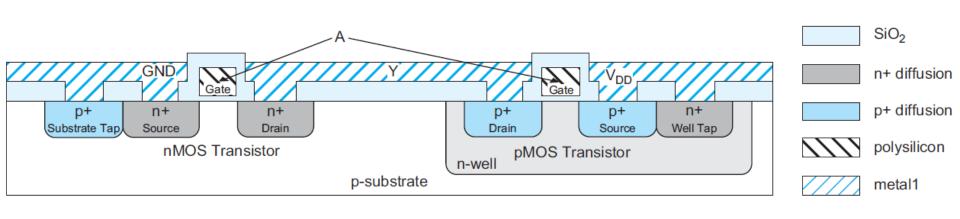
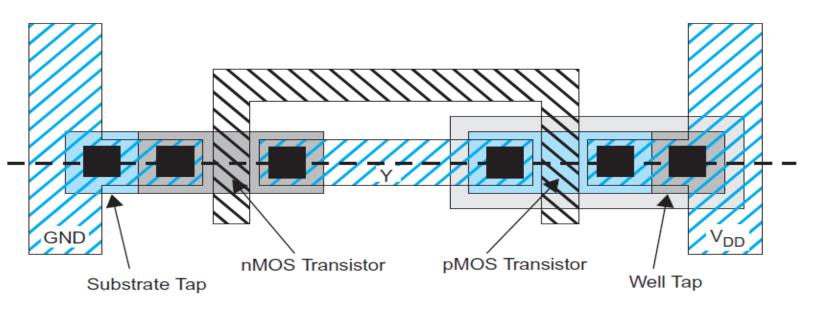
# EE223 Analog Integrated Circuits Fall 2018

Lecture 4: MOS Small Signal Model

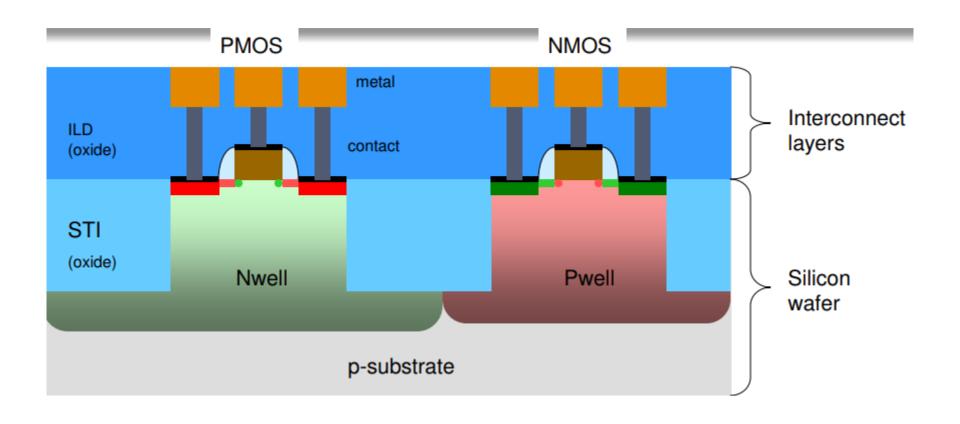
Prof. Sang-Soo Lee sang-soo.lee@sjsu.edu ENG-259

## **Cross-sectional and Top Views**

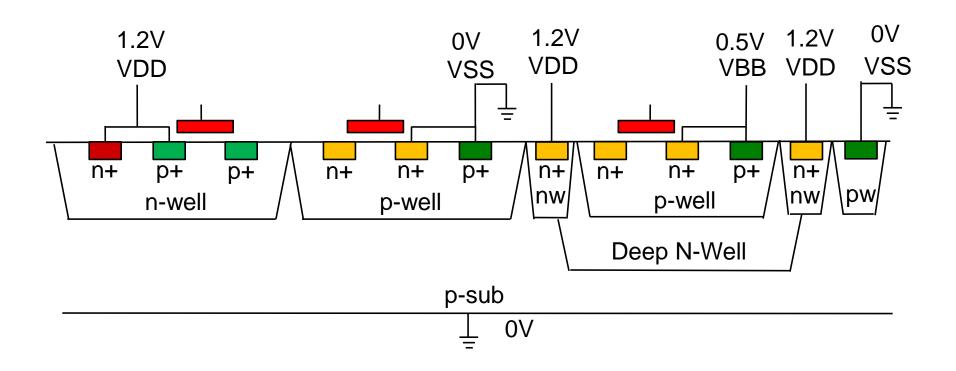




#### **CMOS Cross-section**

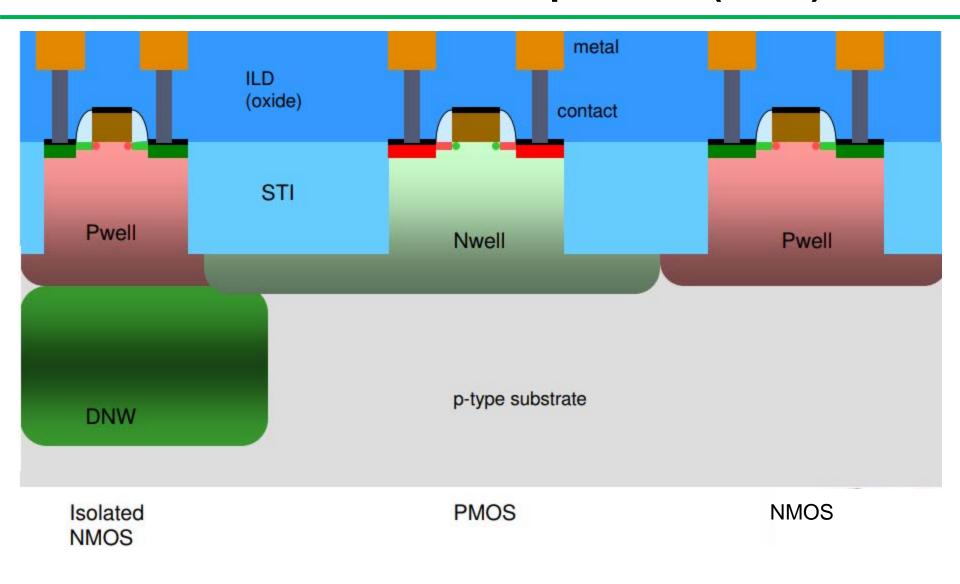


### **Cross-section with Deep N-Well (DNW)**

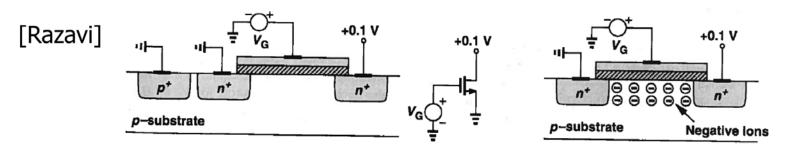


All pn junctions must be reverse-biased at all times.

## **Cross-section with Deep N-Well (DNW)**



## Threshold Voltage, V<sub>T</sub>

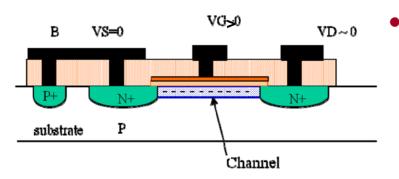


 Applying a positive voltage to the gate repels holes in the p-substrate under the gate, leaving negative ions (depletion region) to mirror the gate charge



- Before a "channel" forms, the device acts as 2 series caps from the oxide cap and the depletion cap
- If V<sub>G</sub> is increased to a sufficient value the area below the gate is "inverted" and electrons flow from source to drain

## Threshold Voltage, V<sub>T</sub>



$$V_{TH} = \Phi_{MS} + 2\Phi_F + \frac{Q_{dep}}{C_{ox}}$$

- The threshold voltage, V<sub>T</sub>, is the voltage at which an "inversion layer" is formed
  - For an NMOS this is when the concentration of electrons equals the concentration of holes in the p<sup>-</sup> substrate

 $\Phi_{MS}$  is the difference between the work functions of the polysilicon gate and the silicon substrate

$$\Phi_F$$
 is the Fermi potential,  $\Phi_F = \frac{kT}{q} \ln \left( \frac{N_{sub}}{n_i} \right)$ 

$$Q_{dep}$$
 is the depletion region charge,  $Q_{dep} = \sqrt{4q\varepsilon_{si}|\Phi_F|N_{sub}}$ 

$$C_{ox}$$
 is the gate cap/area,  $C_{ox} = \frac{\mathcal{E}_{ox}}{t_{ox}}$ 

## NMOS with $Vgs > V_T$ , $Vds < Vgs-V_T$

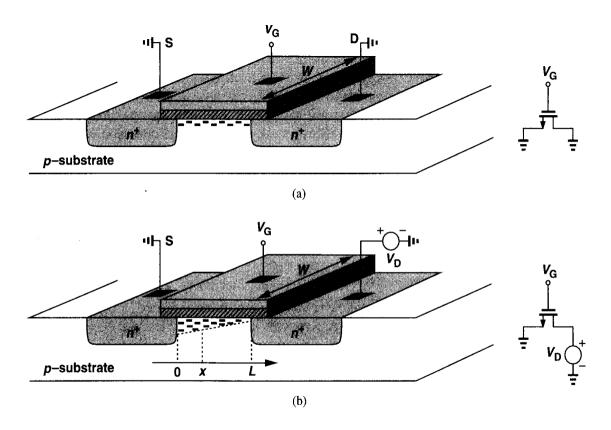
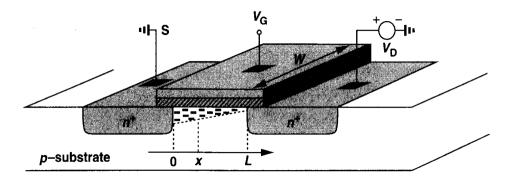


Figure 2.10 Channel charge with (a) equal source and drain voltages, (b) unequal source and drain voltages.

## NMOS with $Vgs > V_T$ , $Vds < Vgs-V_T$



$$I = Q_{d} \cdot v.$$

$$Q_{d} = WC_{ox}(V_{GS} - V_{TH})$$

$$Q_{d}(x) = WC_{ox}[V_{GS} - V(x) - V_{TH}]$$

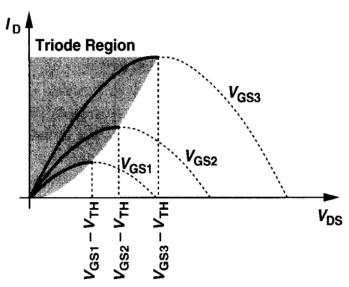
$$I_{D} = -WC_{ox}[V_{GS} - V(x) - V_{TH}]v$$

$$I_{D} = WC_{ox}[V_{GS} - V(x) - V_{TH}]\mu_{n}\frac{dV(x)}{dx}$$

$$\int_{x=0}^{L} I_{D}dx = \int_{V=0}^{V_{DS}} WC_{ox}\mu_{n}[V_{GS} - V(x) - V_{TH}]dV.$$

$$I_D = \mu_n C_{ox} \frac{W}{L} \left[ (V_{GS} - V_{TH}) V_{DS} - \frac{1}{2} V_{DS}^2 \right]$$

## **NMOS** in Triode Region



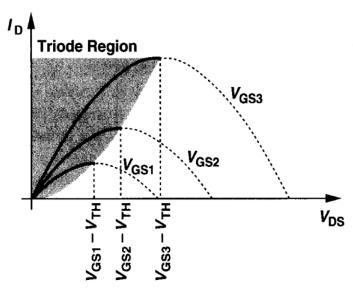
$$I_D = \mu_n C_{ox} \frac{W}{L} \left[ (V_{GS} - V_{TH}) V_{DS} - \frac{1}{2} V_{DS}^2 \right]$$

If  $V_{DS}$  is small,

$$I_D = \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH}) V_{DS}$$

**Figure 2.11** Drain current versus drain-source voltage in the triode region.

## **NMOS** in Triode Region



$$I_D = \mu_n C_{ox} \frac{W}{L} \left[ (V_{GS} - V_{TH}) V_{DS} - \frac{1}{2} V_{DS}^2 \right]$$

If  $V_{DS}$  is small,

$$I_D = \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH}) V_{DS}$$

**Figure 2.11** Drain current versus drain-source voltage in the triode region.

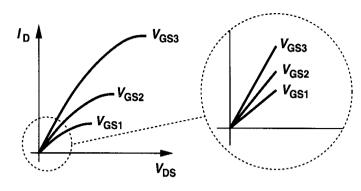
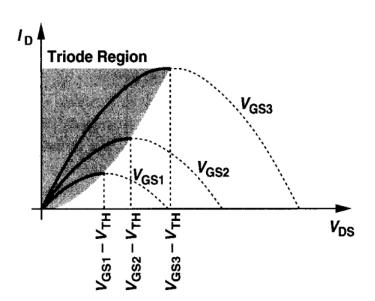


Figure 2.12 Linear operation in deep triode region.

$$R_{on} = \frac{1}{\mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})}$$

### **Peak Current in Triode Region**



$$I_D = \mu_n C_{ox} \frac{W}{L} \left[ (V_{GS} - V_{TH}) V_{DS} - \frac{1}{2} V_{DS}^2 \right]$$

$$\frac{\partial I_D}{\partial V_{DS}} = \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH} - V_{DS})$$

$$I_D$$
 peaks at  $V_{DS} = (V_{GS} - V_{TH})$ 

**Figure 2.11** Drain current versus drain-source voltage in the triode region.

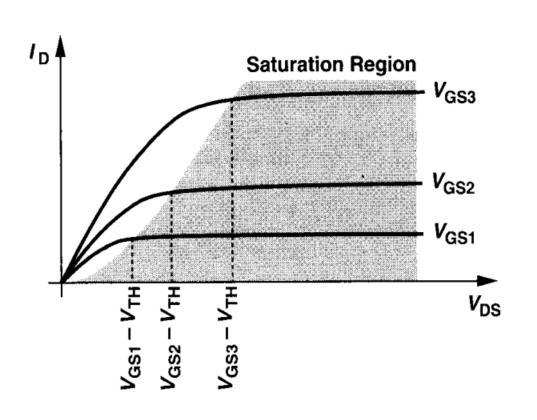
#### What is the peak current?

$$I_{D,max} = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2$$

### **NMOS** in Saturation Region

$$I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2$$





$$k'_n = \mu_n C_{ox}$$

$$V_{Dsat} = V_{GS} - V_{TH}$$

#### **NMOS Current Source**

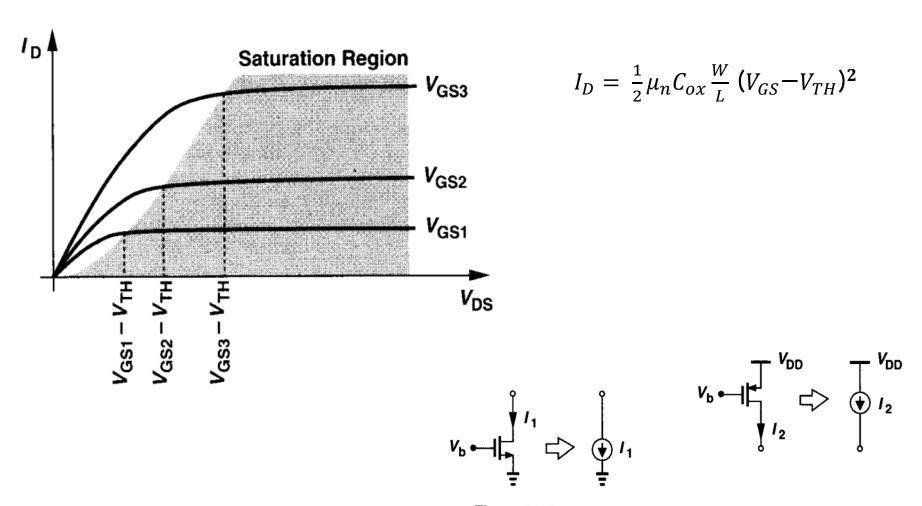
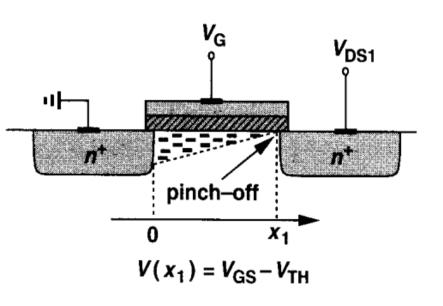
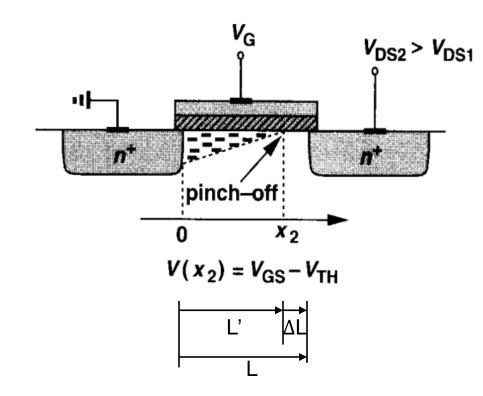


Figure 2.17 Saturated MOSFETs operating as current sources.

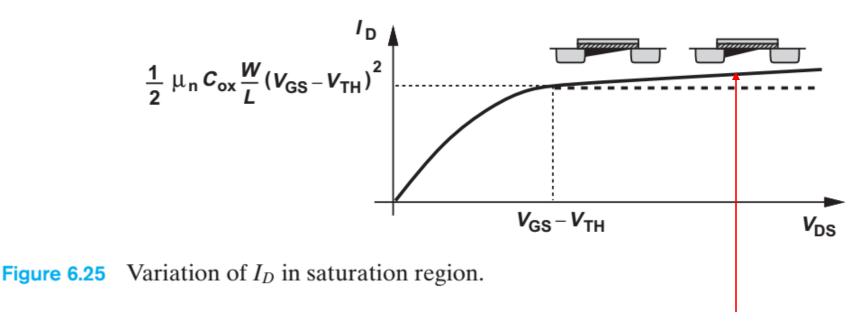
#### **Channel Pinch-off**





$$I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L'} (V_{GS} - V_{TH})^2$$
, where  $L' = L - \Delta L$ 

### **Channel Length Modulation**



#### Slope represents 1/r<sub>o</sub>

$$I_D = \frac{1}{2}\mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2 (1 + \lambda V_{DS}) \qquad r_O = \frac{\Delta V_{DS}}{\Delta I_D}$$

## Channel Length Modulation Coefficient ( $\lambda$ )

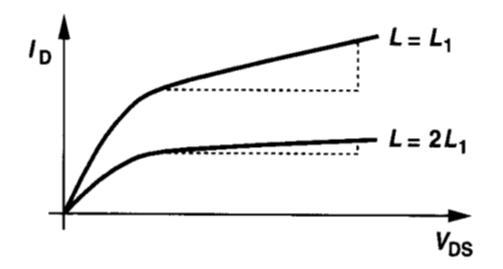
$$r_O = rac{\Delta v_{DS}}{\Delta I_D}$$
 Longer channel length has smaller  $\lambda$ 

Figure 6.26 Channel-length modulation.

$$I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2 (1 + \lambda V_{DS})$$

## **Effect of Channel Length Modulation**

$$I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2 (1 + \lambda V_{DS})$$



Effect of doubling channel length.

Good current source requires Longer channel length.

## **Effect of Channel Length Modulation**

$$I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2 (1 + \lambda V_{DS})$$

$$\frac{\Delta I_D}{\Delta V_{DS}} = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2 \lambda \approx \lambda I_D$$

$$r_o = \frac{\Delta V_{DS}}{\Delta I_D} = \frac{1}{\lambda I_D}$$
  $\lambda \propto \frac{1}{L}$   $A_v = g_m r_o$ 

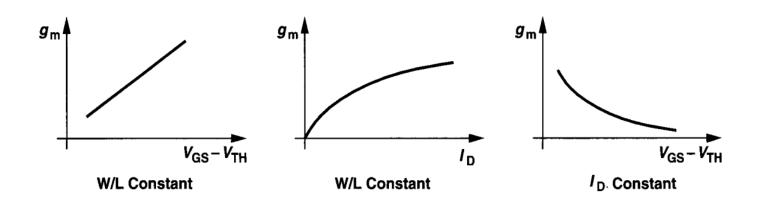
$$L \uparrow \lambda \downarrow r_o \uparrow A_v \uparrow$$

For higher amplifier gain, use Longer channel length.

#### **MOS Transconductance in Saturation**

$$I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2$$

$$g_m = \frac{\partial I_D}{\partial V_{GS}} \Big|_{VDS, \text{const.}} = \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})$$
$$= \sqrt{2\mu_n C_{ox} \frac{W}{L} I_D} = \frac{2I_D}{V_{GS} - V_{TH}}$$



#### **MOS Transconductance in Triode**

#### **Saturation**

$$I_D = \frac{1}{2}\mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2$$

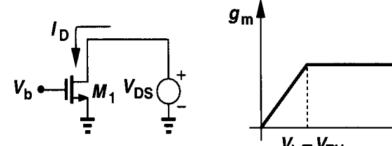
$$g_{m} = \frac{\partial I_{D}}{\partial V_{GS}} \Big|_{VDS, \text{const.}}$$

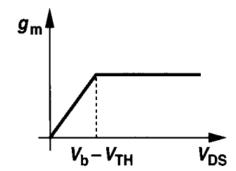
$$= \mu_{n} C_{ox} \frac{W}{L} (V_{GS} - V_{TH})$$

#### **Triode**

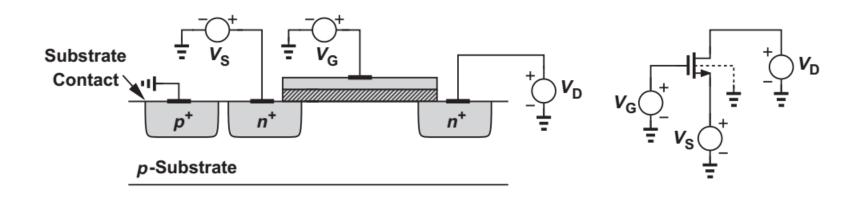
$$I_D = \mu_n C_{ox} \frac{W}{L} \left[ (V_{GS} - V_{TH}) V_{DS} - \frac{1}{2} V_{DS}^2 \right]$$

$$g_{m} = \frac{\partial}{\partial V_{GS}} \left\{ \frac{1}{2} \mu_{n} C_{ox} \frac{W}{L} \left[ 2(V_{GS} - V_{TH}) V_{DS} - V_{DS}^{2} \right] \right\}$$
$$= \mu_{n} C_{ox} \frac{W}{L} V_{DS}.$$





## **Body Effect**



$$V_{\scriptscriptstyle T} = V_{\scriptscriptstyle T0} + \gamma \Big( \sqrt{\left| 2\Phi_{\scriptscriptstyle F} + V_{\scriptscriptstyle SB} \right|} - \sqrt{\left| 2\Phi_{\scriptscriptstyle F} \right|} \Big)$$

Body effect coefficient, 
$$\gamma = \frac{\sqrt{2q\varepsilon_{si}N_{sub}}}{C_{ox}}$$

 $\gamma$  typically ranges from 0.3 to 0.4V<sup>1/2</sup>

## Body (or Bulk) Transconductance, g<sub>mb</sub>

The small-signal drain current changes with  $V_{\text{BS}}$  modulation due to changes in  $V_{\text{T}}$ 

$$I_{D} = \frac{1}{2}\mu_{n}C_{ox}\frac{W}{L'}(V_{GS} - V_{TH})^{2}$$

$$V_{TH} = V_{TH0} + \gamma \left(\sqrt{|2\Phi_{F} + V_{SB}|} - \sqrt{|2\Phi_{F}|}\right)$$

$$g_{mb} = \frac{\partial I_{D}}{\partial V_{BS}} = \mu_{n}C_{ox}\frac{W}{L}(V_{GS} - V_{TH})\left(-\frac{\partial V_{TH}}{\partial V_{BS}}\right)$$

$$\frac{\partial V_{TH}}{\partial V_{BS}} = -\frac{\partial V_{TH}}{\partial V_{SB}} = -\frac{\gamma}{2}(2\Phi_{F} + V_{SB})^{-1/2}$$

$$g_{mb} = g_{m}\frac{\gamma}{2\sqrt{2\Phi_{F} + V_{SB}}} = \eta g_{m}$$