## EE230-02 RFIC II Fall 2018

Lecture 22: Power Amplifier

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#### **Schedule**

No class on Thursday, Dec. 6 - IEDM conference

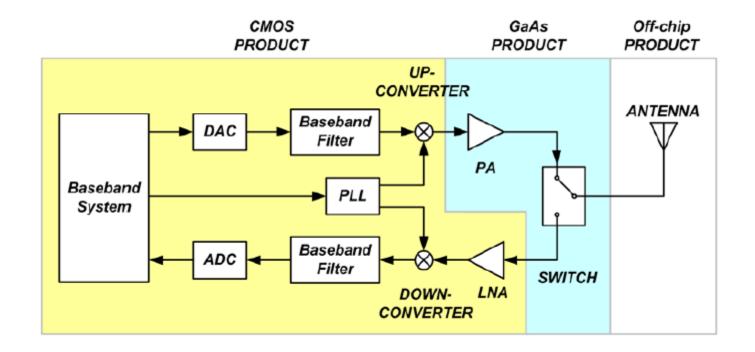
Project Report Due: Dec. 10

Final Exam: Dec. 14, Friday 2:45 PM
 One-page Aid sheet on Front side only
 Bring a Calculator

### **Final Exam Topic**

- Matching Network
- LNA and Noise
- VCO
- PLL
- PA
- Misc. questions

# **Block Diagram of Direct Conversion System**



### **Power Amplifier Performance Metrics**

- Metrics defined in standards
  - Output Power
  - Spectral Mask
  - ACPR (Adjacent Channel Power Ratio)
  - Signal Modulation
- Metrics not defined in standards
  - PAE (Power Added Efficiency)
  - Drain Efficiency
  - Power Gain
  - IP3
  - P1dB

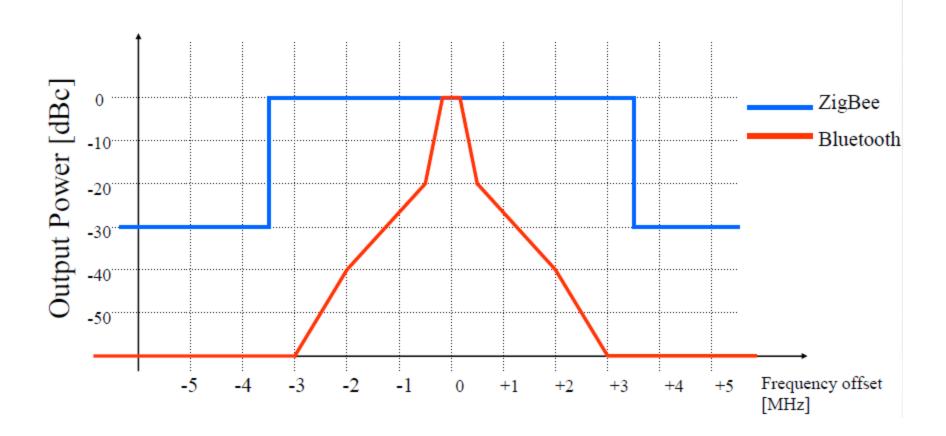
## **Output Power**

Maximum output power varies drastically among different standards

Standard	Modulation	Max. P <sub>out</sub>
AMPS	FM	31 dBm
GSM	GMSK	36 dBm
CDMA	O-QPSK	28 dBm
DECT	GFSK	27 dBm
PDC	π/4 DQPSK	30 dBm
Bluetooth	FSK	16 dBm
802.11a	OFDM	14-19 dBm
802.11b	PSK-CCK	16-20 dBm

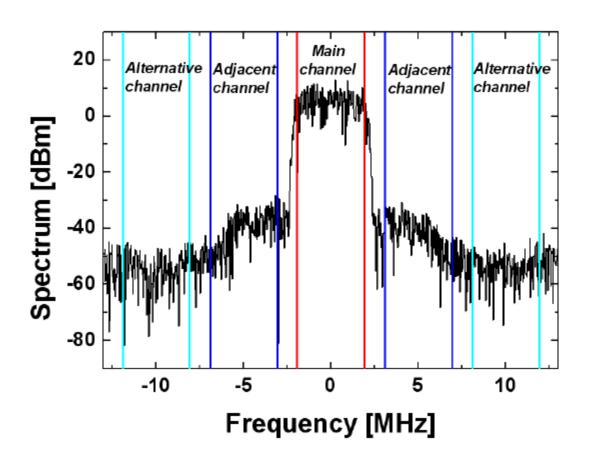
### **Spectral Mask**

Power mask is an indication of how much spectrum regrowth is allowed

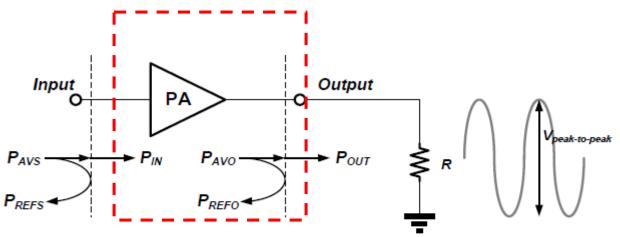


#### **ACPR**

 $ACLR \text{ (dBc)} \equiv 10 \log \left( \frac{\text{Power in Adjacent or Alternative Channel in Watt}}{\text{Power in Main Channel in Watt}} \right)$ 



#### **Definition of Power and Gain**

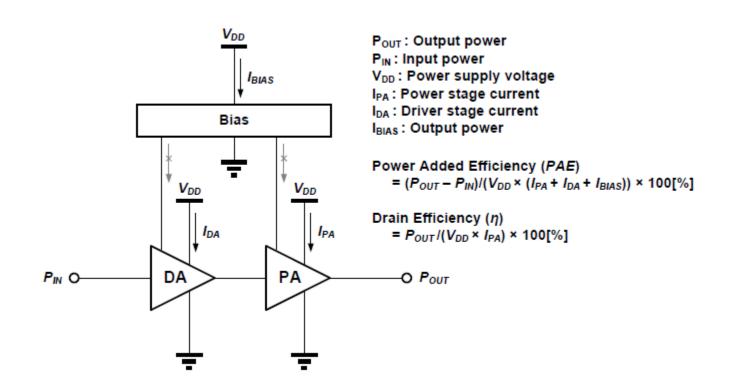


Transducer Gain  $(G_T) = P_{OUT} / P_{AVS}$ Power Gain  $(G_P) = P_{OUT} / P_{IN}$ Available Gain  $(G_A) = P_{AVO} / P_{AVS}$ 

$$P_{OUT} = \frac{\left(\frac{V_{\text{peak-to-peak}}}{2}\right)^2}{2 \cdot R}$$

$$\begin{aligned} & \text{Transducer Gain } (G_T) = \frac{P_{OUT}}{P_{AVS}}, \\ & \text{Power Gain } (G_P) = \frac{P_{OUT}}{P_{IN}} = G_T \left( 1 + \frac{P_{REFS}}{P_{IN}} \right), \\ & \text{Available Gain } (G_A) = \frac{P_{AVO}}{P_{AVS}} = G_T \left( 1 + \frac{P_{REFO}}{P_{OUT}} \right) \end{aligned}$$

# **Efficiency of PA**



#### **Drain Efficiency**

$$\eta(DE) = \frac{P_{OUT}}{P_{DC}} = \frac{P_{OUT}}{P_{DC} \cdot I_{PA}}$$

#### **Power Added Efficiency**

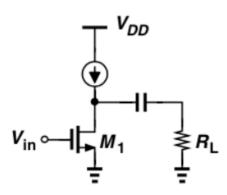
$$PAE = \frac{P_{OUT} - P_{IN}}{P_{DC}}$$

## **Output Power and Voltage Swing**

Ex: 1 W (30 dBm) into a resistive 50 Ω load (e.g. antenna).

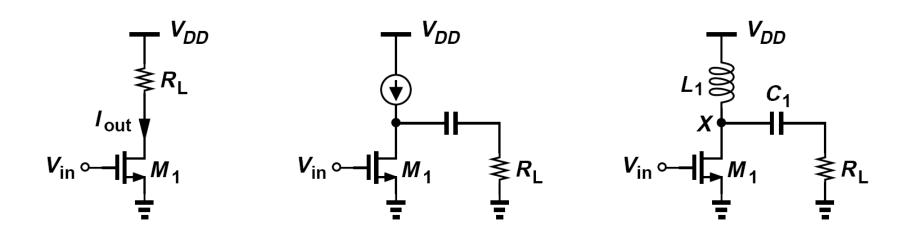
$$P = \frac{V_p^2}{2R_L}$$

$$=> 10 \text{ V}_p, \text{ I}_p = 200 \text{ mA}.$$



- How can we achieve this with nm-CMOS?
- => Impedance transformation: lower voltage, more current
- For high-power PAs: as high supply voltage as possible, and impedance transformation.

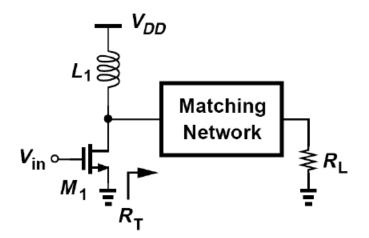
### **Output Power and Voltage Swing**

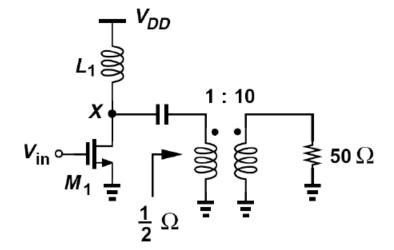


- For a common-source (or common-emitter) stage to drive the load directly, a supply voltage greater than  $V_{pp}$  is required.
- If the load is realized as an inductor, the drain ac voltage exceeds  $V_{DD}$ , even reaching  $2V_{DD}$  (or higher). But the maximum drain-source voltage experienced by  $M_1$  is still at least 20 V if the stage must deliver 1 W to a 50-Ω load.

### **Matching Network**

 In order to reduce the peak voltage experienced by the output transistor, a <u>matching network</u> is interposed between the PA and the load. This network transforms the load resistance to a lower value, R<sub>T</sub>, so that smaller voltage swings still deliver the required power.

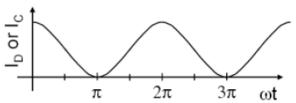




#### **Linear PA Classes**

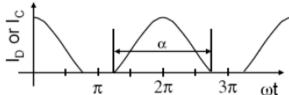
Conduction Angle:

Class A:



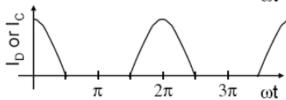
 $\alpha = 2\pi$ 

Class AB:



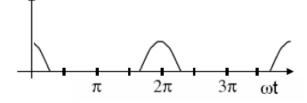
 $\pi < \alpha < 2\pi$ 

Class B:



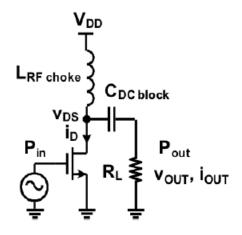
 $\alpha = \pi$ 

Class C:



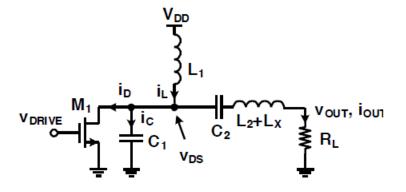
 $\alpha < \pi$ 

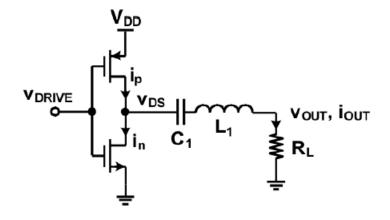
#### **PA Classes**



class-A/AB/B/C (linear)

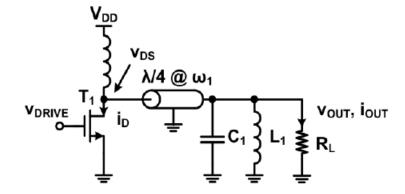
class-E (switched)





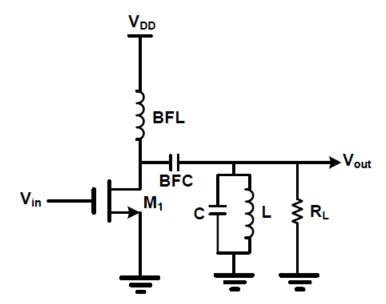
inverter-based class-D (switched)

class-F (switched)



### **Linear PA Classes – A,B,C**

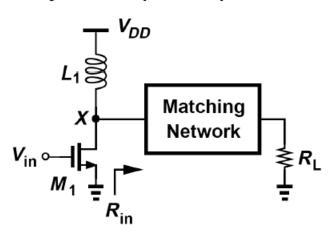
- Output power delivered to R<sub>L</sub>.
- A "big fat" inductor (BFL) feeds DC power to the drain. It is big enough to create a constant current.
- BFC prevents DC dissipation in the load.
- The tank absorbs the parasitics of the transistor.
- LC tank filters out of band emissions created by nonlinearities in the transistor.
- Different gate-biases
  => linear class A, AB, B, C.

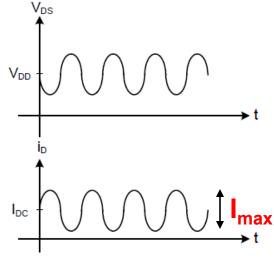


#### Class A

- Since BFL presents a DC short, the drain voltage (which is the sum of DC and the signal voltage) has a symmetrical swing around V<sub>DD</sub>.
- The drain voltage and current has a 180° phase difference.

 The product of drain current and voltage is positive; the transistor always dissipates power.



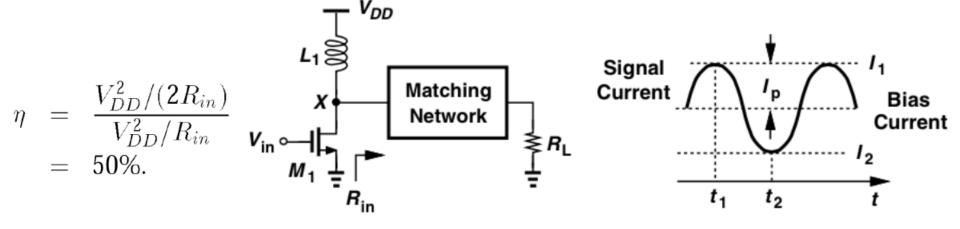


#### Class A

Device biased to ~ I<sub>max</sub>/2 to never switch off.

$$\frac{I_{max}}{2} = \frac{V_{DD}}{R_L}$$

- Good linearity.
- Efficiency <= 50 %.</li>
- V<sub>x</sub> swings up to 2 x V<sub>DD</sub> and the peak drain current is 2V<sub>DD</sub>/R<sub>L</sub>.
  The device must be able to manage this stress!



### **Efficiency of Class-A**

$$\eta = \frac{P_{1}}{P_{dc}} = \frac{I_{1,rms}.V_{1,rms}}{I_{dc}.V_{dc}}$$

$$\begin{cases} I_{1} = \frac{I_{MAX}}{2}, \ I_{dc} = \frac{I_{MAX}}{2} \\ \eta = \frac{\left(\frac{I_{MAX}/2}{\sqrt{2}}\right)\!\left(\frac{V_{DD}}{\sqrt{2}}\right)}{\left(\frac{I_{MAX}}{2}\right)\!.V_{DD}} = 50\% \text{ max} \,. \end{cases}$$

### **Efficiency of Class-B**

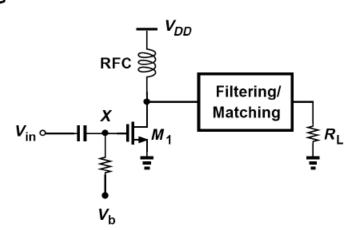
$$\begin{cases} I_1 = \frac{I_{MAX}}{2}, \ I_{dc} = \frac{I_{MAX}}{\pi} \\ \\ \eta = \frac{\left(\frac{I_{MAX}/2}{\sqrt{2}}\right)\!\left(\frac{V_{DD}}{\sqrt{2}}\right)}{\left(\frac{I_{MAX}}{\pi}\right)\!.V_{DD}} = 78\% \text{ max}. \end{cases}$$

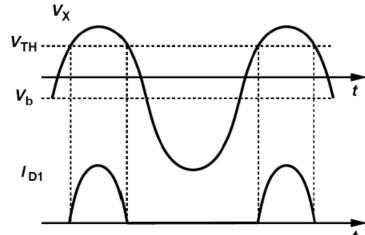
#### Class AB

- In a class A amplifier, the device conducts 100 % of the time, and in a class B, it conducts 50 % of the time.
- A class AB amplifier is something in-between; the device conducts between 50 % and 100% of the time.
- The efficiency and the linearity are intermediate between a class A and class B amplifier.
- Due to these trade-offs, class AB power amplifiers are popular in many applications.

#### Class C

- In a class C power amplifier, the time in which the transistor conducts is decreased to less than half period.
- The drain current consists of a periodic train of pulses, which can be approximated by the top pieces of a sine wave





#### **Output Voltage Shape**

If load tank filters out all harmonics, output voltage is pure sinusoidal even when there is current discontinuity

