULATIONS AND WILL BE CARRIED OUT TO THE SATISFACTION OF THE BUILDING CONTROL INSPECTOR.

ALL STAGES OF WORK ARE TO BE CHECKED AND AGREED ON SITE WITH THE BUILDING INSPECTOR BEFORE COVERING OVER.

THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL THE TEMPORARY WORKS, THE STABILITY OF THE EXISTING STRUCTURE, EARTHWORKS, EXCAVATIONS, ETC; THE CONTRACTOR WILL ENSURE THAT THE BUILDINGS WILL BE ADEQUATELY SUPPORTED AT ALL STAGES OF CONSTRUCTION, INCLUDING ANY EARTHWORK SUPPORTS MADE NECESSARY BY EXCAVATIONS AND GROUND CONDITIONS. THE SUPPORTS AND PROPS TO BE PROVIDED TILL THE FINAL RETAINING WALL IS IN PLACE.

Note: The dimension deviation can be up to +/-75mm due to the tolerances and human errors as the dimensions are recorded manually. All the dimensios must check on site by contractor and such dimensions to be their responsibility

Client Name

Project Address

Section

GARAGE CONVERSION

Stage

ARCHITECTURAL

Drawing Title

STRUCTURAL PLAN

Drawing Status

FOR APPROVAL

Revisions and Notes

roject No. 2024-03-CR0 8XW

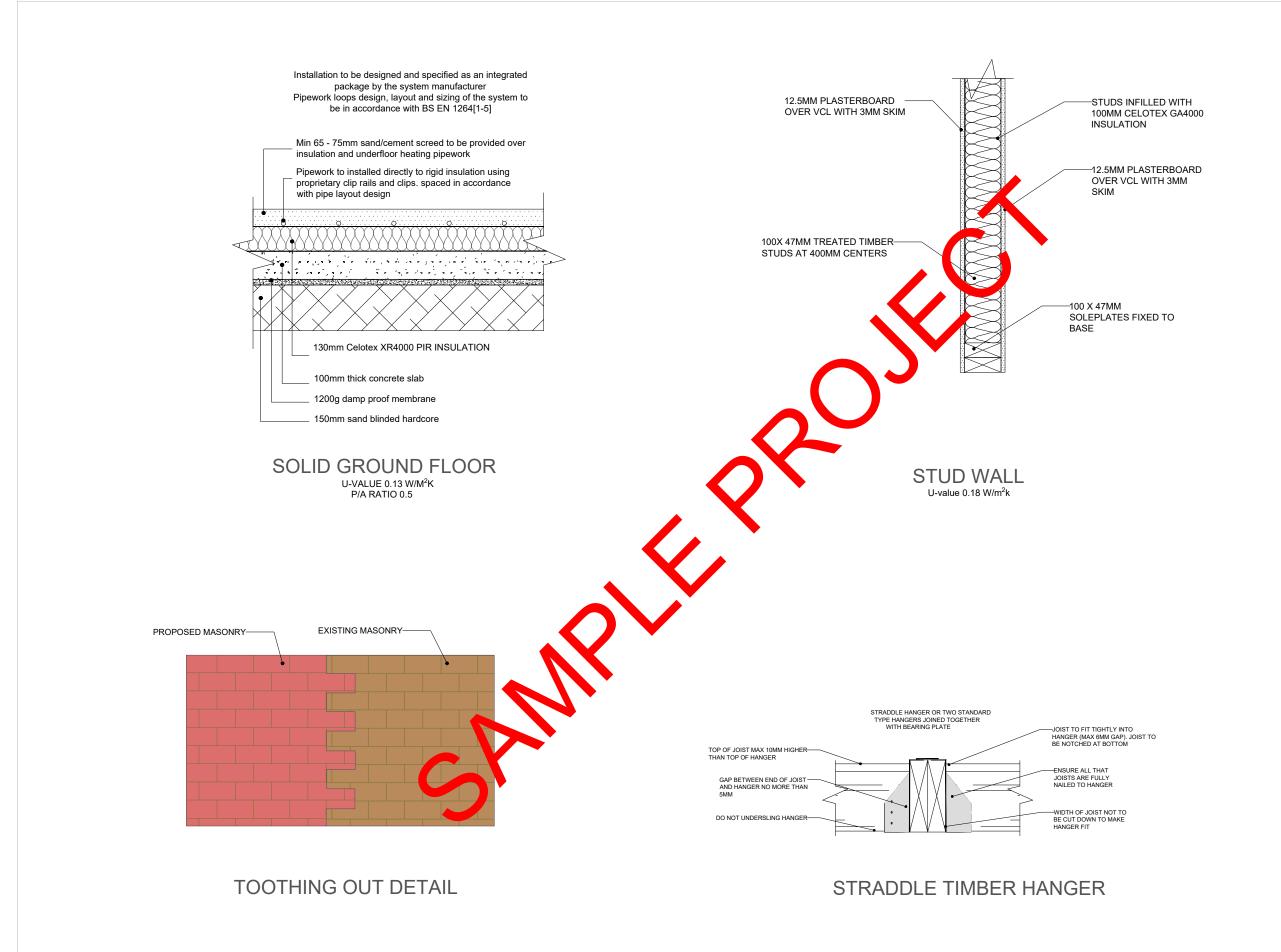
Drawing No. PLANNING-008
Revision 00



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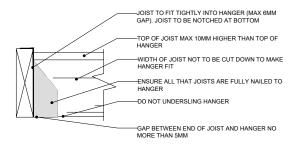
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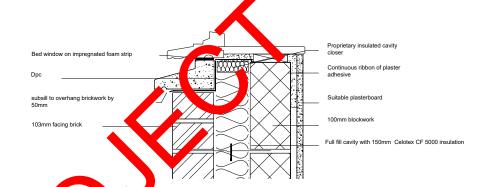
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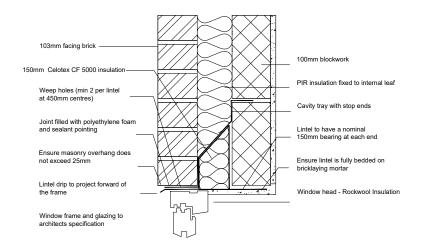
# STANDARD TIMBER HANGER

# WHERE THE WALL SUPPORTING THE JOISTS IS OVER 3M LONG RESTRAINT TYPE HANGERS ARE REQUIRED TOP OF JOIST MAX 10MM HIGHER THAN TOP OF HANGER MASONRY HANGER TO BS 5628. TO BE USED WITH CORRECT STRENGTH BLOCK HEIGHT OF MASONRY ABOVE FLANGE 675MM OR AS RECOMMENDED BY MANUFACTURER ALLOW TO HARDEN BEFORE APPLYING LOADS HEIGHT OF MASONRY ABOVE FLANGE 675MM OR AS RECOMMENDED BY MANUFACTURER ALLOW TO HARDEN BEFORE APPLYING LOADS MANUFACTURER ALLOW TO HARDEN BEFORE APPLYING LOADS WIDTH OF MESTINGTURE ALLOW TO HARDEN BEFORE APPLYING LOADS SUPPORT HANGER ON FULL MASONRY BLOCK HANGER TO BE TIGHT TO THE WALL

RESTRAINT MASONRY HANGER



# WINDOW SILL



WINDOW HEAD AND LINTEL

Note: The dimension deviation can be up to +/-75mm due to the tolerances and human errors as the dimensions are recorded manually.

All the dimensios must check on site by contractor and such dimensions to be their responsibility

Client Name

Project Address

Section

GARAGE CONVERSION

Stage

ARCHITECTURAL

Drawing Title

STRUCTURAL DETAILS

Drawing Status

FOR APPROVAL

Revisions and Notes

 Project No.
 2024-03-CR0 8XW

 Drawing No.
 PLANNING-010

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 Scale at A3
 N.T.S

 Date
 06-03-24

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 MM

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 MM



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# STRUCTURAL CALCULATION REPORT

Client Name Axxxx
Client Address xxxx

Project Reference: 2024-03- CR08XW

02 TOWERFIELDS WESTERHAM ROAD BROMLEY, BR2 6HF

info@ Pearlepp.co.uk

www. Pearlepp.co.uk

Tel no. 02035763199



> Email: info@Pearlepp.co.uk Website: www. pearlepp.co.uk Tel no. 02035763199

Project: xxx	Sheet No./Rev.
Filipect. XXX	2

Job Ref. 2024-03-CR08XW Structural Engineer

MM

Date 22/03/2024

# **Document Control:**

Purpose/Status	Date	Rev.	Comments	Structural Engineer	
Approval Issue	22/03/2024		B'Regs Issue	ММ	

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# **Project Information**

Design Codes – Eurocodes and their respective National Annexes:

BS EN 1990. Eurocode 0: 'Basis of structural design'

BS EN 1991. Eurocode 1: 'Actions on structures'

BS EN 1992. Eurocode 2: 'Design of concrete structures'

BS EN 1993. Eurocode 3: 'Design of steel structures'

BS EN 1995. Eurocode 5: 'Design of timber structures'

BS EN 1996. Eurocode 6: 'Design of masonry structures' BS EN

1997. Eurocode 7: 'Geotechnical Design'

#### **ASSUMPTIONS**

THE FOLLOWING ASSUMPTIONS ARE MADE ABOUT THE TE. THEY ARE TO BE CHECKED ON SITE BY
THE CONTRACTOR AND BUILDING CONTROL OFFICE REGION TO THE START OF THE WORKS. ANY DIFFERENCES ARE
TO BE REPORTED TO PEPP IMMEDIATELY

- 1. The existing masonry is assumed to be inimpositely 3.6N/mm<sup>2</sup> blockwork in a 1:2:8 mortar
- 2. Floor joists are assumed to pan as indicated on the drawings.
- 3. The external walls are assumed be avity brickwork.

#### **NOTES**

Contracto chick and imensions before ordering any steel.

All materia and whemanship must fully comply with all relevant current British Standard and Codes of practice.



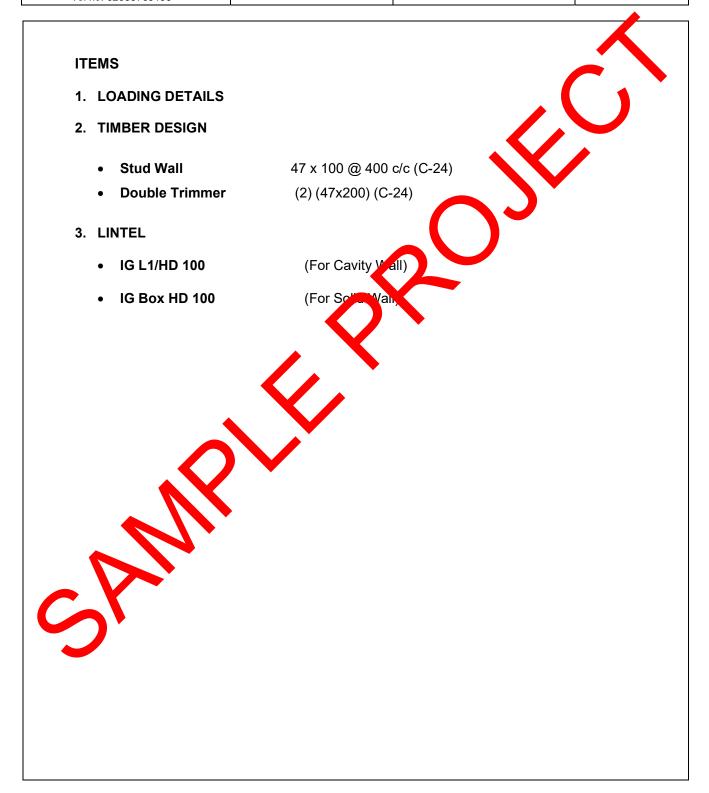
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# 1. LOADING DETAILS

PITCHED ROOF			
Clay Tiles	=	0.65	KN/m <sup>2</sup>
Felt and battens	=	0.05	KN/m <sup>2</sup>
Timber rafters	=	0.1	KN/11 <sup>2</sup>
Insulations and other membranes	=	0.1	1 1/m <sup>2</sup>
Ceiling and services	=	0.2	KN).
Total dead load on the slope	=	1.1	K. (m²
Live Load	=	0.6	KN/ <sup>2</sup>
LOFT FLOOR		0.0	Kiv/i
Plywood Flooring		0.1	KN/m <sup>2</sup>
Timber Joists	=	.2	KN/m <sup>2</sup>
Insulation	<b>⋖</b> ⊿		KN/m²
Ceiling and services	X	0.2	KN/m <sup>2</sup>
Partitions	_	0.5	, KN/m²
Total dead load	=	1.10	KN/m²
Live Load	=	1.5	KN/m²
FIRST FLOOR			•
Plywood Flooring	=	0.15	KN/m2
Timber Joists	=	0.2	KN/m2
Insulation	=	0.05	KN/m2
Ceiling and services	=	0.2	KN/m2
Partitions	=	0.5	KN/m <sup>2</sup>
Total dead loa	=	1.10	KN/m²
Live Load	=	1.5	KN/m <sup>2</sup>
WALL L. Y.			
Brick wall (192 mm.)	=	2	KN/m <sup>2</sup>
B. ck w. "with plaster	=	1.9	KN/m <sup>2</sup>
Glair <sub>3</sub>	=	0.5	KN/m <sup>2</sup>



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#### 2. TIMBER DESIGN

Stud Wall

47 x 100 @ 400 c/c (C-24)

#### TIMBER STUD DESIGN (BS5268-2:2002)



#### Stud details

Stud breadth; b = 47 mm Stud depth; h = 100 mm Number of studs;  $N_s = 1$ 

Strength class Caltimus (Table 8 BS5268:Pt 2:2002)

# Section prop

Cross sectional are:  $A = N_s \times b \times h = 4700 \text{ mm}^2$  Section, for this,  $Z = N_s \times b \times h^2 / 6 = 78333 \text{ mm}^3$  Moment on pertia in the major axis;  $I_x = N_s \times b \times h^3 / 12 = 3916667 \text{ mm}^4$ 

ome, of inexia in the minor axis;  $I_y = N_s \times h \times b^3 / 12 = 865192 \text{ mm}^4$ 

Radius of gyration in the major axis;  $r_x = \sqrt{(I_x / A)} = 28.9 \text{ mm}$ Radius of gyration in the minor axis;  $r_y = \sqrt{(I_y / A)} = 13.6 \text{ mm}$ 

# nel details - Studs restrained by sheathing in the plane of the panel

Panel height; L = 2400 mmStud length;  $L_s = L - (2 \times b) = 2306 \text{ mm}$ 

Standard stud spacing;  $s_s = 400 \text{ mm}$ Panel opening; O = 0 mm

Loaded panel length;  $s = max(s_s, (O + s_s) / 2) = 400 \text{ mm}$ 

Effective length in the major axis;  $L_{ex} = 0.85 \times L_{s} = 1960 \text{ mm}$ 

Slenderness ratio;  $\lambda = L_{ex} / r_x = 67.90$ 



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Vertical loading details Dead loads Imposed loads

Roof UDL;  $U_{r_d} = 5.00 \text{ kN/m};$   $U_{r_i} = 5.00 \text{ kN/m};$   $U_{f_i} = 5.00 \text{ kN/m};$   $U_{f_i} = 5.00 \text{ kN/m};$   $U_{f_i} = 5.00 \text{ kN/m};$ 

Imposed floor load duration; Long term

**Modification factors** 

Section depth factor;  $K_7 = (300 \text{ mm / h})^{0.11} = 1.13$ 

Load sharing factor;  $K_8 = 1.10$ 

Consider axial compression without bending under medium term loads

Load duration factor;  $K_3 = 1.25$ 

Vertical loading;  $F = (U_{r_d} + U_{f_d} + U_{f_d} + U_{f_d})$  s = **.00** kN

Check compressive stress on stud

Compression member factor;  $K_{12} = 0.57$ 

Compression parallel to grain;  $\sigma_c = 7 \ \text{JO} \ \text{nm}^2$ 

Permissible compressive stress;  $\sigma_c = \sigma_c \times K_8 \times K_{12} = 6.200 \text{ N/mm}^2$ Applied compressive stress;  $(N_s \times b \times h) = 1.702 \text{ N/mm}^2$ 

PASS - Applied compressive stress under measure term loads is within permissible limits

Check compressive stress on rail

Bearing stress modification factor; = 1.24

Compression perpendicular to grain  $\sigma$  wane);  $\sigma_{cp} = 2.400 \text{ N/mm}^2$ 

Permissible compressive stress;  $\sigma_{cp1\_adm} = \sigma_{cp1} \times K_3 \times K_4 = 3.717 \text{ N/mm}^2$ 

Applied compressive stress;  $\sigma_{cp1\_max} = F / (N_s \times b \times h) = 1.702 \text{ N/mm}^2$ 

PASS - Applied compress stress under medium term loads is within permissible limits

Consider axial committee ion it it is ending under long term loads

Load duration factor;  $K_3 = 1.00$ 

Vertical loading:  $F = (U_{r_d} + U_{f_d} + U_{f_i})$  s = 6.00 kN

Check compress to st. ss on stud

Composion member factor;  $K_{12} = 0.61$ 

Compression lel to grain;  $\sigma_c = 7.900 \text{ N/mm}^2$ 

missible ampressive stress;  $\sigma_{c\_adm} = \sigma_c \times K_3 \times K_8 \times K_{12} = 5.301 \text{ N/mm}^2$ applies a pressive stress;  $\sigma_{c\_max} = F / (N_s \times b \times h) = 1.277 \text{ N/mm}^2$ 

PASS - Applied compressive stress under long term loads is within permissible limits

he k compressive stress on rail

earing stress modification factor;  $K_4 = 1.24$ 

Compression perpendicular to grain (no wane);  $\sigma_{cp1} = 2.400 \text{ N/mm}^2$ 

Permissible compressive stress;  $\sigma_{\text{cp1\_adm}} = \sigma_{\text{cp1}} \times \text{K}_3 \times \text{K}_4 = \textbf{2.974 N/mm}^2$  Applied compressive stress;  $\sigma_{\text{cp1\_max}} = \text{F} / (\text{N}_s \times \text{b} \times \text{h}) = \textbf{1.277 N/mm}^2$ 

PASS - Applied compressive stress under long term loads is within permissible limits



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# **Applied loading**

#### **Beam loads**

SW DL LL

Dead self weight of beam 1 Dead full UDL 3.000 kN/m Imposed full UDL 2.000 kN/m

#### Load combination

Load combir

Dead 1.00 Support A Imposed 1.00

Dead 1.00 Span 1

Imposed 1.00

Dead 1.00 Support B

Imposed 1.00

#### vsis results

aximum moment;

 $M_{max} = 0.768 \text{ kNm};$ 

 $M_{min} = 0.000 \text{ kNm}$ 

esign moment; Maximum shear;  $M = max(abs(M_{max}), abs(M_{min})) = 0.768 \text{ kNm}$ 

Design shear;

 $F_{max} = 2.793 \text{ kN};$  $F = max(abs(F_{max}), abs(F_{min})) = 2.793 \text{ kN}$ 

 $F_{min} = -2.793 \text{ kN}$ 

Total load on beam;

 $W_{tot} = 5.585 \text{ kN}$ 

 $R_{A_{max}} = 2.793 \text{ kN};$ 

 $R_{A_{min}} = 2.793 \text{ kN}$ 

Reactions at support A;

R<sub>A\_Dead</sub> = **1.693** kN

Unfactored dead load reaction at support A;

R<sub>A Imposed</sub> = 1.100 kN

Unfactored imposed load reaction at support A; Reactions at support B;

 $R_{B_{max}} = 2.793 \text{ kN};$ 

 $R_{B min} = 2.793 kN$ 



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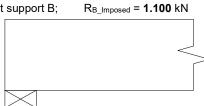
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Unfactored dead load reaction at support B;

Unfactored imposed load reaction at support B;





ng term

 $L_b = 100 \text{ mm}$ 

L<sub>s</sub> 1100 mm

A = N × b × h = **18800** mm<sup>2</sup>  $Z_x = N \times b \times h^2 / 6 =$ **626667**mm<sup>3</sup>

 $i_x = \sqrt{(I_x / A)} = 57.7 \text{ mm}$  $i_y = \sqrt{(I_y / A)} = 27.1 \text{ mm}$ 

 $K_3 = 1.00$ 

 $K_4 = 1.00$ 

 $Z_v = h \times (N \times b)^2 / 6 = 294533 \text{ mm}^3$ 

 $I_x = N \times b \times h^3 / 12 = 62666667 \text{ mm}^4$  $I_y = h \times (N \times b)^3 / 12 = 13843067 \text{ mm}^4$ 

R<sub>B\_Dead</sub> = **1.693** kN

#### **Timber section details**

Breadth of sections; b = 47 mmDepth of sections; h = 200 mm

Number of sections in member; N = 2Overall breadth of member;  $b_b = 14 \text{ mm}$ Timber strength class;

**←**100**→** 

#### Member details

Service class of timber;

Load duration;

Length of span;

Length of bearing;

#### Section properties

Cross sectional area of meber;

Section modulus;

Second moment of rea

Radius of gyratin;

# dification factors

Uratic Le bading - Table 17; Burng stress - Table 18;

[ot] depth of member - cl.2.10.6;  $K_7 = (300 \text{ mm / h})^{0.11} = 1.05$ 

ad sharing - cl.2.9; K<sub>8</sub> = **1.00** 

#### Lateral support - cl.2.10.8

Ends held in position

Permissible depth-to-breadth ratio - Table 19; 3.00

Actual depth-to-breadth ratio;  $h / (N \hat{b}) = 2.13$ 

PASS - Lateral support is adequate

#### Compression perpendicular to grain

Permissible bearing stress (no wane);  $\sigma_{c\_adm} = \sigma_{cp1} - K_3 - K_4 - K_8 = 2.400 \text{ N/mm}^2$ 



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Applied bearing stress;

$$\sigma_{c_a} = R_{A_{max}} / (N - b - L_b) = 0.297 \text{ N/mm}^2$$

 $\sigma_{c_a} / \sigma_{c_adm} = 0.124$ 

PASS - Applied compressive stress is less than permissible compressive stress thearing

Bending parallel to grain

Permissible bending stress;  $\sigma_{m \text{ adm}} = \sigma_{m} \stackrel{\frown}{K}_{3} \stackrel{\frown}{K}_{7} \stackrel{\frown}{K}_{8} = 7.842 \text{ N/r}$ 

Applied bending stress;  $\sigma_{m_a} = M / Z_x = 1.225 \text{ N/mm}^2$ 

 $\sigma_{m_a} / \sigma_{m_adm} = 0.156$ 

PASS - Applied bending stress is less than rmis ble be ding stress

Shear parallel to grain

Permissible shear stress;  $\tau_{adm} = \tau - K_3 - V_{mm}$ 

Applied shear stress;  $\tau_a = 3 \cdot F / (2 \cdot A) = 0.2.3 \text{ N/mm}^2$ 

 $\tau_a / \tau_{adm} = 0.314$ 

PASS - Applied short stress is man permissible shear stress

Deflection

Modulus of elasticity for deflection;

Permissible deflection;

Bending deflection; Shear deflection;

Total deflection;

Em. **7200** N/mm<sup>2</sup>

 $\delta_{ad}$  = min 551 in, 0.003  $L_{s1}$  = **3.300** mm

s<sub>1</sub> = **0.215** mm s<sub>1</sub> = **0.109** mm

 $\delta_a = \delta_{b_s1} + \delta_{v_s1} = 0.323 \text{ mm}$ 

 $\delta_a$  /  $\delta_{adm}$  = 0.098

ASS - Total deflection is less than permissible deflection



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# 3. LINTEL

• IG L1/HD 100

(For Cavity walls with 90-105mm cavity)

We had taken loadings being applied on our lintel:

- Floor Load
- · Cavity wall Load

Our load derivation for each source for lintel is as follows;

#### Floor Load;

Dead Load: 1.1 kN/m<sup>2</sup>

Live Lead: 0.6 kN/m<sup>2</sup>

Tributary Length = 1.5 m

Dead Load (UDL) = 1.1 x 1.5 = 1.65 kN/

Live Load (UDL) =  $0.6 \times 1.5 = 0.96 \text{ M/m}$ 

# **Cavity Wall Load;**

Dead Load: 4.4 kN/m<sup>2</sup>

Dead Load (UDL) = 112 km

Total Dead Load (): = 3.85 KN/m

Total Live Day (ULL): = 1 KN/m

Tot | \_ \_ d (UDL = 13.85 KN/m

Hence

required Load Carrying Capacity = 13.85 KN Required

gth = 1000 (with bearing on both sides)

IG L1/HD 100 Lintel for 100 mm cavity of 1000 mm as Per Requirement can carry = 22 KN

Load Carrying capacity of Provided Lintel = 22 KN

Hence,

# Provided > Required



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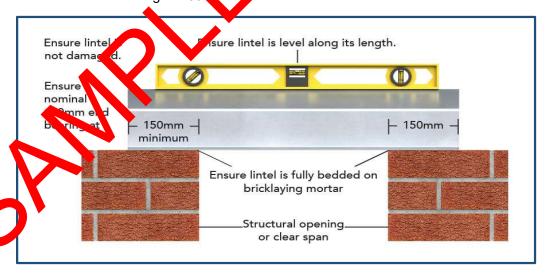
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# Select a suitable lintel according to the span

Length	Height	Thickness	Total UDL KN 3:1	Total UDL KN 19:1
600	110	2.9	30	22
1200				
1350	135	2.9	30	
1500				
1650	163	2.9	40	35
2100				
2250	203	2.9		35
2550				
2700	203	3.2	0	35
3000				
3150	203	3.2		32
3600				
3750	203		33	28
4200				

# **Installation**

Provide a minimum bearing of 150 m or both sides





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• IG Box HD 100

(For solid wall)

Select a suitable lintel according to the span

Length (mm)	Height (mm)	Thickness (mm)	otal UDL kN
600	150	2.5	50
1200	150		
1350	150	2.5	45
1800	150		
1950	215	25	50
2400	210		
2550	215	2.5	40
2700	210		

# **Installation**

Provide a minimum bearing of 150 m on both sees

