

moment of inertia gross without shear lag: 131997495506.10445

Buckling Proof according to EC 1993 Part 1-5

3.2 Effective width for elastic shear lag

Shear lag reduction for flange 1

Shear Lag is not neglectable

alpha_0: 1.7

Beta: 0.31395004434548573

Shear lag reduction for flange 3

Shear Lag is not neglectable

alpha_0: 1.3

Beta: 0.44121107679637916

4.4 Plate elements without longitudinal stiffeners

Iteratively changing the widths until M_Rd_el_eff converges to a limit of 0.02

moment of inertia gross with shear lag: 60364468595.56615

moment of inertia eff without shear lag: 114100942203.74236

moment of inertia eff with shear lag: 54037465137.15008

4.5 Stiffened plate elements with longitudinal stiffeners

Side 2

4.5.2 Plate type behaviour

 $sigma_cr = 2555.282079228872$

Lambda: 0.30051392531926124

Rho_Global: 1.0

4.5.3 Column type buckling behaviour

Column number 9

A_sl=13548.45, A_sl_eff=13190.5, I_sl=27291618.43

sigma_cr_c=665.72

e1=72.7, e2=59.95

All tension =False

Buckling Values 9

beta_A_c = 0.9735800820732999

lambda_c_bar =0.5862351201416552

Phi_c =0.7482247121240821

Chi_c = 0.8242908170231383

Critical buckling values

Chi c: 0.8242908170231383

sigma_cr_c: 665.7265499312396

4.5.4 Interaction between plate and column buckling

all_tension: False

 $rho_c = 1.0$

Side 3

4.5.2 Plate type behaviour

 $sigma_cr = 763.4573757020646$

Lambda: 0.5017485584496578

Rho_Global: 1.0

4.5.3 Column type buckling behaviour

Column number 10

A_sl=16998.1, A_sl_eff=13902.39, I_sl=27320365.52

sigma_cr_c=208.2

e1=84.87, e2=47.78

All tension =False

Buckling Values 10

beta A c =0.8178792681216397

lambda_c_bar =0.960806674379394

Phi_c =1.10708338313521

Chi_c = 0.6034751810906328

Column number 11

A_sl=16998.1, A_sl_eff=13902.39, I_sl=27320365.52

sigma_cr_c=208.2

e1=84.87, e2=47.78

All tension =False

Buckling Values 11

beta_A_c = 0.8178792681216398

lambda_c_bar =0.960806674379394

Phi_c =1.10708338313521

Chi_c = 0.6034751810906328

Critical buckling values

Chi_c: 0.6034751810906328

sigma_cr_c: 208.20206822935626

4.5.4 Interaction between plate and column buckling

all_tension: False

 $rho_c = 1.0$

Side 4

4.5.2 Plate type behaviour

 $sigma_cr = 2555.282079228872$

Lambda: 0.30051392531926124

Rho Global: 1.0

4.5.3 Column type buckling behaviour

Column number 12

A_sl=13548.45, A_sl_eff=13190.5, I_sl=27291618.43

sigma_cr_c=665.72

e1=72.7, e2=59.95

All tension =False

Buckling Values 12

beta_A_c = 0.9735800820732999

lambda_c_bar =0.5862351201416554

Phi_c =0.7482247121240823

Chi_c = 0.8242908170231382

Critical buckling values

Chi_c: 0.8242908170231382

sigma_cr_c: 665.7265499312393

4.5.4 Interaction between plate and column buckling

all_tension: False

rho c = 1.0

Resistance to shear and interaction shear force and bending moment for side 1

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 1: 0.19

lambda_w_bar_loc of the trapezoid line nr. 2: 0.19

lambda_w_bar_loc of the trapezoid line nr. 3: 0.19

lambda_w_bar_loc of the trapezoid line nr. 4: 0.19

lambda_w_bar_loc of the trapezoid line nr. 5: 0.19

lambda_w_bar_loc of the trapezoid line nr. 6: 0.19

lambda_w_bar_loc of the trapezoid line nr. 7: 0.19

lambda_w_bar_loc of the trapezoid line nr. 8: 0.19

lambda_w_bar_loc of the trapezoid line nr. 9: 0.19

lambda_w_bar_loc of the trapezoid line nr. 10: 0.19

lambda_w_bar_loc of the trapezoid line nr. 11: 0.19

lambda_w_bar_loc of the trapezoid line nr. 12: 0.19

lambda_w_bar_loc of the trapezoid line nr. 13: 0.19

lambda_w_bar_loc of the trapezoid line nr. 14: 0.19

lambda_w_bar_loc of the trapezoid line nr. 15: 0.19

lambda_w_bar_loc of the trapezoid line nr. 16: 0.19

lambda_w_bar_loc of the trapezoid line nr. 17: 0.19

stiffened plate; EBPlate

k_tau: 1571.0214527033982

eta_3: 0.25205626496949346

7.1 Interaction between shear force, bending moment and axial force

Flange -> (7.1), comment (5)

eta_3 <= 0.5; no interaction needed

utilisation: -1

Proofing Resistance to shear for each subpanel

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 1: 0.19

k_tau: 5.353840830449827

eta_3: 0.15703164083436558

eta_3_panel < 1: pass subpanel

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 2: 0.19

unstiffened plate; (A.5)

k tau: 5.353840830449827

eta_3: 0.13987046328644648

eta_3_panel < 1: pass subpanel

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 3: 0.19

unstiffened plate; (A.5)

k_tau: 5.353840830449827

eta_3: 0.12270928573852742

eta_3_panel < 1: pass subpanel

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 4: 0.19

unstiffened plate; (A.5)

k_tau: 5.353840830449827

eta_3: 0.10554810819060838

eta_3_panel < 1: pass subpanel

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 5: 0.19

k_tau: 5.353840830449827

eta_3: 0.0883869306426893

eta_3_panel < 1: pass subpanel

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 6: 0.19

unstiffened plate; (A.5)

k tau: 5.353840830449827

eta_3: 0.07122575309477024

eta_3_panel < 1: pass subpanel

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 7: 0.19

unstiffened plate; (A.5)

k_tau: 5.353840830449827

eta_3: 0.05406457554685117

eta_3_panel < 1: pass subpanel

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 8: 0.19

unstiffened plate; (A.5)

k_tau: 5.353840830449827

eta_3: 0.03690339799893212

eta_3_panel < 1: pass subpanel

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 9: 0.19

k_tau: 5.353840830449827

eta 3: 0.01974222045101305

eta_3_panel < 1: pass subpanel

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 10: 0.19

unstiffened plate; (A.5)

k tau: 5.353840830449827

eta_3: 0.03690339799893209

eta_3_panel < 1: pass subpanel

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 11: 0.19

unstiffened plate; (A.5)

k_tau: 5.353840830449827

eta_3: 0.05406457554685115

eta_3_panel < 1: pass subpanel

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 12: 0.19

unstiffened plate; (A.5)

k_tau: 5.353840830449827

eta_3: 0.07122575309477021

eta_3_panel < 1: pass subpanel

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 13: 0.19

k_tau: 5.353840830449827

eta_3: 0.08838693064268928

eta_3_panel < 1: pass subpanel

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 14: 0.19

unstiffened plate; (A.5)

k tau: 5.353840830449827

eta_3: 0.10554810819060838

eta_3_panel < 1: pass subpanel

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 15: 0.19

unstiffened plate; (A.5)

k_tau: 5.353840830449827

eta_3: 0.12270928573852743

eta_3_panel < 1: pass subpanel

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 16: 0.19

unstiffened plate; (A.5)

k_tau: 5.353840830449827

eta_3: 0.13987046328644648

eta_3_panel < 1: pass subpanel

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 17: 0.19

k_tau: 5.353840830449827

eta_3: 0.15703164083436558

eta_3_panel < 1: pass subpanel

Resistance to shear and interaction shear force and bending moment for side 2

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 18: 1.33

lambda_w_bar_loc of the trapezoid line nr. 19: 0.34

lambda_w_bar_loc of the trapezoid line nr. 20: 0.65

stiffened plate; EBPlate

k_tau: 21.01369360902256

(5.3) lambda_w_bar_1= 1.2

(5.6) lambda_w_bar_2= 1.2

(5.7) lambda_w_bar_3= 1.33 max single plate slenderness

chosen lambda_w_bar= 1.33

eta_3: 0.5772423151566441

7.1 Interaction between shear force, bending moment and axial force

Web -> (7.1) without iterating

eta_3 > 0.5; interaction needed

utilisation: 0.6145459880467096

Resistance to shear and interaction shear force and bending moment for side 3

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 21: 0.93

lambda_w_bar_loc of the trapezoid line nr. 22: 0.34

lambda_w_bar_loc of the trapezoid line nr. 23: 0.85

lambda_w_bar_loc of the trapezoid line nr. 24: 0.34

lambda_w_bar_loc of the trapezoid line nr. 25: 0.93

stiffened plate; EBPlate

k_tau: 94.90997656054232

eta 3: 0.23801478429570364

7.1 Interaction between shear force, bending moment and axial force

Flange -> (7.1), comment (5)

eta_3 <= 0.5; no interaction needed

utilisation: -1

Proofing Resistance to shear for each subpanel

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 21: 0.93

unstiffened plate; (A.5)

k_tau: 5.51015625

 $(5.3) lambda_w_bar_1 = 0.93$

(5.6) lambda_w_bar_2= 0.93

(5.7) lambda_w_bar_3= 0.93 max single plate slenderness

chosen lambda_w_bar= 0.93

eta_3: 0.18367443224609442

eta_3_panel < 1: pass subpanel

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 22: 0.34

```
unstiffened plate; (A.5)
 k tau: 5.3625
 eta_3: 0.09261316350554184
 eta_3_panel < 1: pass subpanel
5. Resistance to shear
   lambda_w_bar_loc of the trapezoid line nr. 23: 0.85
 unstiffened plate; (A.5)
  k_tau: 5.480625
   (5.3) lambda_w_bar_1= 0.85
   (5.6) lambda_w_bar_2= 0.85
   (5.7) lambda_w_bar_3= 0.85 max single plate slenderness
   chosen lambda_w_bar= 0.85
 eta_3: 0.0524731734960991
 eta_3_panel < 1: pass subpanel
5. Resistance to shear
   lambda_w_bar_loc of the trapezoid line nr. 24: 0.34
 unstiffened plate; (A.5)
 k_tau: 5.3625
 eta_3: 0.09261316350554184
 eta_3_panel < 1: pass subpanel
5. Resistance to shear
   lambda_w_bar_loc of the trapezoid line nr. 25: 0.93
 unstiffened plate; (A.5)
```

k tau: 5.51015625

- (5.3) lambda_w_bar_1= 0.93
- (5.6) lambda_w_bar_2= 0.93
- (5.7) lambda_w_bar_3= 0.93 max single plate slenderness

chosen lambda_w_bar= 0.93

eta_3: 0.18367443224609442

eta_3_panel < 1: pass subpanel

Resistance to shear and interaction shear force and bending moment for side 4

5. Resistance to shear

lambda_w_bar_loc of the trapezoid line nr. 26: 0.65

lambda_w_bar_loc of the trapezoid line nr. 27: 0.34

lambda_w_bar_loc of the trapezoid line nr. 28: 1.33

stiffened plate; EBPlate

k_tau: 21.01353383458647

- (5.3) lambda_w_bar_1= 1.2
- (5.6) lambda_w_bar_2= 1.2
- (5.7) lambda_w_bar_3= 1.33 max single plate slenderness

chosen lambda_w_bar= 1.33

eta_3: 0.6660488251807434

7.1 Interaction between shear force, bending moment and axial force

Web -> (7.1) without iterating

eta_3 > 0.5; interaction needed

utilisation: 0.6590458276836744

cross-section with b_sup=4000, b_inf=3000, h=2000

```
trapezoid plate on side 1 with the number 1
a=(2000, 0) \quad p1=(1882, 0) \quad p2=(1882, 0) \quad b=(1764, 0)t=14.0
```

trapezoid plate on side 1 with the number 2

trapezoid plate on side 1 with the number 3

trapezoid plate on side 1 with the number 4

trapezoid plate on side 1 with the number 5

trapezoid plate on side 1 with the number 6

trapezoid plate on side 1 with the number 7

trapezoid plate on side 1 with the number 8

trapezoid plate on side 1 with the number 9

trapezoid plate on side 1 with the number 10

trapezoid plate on side 1 with the number 11

trapezoid plate on side 1 with the number 12

trapezoid plate on side 1 with the number 13

trapezoid plate on side 1 with the number 14

trapezoid plate on side 1 with the number 15

trapezoid plate on side 1 with the number 16

```
trapezoid plate on side 1 with the number 17
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trapezoid plate on side 2 with the number 18

trapezoid plate on side 2 with the number 19

trapezoid plate on side 2 with the number 20

trapezoid plate on side 3 with the number 21

trapezoid plate on side 3 with the number 22

trapezoid plate on side 3 with the number 23

trapezoid plate on side 3 with the number 24

- trapezoid plate on side 3 with the number 25
 - a=(675, 2000) p1=(916, 2000) p2=(1258, 2000) b=(1500, 2000)t=10.0
- sigma_a_red=170.43 sigma_b_red=170.43
- trapezoid plate on side 4 with the number 26
 - a=(1500, 2000) p1=(1554, 1780) p2=(1570, 1717) b=(1638, 1445)t=10.0 sigma_a_red=170.43 sigma_b_red=88.34
- trapezoid plate on side 4 with the number 27
 - a=(1638, 1445) p1=(1671, 1315) p2=(1671, 1315) b=(1711, 1154)t=10.0
 - sigma_a_red=88.34 sigma_b_red=45.26
- trapezoid plate on side 4 with the number 28
 - a=(1711, 1154) p1=(1741, 1032) p2=(1741, 1032) b=(2000, 0)t=10.0 sigma_a_red=45.26 sigma_b_red=-125.65
- stiffener plate on side 1 of stiffener nr 1 on stiffener plate position 2 $a=(1529,0) \quad p1=(1564,130) \quad p2=(1564,130) \quad b=(1599,260)t=10.0$ $sigma_a_red=-125.65 \quad sigma_b_red=-87.16$
- stiffener plate on side 1 of stiffener nr 1 on stiffener plate position 3 $a=(1599, 260) \quad p1=(1647, 260) \quad p2=(1647, 260) \quad b=(1695, 260)t=10.0$ $sigma_a_red=-87.16 \quad sigma_b_red=-87.16$
- stiffener plate on side 1 of stiffener nr 1 on stiffener plate position 4 $a=(1695, 260) \quad p1=(1729, 130) \quad p2=(1729, 130) \quad b=(1764, 0)t=10.0$ $sigma_a_red=-87.16 \quad sigma_b_red=-125.65$
- stiffener plate on side 1 of stiffener nr 2 on stiffener plate position 2 $a=(1058,0) \quad p1=(1093,130) \quad p2=(1093,130) \quad b=(1128,260)t=10.0$ $sigma_a_red=-125.65 \quad sigma_b_red=-87.16$

- stiffener plate on side 1 of stiffener nr 2 on stiffener plate position 3 $a=(1128, 260) \quad p1=(1176, 260) \quad p2=(1176, 260) \quad b=(1224, 260)t=10.0$ $sigma_a_red=-87.16 \quad sigma_b_red=-87.16$
- stiffener plate on side 1 of stiffener nr 2 on stiffener plate position 4 $a=(1224,\,260) \quad p1=(1259,\,130) \quad p2=(1259,\,130) \quad b=(1294,\,0)t=10.0$ $sigma_a_red=-87.16 \quad sigma_b_red=-125.65$
- stiffener plate on side 1 of stiffener nr 3 on stiffener plate position 2 $a=(588,0) \quad p1=(623,130) \quad p2=(623,130) \quad b=(657,260)t=10.0$ $sigma_a_red=-125.65 \quad sigma_b_red=-87.16$
- stiffener plate on side 1 of stiffener nr 3 on stiffener plate position 3 $a=(657, 260) \quad p1=(705, 260) \quad p2=(705, 260) \quad b=(753, 260)t=10.0$ sigma a red=-87.16 sigma b red=-87.16
- stiffener plate on side 1 of stiffener nr 3 on stiffener plate position 4 $a=(753, 260) \quad p1=(788, 130) \quad p2=(788, 130) \quad b=(823, 0)t=10.0$ $sigma_a_red=-87.16 \quad sigma_b_red=-125.65$
- stiffener plate on side 1 of stiffener nr 4 on stiffener plate position 2 $a=(117,0) \quad p1=(152,130) \quad p2=(152,130) \quad b=(187,260)t=10.0$ $sigma_a_red=-125.65 \quad sigma_b_red=-87.16$
- stiffener plate on side 1 of stiffener nr 4 on stiffener plate position 3 $a=(187, 260) \quad p1=(235, 260) \quad p2=(235, 260) \quad b=(283, 260)t=10.0$ $sigma_a_red=-87.16 \quad sigma_b_red=-87.16$
- stiffener plate on side 1 of stiffener nr 4 on stiffener plate position 4 $a=(283, 260) \quad p1=(318, 130) \quad p2=(318, 130) \quad b=(352, 0)t=10.0$ $sigma_a_red=-87.16 \quad sigma_b_red=-125.65$

- stiffener plate on side 1 of stiffener nr 5 on stiffener plate position 2 $a=(-352, 0) \quad p1=(-318, 130) \quad p2=(-318, 130) \quad b=(-283, 260)t=10.0$ $sigma_a_red=-125.65 \quad sigma_b_red=-87.16$
- stiffener plate on side 1 of stiffener nr 5 on stiffener plate position 3 $a=(-283, 260) \quad p1=(-235, 260) \quad p2=(-235, 260) \quad b=(-187, 260)t=10.0$ $sigma_a_red=-87.16 \quad sigma_b_red=-87.16$
- stiffener plate on side 1 of stiffener nr 5 on stiffener plate position 4 $a=(-187, 260) \quad p1=(-152, 130) \quad p2=(-152, 130) \quad b=(-117, 0)t=10.0$ $sigma_a_red=-87.16 \quad sigma_b_red=-125.65$
- stiffener plate on side 1 of stiffener nr 6 on stiffener plate position 2 $a=(-823, 0) \quad p1=(-788, 130) \quad p2=(-788, 130) \quad b=(-753, 260)t=10.0$ $sigma_a_red=-125.65 \quad sigma_b_red=-87.16$
- stiffener plate on side 1 of stiffener nr 6 on stiffener plate position 3 $a=(-753, 260) \quad p1=(-705, 260) \quad p2=(-705, 260) \quad b=(-657, 260)t=10.0$ $sigma_a_red=-87.16 \quad sigma_b_red=-87.16$
- stiffener plate on side 1 of stiffener nr 6 on stiffener plate position 4 $a=(-657, 260) \quad p1=(-623, 130) \quad p2=(-623, 130) \quad b=(-588, 0)t=10.0$ $sigma_a_red=-87.16 \quad sigma_b_red=-125.65$
- stiffener plate on side 1 of stiffener nr 7 on stiffener plate position 2 $a=(-1294, 0) \quad p1=(-1259, 130) \quad p2=(-1259, 130) \quad b=(-1224, 260)t=10.0$ $sigma_a_red=-125.65 \quad sigma_b_red=-87.16$
- stiffener plate on side 1 of stiffener nr 7 on stiffener plate position 3 $a=(-1224, 260) \quad p1=(-1176, 260) \quad p2=(-1176, 260) \quad b=(-1128, 260)t=10.0$ $sigma_a_red=-87.16 \quad sigma_b_red=-87.16$

- stiffener plate on side 1 of stiffener nr 7 on stiffener plate position 4 $a=(-1128, 260) \quad p1=(-1093, 130) \quad p2=(-1093, 130) \quad b=(-1058, 0)t=10.0$ $sigma_a_red=-87.16 \quad sigma_b_red=-125.65$
- stiffener plate on side 1 of stiffener nr 8 on stiffener plate position 2 $a=(-1764, 0) \quad p1=(-1729, 130) \quad p2=(-1729, 130) \quad b=(-1695, 260)t=10.0$ $sigma_a_red=-125.65 \quad sigma_b_red=-87.16$
- stiffener plate on side 1 of stiffener nr 8 on stiffener plate position 3 $a=(-1695, 260) \quad p1=(-1647, 260) \quad p2=(-1647, 260) \quad b=(-1599, 260)t=10.0$ $sigma_a_red=-87.16 \quad sigma_b_red=-87.16$
- stiffener plate on side 1 of stiffener nr 8 on stiffener plate position 4 $a=(-1599, 260) \quad p1=(-1564, 130) \quad p2=(-1564, 130) \quad b=(-1529, 0)t=10.0$ $sigma_a_red=-87.16 \quad sigma_b_red=-125.65$
- stiffener plate on side 2 of stiffener nr 9 on stiffener plate position 2 $a=(-1638, 1445) \quad p1=(-1551, 1398) \quad p2=(-1551, 1398) \quad b=(-1456, 1348)t=10.0$ $sigma_a_red=88.34 \quad sigma_b_red=73.98$
- stiffener plate on side 2 of stiffener nr 9 on stiffener plate position 3 $a=(-1456, 1348) \quad p1=(-1478, 1260) \quad p2=(-1478, 1260) \quad b=(-1505, 1154)t=10.0$ $sigma_a_red=73.98 \quad sigma_b_red=45.26$
- stiffener plate on side 2 of stiffener nr 9 on stiffener plate position 4 $a=(-1505, 1154) \quad p1=(-1608, 1154) \quad p2=(-1608, 1154) \quad b=(-1711, 1154)t=10.0$ $sigma_a_red=45.26 \quad sigma_b_red=45.26$
- stiffener plate on side 3 of stiffener nr 10 on stiffener plate position 2 $a=(-375,\,2000)\quad p1=(-398,\,1904)\quad p2=(-398,\,1904)\quad b=(-425,\,1800)t=10.0$ sigma a red=170.43 sigma b red=140.82

- stiffener plate on side 3 of stiffener nr 10 on stiffener plate position 3 $a=(-425,\,1800) \quad p1=(-525,\,1800) \quad p2=(-525,\,1800) \quad b=(-625,\,1800)t=10.0$ $sigma_a_red=140.82 \quad sigma_b_red=140.82$
- stiffener plate on side 3 of stiffener nr 10 on stiffener plate position 4 $a=(-625, 1800) \quad p1=(-651, 1904) \quad p2=(-651, 1904) \quad b=(-675, 2000)t=10.0$ $sigma_a_red=140.82 \quad sigma_b_red=170.43$
- stiffener plate on side 3 of stiffener nr 11 on stiffener plate position 2 $a=(675, 2000) \quad p1=(651, 1904) \quad p2=(651, 1904) \quad b=(625, 1800)t=10.0$ $sigma_a_red=170.43 \quad sigma_b_red=140.82$
- stiffener plate on side 3 of stiffener nr 11 on stiffener plate position 3 $a=(625, 1800) \quad p1=(525, 1800) \quad p2=(525, 1800) \quad b=(425, 1800)t=10.0$ $sigma_a_red=140.82 \quad sigma_b_red=140.82$
- stiffener plate on side 3 of stiffener nr 11 on stiffener plate position 4 $a=(425, 1800) \quad p1=(398, 1904) \quad p2=(398, 1904) \quad b=(375, 2000)t=10.0$ $sigma_a_red=140.82 \quad sigma_b_red=170.43$
- stiffener plate on side 4 of stiffener nr 12 on stiffener plate position 2 $a=(1711, 1154) \quad p1=(1608, 1154) \quad p2=(1608, 1154) \quad b=(1505, 1154)t=10.0$ $sigma_a_red=45.26 \quad sigma_b_red=45.26$
- stiffener plate on side 4 of stiffener nr 12 on stiffener plate position 3 $a=(1505, 1154) \quad p1=(1478, 1260) \quad p2=(1478, 1260) \quad b=(1456, 1348)t=10.0$ $sigma_a_red=45.26 \quad sigma_b_red=73.98$
- stiffener plate on side 4 of stiffener nr 12 on stiffener plate position 4 $a=(1456,\,1348)\quad p1=(1551,\,1398)\quad p2=(1551,\,1398)\quad b=(1638,\,1445)t=10.0$ $sigma_a_red=73.98\quad sigma_b_red=88.34$

moment of inertia including all reductions: 54037465137.15008

