

# Path-loss and Shadowing (Large-scale Fading)

PROF. MICHAEL TSAI

2011/10/20

# Friis Formula

TX Antenna



$$\text{EIRP} = P_t G_t$$

RX Antenna



$$\times A_e$$

$$\Rightarrow P_r = \frac{P_t G_t A_e}{4\pi d^2}$$

$d$

Power spatial density  $\left(\frac{W}{m^2}\right)$

$$\times \frac{1}{4\pi d^2}$$

# Antenna Aperture

$$P_r = \frac{P_t G_t A_e}{4\pi d^2}$$

- Antenna Aperture=Effective Area
- Isotropic Antenna's effective area  $A_{e,iso} \doteq \frac{\lambda^2}{4\pi}$
- Isotropic Antenna's Gain=1
- $G = \frac{4\pi}{\lambda^2} A_e$
- Friis Formula becomes:  $P_r = \frac{P_t G_t G_r \lambda^2}{(4\pi d)^2} = \frac{P_t A_t A_r}{\lambda^2 d^2}$

# Friis Formula

$$P_r = \frac{P_t G_t G_r \lambda^2}{(4\pi d)^2}$$

- $\frac{\lambda^2}{(4\pi d)^2}$  is often referred as “Free-Space Path Loss” (FSPL)
- Only valid when  $d$  is in the “far-field” of the transmitting antenna
- Far-field: when  $d > d_f$ , Fraunhofer distance
- $d_f = \frac{2D^2}{\lambda}$ , and it must satisfies  $d_f \gg D$  and  $d_f \gg \lambda$ 
  - $D$ : Largest physical linear dimension of the antenna
  - $\lambda$ : Wavelength
- We often choose a  $d_0$  in the far-field region, and smaller than any practical distance used in the system
- Then we have  $P_r(d) = P_r(d_0) \left(\frac{d}{d_0}\right)^2$

# Received Signal after Free-Space Path Loss

phase difference due to propagation distance

$$r(t) = \text{Re} \left\{ \underbrace{\frac{\lambda \sqrt{G_t G_r}}{4\pi d}}_{\text{Free-Space Path Loss}} \underbrace{\exp\left(-\frac{j2\pi d}{\lambda}\right)}_{\text{phase difference due to propagation distance}} \underbrace{\tilde{g}(t)}_{\text{Complex envelope}} \underbrace{\exp(j2\pi f_c t)}_{\text{Carrier (sinusoid)}} \right\}$$

Free-Space Path Loss

Complex envelope

Carrier (sinusoid)

## Example: Far-field Distance

- Find the far-field distance of an antenna with maximum dimension of 1m and operating frequency of 900 MHz (GSM 900)
- Ans:
- Largest dimension of antenna:  $D=1\text{m}$
- Operating Frequency:  $f=900\text{ MHz}$
- Wavelength:  $\lambda = \frac{c}{f} = \frac{3 \times 10^8}{900 \times 10^6} = 0.33$
- $d_f = \frac{2D^2}{\lambda} = \frac{2}{0.33} = 6.06\text{ (m)}$

## Example: FSPL

- If a transmitter produces 50 watts of power, express the transmit power in units of (a) dBm and (b) dBW.
- If 50 watts is applied to a unity gain antenna with a 900 MHz carrier frequency, find the received power in dBm at a free space distance of 100 m from the antenna. What is the received power at 10 km? Assume unity gain for the receiver antenna.

- Ans:

- $10 \log_{10}(50) = 17 \text{ dBW} = 47 \text{ dBm}$

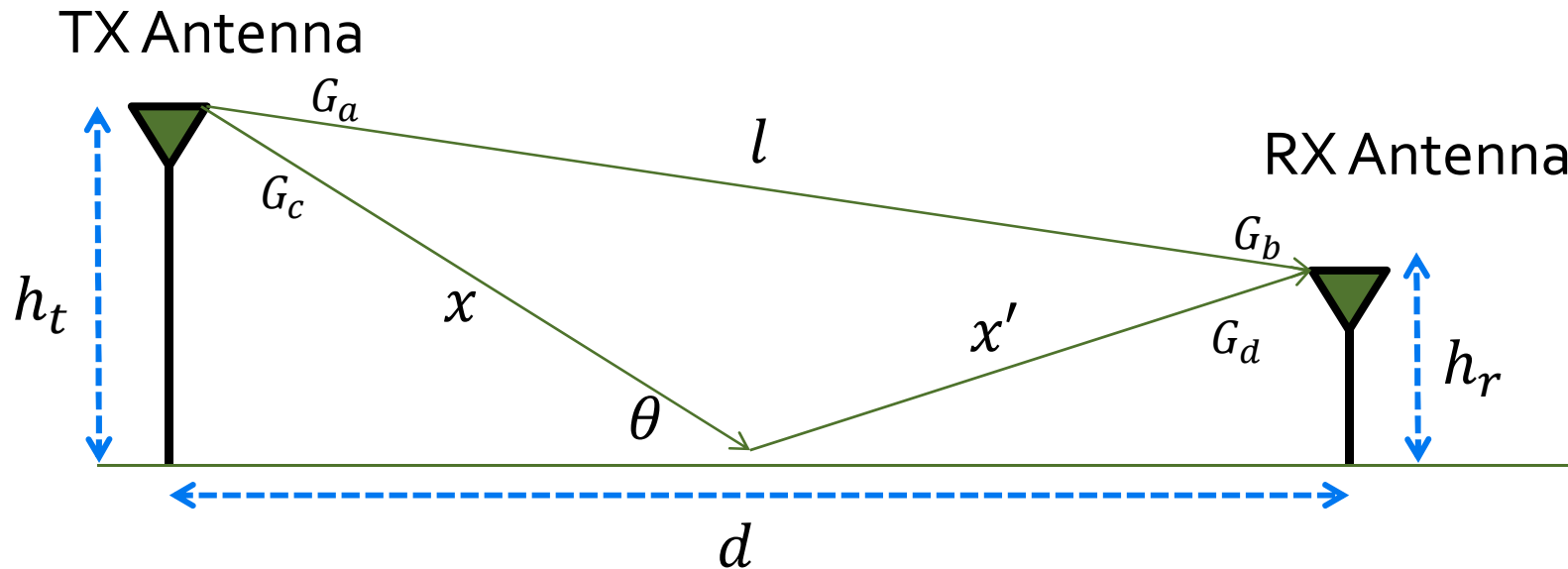
- Received Power at 100m

$$P_r(100m) = \frac{50 \times 1 \times 1 \times \left( \frac{3 \times 10^8}{900 \times 10^6} \right)^2}{(4\pi \times 100)^2} = 3.5 \times 10^{-6} \text{ (W)}$$
$$= -54.5 \text{ (dBW)}$$

- Received Power at 10km

$$P_r(10km) = P_r(100m) \left( \frac{100}{10000} \right)^2 = 3.5 \times 10^{-10} \text{ (W)}$$
$$= -94.5 \text{ (dBW)}$$

# Two-ray Model



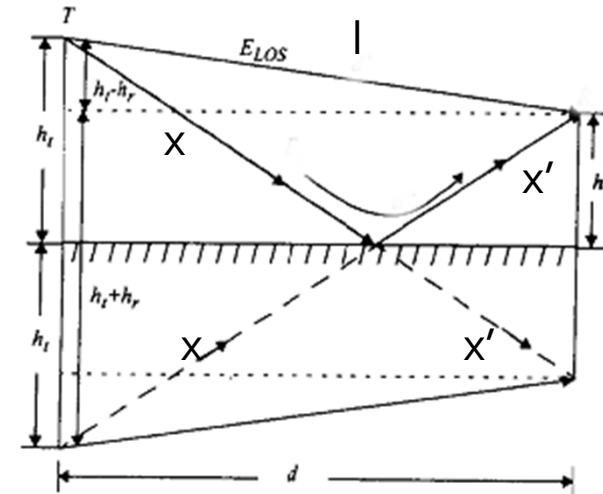
Delayed since  $x+x'$  is longer.  $\tau = (x + x' - l)/c$

$$r_{2\text{-ray}}(t) = \text{Re} \left\{ \frac{\lambda}{4\pi} \left[ \frac{\sqrt{G_a G_b} \tilde{g}(t) \exp\left(-\frac{j2\pi l}{\lambda}\right)}{l} + \frac{R \sqrt{G_c G_d} \tilde{g}(t - \tau) \exp\left(-\frac{j2\pi(x + x')}{\lambda}\right)}{x + x'} \right] \exp(j2\pi f_c t) \right\}$$

$R$ : ground reflection coefficient (phase and amplitude change)



# Two-ray Model: Received Power

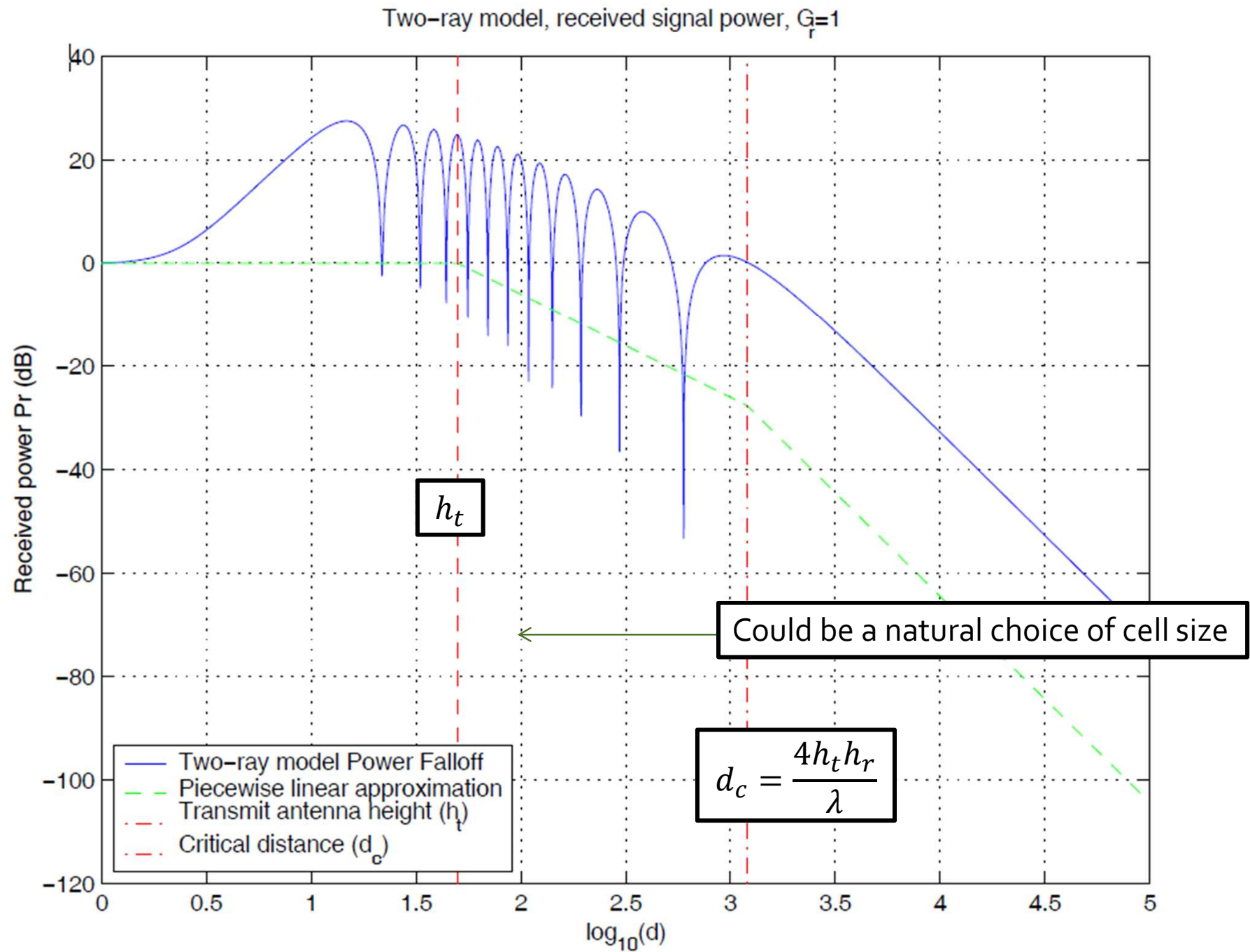


- $$P_r = P_t \left[ \frac{\lambda}{4\pi} \right]^2 \left| \frac{\sqrt{G_a G_b}}{l} + \frac{\sqrt{G_c G_d} \exp(-j\Delta\phi)}{x+x'} \right|^2$$
- The above is verified by empirical results.
- $$\Delta\phi = 2\pi(x + x' - l)/\lambda$$
- $$x + x' - l = \sqrt{(h_t + h_r)^2 + d^2} - \sqrt{(h_t - h_r)^2 + d^2}$$

# Two-ray Model: Received Power

- When  $d \gg h_t + h_r$ ,  $\Delta\phi = \frac{2\pi(x+x'-l)}{\lambda} \approx \frac{4\pi h_t h_r}{\lambda d}$
- For asymptotically large  $d$ ,  $x + x' \approx l \approx d$ ,  $\theta \approx 0$ ,  $G_a G_b \approx G_c G_d$ ,  $R \approx -1$  (phase is inverted after reflection)
- $\left| \frac{\sqrt{G_a G_b}}{l} + \frac{\sqrt{G_c G_d} \exp(-j\Delta\phi)}{x+x'} \right|^2 \approx \left| \frac{\sqrt{G_a G_b}}{d} \right|^2 |1 + \exp(-j\Delta\phi)|^2$
- $|1 + \exp(-j\Delta\phi)|^2 = (1 - \cos(\Delta\phi))^2 + \sin^2 \Delta\phi = 2 - 2\cos(\Delta\phi) = 4\sin^2\left(\frac{\Delta\phi}{2}\right) \approx \Delta\phi^2$
- $P_r \approx \left[ \frac{\lambda \sqrt{G_a G_b}}{4\pi d} \right]^2 \left[ \frac{4\pi h_t h_r}{\lambda d} \right]^2 P_t = \left[ \frac{\sqrt{G_a G_b} h_t h_r}{d^2} \right]^2 P_t$

Independent of  $\lambda$  now



# Indoor Attenuation

- **Factors which affect the indoor path-loss:**
  - Wall/floor materials
  - Room/hallway/window/open area layouts
  - Obstructing objects' location and materials
  - Room size/floor numbers
- **Partition Loss:**

Partition type	Partition Loss (dB) for 900-1300 MHz
Floor	10-20 for the first one, 6-10 per floor for the next 3, A few dB per floor afterwards.
Cloth partition	1.4
Double plasterboard wall	3.4
Foil insulation	3.9
Concrete wall	13
Aluminum siding	20.4
All metal	26

# Simplified Path-Loss Model

- **Back to the simplest:**

$$P_r = P_t K \left[ \frac{d_0}{d} \right]^\gamma$$

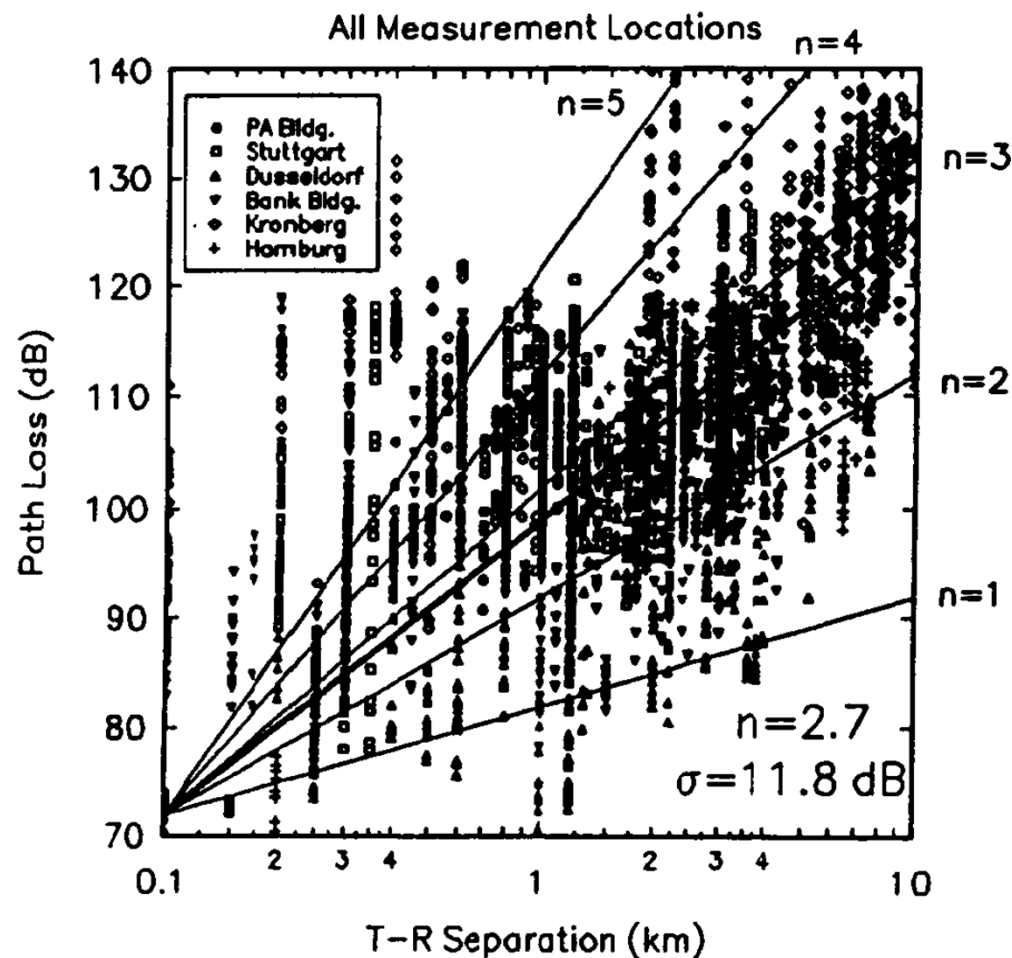
- $d_0$ : reference distance for the antenna far field (usually 1-10m indoors and 10-100m outdoors)
- $K$ : constant path-loss factor (antenna, average channel attenuation), and sometimes we use

$$K = \left( \frac{\lambda}{4\pi d_0} \right)^2$$

- $\gamma$ : path-loss exponent

# Some empirical results

Measurements in Germany Cities



Environment	Path-loss Exponent
Free-space	2
Urban area cellular radio	2.7-3.5
Shadowed urban cellular radio	3-5
In building LOS	1.6 to 1.8
Obstructed in building	4 to 6
Obstructed in factories	2 to 3

# Empirical Path-Loss Model

- **Based on empirical measurements**
  - over a given distance
  - in a given frequency range
  - for a particular geographical area or building
- **Could be applicable to other environments as well**
  - Less accurate in a more general environment
- **Analytical model:  $P_r/P_t$  is characterized as a function of distance.**
- **Empirical Model:  $P_r/P_t$  is a function of distance including the effects of path loss, shadowing, and multipath.**
  - Need to average the received power measurements to remove multipath effects → Local Mean Attenuation (LMA) at distance  $d$ .

# Example: Okumura Model

- **Okumura Model:**

$$P_L(d)dB = L(f_c, d) + A_\mu(f_c, d) - G(h_t) - G(h_r) - G_{AREA}$$

- $L(f_c, d)$ : FSPL,  $A_\mu(f_c, d)$ : median attenuation in addition to FSPL

- $G(h_t) = 20 \log_{10}(\frac{h_t}{200}), G(h_r) = \begin{cases} 10 \log_{10}(\frac{h_r}{3}), h_r \leq 3m, \\ 20 \log_{10}(\frac{h_r}{3}), 3m < h_r < 10m. \end{cases}$

:antenna height gain factor.

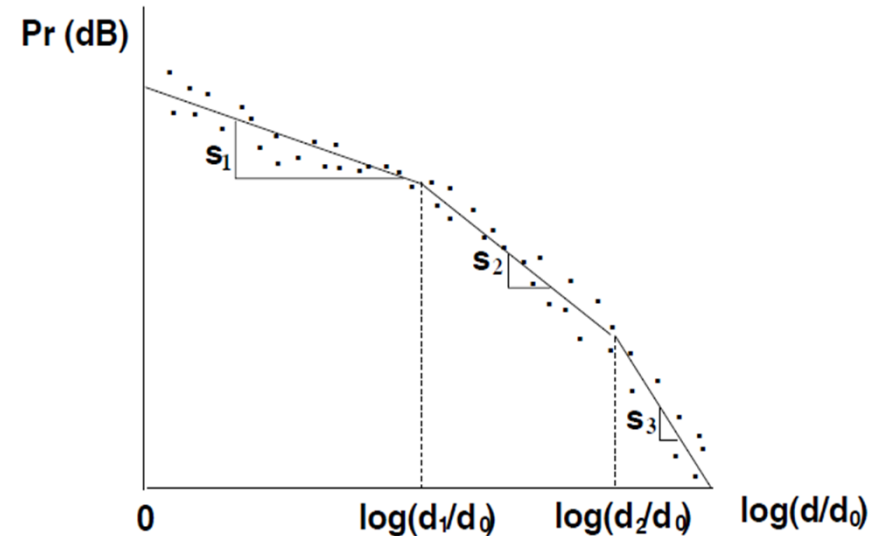
- $G_{AREA}$ : gain due to the type of environment



# Example: Piecewise Linear Model

- **N segments with N-1 “breakpoints”**
- **Applicable to both outdoor and indoor channels**
- **Example – dual-slope model**

$$P_r(d) = \begin{cases} P_t K \left( \frac{d_0}{d} \right)^{\gamma_1} \\ P_t K \left( \frac{d_c}{d} \right)^{\gamma_1} \left( \frac{d}{d_c} \right)^{\gamma_2} \end{cases}$$



$$d_0 \leq d \leq d_c,$$

$$d > d_c.$$

- $K$ : constant path-loss factor
- $\gamma_1$ : path-loss exponent for  $d_0 \sim d_c$
- $\gamma_2$ : path-loss exponent after  $d_c$

# Shadow Fading

- **Same T-R distance usually have different path loss**
  - Surrounding environment is different
- **Reality: simplified Path-Loss Model represents an “average”**
- **How to represent the difference between the average and the actual path loss?**
- **Empirical measurements have shown that**
  - it is random (and so is a random variable)
  - Log-normal distributed

# Log-normal distribution

- A log-normal distribution is a probability distribution of a random variable whose logarithm is normally distributed:

logarithm of the random variable

$$f_X(x; \mu, \sigma^2) = \frac{1}{x\sigma\sqrt{2\pi}} \exp\left(-\frac{(\log x - \mu)^2}{2\sigma^2}\right)$$

normalized so that the integration of the pdf=1

- $x$ : the random variable (linear scale)
- $\mu, \sigma^2$ : mean and variance of the distribution (in dB)

# Log-normal Shadowing

- Expressing the path loss in dB, we have

$$P_L(d)[dB] = \overline{P_L}(d) + X_\sigma = \overline{P_L}(d_0) + 10\gamma \log\left(\frac{d}{d_0}\right) + X_\sigma$$

- $X_\sigma$ : Describes the random shadowing effects
- $X_\sigma \sim N(0, \sigma^2)$   
(normal distribution with zero mean and  $\sigma^2$  variance)
- Same T-R distance, but different levels of clutter.
- Empirical Studies show that  $\sigma$  ranges from 4 dB to 13dB in an outdoor channel

# Why is it log-normal distributed?

- Attenuation of a signal when passing through an object of depth  $d$  is *approximately*:

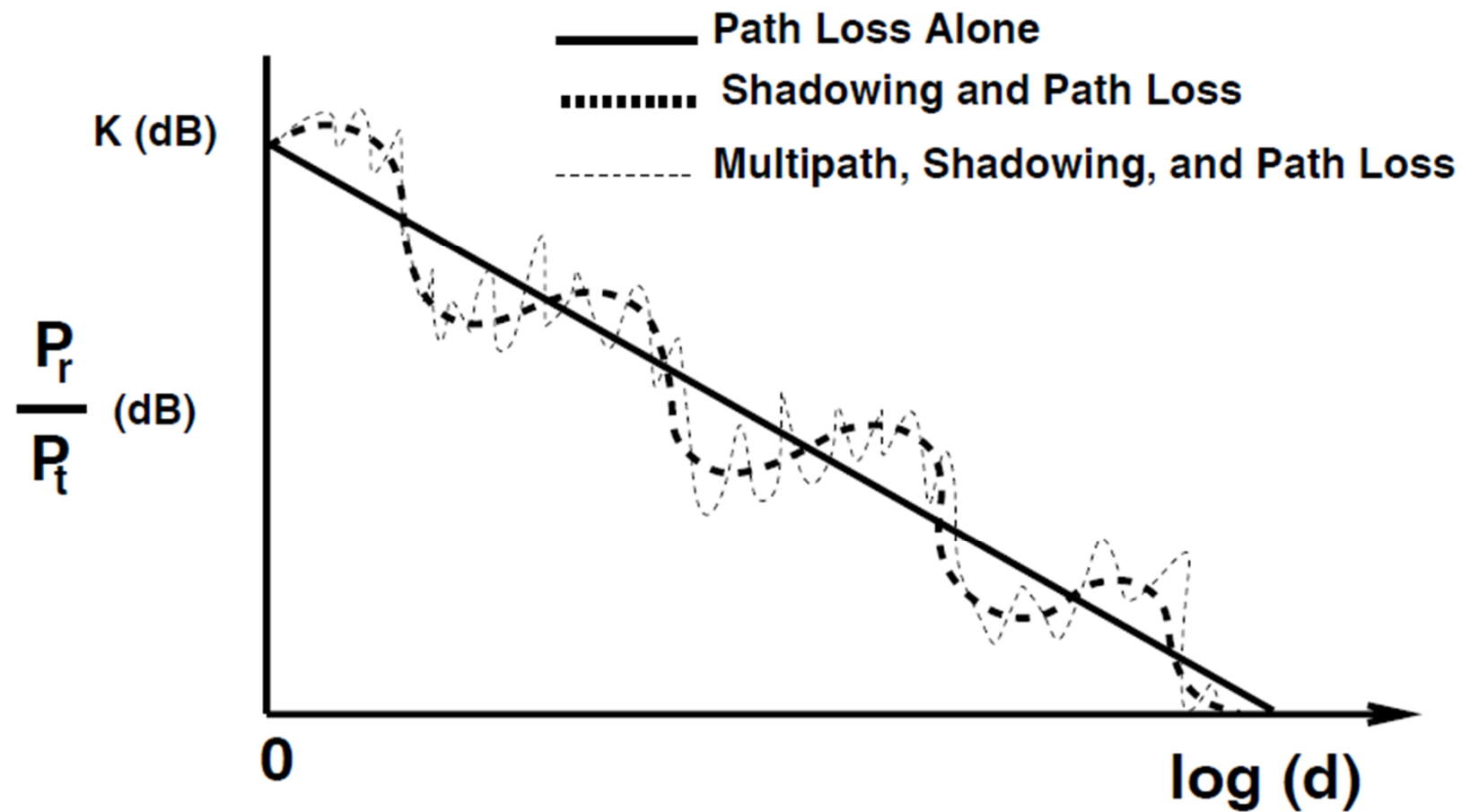
$$s(d) = \exp(-\alpha d)$$

- $\alpha$ : Attenuation factor which depends on the material
- **If  $\alpha$  is approximately the same for all blocking objects:**

$$s(d_t) = \exp\left(-\alpha \sum_i d_i\right) = \exp(-\alpha d_t)$$

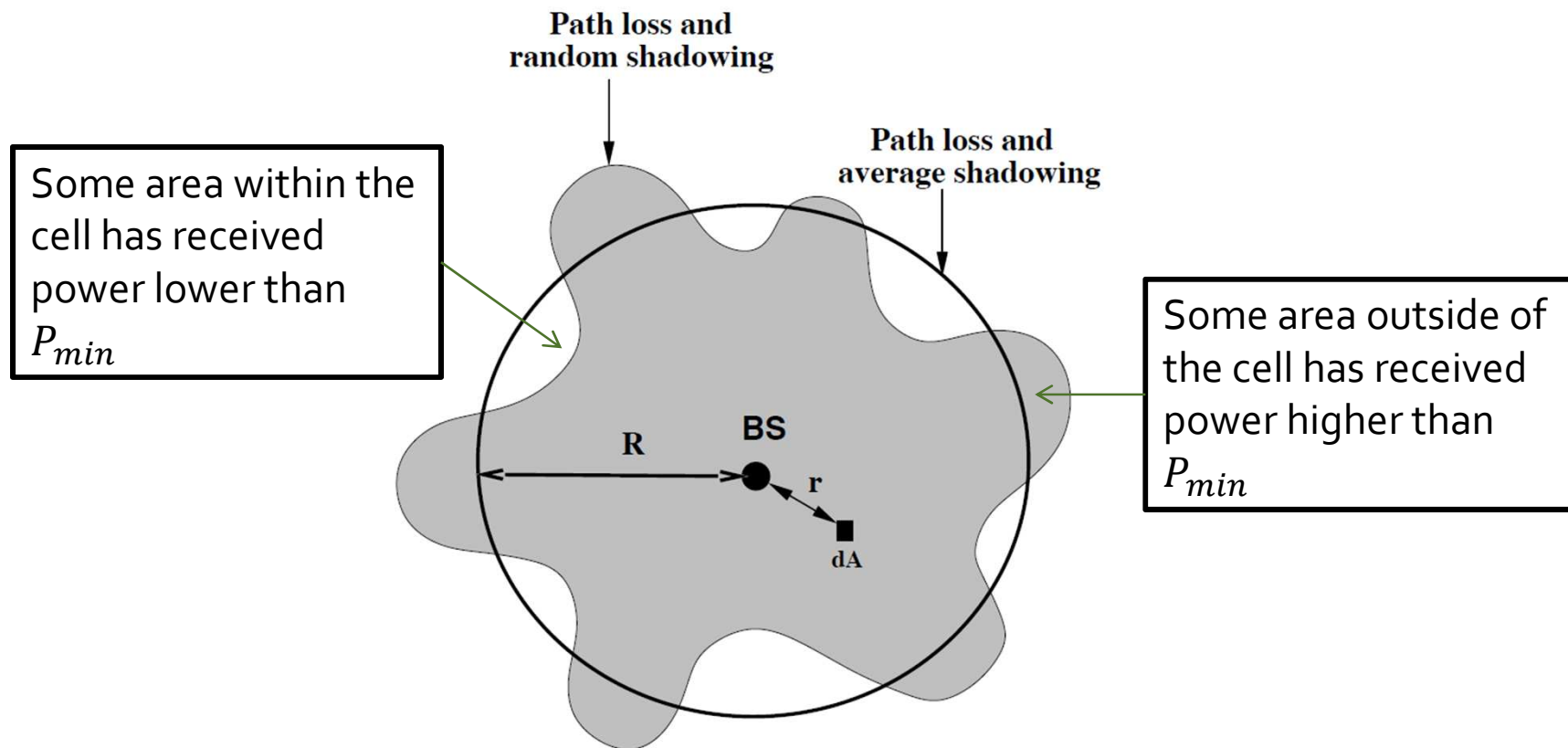
- $d_t = \sum_i d_i$ : sum of all object depths
- **By central limit theorem,  $d_t \sim N(\mu, \sigma^2)$  when the number of object is large (which is true).**

# Path Loss, Shadowing, and Multi-Path



# Cell Coverage Area

- Cell coverage area: expected percentage of locations within a cell where the received power at these locations is above a given minimum.



# Cell Coverage Area

- **We can boost the transmission power at the BS**
  - Extra interference to the neighbor cells
- **In fact, any mobile in the cell has a nonzero probability of having its received power below  $P_{min}$ .**
  - Since Normal distribution has infinite tails
  - Make sense in the real-world:  
in a tunnel, blocked by large buildings, doesn't matter if it is very close to the BS



# Cell Coverage Area

- Cell coverage area is given by  $\mathbf{1}$  if the statement is true, 0 otherwise.  
(indicator function)

$$\begin{aligned} C &= E \left[ \frac{1}{\pi R^2} \int_{\text{cell area}} \overbrace{\mathbf{1}[P_r(r) > P_{min} \text{ in } dA]} dA \right] \\ &= \frac{1}{\pi R^2} \int_{\text{cell area}} E[\mathbf{1}[P_r(r) > P_{min} \text{ in } dA]] dA \end{aligned}$$

- $P_A \doteq p(P_r(r) > P_{min})$

$$C = \frac{1}{\pi R^2} \int_{\text{cell area}} P_A dA = \frac{1}{\pi R^2} \int_0^{2\pi} \int_0^R P_A r dr d\theta$$

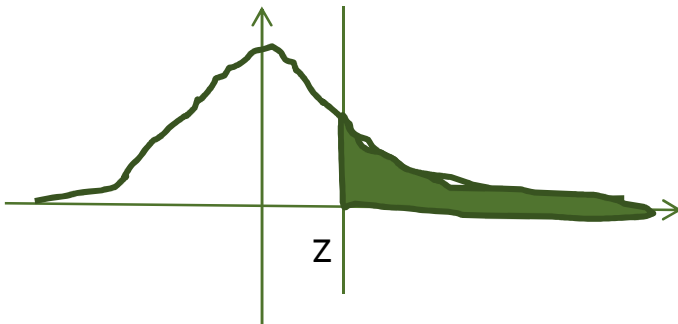
# Cell Coverage Area

$$P_A = p(\bar{P}_r(r) \geq P_{min}) = Q\left(\frac{P_{min} - (P_t - \bar{P}_L(r))}{\sigma}\right)$$

Log-normal distribution's standard deviation

- **Q-function:**

$$Q(z) \doteq p(X > z) = \int_z^{\infty} \frac{1}{\sqrt{2\pi}} \exp\left(-\frac{y^2}{2}\right) dy$$



# Cell Coverage Area

- Solving the equations yield:

$$C = Q(a) + \exp\left[\frac{2 - 2ab}{b^2}\right] Q\left(\frac{2 - ab}{b}\right)$$

- $a = \frac{P_{min} - \overline{P_r}(R)}{\sigma}$ ,  $b = \frac{10\gamma \log_{10}(e)}{\sigma}$

average received power at cell boundary (distance=R)

- If  $P_{min} = \overline{P_r}(R)$

$$C = \frac{1}{2} + \exp\left[\frac{2}{b^2}\right] Q\left(\frac{2}{b}\right)$$

$$C = Q(a) + \exp\left[\frac{2 - 2ab}{b^2}\right] Q\left(\frac{2 - ab}{b}\right)$$

## Example

$$a = \frac{P_{min} - \overline{P_r}(R)}{\sigma}, b = \frac{10\gamma \log_{10}(e)}{\sigma}$$

- Find the coverage area for a cell with
  - a cell radius of 600m
  - a base station transmission power of 20 dBm
  - a minimum received power requirement of -110 dBm.
  - path loss model:  $P_r(d) = P_t K \left(\frac{d_0}{d}\right)^\gamma$ ,  $\gamma = 3.71$ ,  $K = -31.54$  dB,  $d_0 = 1$ , shadowing standard deviation  $\sigma = 3.65$  dB
- Ans:
- $\overline{P_r}(R) = 20 - 31.54 - 10 \times 3.71 \times \log_{10}(600) = -114.6$  dBm
- $a = \frac{-110 + 114.6}{3.65} = 1.26$ ,  $b = \frac{10 \times 3.71 \times 0.434}{3.65} = 4.41$
- $C = Q(1.26) + \exp(-0.46)Q(-0.807) = 0.6$  (not good)
- If we calculate C for a minimum received power requirement of -120 dBm
  - C=0.988!

# Example: road corners path loss

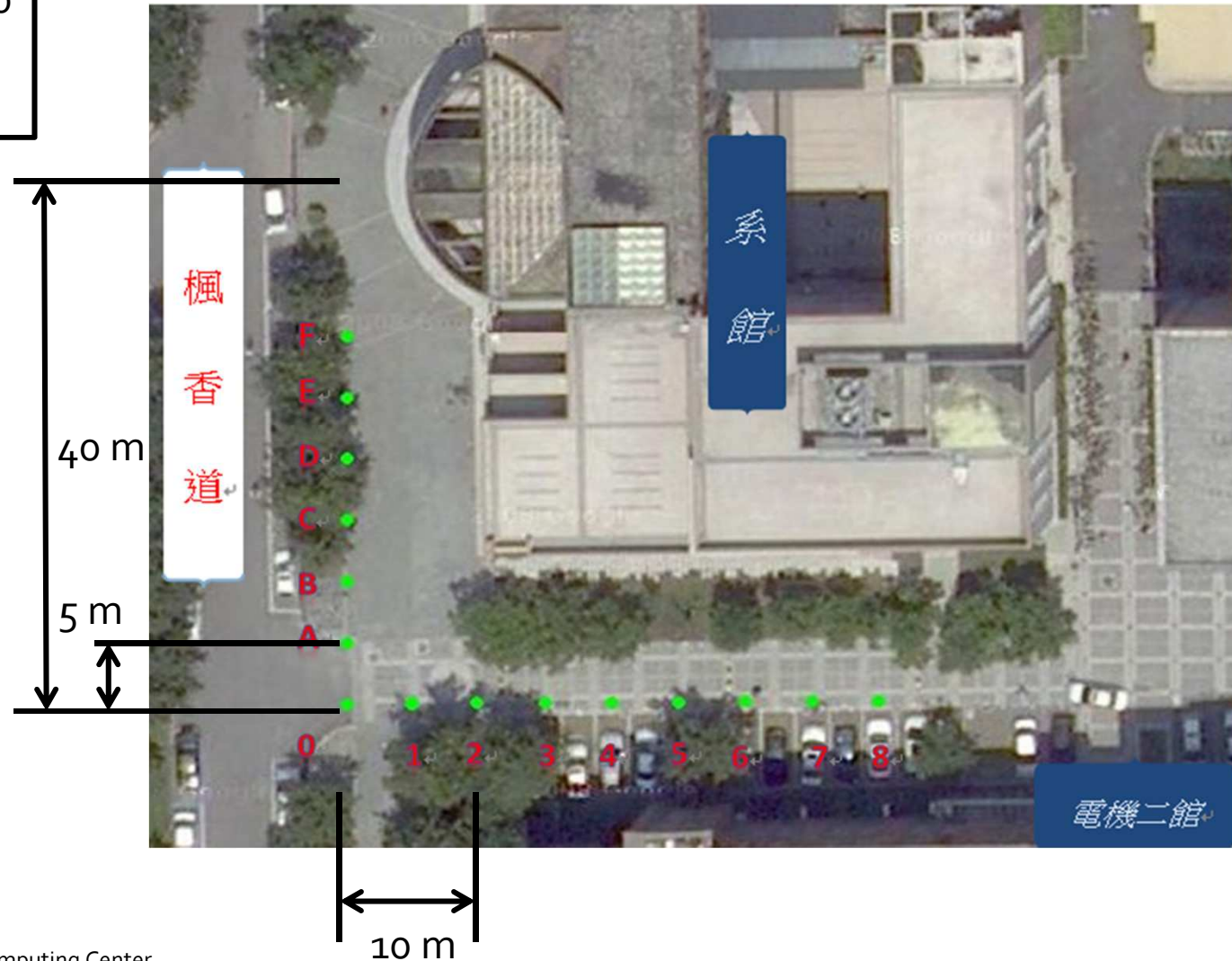
Radio: Chipcon CC2420  
IEEE 802.15.4, 2.4 GHz  
TX pwr: 0 dBm



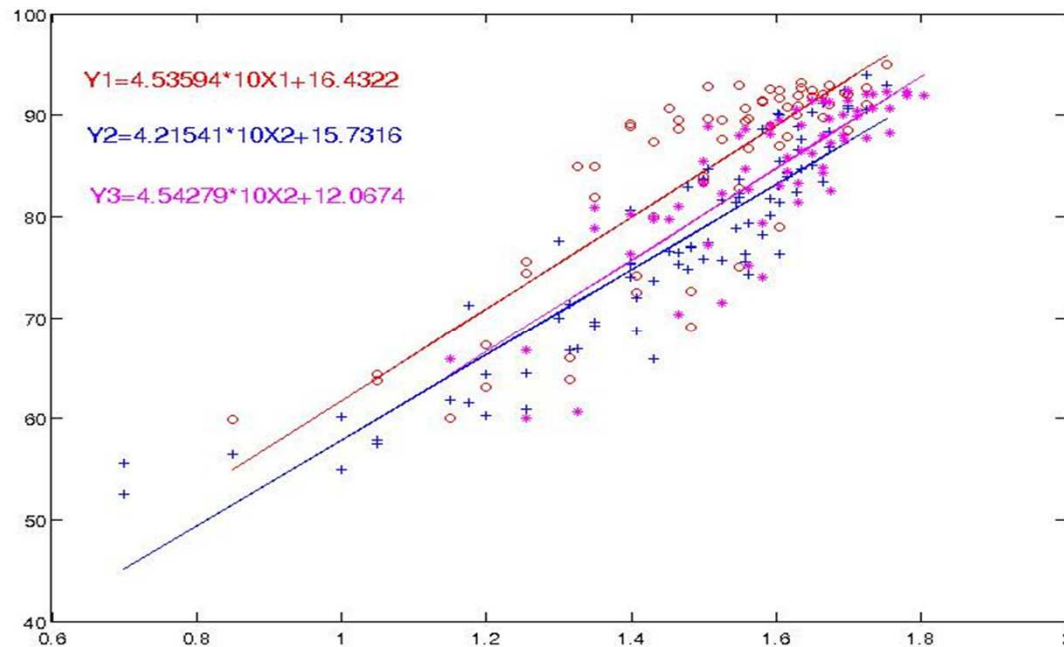
8 dBi peak gain  
omni-directional  
antenna



Intel-NTU Connected Context Computing Center

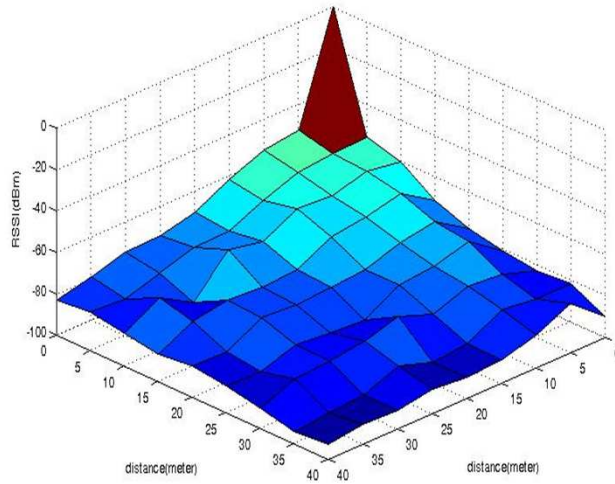


# Link Measurements – Path loss around the corner building

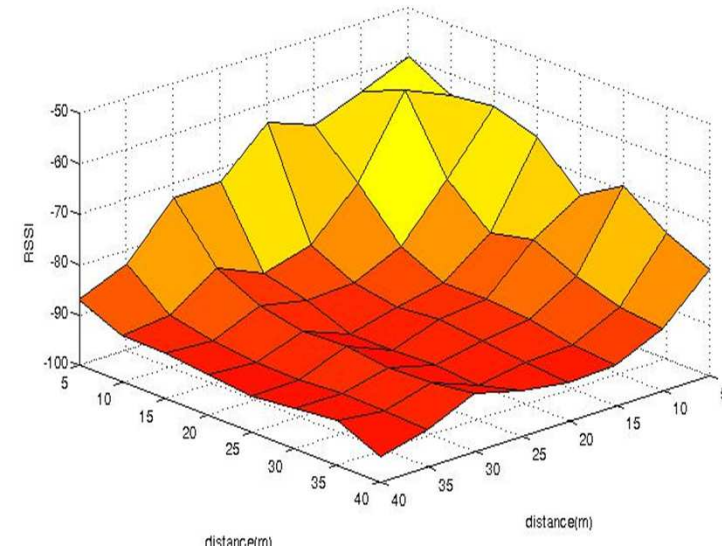


- Compare the path-loss exponent of three different locations:
  1. Corner of NTU\_CSIE building
  2. XinHai-Keelong intersection
  3. FuXing-HePing intersection

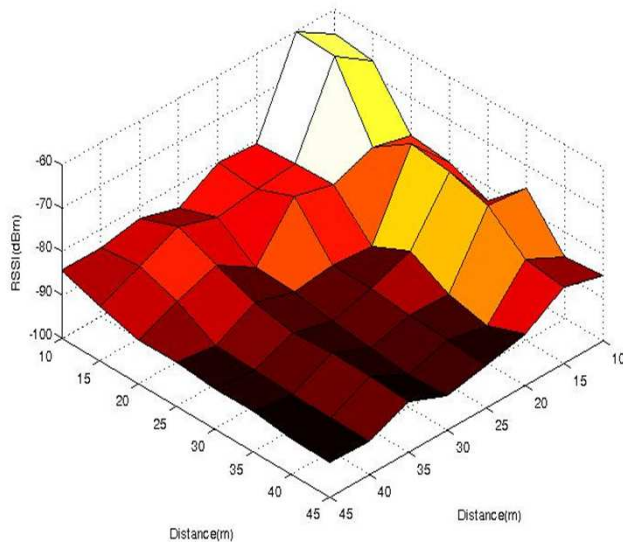
1



2

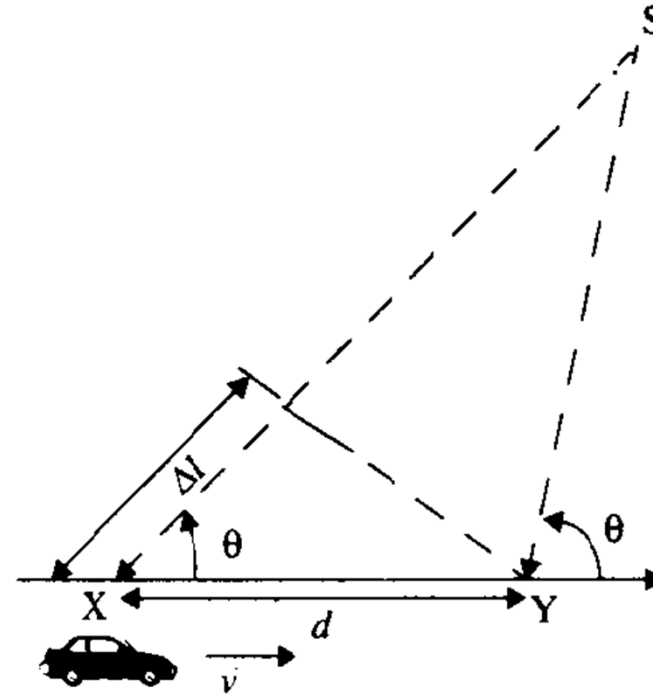


3



	1	2	3
Passing-by vehicles	Occasionally	Frequently	Frequently
Buildings Around	No	Few buildings	Some high buildings
Intersection	Narrow	Wide	Wide

# Doppler Effect



- Difference in path lengths  $\Delta l = d \cos \theta = v \Delta t \cos \theta$
- Phase change  $\Delta \phi = \frac{2\pi \Delta l}{\lambda} = \frac{2\pi v \Delta t}{\lambda} \cos \theta$
- Frequency change, or Doppler shift,

$$f_d = \frac{1}{2\pi} \frac{\Delta \phi}{\Delta t} = \frac{v}{\lambda} \cos \theta$$



# Example

$$f_d = \frac{1}{2\pi} \frac{\Delta\phi}{\Delta t} = \frac{v}{\lambda} \cos\theta$$

- Consider a transmitter which radiates a sinusoidal carrier frequency of 1850 MHz. For a vehicle moving 60 mph, compute the received carrier frequency if the mobile is moving
  1. directly toward the transmitter.
  2. directly away from the transmitter
  3. in a direction which is perpendicular to the direction of arrival of the transmitted signal.
- **Ans:**
  - Wavelength  $\lambda = \frac{c}{f_c} = \frac{3 \times 10^8}{1850 \times 10^6} = 0.162 \text{ (m)}$
  - Vehicle speed  $v = 60 \text{ mph} = 26.82 \left( \frac{\text{m}}{\text{s}} \right)$ 
    1.  $f_d = \frac{26.82}{0.162} \cos(0) = 160 \text{ (Hz)}$
    2.  $f_d = \frac{26.82}{0.162} \cos(\pi) = -160 \text{ (Hz)}$
    3. Since  $\cos\left(\frac{\pi}{2}\right) = 0$ , there is no Doppler shift!

# Doppler Effect

- If the car (mobile) is moving toward the direction of the arriving wave, the Doppler shift is positive
- Different Doppler shifts if different  $\theta$  (incoming angle)
- Multi-path: all different angles
- Many Doppler shifts  $\rightarrow$  Doppler spread