

EE 538B CMOS RF IC DESIGN

Midterm Examination No. 1: April 28, 2004

Time Allowed: 110 Minutes

Student Name: Solutions

UW Student ID #: 1234567

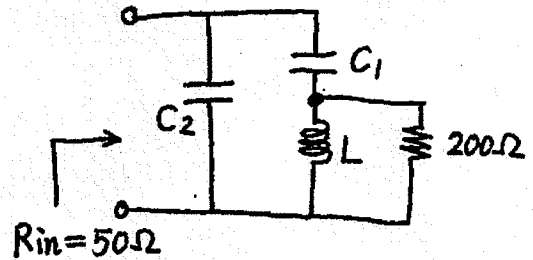
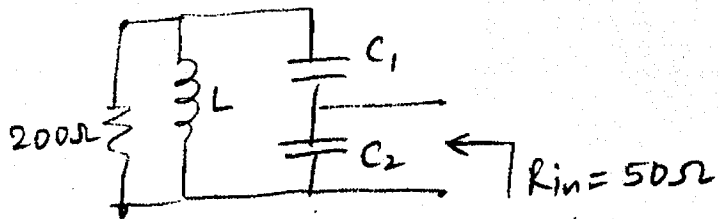
You are allowed one sheet of notes. Write legibly. Show all work. State assumptions.

Problem #	Points Possible	Points
1	10	10
2	20	20
3	25	25
4	25	25
5	20	20

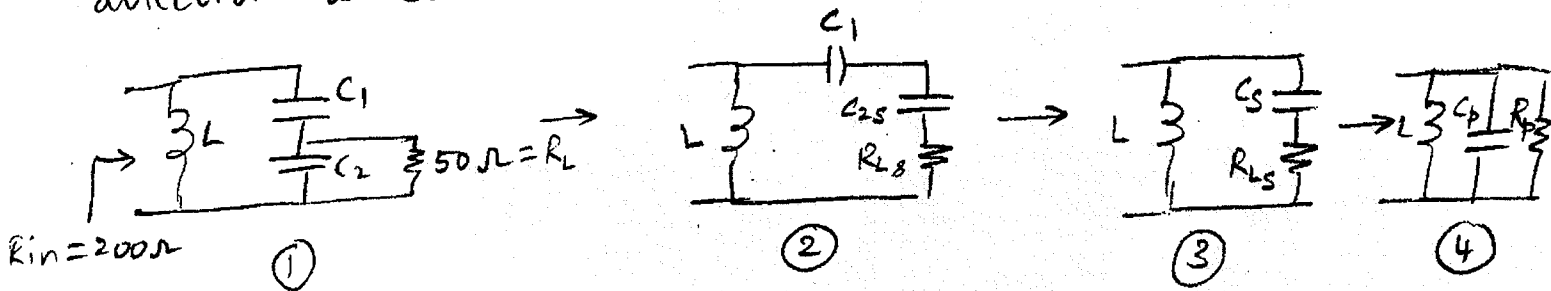
100

1. (10 points) With $Q=10$, the matching circuit below is used to convert $R_L = 200\Omega$ to $R_{IN} = 50\Omega$ at $f_0 = 2.4\text{GHz}$. Determine the required component values. (Sorry Jeff, No Smith Charts are provided ☹)

The ckt can be redrawn as a tapped capacitor match.



The ckt is reciprocal, and analysing the reverse direction is easier.



$$\textcircled{4} : R_p = 200\Omega, Q = 10 \Rightarrow L = \frac{R_p}{Q\omega_0} = \underline{1.326\text{nH}}$$

$$C_p = \frac{Q}{\omega_0 R_p} = 3.316\text{pF} \Rightarrow C_s = 3.35\text{pF}$$

$$R_{Ls} = \frac{R_p}{1+Q^2} = 1.98\Omega$$

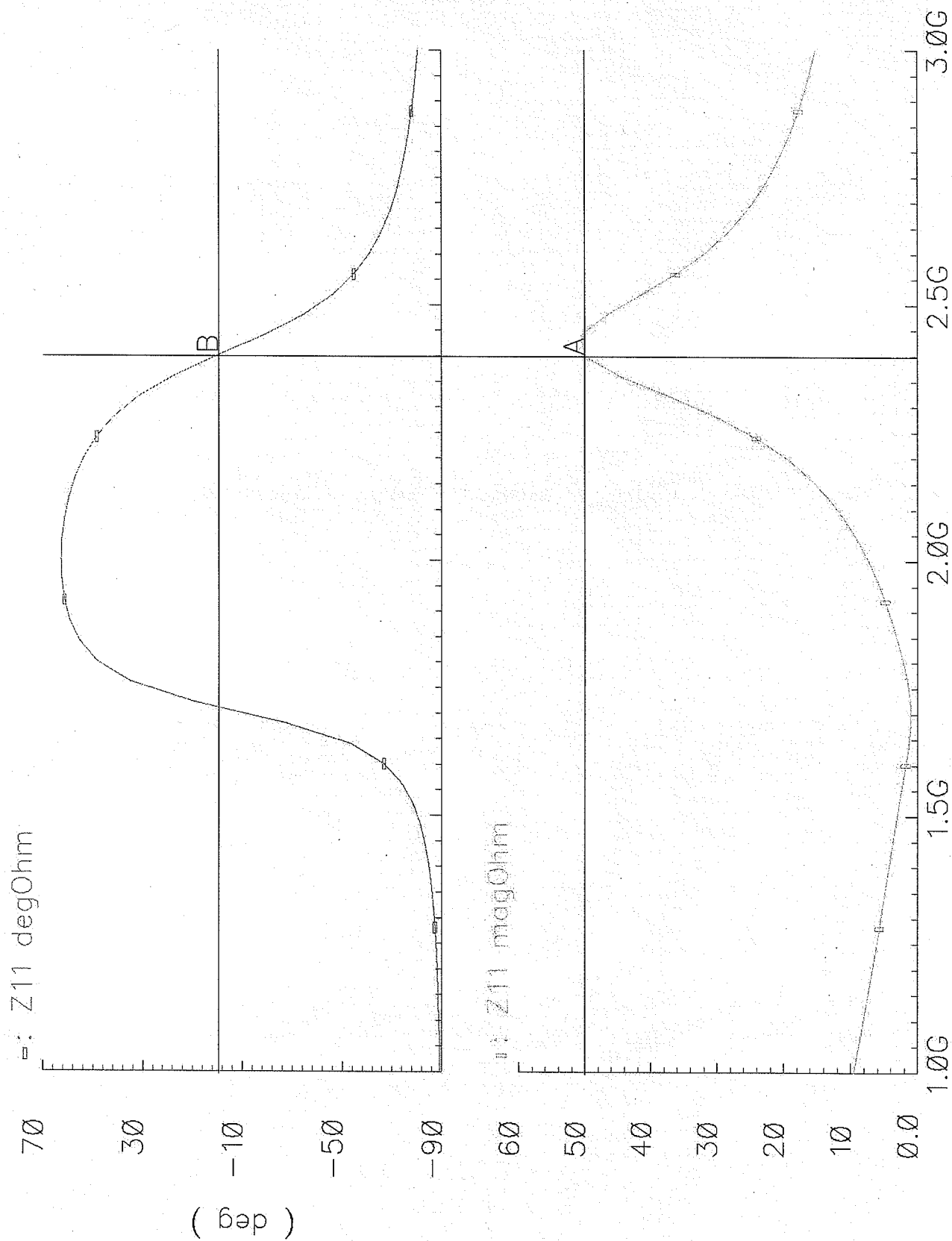
$$\textcircled{2} : Q_R = \sqrt{\frac{R_L}{R_{Ls}}} - 1 = 4.925$$

$$C_2 = \frac{Q_R}{\omega_0 R_L} = \underline{6.53\text{pF}} \Rightarrow C_{2s} = 6.8\text{pF}$$

$$\frac{1}{C_s} = \frac{1}{C_1} + \frac{1}{C_{2s}} \Rightarrow \underline{C_1 = 6.60\text{pF}}$$

S-Parameter Response

1

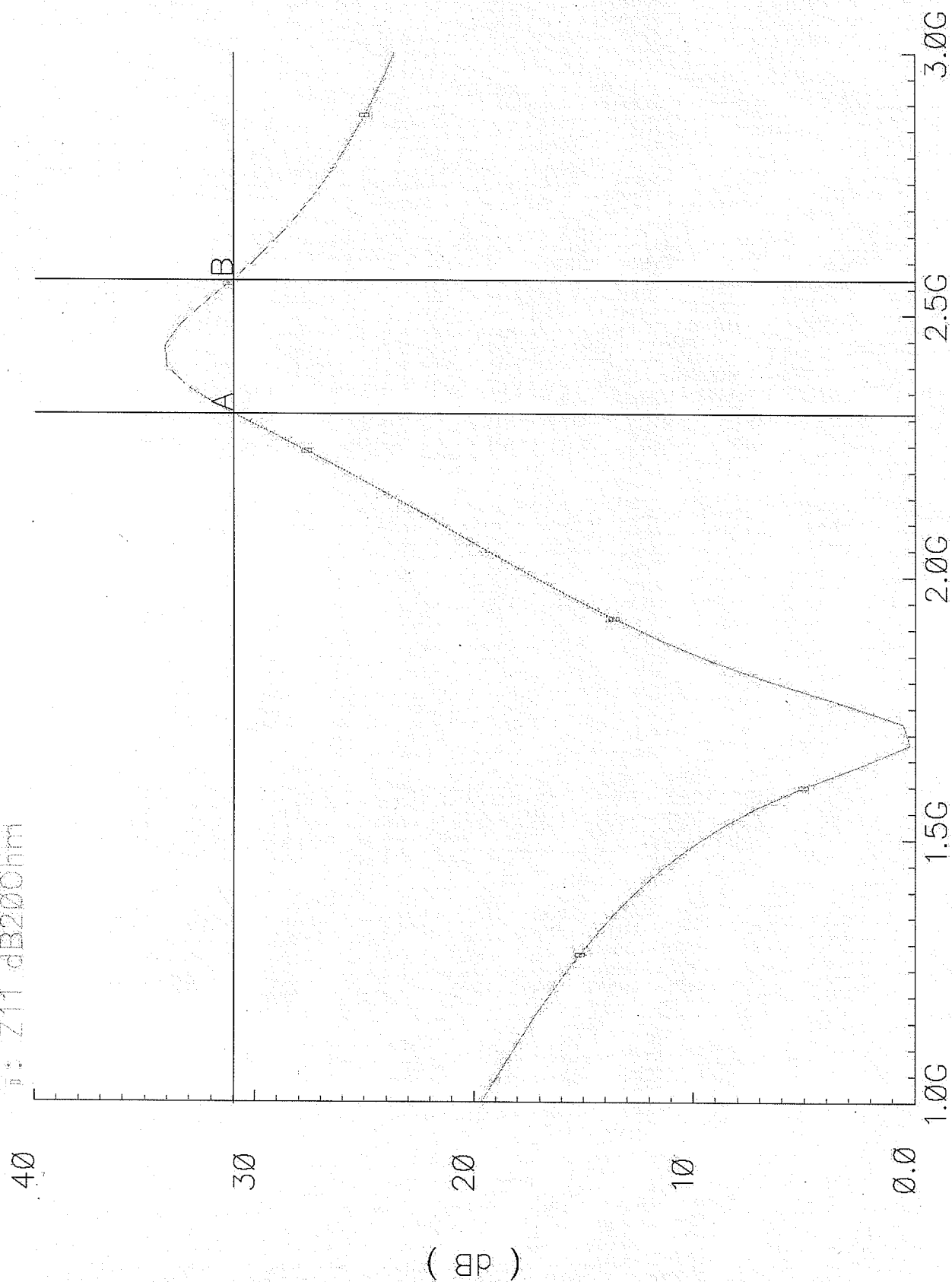


A: (2.4G 50.0522) delta: (0 -50.1634)
 B: (2.4G -111.149m) slope: undefined

S-Parameter Response

1

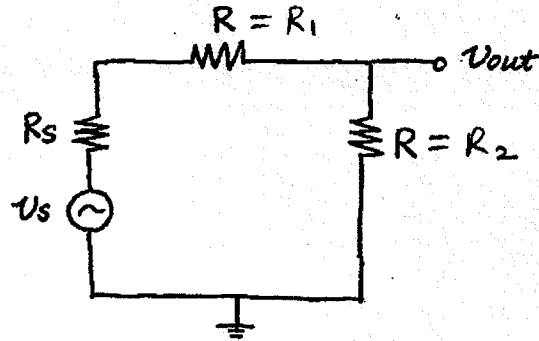
Y: Z11 dB200hm



A: (2.31187G 30.9885) delta: (256.069M -2.02521u)

B: (2.56794G 30.9885) slope: -7.90885f

2. (20 points) A resistive network is shown below:



(a) What is the noise factor of the above circuit with respect to source resistance R_s ?

$$\overline{V_{n,R_s}^2} = 4kTR_s \Delta f \cdot \left(\frac{R}{2R + R_s} \right)^2; \quad \overline{V_{n,R_1}^2} = 4kTR \Delta f \left(\frac{R}{2R + R_s} \right)^2$$

$$\overline{V_{n,R_2}^2} = 4kTR \Delta f \cdot \left(\frac{R + R_s}{2R + R_s} \right)^2$$

$$NF = \frac{\overline{V_{n,tot}^2}}{\overline{V_{n,R_s}^2}} = 1 + \frac{\overline{V_{n,R_1}^2} + \overline{V_{n,R_2}^2}}{\overline{V_{n,R_s}^2}}$$

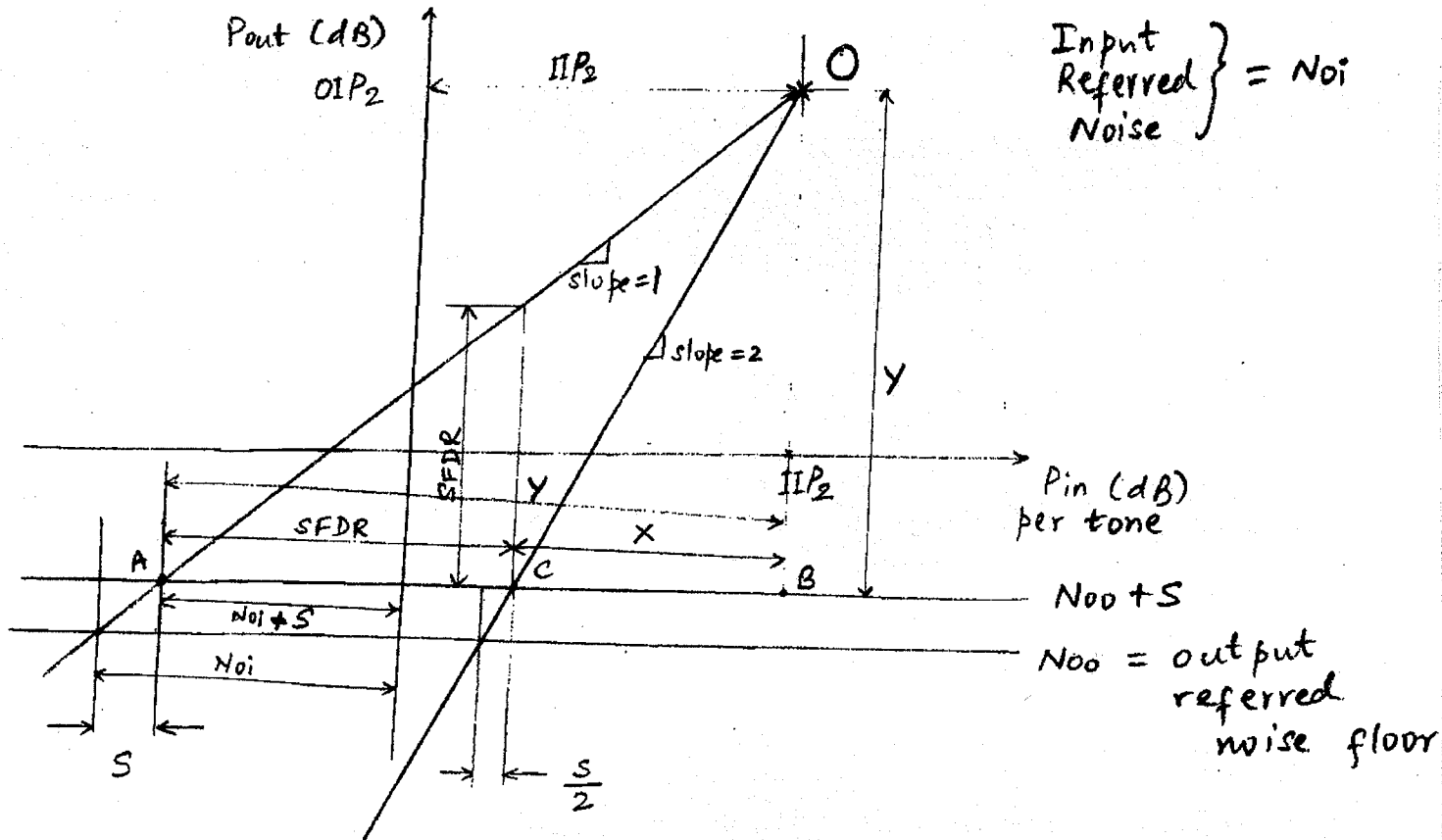
$$= 1 + \frac{4kTR \Delta f \left\{ \frac{R^2}{(2R + R_s)^2} + \frac{(R + R_s)^2}{(2R + R_s)^2} \right\}}{4kTR_s \Delta f \cdot \frac{R^2}{(2R + R_s)^2}} = 1 + \frac{2R^2 + 2RR_s + R_s^2}{RR_s}$$

$$= \underline{3 + \frac{2R}{R_s} + \frac{R_s}{R}}$$

(b) What value of R minimizes the noise factor F ?

$$\frac{dNF}{dR} = 0 \Rightarrow \frac{2}{R_s} - \frac{R_s}{R^2} = 0 \Rightarrow \boxed{R = \frac{R_s}{\sqrt{2}}}$$

3. (25 points) Assume that in a Direct Conversion Receiver (DCR), IIP2 (2nd order intermodulation) is the dominant non-linearity component in the system. Determine the relation between SFDR, IIP2 and Input-Referred Noise of the system, using a graphical method. Assume that the system requires a minimum Input SNR 'S' to work properly.



The IM2 curve has a slope of 2; x is the distance between points B & C.

$$\frac{x}{y} = \frac{1}{2} ; \quad \frac{x + \text{SFDR}}{y} = 1 \quad (\text{slope of fundamental curve is 1})$$

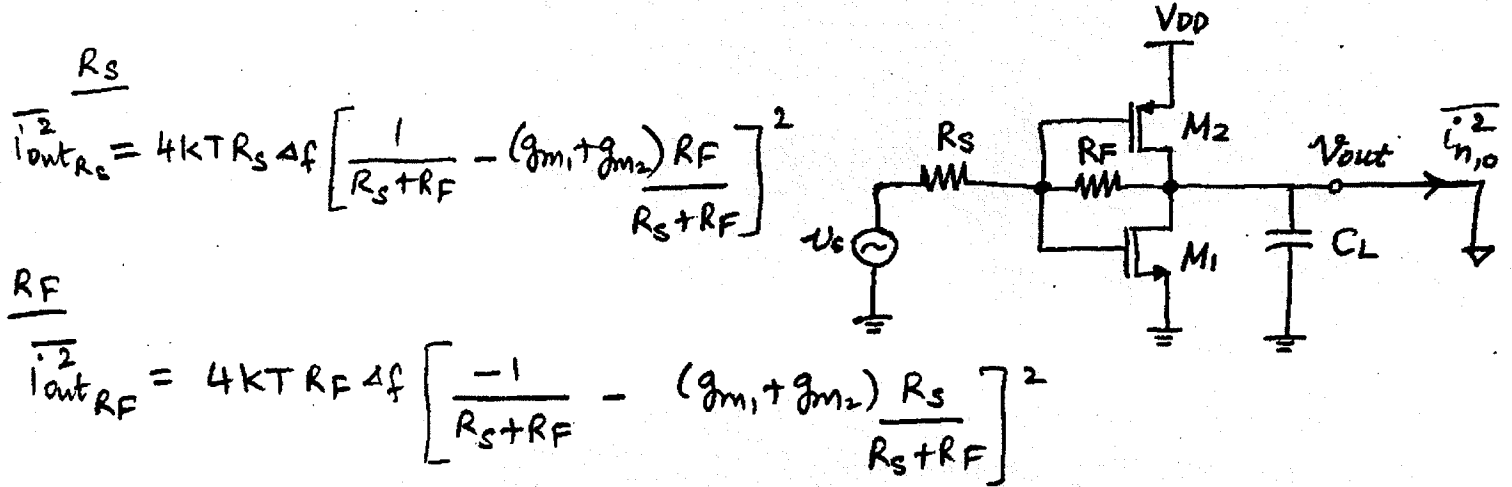
$$\therefore x = \text{SFDR} = \frac{y}{2}$$

$$y = x \text{ co-ord (B)} - x \text{ co-ord (A)}$$

$$= \text{IIP}_2 - (N_{oi} + S)$$

$$\therefore \text{SFDR} = \frac{1}{2} [\text{IIP}_2 - N_{oi} - S]$$

4. (25 points) Determine the noise factor of the circuit shown below with respect to the source resistance R_S . Neglect channel length modulation effects, all parasitic capacitors and induced gate noise of the MOSFETs. Assume that all the MOSFETs work in saturation region.



$$\frac{R_S}{i_{out,R_S}^2} = 4KT R_S \Delta f \left[\frac{1}{R_S + R_F} - \frac{(g_{m1} + g_{m2}) R_F}{R_S + R_F} \right]^2$$

$$\frac{R_F}{i_{out,R_F}^2} = 4KT R_F \Delta f \left[\frac{-1}{R_S + R_F} - \frac{(g_{m1} + g_{m2}) R_S}{R_S + R_F} \right]^2$$

$$\frac{M_1}{i_{out,M_1}^2} = 4KT \gamma g_{d01} \Delta f$$

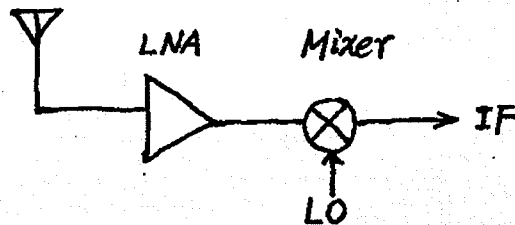
$$\frac{M_2}{i_{out,M_2}^2} = 4KT \gamma g_{d02} \Delta f$$

$$F = 1 + \frac{i_{R_F}^2 + i_{M_1}^2 + i_{M_2}^2}{i_{R_S}^2}$$

$$= 1 + \frac{4KT \Delta f \left[\gamma (g_{d01} + g_{d02}) + \frac{R_F}{(R_S + R_F)^2} \{1 + (g_{m1} + g_{m2}) R_S\}^2 \right]}{4KT \Delta f \left[\frac{R_S}{(R_S + R_F)^2} \{1 - (g_{m1} + g_{m2}) R_F\}^2 \right]}$$

$$= 1 + \frac{\gamma (g_{d01} + g_{d02}) (R_S + R_F)^2 + R_F [1 + (g_{m1} + g_{m2}) R_S]^2}{R_S [1 - (g_{m1} + g_{m2}) R_F]^2}$$

5. (20 points) Calculate the overall Noise Figure and IIP3 for the RF front end shown below.



$$\begin{array}{ll} A_p = 18 \text{ dB} & 20 \text{ dB} \\ NF = 2.5 \text{ dB} & 12 \text{ dB} \\ IIP3 = -15 \text{ dBm} & +5 \text{ dBm} \end{array}$$

$$F_1 = 1.78; F_2 = 15.85; A_{p1} = 63.1$$

$$F_{tot.} = F_1 + \frac{F_2 - 1}{A_{p1}} = 1.78 + \frac{14.85}{63.1} = 2.02$$

$$NF_{tot.} = 10 \log F_{tot.} = 3.04 \text{ dB}$$

$$\frac{1}{IIP_{3,tot}^2} = \frac{1}{IIP_{3,1}^2} + \frac{A_p}{IIP_{3,2}^2}; \quad IIP_{3,1}^2 = 3.16 \times 10^{-5}$$

$$IIP_{3,2}^2 = 3.16 \times 10^{-3}$$

$$\frac{1}{IIP_{3,tot}^2} = \frac{1}{3.16 \times 10^{-5}} + \frac{63.1}{3.16 \times 10^{-3}} = 51613.92$$

$$IIP_{3,tot}^2 = 1.94 \times 10^{-5} = \underline{\underline{-17.12 \text{ dBm}}}$$