

# MPC-QP Controller for CL686 Expermental Project

## 1 Control Relevant Perturbation Model and Kalman Predictor Design

Consider the discrete time linear model obtained through linearization of the mechanistic model in the neighborhood of  $(\mathcal{X}_s, \mathcal{U}_s, \mathcal{D}_s)$

$$\mathbf{x}(k+1) = \mathbf{\Phi}\mathbf{x}(k) + \mathbf{\Gamma}_u \mathbf{u}(k) + \mathbf{\Gamma}_d \mathbf{d}(k) \quad (1)$$

$$\mathbf{y}(k) = \mathbf{C}\mathbf{x}(k) + \mathbf{D} \begin{bmatrix} \mathbf{u}(k) \\ \mathbf{d}(k) \end{bmatrix} + \mathbf{v}(k) \quad (2)$$

$$\mathbf{x}(k) = \mathcal{X}(k) - \mathcal{X}_s, \mathbf{u}(k) = \mathcal{U}(k) - \mathcal{U}_s, \quad (3)$$

$$\mathbf{d} = \mathcal{D}(k) - \mathcal{D}_s, \mathbf{y}(k) = \mathcal{Y}(k) - \mathbf{C}\mathcal{X}_s \quad (4)$$

where  $\mathbf{d}(k)$  and  $\mathbf{v}(k)$  are a zero mean Gaussian white noise sequences with covariance matrices  $\mathbf{Q}_d$  and  $\mathbf{R}$ , respectively. Here,  $\mathbf{D}$  is a **null matrix** of dimension  $r \times (m + d)$ . Also, define covariance matrix

$$\mathbf{N} = E [\mathbf{d}(k)\mathbf{v}(k)^T] = [\mathbf{0}]_{d \times r}$$

which is a null matrix since disturbance  $\mathbf{d}(k)$  and measurement noise  $\mathbf{v}(k)$  are uncorrelated.

This model can be used to develop Kalman predictor of the form

$$\mathbf{y}(k) = \mathcal{Y}(k) - \mathcal{Y}_s \quad (5)$$

$$\mathbf{e}(k) = \mathbf{y}(k) - \mathbf{C}\hat{\mathbf{x}}(k) \quad (6)$$

$$\hat{\mathbf{x}}(k+1) = \mathbf{\Phi}\hat{\mathbf{x}}(k) + \mathbf{\Gamma}_u \mathbf{u}(k) + \mathbf{L}_p \mathbf{e}(k) \quad (7)$$

where the steady state Kalman gain is obtained by solving the algebraic Riccati equation (ARE)

$$\mathbf{L}_p = [\mathbf{\Phi}\mathbf{P}_\infty \mathbf{C}^T + \mathbf{N}] [\mathbf{C}\mathbf{P}_\infty \mathbf{C}^T + \mathbf{R}]^{-1} \quad (8)$$

$$\mathbf{P}_\infty = \mathbf{\Phi}\mathbf{P}_\infty \mathbf{\Phi}^T + \mathbf{\Gamma}_d \mathbf{Q}_d \mathbf{\Gamma}_d^T - \mathbf{L}_p [\mathbf{C}\mathbf{P}_\infty \mathbf{C}^T + \mathbf{R}] \mathbf{L}_p^T \quad (9)$$

Solution of the ARE can be found using Matlab Control System Toolbox function *kalman* as follows

1. Step 1: Create a state space object using ss command

$$dmod = ss(\mathbf{\Phi}, \begin{bmatrix} \mathbf{\Gamma}_u & \mathbf{\Gamma}_d \end{bmatrix}, \mathbf{C}, \mathbf{D}, T)$$

where  $T$  represents sampling interval.

2. Call Matlab function *kalman*

$$[KEST, \mathbf{L}_p, \mathbf{P}_\infty] = kalman(dmod, \mathbf{Q}_d, \mathbf{R}, \mathbf{N});$$

Use the Kalman predictor for MPC implementation. For the purpose of innovation bias based MPC implementation, the filtered innovation sequence is computed as follows

$$\mathbf{e}_f(k) = \mathbf{\Phi}_e \mathbf{e}_f(k-1) + [\mathbf{I} - \mathbf{\Phi}_e] \mathbf{e}(k) \quad (10)$$

$$\mathbf{\Phi}_e = \alpha \mathbf{I}_{r \times r} \quad (11)$$

$0 \leq \alpha < 1$  is tuning parameter

The innovation signal,  $\mathbf{e}(k)$ , is computed using eq. (5). Further, the target steady state  $\mathbf{x}_s(k)$  and target input  $\mathbf{u}_s(k)$  are computed as follows

$$\mathbf{u}_s(k) = \mathbf{K}_u^{-1} [\mathbf{r}(k) - \mathbf{K}_e \mathbf{e}_f(k)] \quad (12)$$

$$\mathbf{x}_s(k) = (\mathbf{I} - \mathbf{\Phi})^{-1} [\mathbf{\Gamma}_u \mathbf{u}_s(k) + \mathbf{L}_p \mathbf{e}_f(k)] \quad (13)$$

$$\mathbf{K}_u = \mathbf{C} (\mathbf{I} - \mathbf{\Phi})^{-1} \mathbf{\Gamma}_u \quad ; \quad \mathbf{K}_e = \mathbf{C} (\mathbf{I} - \mathbf{\Phi})^{-1} \mathbf{L}_p + \mathbf{I} \quad (14)$$

where  $\mathbf{r}(k)$  denotes desired setpoint at instant  $k$ .

## 2 Model Identified from Data

Alternatively, you may have innovation form of state space model of the form

$$\mathbf{x}(k+1) = \mathbf{\Phi} \mathbf{x}(k) + \mathbf{\Gamma}_u \mathbf{u}(k) + \mathbf{L}_p \mathbf{e}(k)$$

identified directly from input-output data.

$$\mathbf{y}(k) = \mathcal{Y}(k) - \mathcal{Y}_s \quad (15)$$

$$\mathbf{e}(k) = \mathbf{y}(k) - \mathbf{C} \hat{\mathbf{x}}(k) \quad (16)$$

$$\hat{\mathbf{x}}(k+1) = \mathbf{\Phi} \hat{\mathbf{x}}(k) + \mathbf{\Gamma}_u \mathbf{u}(k) + \mathbf{L}_p \mathbf{e}(k) \quad (17)$$

For the purpose of innovation bias based MPC implementation, the filtered innovation sequence is computed as follows

$$\mathbf{e}_f(k) = \mathbf{\Phi}_e \mathbf{e}_f(k-1) + [\mathbf{I} - \mathbf{\Phi}_e] \mathbf{e}(k) \quad (18)$$

$$\mathbf{\Phi}_e = \alpha \mathbf{I}_{r \times r} \quad (19)$$

$0 \leq \alpha < 1$  is tuning parameter

The innovation signal,  $\mathbf{e}(k)$ , is computed using eq. (5). Further, the target steady state  $\mathbf{x}_s(k)$  and target input  $\mathbf{u}_s(k)$  are computed as follows

$$\mathbf{u}_s(k) = \mathbf{K}_u^{-1} [\mathbf{r}(k) - \mathbf{K}_e \mathbf{e}_f(k)] \quad (20)$$

$$\mathbf{x}_s(k) = (\mathbf{I} - \mathbf{\Phi})^{-1} [\mathbf{\Gamma}_u \mathbf{u}_s(k) + \mathbf{L}_p \mathbf{e}_f(k)] \quad (21)$$

$$\mathbf{K}_u = \mathbf{C} (\mathbf{I} - \mathbf{\Phi})^{-1} \mathbf{\Gamma}_u \quad ; \quad \mathbf{K}_e = \mathbf{C} (\mathbf{I} - \mathbf{\Phi})^{-1} \mathbf{L}_p + \mathbf{I} \quad (22)$$

where  $\mathbf{r}(k)$  denotes desired setpoint at instant  $k$ .

## 3 MPC QP Formulation

The model predictive control problem at the sampling instant  $k$  is defined as a constrained optimization problem whereby the future manipulated input moves

$$\mathcal{U}_f = \{\mathbf{u}(k+j|k) : j = 0, 1, \dots, q-1\}$$

are determined by minimizing a cost function defined over prediction horizon  $p$ . Here,  $q$  is known as the control horizon. Note that use of control horizon  $q < p$  implies inclusion of the following constraints on the future manipulated inputs

$$\mathbf{u}(k+q|k) = \mathbf{u}(k+q+1|k) = \dots = \mathbf{u}(k+p-1|k) = \mathbf{u}(k+q-1|k) \quad (23)$$

Let  $\mathbf{w}_x, \mathbf{w}_u$  represent +ve definite matrices. As part the course project, you are expected to implement the following MPC algorithm

$$\arg \min_{\mathcal{U}_f} J = \sum_{j=1}^p \boldsymbol{\varepsilon}(k+j|k)^T \mathbf{w}_x \boldsymbol{\varepsilon}(k+j|k) + \sum_{j=0}^{q-1} \delta \mathbf{u}(k+j|k)^T \mathbf{w}_u \delta \mathbf{u}(k+j|k) \quad (24)$$

$$\begin{aligned} \boldsymbol{\varepsilon}(k+j|k) &= \hat{\mathbf{z}}(k+j) - \mathbf{x}_s(k) \text{ for } j = 1, 2, \dots, p \\ \mathbf{x}_s(k) &: \text{ computed using (13)} \end{aligned} \quad (25)$$

$$\begin{aligned} \delta \mathbf{u}(k+j|k) &= \mathbf{u}(k+j|k) - \mathbf{u}_s(k) \text{ for } j = 1, \dots, q-1 \\ \mathbf{u}_s(k) &: \text{ computed using (12)} \end{aligned} \quad (26)$$

Subject to

$$\hat{\mathbf{z}}(k+j+1) = \boldsymbol{\Phi} \hat{\mathbf{z}}(k+j) + \boldsymbol{\Gamma} \mathbf{u}(k+j|k) + \mathbf{L}_p \mathbf{e}_f(k) \quad (27)$$

$$\text{for } j = 1, 2, \dots, p. \text{ with } \hat{\mathbf{z}}(k) = \hat{\mathbf{x}}(k) \quad (28)$$

$$\hat{\mathbf{x}}(k) : \text{ computed using eq. (7)}$$

$$\mathbf{e}_f(k) : \text{ computed using eq. (10)}$$

$$\begin{aligned} \mathbf{u}_L &\leq \mathbf{u}(k+j|k) \leq \mathbf{u}_H \\ j &= 0, 1, 2, \dots, q-1 \end{aligned} \quad (29)$$

Defining vector of future inputs and outputs, as

$$\mathbf{U}_f(k) = \begin{bmatrix} \mathbf{u}(k|k)^T & \mathbf{u}(k+1|k)^T & \dots & \mathbf{u}(k+q-1|k)^T \end{bmatrix}^T \quad (30)$$

$$\hat{\mathbf{Z}}(k) = \begin{bmatrix} \hat{\mathbf{z}}(k+1)^T & \hat{\mathbf{z}}(k+2)^T & \dots & \hat{\mathbf{z}}(k+p)^T \end{bmatrix}^T \quad (31)$$

the model based prediction equations and future prediction error can be expressed as follows

$$\hat{\mathbf{Z}}(k) = \mathbf{S}_x \hat{\mathbf{x}}(k|k-1) + \mathbf{S}_e \hat{\mathbf{e}}_f(k) + \mathbf{S}_u \mathbf{U}_f(k) \quad (32)$$

$$\mathbf{S}_x = \begin{bmatrix} \boldsymbol{\Phi} \\ \boldsymbol{\Phi}^2 \\ \dots \\ \boldsymbol{\Phi}^p \end{bmatrix} ; \quad \mathbf{S}_e = \begin{bmatrix} \mathbf{L} \\ (\boldsymbol{\Phi} + \mathbf{I})\mathbf{L} \\ \dots \\ (\boldsymbol{\Phi}^{p-1} + \boldsymbol{\Phi}^{p-2} + \dots + \mathbf{I})\mathbf{L} \end{bmatrix} ; \quad \mathbf{S}_{xI} = \begin{bmatrix} \mathbf{I}_n \\ \mathbf{I}_n \\ \dots \\ \mathbf{I}_n \end{bmatrix} \quad (33)$$

$$\mathbf{S}_u = \begin{bmatrix} \mathbf{\Gamma}_u & [0] & [0] & \dots & [0] \\ \mathbf{\Phi}\mathbf{\Gamma}_u & \mathbf{\Gamma}_u & [0] & \dots & [0] \\ \dots & \dots & \dots & \dots & [0] \\ \mathbf{\Phi}^{q-1}\mathbf{\Gamma}_u & \mathbf{\Phi}^{q-2}\mathbf{\Gamma}_u & \dots & \dots & \mathbf{\Gamma}_u \\ \mathbf{\Phi}^q\mathbf{\Gamma}_u & \mathbf{\Phi}^{q-1}\mathbf{\Gamma}_u & \dots & \dots & (\mathbf{\Phi} + I)\mathbf{\Gamma}_u \\ \dots & \dots & \dots & \dots & \dots \\ \mathbf{\Phi}^{p-1}\mathbf{\Gamma}_u & \mathbf{\Phi}^{p-2}\mathbf{\Gamma}_u & \dots & \dots & (\mathbf{\Phi}^{p-q} + \dots + I)\mathbf{\Gamma}_u \end{bmatrix}; \quad \mathbf{S}_{uI} = \begin{bmatrix} \mathbf{I}_m \\ \mathbf{I}_m \\ \dots \\ \mathbf{I}_m \end{bmatrix} \quad (34)$$

$$\mathbf{W}_X = \text{block diag} \begin{bmatrix} \mathbf{w}_x & \mathbf{w}_x & \dots & \mathbf{w}_x \end{bmatrix} \quad (35)$$

$$\mathbf{W}_U = \text{block diag} \begin{bmatrix} \mathbf{w}_u & \mathbf{w}_u & \dots & \mathbf{w}_u \end{bmatrix} \quad (36)$$

$$J = \left[ \hat{\mathbf{Z}}(k) - \mathbf{S}_{xI}\mathbf{x}_s(k) \right]^T \mathbf{W}_X \left[ \hat{\mathbf{Z}}(k) - \mathbf{S}_{xI}\mathbf{x}_s(k) \right] + [\mathbf{U}_f(k) - \mathbf{S}_{uI}\mathbf{u}_s(k)]^T \mathbf{W}_U [\mathbf{U}_f(k) - \mathbf{S}_{uI}\mathbf{u}_s(k)]$$

Consider the term

$$\begin{aligned} \hat{\mathbf{Z}}(k) - \mathbf{S}_{xI}\mathbf{x}_s(k) &= \mathbf{S}_x\hat{\mathbf{x}}(k|k-1) + \mathbf{S}_e\hat{\mathbf{e}}_f(k) + \mathbf{S}_u\mathbf{U}_f(k) - \mathbf{S}_{xI}\mathbf{x}_s(k) \\ &= \mathbf{S}_u\mathbf{U}_f(k) + \boldsymbol{\eta}(k) \\ \boldsymbol{\eta}(k) &= \mathbf{S}_x\hat{\mathbf{x}}(k|k-1) + \mathbf{S}_e\hat{\mathbf{e}}_f(k) - \mathbf{S}_{xI}\mathbf{x}_s(k) \end{aligned}$$

The terms that contribute to QP formulation are

$$\begin{aligned} J &= [\mathbf{S}_u\mathbf{U}_f(k) + \boldsymbol{\eta}(k)]^T \mathbf{W}_X [\mathbf{S}_u\mathbf{U}_f(k) + \boldsymbol{\eta}(k)] \\ &\quad + \mathbf{U}_f(k)^T \mathbf{W}_U \mathbf{U}_f(k) - 2(\mathbf{S}_{uI}\mathbf{u}_s(k))^T \mathbf{W}_U \mathbf{U}_f(k) + (\mathbf{S}_{uI}\mathbf{u}_s(k))^T \mathbf{W}_U (\mathbf{S}_{uI}\mathbf{u}_s(k)) \\ &= \mathbf{U}_f(k)^T \mathbf{S}_u^T \mathbf{W}_X \mathbf{S}_u \mathbf{U}_f(k) + 2\boldsymbol{\eta}(k)^T \mathbf{W}_X \mathbf{S}_u \mathbf{U}_f(k) + \boldsymbol{\eta}(k)^T \mathbf{W}_X \boldsymbol{\eta}(k) \\ &\quad + \mathbf{U}_f(k)^T \mathbf{W}_U \mathbf{U}_f(k) - 2(\mathbf{S}_{uI}\mathbf{u}_s(k))^T \mathbf{W}_U \mathbf{U}_f(k) + (\mathbf{S}_{uI}\mathbf{u}_s(k))^T \mathbf{W}_U (\mathbf{S}_{uI}\mathbf{u}_s(k)) \\ &= \mathbf{U}_f(k)^T (\mathbf{S}_u^T \mathbf{W}_X \mathbf{S}_u + \mathbf{W}_U) \mathbf{U}_f(k) + 2 \left[ \boldsymbol{\eta}(k)^T \mathbf{W}_X \mathbf{S}_u - (\mathbf{S}_{uI}\mathbf{u}_s(k))^T \mathbf{W}_U \right] \mathbf{U}_f(k) + \\ &\quad \text{remaining terms not containing } \mathbf{U}_f(k) \end{aligned}$$

Thus, defining matrix  $\mathbf{H}$  and vector  $\mathbf{F}(k)$  as follows

$$\begin{aligned} \mathcal{H} &= 2(\mathbf{S}_u^T \mathbf{W}_X \mathbf{S}_u + \mathbf{W}_U) \\ \mathcal{F}(k) &= 2 \left[ \boldsymbol{\eta}(k)^T \mathbf{W}_X \mathbf{S}_u - (\mathbf{S}_{uI}\mathbf{u}_s(k))^T \mathbf{W}_U \right]^T \\ \boldsymbol{\eta}(k) &= \mathbf{S}_x\hat{\mathbf{x}}(k|k-1) + \mathbf{S}_e\hat{\mathbf{e}}_f(k) - \mathbf{S}_{xI}\mathbf{x}_s(k) \end{aligned}$$

we can formulate QP problem equivalent to MPC-1 as follows

$$\arg \min_{\mathcal{U}_f} \frac{1}{2} \mathbf{U}_f(k)^T \mathcal{H} \mathbf{U}_f(k) + \mathcal{F}(k) \mathbf{U}_f(k)$$

$$\begin{bmatrix} \mathbf{I}_{mq \times mq} \\ -\mathbf{I}_{mq \times mq} \end{bmatrix} \mathbf{U}_f(k) \leq \begin{bmatrix} \mathbf{S}_{uI}\mathbf{u}_H \\ -\mathbf{S}_{uI}\mathbf{u}_L \end{bmatrix}$$

Use Matlab function *quadprog* to implement MPC.

You are expected to implement this formulation using either linearized mechanistic model or state space model identified from data. The controller tuning parameters are

- Mechanistic model based MPC

$$\begin{aligned}
\mathbf{w}_x &= \mathbf{I}_{2 \times 2} \ ; \ \mathbf{w}_u = \mathbf{I}_{2 \times 2} \ ; \ p = 75 \ ; q = 5 \ ; \alpha = 0.9 \\
\mathbf{U}_L &= [0 \ 0]^T; \ \mathbf{U}_H = [100 \ 100]^T; \\
\mathbf{u}_L &= \mathbf{U}_L - \mathbf{U}_s \ ; \ \mathbf{u}_H = \mathbf{U}_H - \mathbf{U}_s
\end{aligned}$$

- State space model identified from data

$$\begin{aligned}
\mathbf{w}_x &= \mathbf{C}^T \mathbf{C} \ ; \ \mathbf{w}_u = \mathbf{I}_{2 \times 2} \ ; \ p = 75 \ ; q = 5 \ ; \alpha = 0.9 \\
\mathbf{U}_L &= [0 \ 0]^T; \ \mathbf{U}_H = [100 \ 100]^T; \\
\mathbf{u}_L &= \mathbf{U}_L - \mathcal{U}_s \ ; \ \mathbf{u}_H = \mathbf{U}_H - \mathcal{U}_s
\end{aligned}$$

After finding  $\mathbf{U}_f(k)$  using QP, extract  $\mathbf{u}(k)$  from  $\mathbf{U}_f(k)$ , set

$$\mathcal{U}(k) = \mathbf{u}(k) + \mathcal{U}_s$$

and communicate  $\mathcal{U}(k)$  to the plant.