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# EE288 Data Conversions/Analog Mixed-Signal ICs

## Spring 2018

### Lecture 3: ADC Architectures, Sampling

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ENG-259

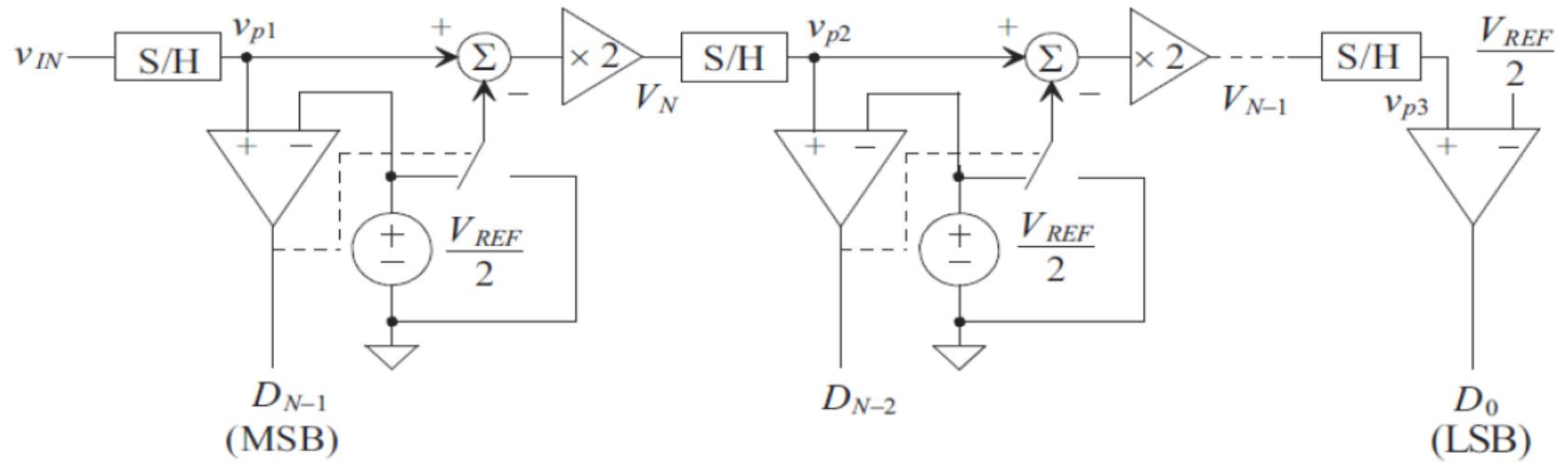
# Course Schedule – Subject to Change

| Date   | Topics   |
|--------|--|
| 24-Jan | <del>Course introduction and ADC architectures</del>                     |
| 29-Jan | <del>Converter basics: AAF, Sampling, Quantization, Reconstruction</del> |
| 31-Jan | <del>ADC dynamic performance metrics, Spectrum analysis using FFT</del>  |
| 5-Feb  | ADC & DAC static performance metrics, INL and DNL                        |
| 7-Feb  | OPAMP and bias circuits review   |
| 12-Feb | SC circuits review   |
| 14-Feb | Sample and Hold Amplifier - Reading materials                            |
| 19-Feb | Flash ADC and Comparators: Regenerative Latch                            |
| 21-Feb | Comparators: Latch offset, preamp, auto-zero                             |
| 26-Feb | Finish Flash ADC   |
| 28-Feb | DAC Architectures - Resistor, R-2R                                       |
| 5-Mar  | DAC Architectures - Current steering, Segmented                          |
| 7-Mar  | DAC Architectures - Capacitor-based                                      |
| 12-Mar | SAR ADC with bottom plate sampling                                       |
| 14-Mar | SAR ADC with top plate sampling  |
| 19-Mar | Midterm Review   |
| 21-Mar | Midterm exam   |
| 26-Mar | Spring break   |
| 28-Mar | Spring break   |
| 2-Apr  | Pipelined ADC stage - comparator, MDAC, x2 gain                          |
| 4-Apr  | Pipelined ADC bit sync and alignment using Full adders                   |
| 9-Apr  | Pipelined ADC 1.5bit vs multi-bit structures                             |
| 11-Apr | Fully-differential OPAMP and Switched-capacitor CMFB                     |
| 16-Apr | Single-slope ADC   |
| 18-Apr | Oversampling & Delta-Sigma ADCs  |
| 23-Apr | Second- and higher-order Delta-Sigma Modulator.                          |
| 25-Apr | Hybrid ADC - Pipelined SAR   |
| 30-Apr | Hybrid ADC - Time-Interleaving   |
| 2-May  | ADC testing and FoM  |
| 7-May  | Project presentation 1   |
| 8-May  | Project presentation 2   |
| 14-May | Final Review   |
| 20-May | Project Report Due by 6 PM   |

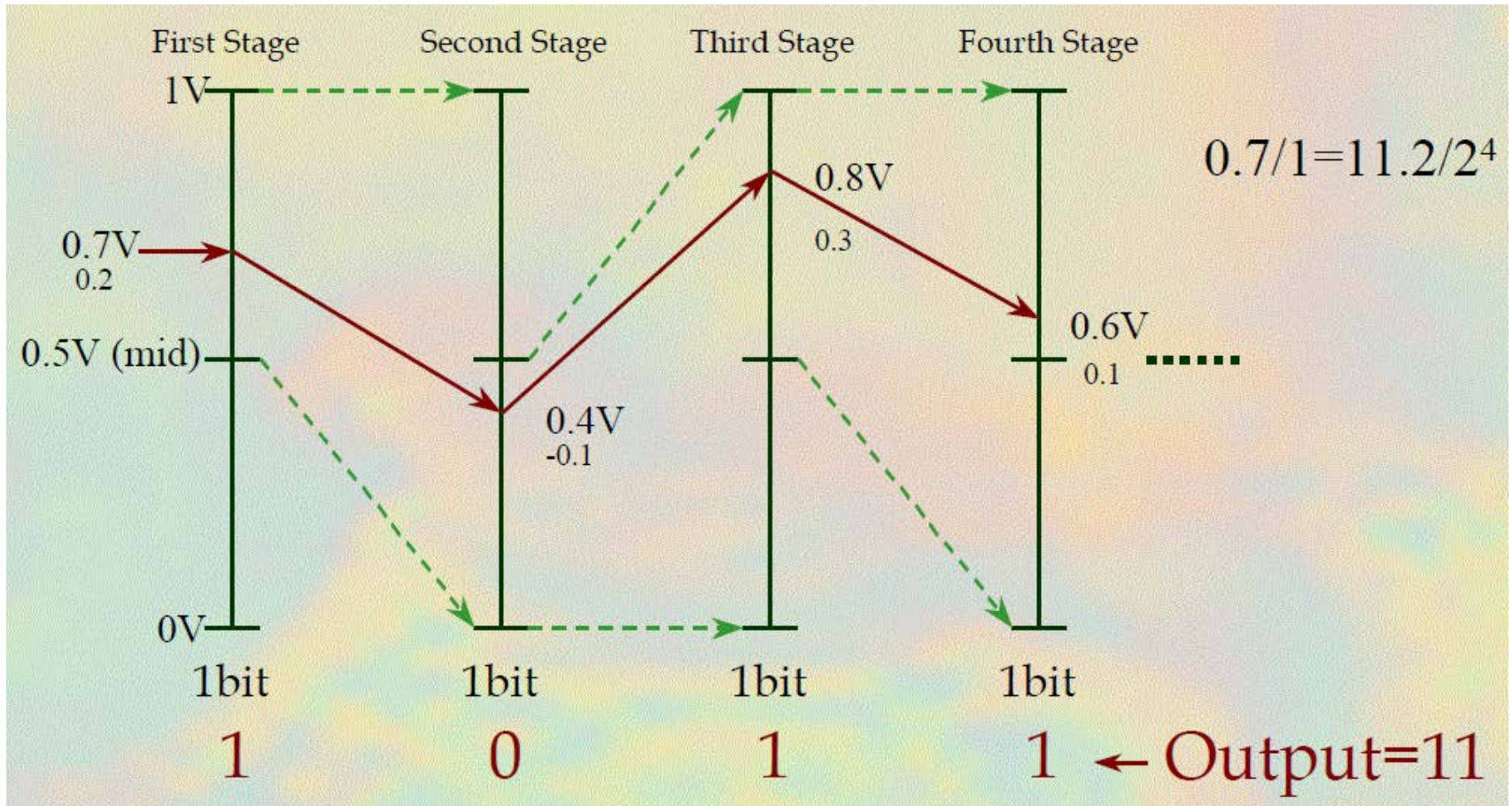
← Sampling

**\*Midterm Exam dates are approximate and subject to change with reasonable notice.**

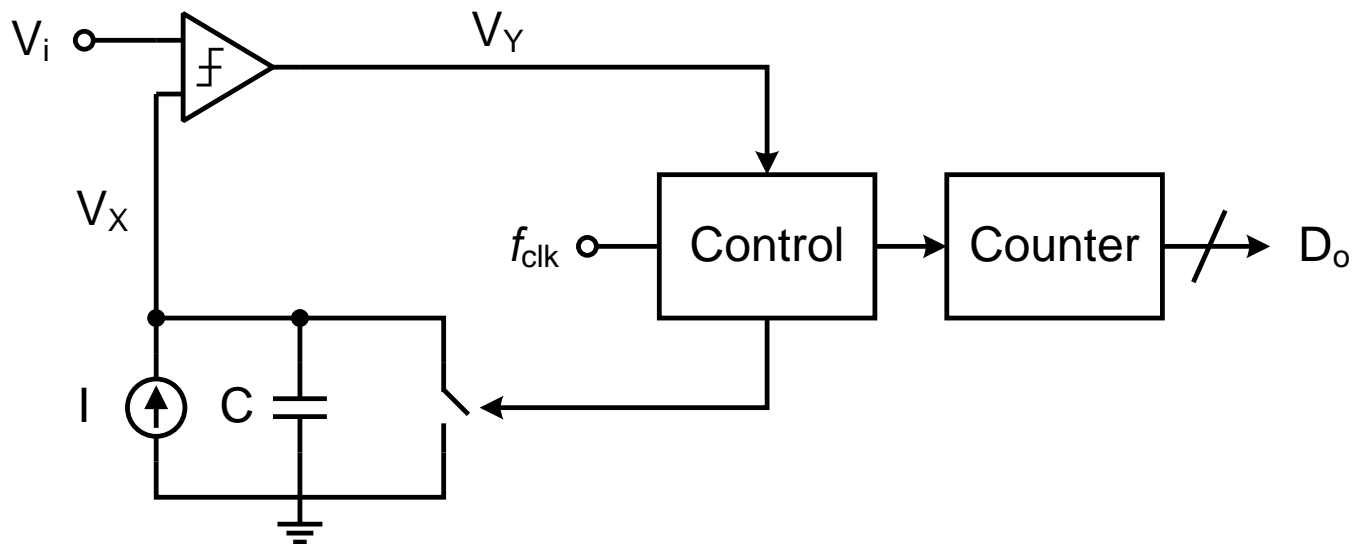
# 1-bit/stage Pipelined ADC



# 1-bit/stage Pipelined ADC

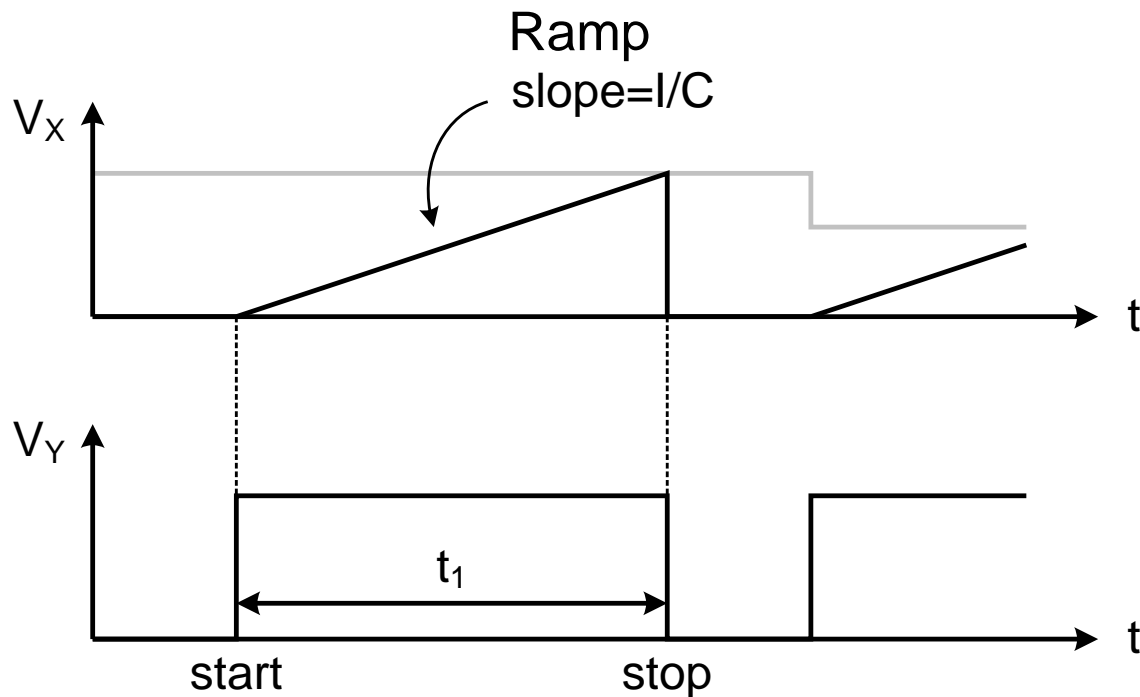


# Single-Slope Integration ADC



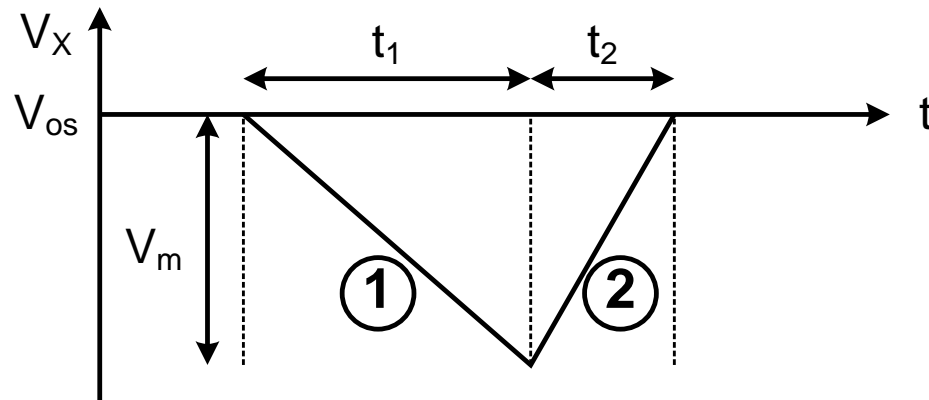
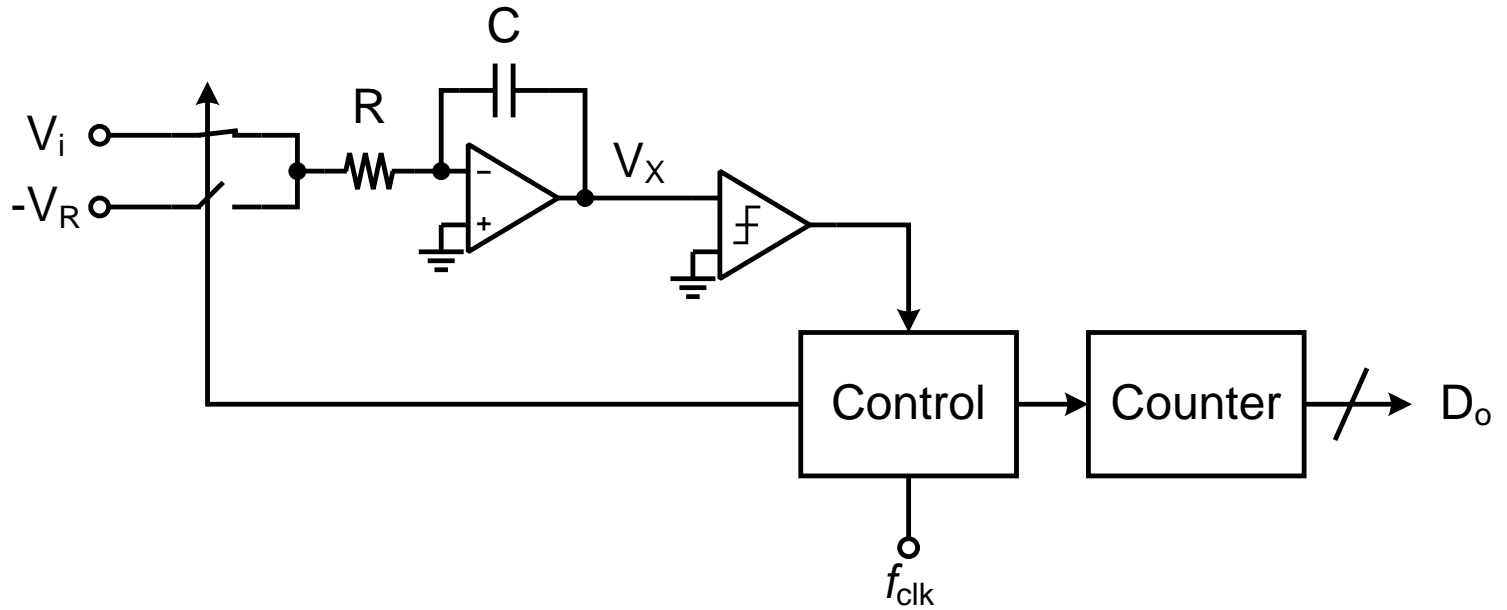
- Sampled-and-held input ( $V_i$ )
- Counter keeps counting until comparator output toggles
- Simple, inherently monotonic, but very slow ( $2^N \cdot T_{clk}/\text{sample}$ )

# Single-Slope Integration ADC

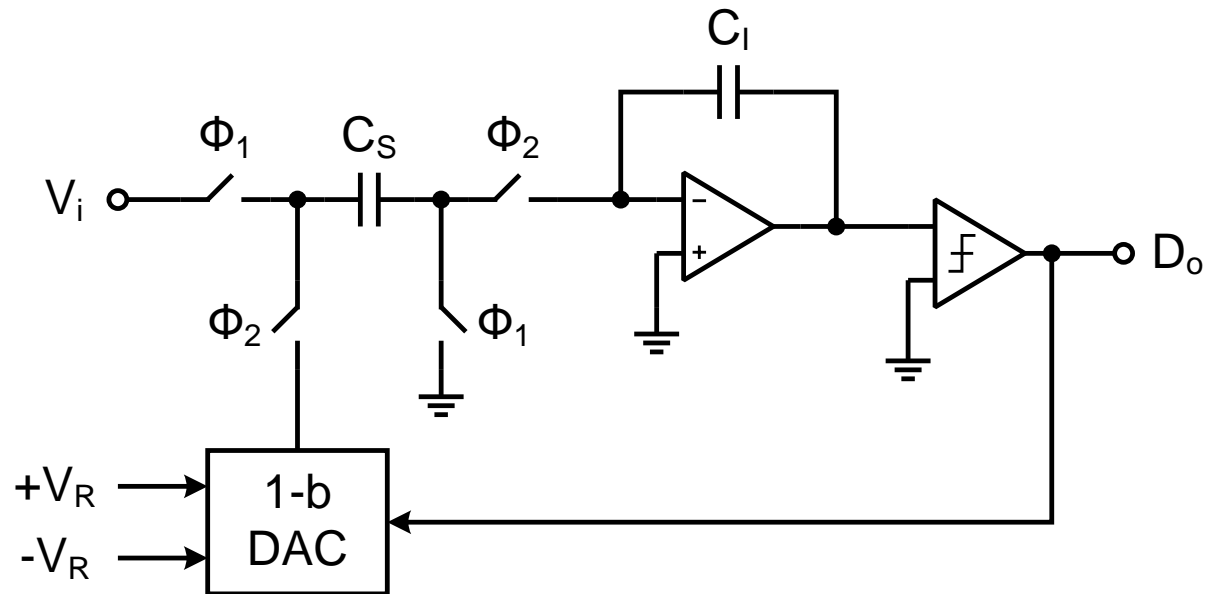
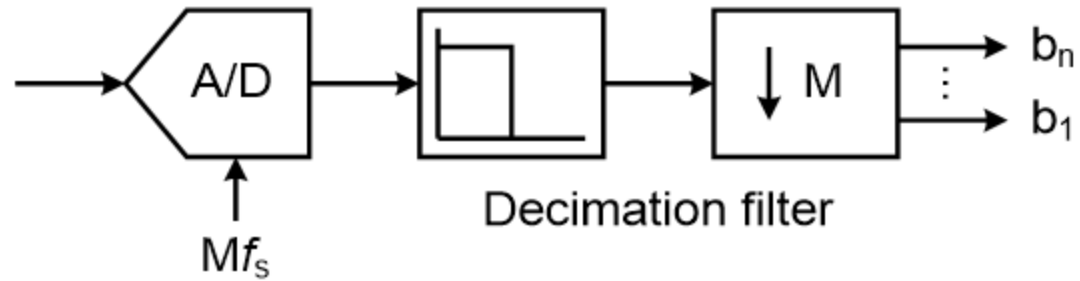


- INL depends on the linearity of the ramp signal
- Precision capacitor ( $C$ ), current source ( $I$ ), and clock ( $T_{\text{clk}}$ ) required
- Comparator must handle wide input range of  $[0, V_{\text{FS}}]$

# Dual Slope Integration ADC



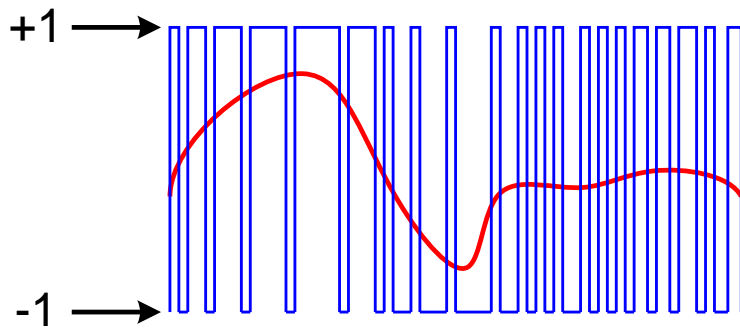
# Oversampling ADC



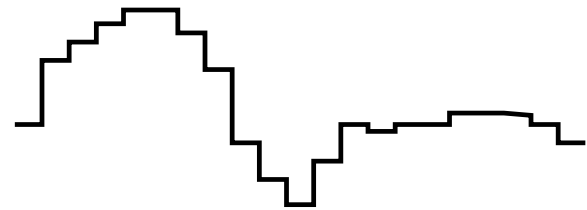


# Sigma Delta vs. Nyquist ADC

$\Sigma\Delta$  ADC output (1-bit)



Nyquist ADC output



- $\Sigma\Delta$  ADC behaves quite differently from Nyquist converters
- Digital codes only display an “average” impression of the input
- INL, DNL, monotonicity, missing code, etc. do not directly apply in  $\Sigma\Delta$  converters → use SNR, SNDR, SFDR instead

# Building Blocks for ADCs

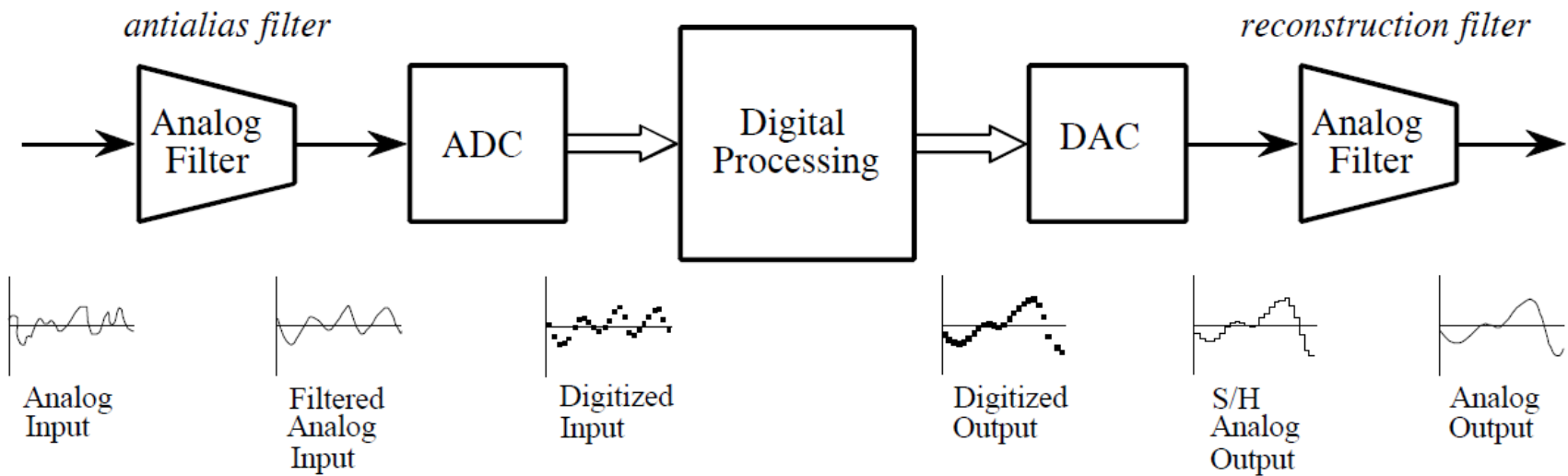
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- Comparators (Preamplifier and Latch)
- Operational Amplifier
- Sample-and-Hold (Track-and-Hold) Amplifier
- Switched-Capacitor Amplifiers, Integrators, and Filters
- Voltage and Current DAC's
- Current Sources
- Voltage/Current/Bandgap References

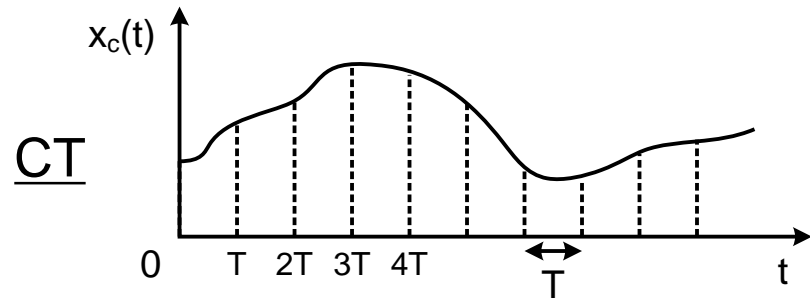
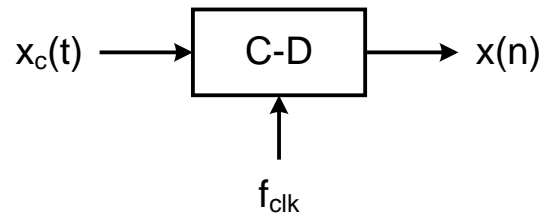
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# Sampling, Quantization, Spectrum Analysis

# Block Diagram of a DSP System

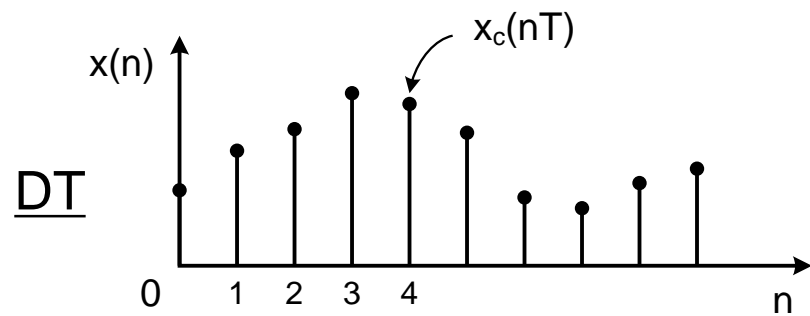


# Sampling

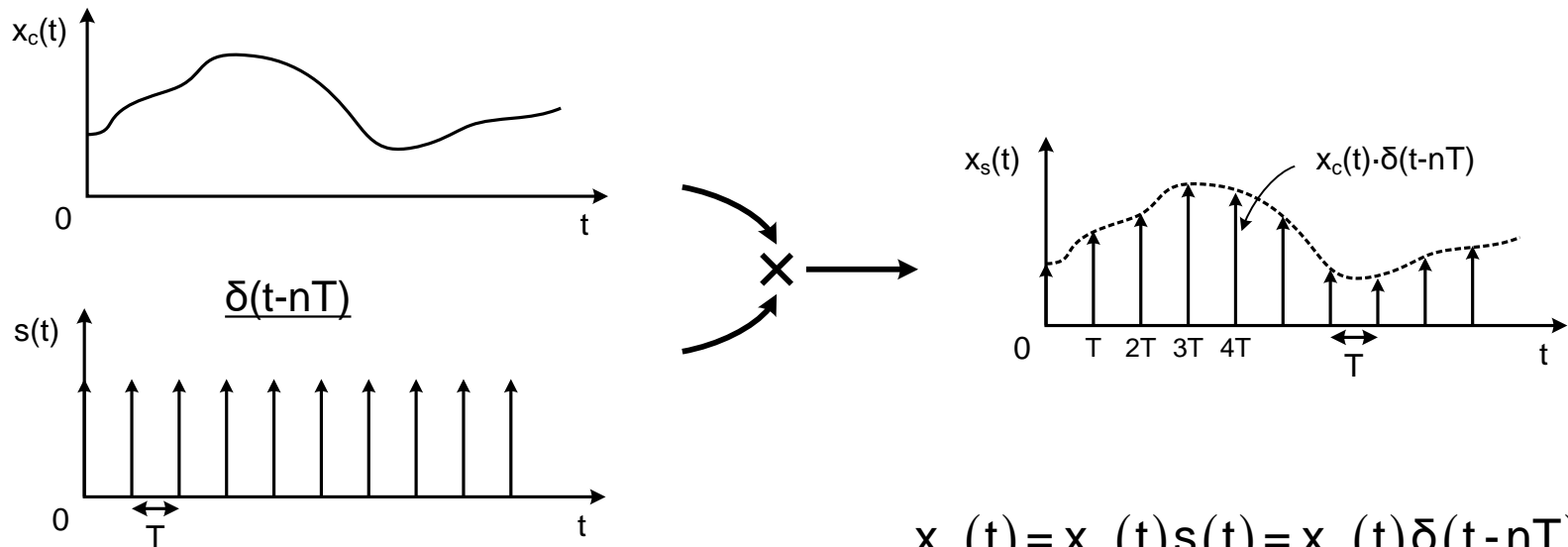


$$x(n) = x_c(t = nT)$$

$$x_c(t) \xLeftrightarrow{FT} X_c(j\Omega)$$



# Sampling



$$\begin{aligned}
 X(e^{j\omega}) &= \sum_{n=-\infty}^{\infty} x(n) z^{-n} \\
 &= X_s(j\Omega) \Big|_{\Omega=\frac{\omega}{T}} = \frac{1}{T} \sum_k X_c(\Omega - k\Omega_s) \Big|_{\Omega=\frac{\omega}{T}}
 \end{aligned}$$

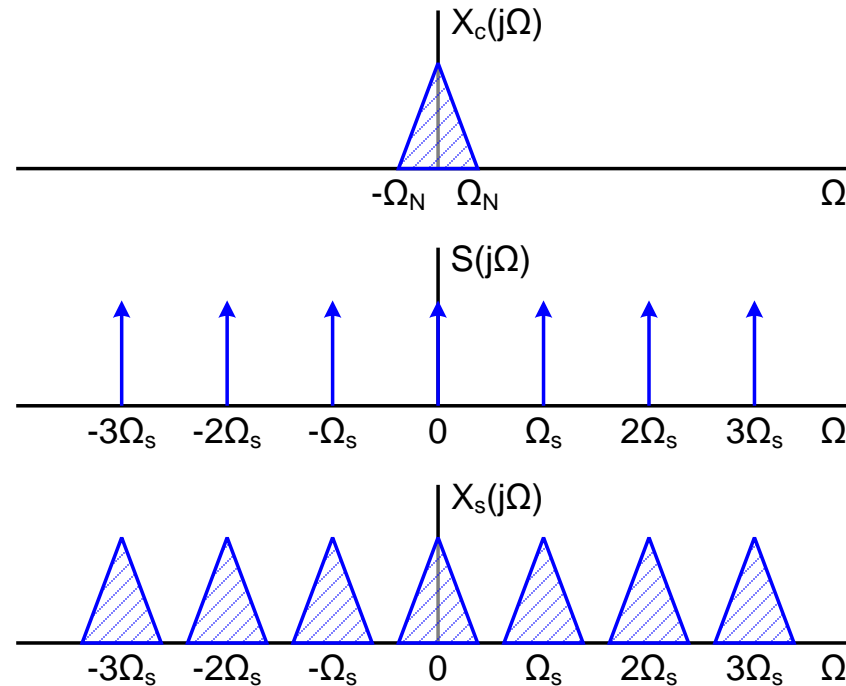
$$x_s(t) = x_c(t)s(t) = x_c(t)\delta(t-nT)$$

$$X_s(j\Omega) = \frac{1}{2\pi} X_c(j\Omega) \otimes S(j\Omega)$$

$$s(t) \stackrel{FT}{\Leftrightarrow} \frac{2\pi}{T} \sum_k \delta(\Omega - k\Omega_s), \quad \Omega_s = \frac{2\pi}{T}$$

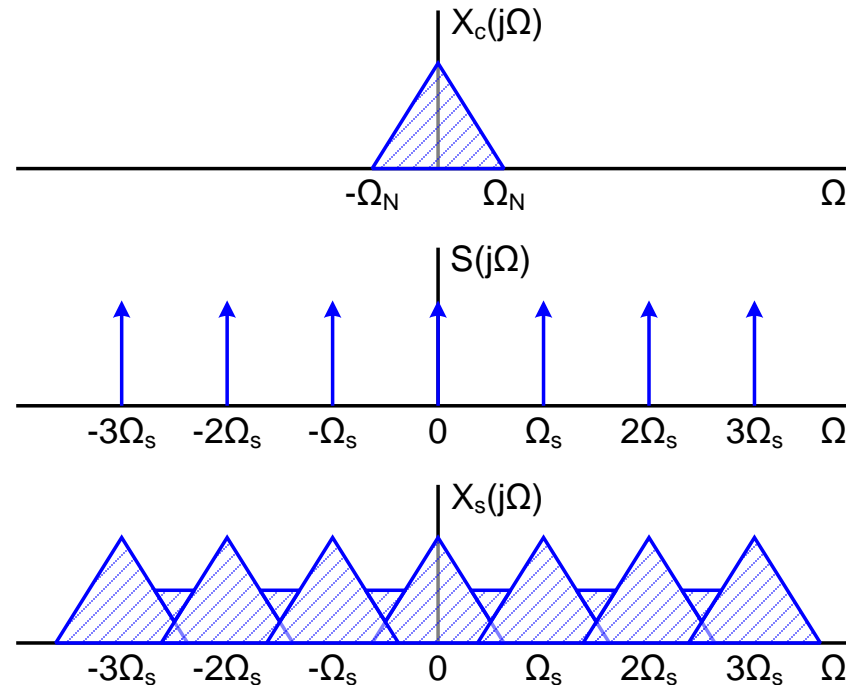
$$X_s(j\Omega) = \frac{1}{T} \sum_k X_c(\Omega - k\Omega_s)$$

# Spectrum of Sampled Signal ( $\Omega_s > 2\Omega_N$ )



The spectrum of the sampled signal is periodic in  $\Omega_s = 2\pi/T$ .

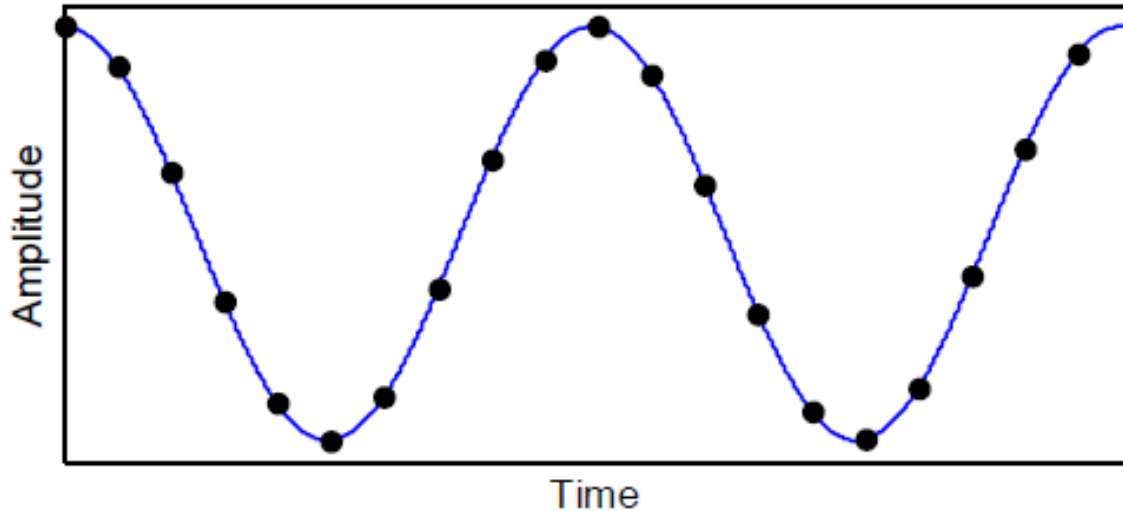
# Spectrum of Sampled Signal ( $\Omega_s < 2\Omega_N$ )



- Aliasing (folding) results in irreversible signal distortion.
- Can only be avoided by using sufficiently high sample rate, or band-limit the input signal with a coarse, continuous-time filter  $\rightarrow$  AAF.



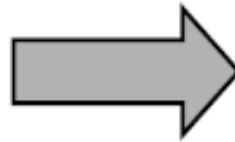
# Aliasing Example



$$f_s = \frac{1}{T_s} = 1000 \text{ kHz}$$

$$f_{sig} = 101 \text{ kHz}$$

$$v_{sig}(t) = \cos(2\pi \cdot f_{in} \cdot t)$$

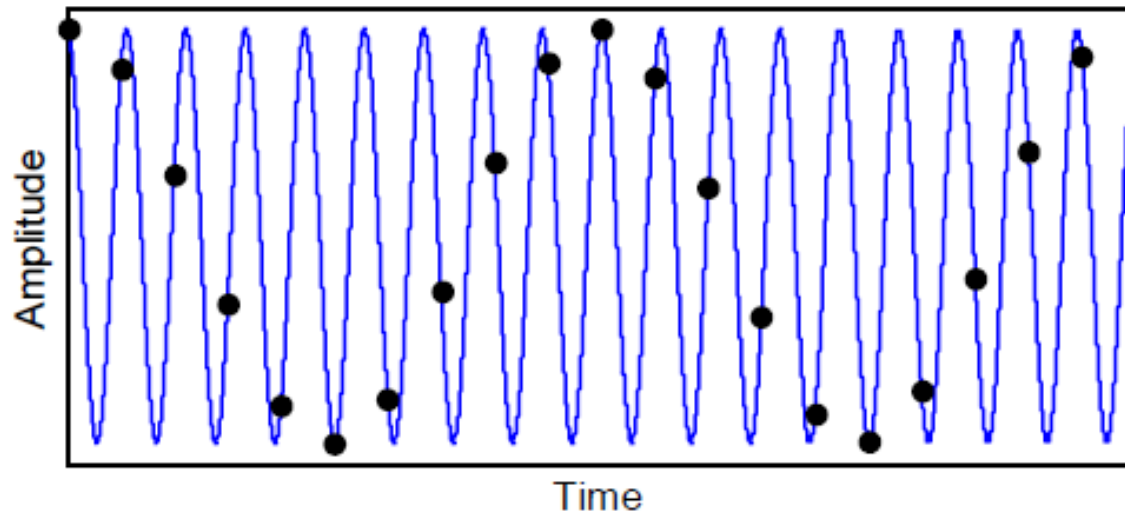


$$v_{sig}(n) = \cos\left(2\pi \cdot \frac{f_{in}}{f_s} \cdot n\right)$$

$$t \rightarrow n \cdot T_s = \frac{n}{f_s}$$

$$= \cos\left(2\pi \cdot \frac{101}{1000} \cdot n\right)$$

# Aliasing Example

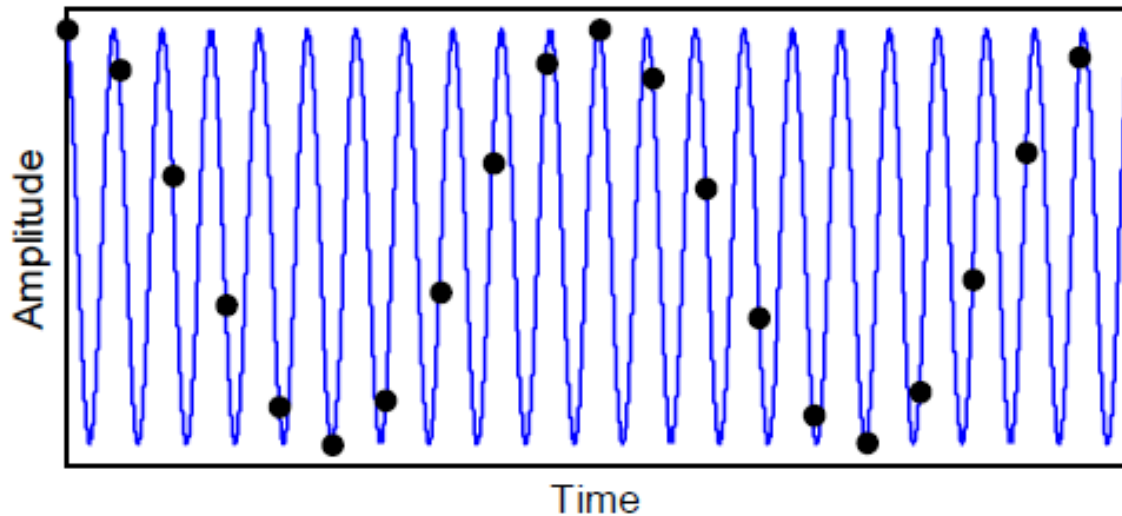


$$f_s = \frac{1}{T_s} = 1000 \text{ kHz}$$

$$f_{sig} = 899 \text{ kHz}$$

$$v_{sig}(n) = \cos\left(2\pi \cdot \frac{899}{1000} \cdot n\right) = \cos\left(2\pi \cdot \left[\frac{899}{1000} - 1\right] \cdot n\right) = \cos\left(2\pi \cdot \frac{101}{1000} \cdot n\right)$$

# Aliasing Example

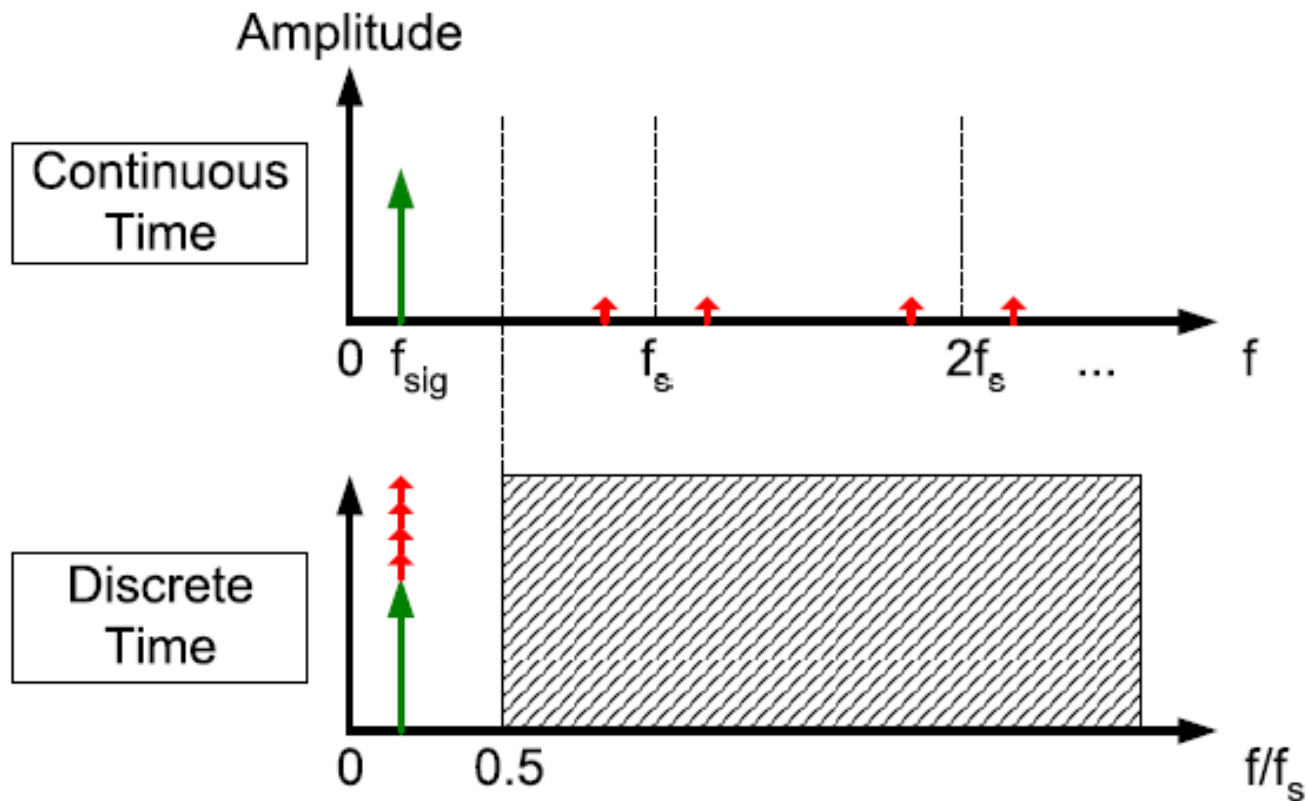


$$f_s = \frac{1}{T_s} = 1000 \text{ kHz}$$

$$f_{sig} = 1101 \text{ kHz}$$

$$v_{sig}(n) = \cos\left(2\pi \cdot \frac{1101}{1000} \cdot n\right) = \cos\left(2\pi \cdot \left[\frac{1101}{1000} - 1\right] \cdot n\right) = \cos\left(2\pi \cdot \frac{101}{1000} \cdot n\right)$$

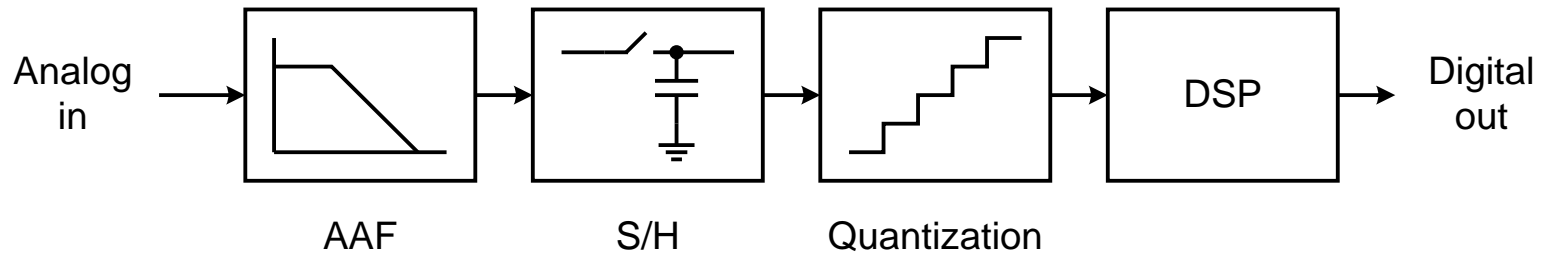
# Aliasing Consequence



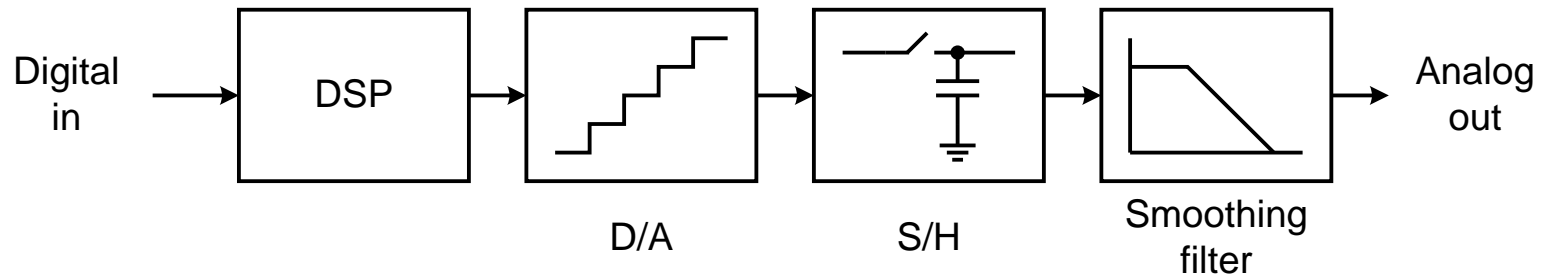
- The frequencies  $f_{\text{sig}}$  and  $N \cdot f_s \pm f_{\text{sig}}$  ( $N$  integer), are indistinguishable in the discrete time domain

# Recap A/D and D/A Signal Path

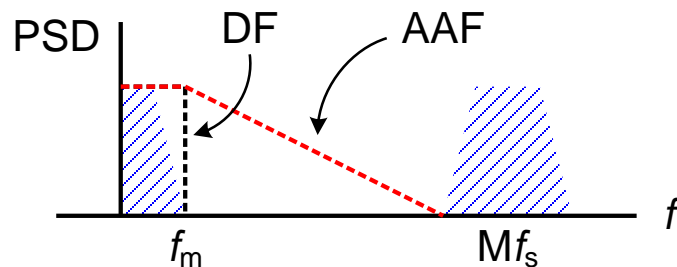
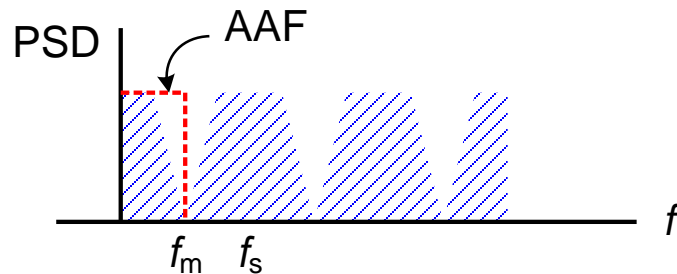
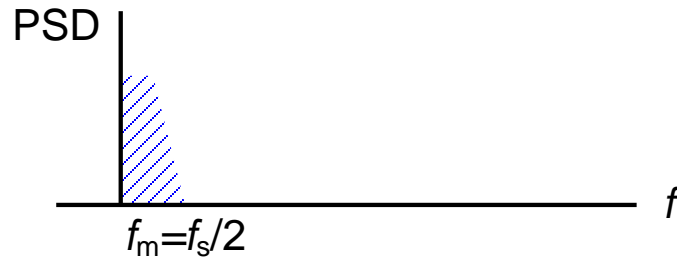
## A/D Conversion



## D/A Conversion



# Anti-Aliasing Filter (AAF)



- Input signal must be band-limited prior to sampling
- Nyquist sampling places stringent requirement on the roll-off characteristic of AAF
- Often some oversampling is employed to relax the AAF design (better phase response too)
- Decimation filter (digital) can be linear-phase

# Sampling Theorem

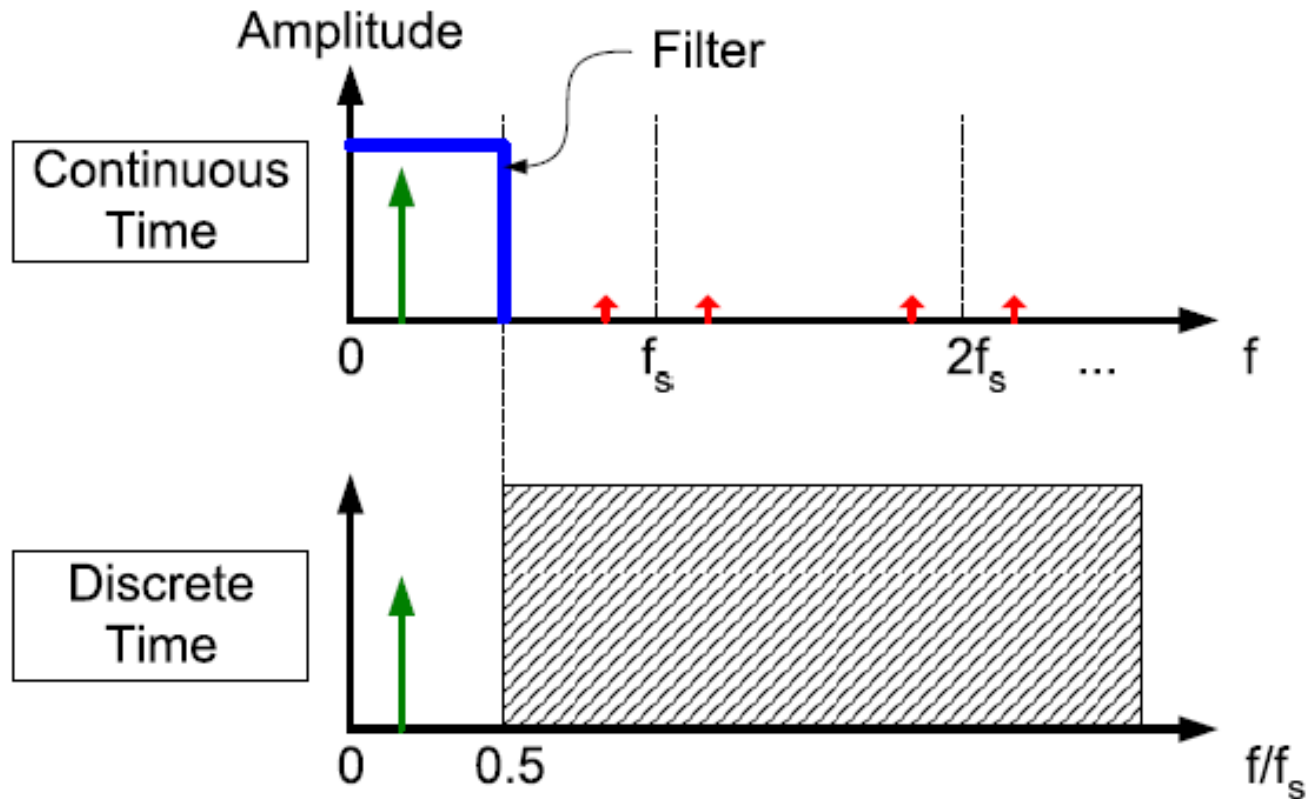
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- In order to prevent aliasing, we need

$$f_{sig,max} < \frac{f_s}{2}$$

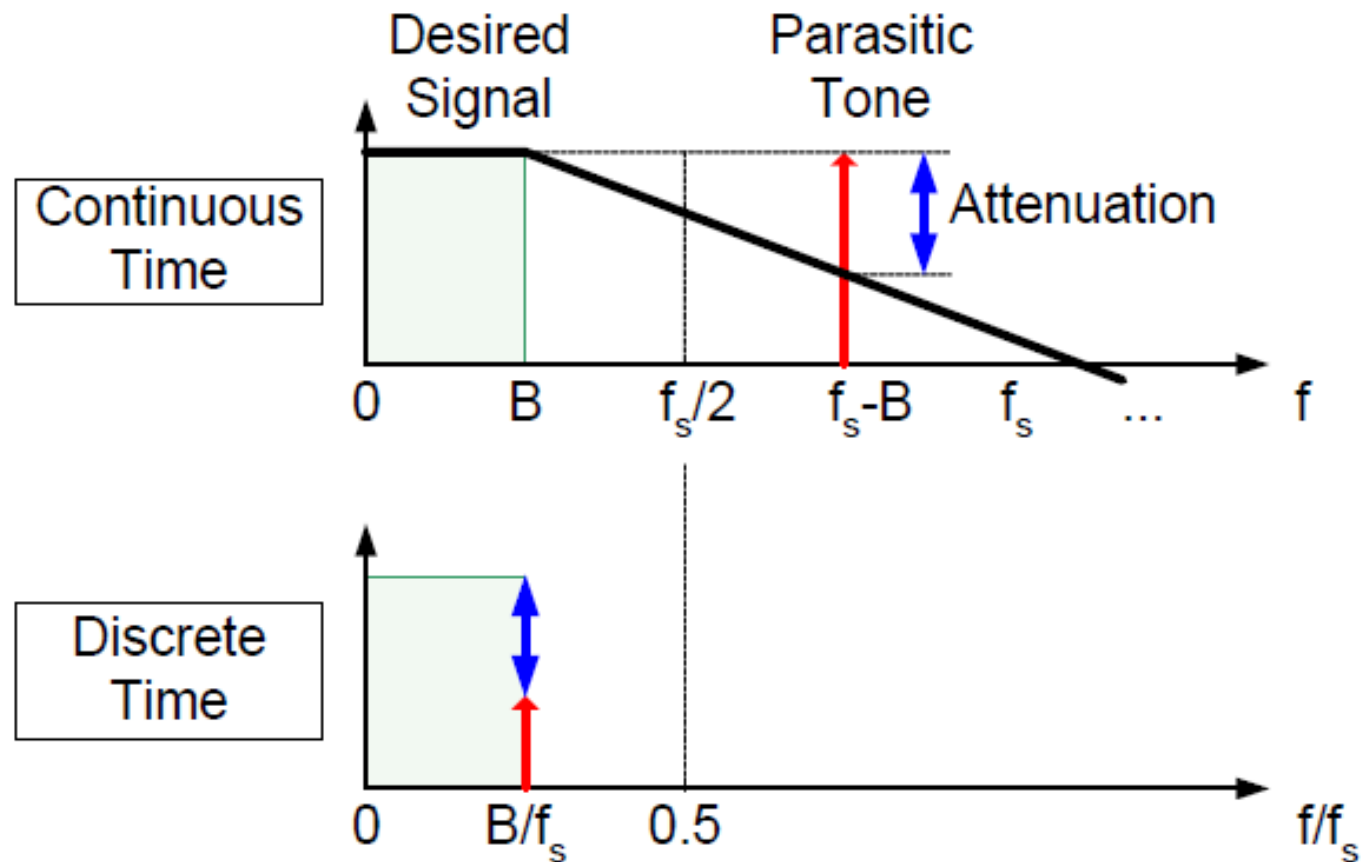
- The sampling rate  $f_s = 2 \cdot f_{sig,max}$  is called the Nyquist rate
- To avoid aliasing
  - Sample fast enough to cover all spectral components, including "parasitic" ones outside band of interest
  - Limit  $f_{sig,max}$  through filtering

# Brick Wall Anti-Alias Filter



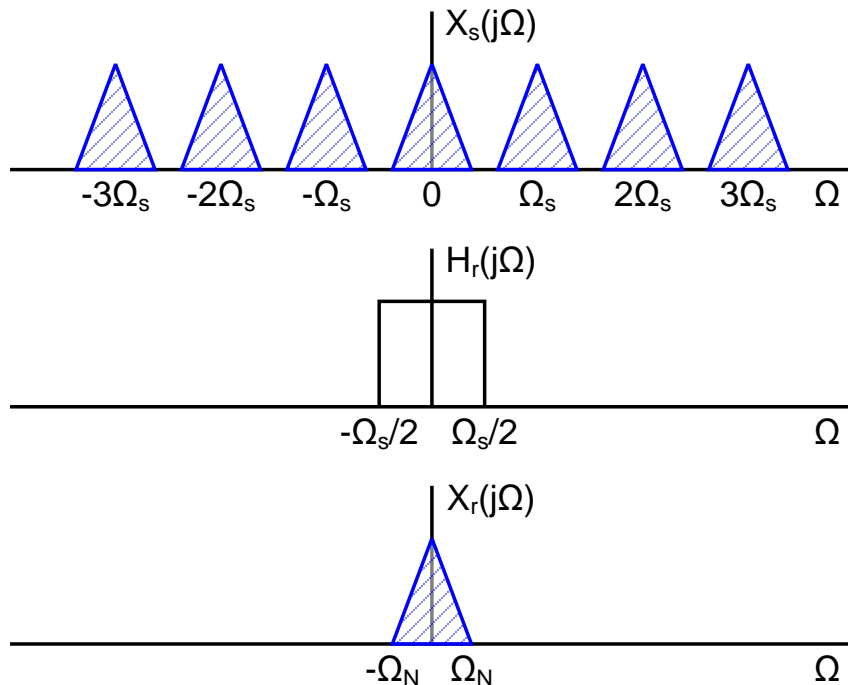


# Practical Anti-Alias Filter



- Need to sample faster than Nyquist rate to get good attenuation
  - "Oversampling"

# Reconstruction Filter (Nyquist)

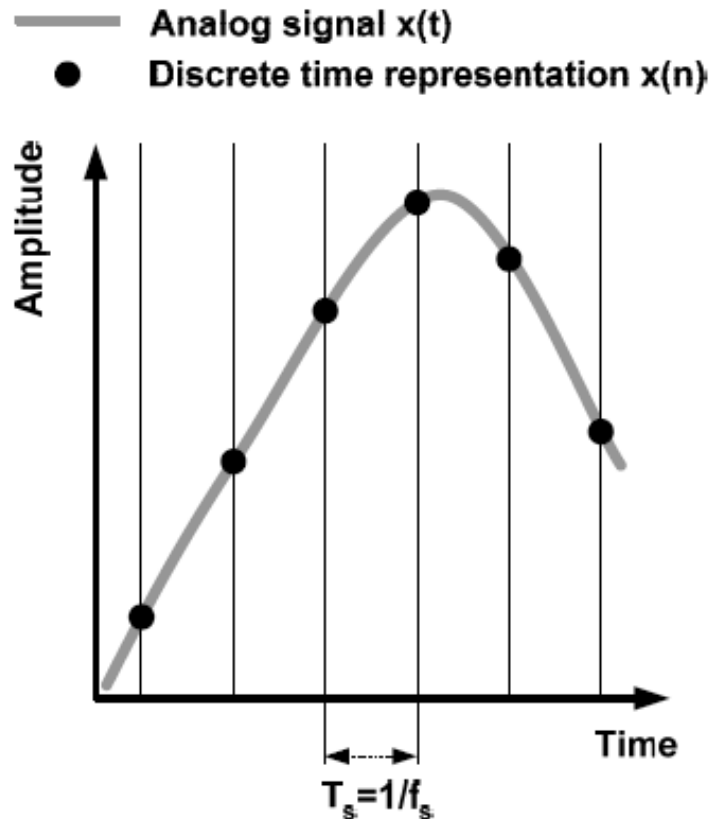


$$h_r(t) = \frac{\sin(\pi t / T)}{\pi t / T}$$

$$\begin{aligned} x_r(t) &= \sum_{n=-\infty}^{\infty} x(n) h_r(t - nT) \\ &= \sum_{n=-\infty}^{\infty} x(n) \frac{\sin[\pi(t - nT) / T]}{\pi(t - nT) / T} \end{aligned}$$

Reconstruction filter = “smoothing” filter = “interpolation” filter

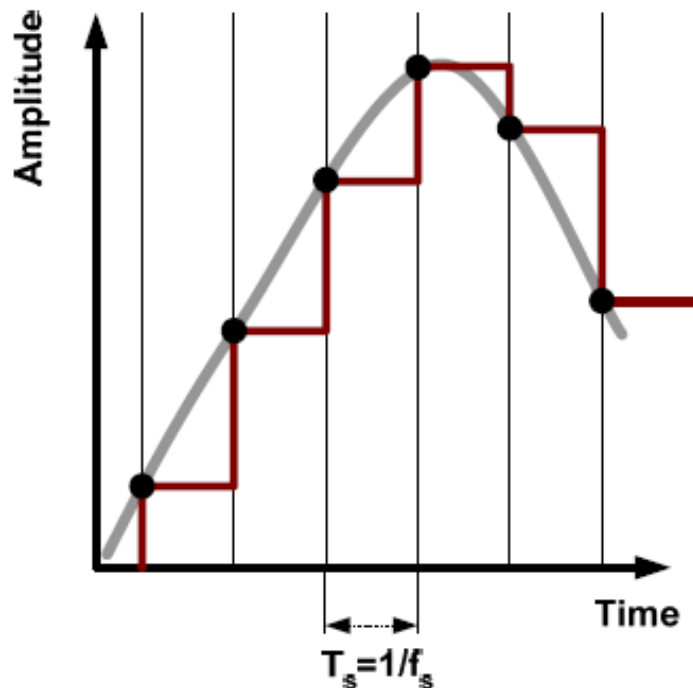
# Signal Reconstruction



- As long as we sample fast enough,  $x(n)$  contains all information about  $x(t)$ 
  - $f_s > 2 \cdot f_{\text{sig,max}}$
- How to reconstruct  $x(t)$  from  $x(n)$ ?
- Ideal interpolation formula
$$x(t) = \sum_{n=-\infty}^{\infty} x(n) \cdot g(t - nT_s)$$
$$g(t) = \frac{\sin(\pi f_s t)}{\pi f_s t}$$
- Very hard to build an analog circuit that does this...

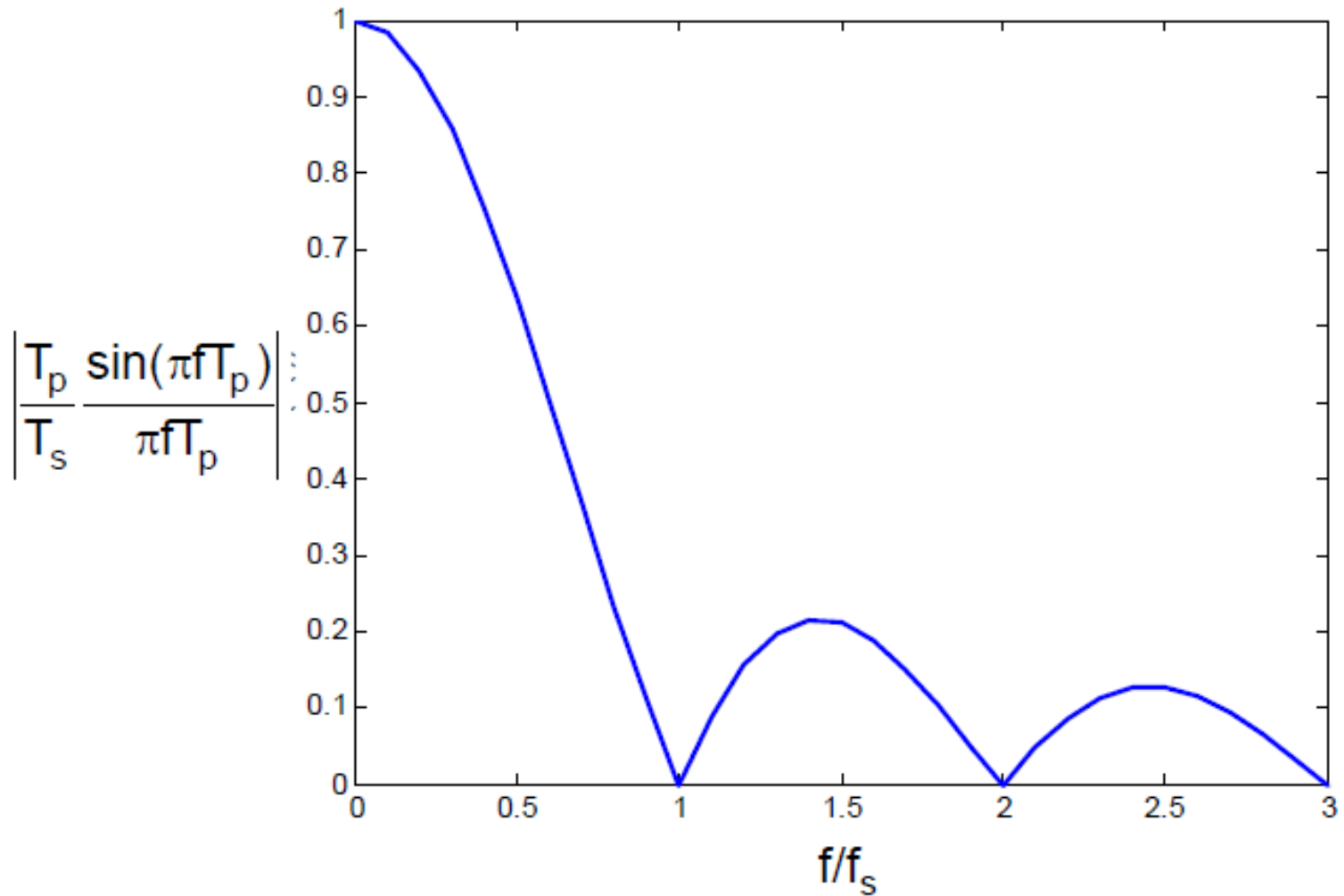
# Zero-Order Hold

- Analog signal  $x(t)$
- Discrete time representation  $x(n)$
- Zero order hold approximation



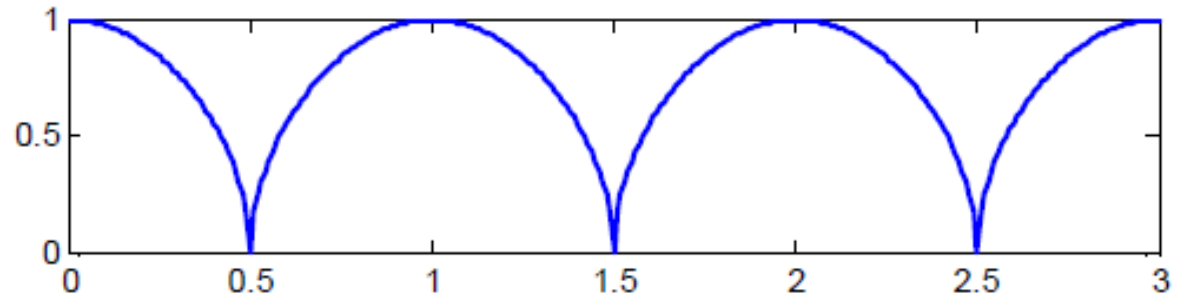
- The most practical way of reconstructing the continuous time signal is to simply "hold" the discrete time values
  - Either for full period  $T_s$  or a fraction thereof
  - Other schemes exist, e.g. "partial-order hold"
    - See [Jha, TCAS II, 11/2008]
- What does this do to the signal spectrum?

# Envelope with Hold Pulse $T_p=T_s$

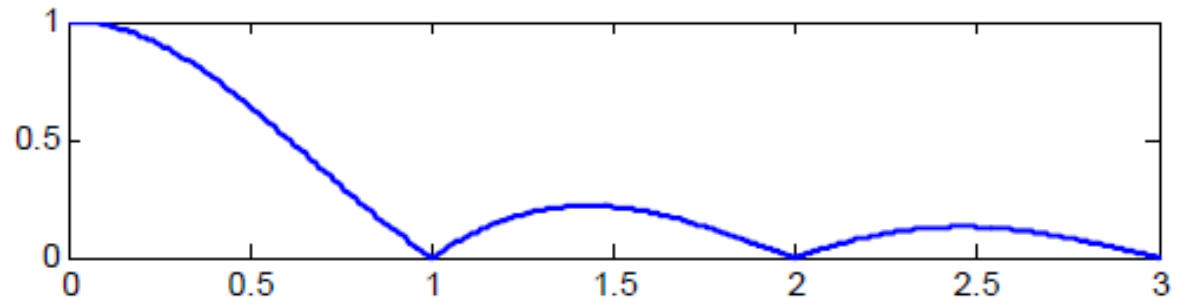


# Signal Spectrum Example

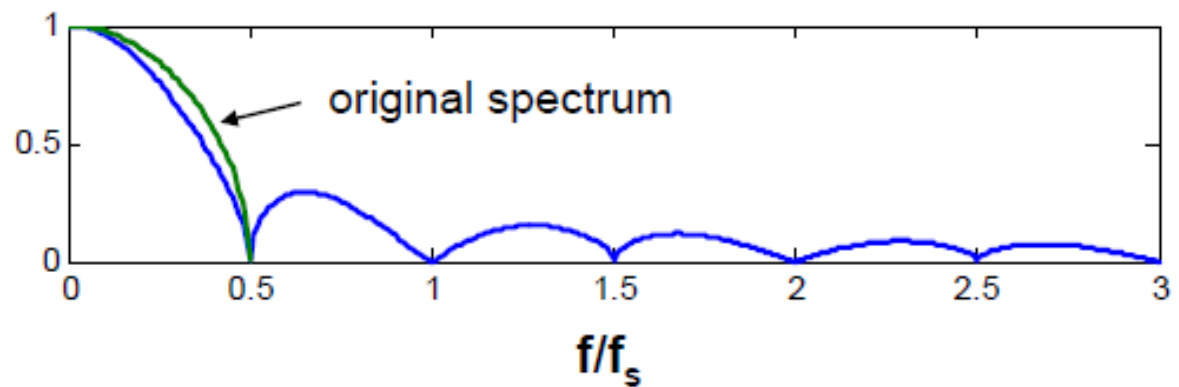
**Spectrum of  
Continuous Time  
Pulse Train (Arbitrary  
Example)**



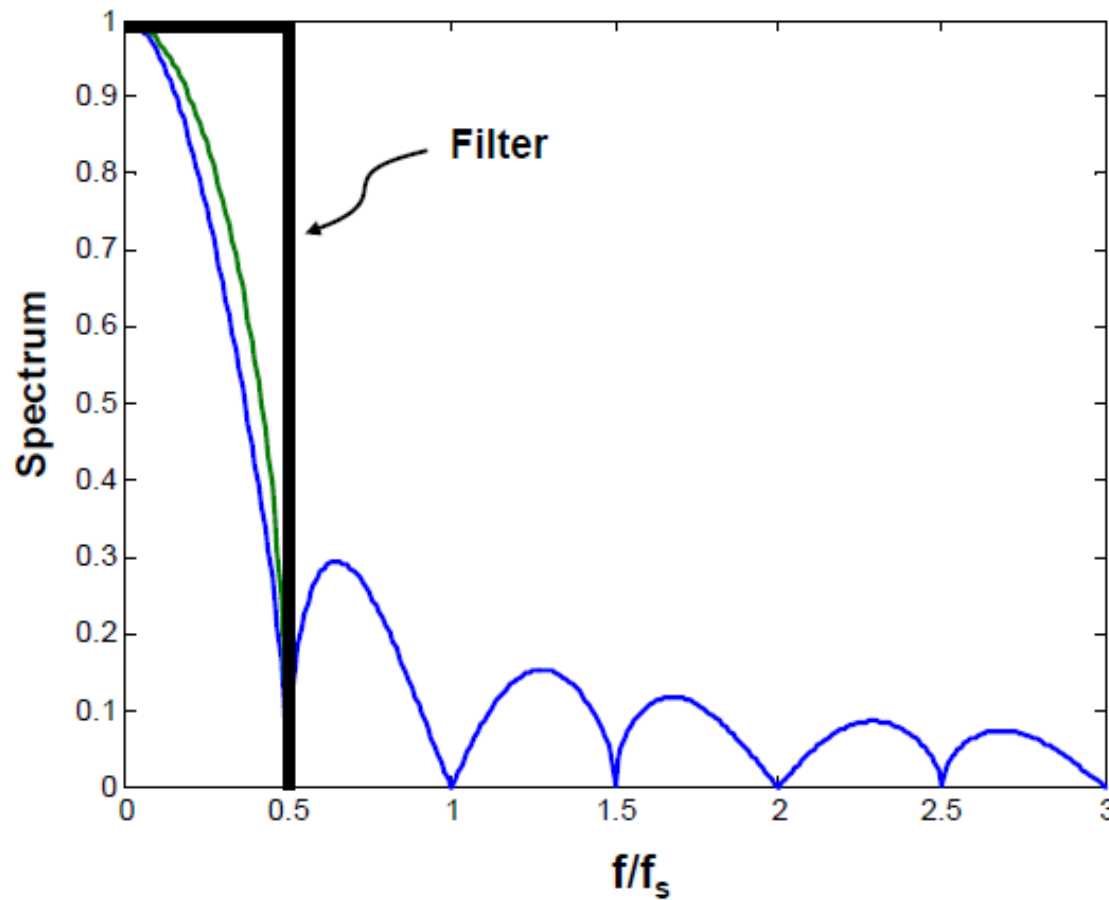
**ZOH Transfer  
Function  
("Sinc Distortion")**



**ZOH output,  
Spectrum of  
Staircase  
Approximation**



# Reconstruction Filter



- Also called smoothing filter
- Same situation as with anti-alias filter
  - A brick wall filter would be nice
  - Oversampling helps reduce filter order

# Summary of Signal Reconstruction

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- Must obey sampling theorem  $f_s > 2 \cdot f_{\text{sig,max}}$ ,
  - Usually dictates anti-aliasing filter
- If sampling theorem is met, continuous time signal can be recovered from discrete time sequence without loss of information
- A zero order hold in conjunction with a smoothing filter is the most common way to reconstruct
  - May need to add pre- or post-emphasis to cancel droop due to sinc envelope
- Oversampling helps reduce order of anti-aliasing and reconstruction filters