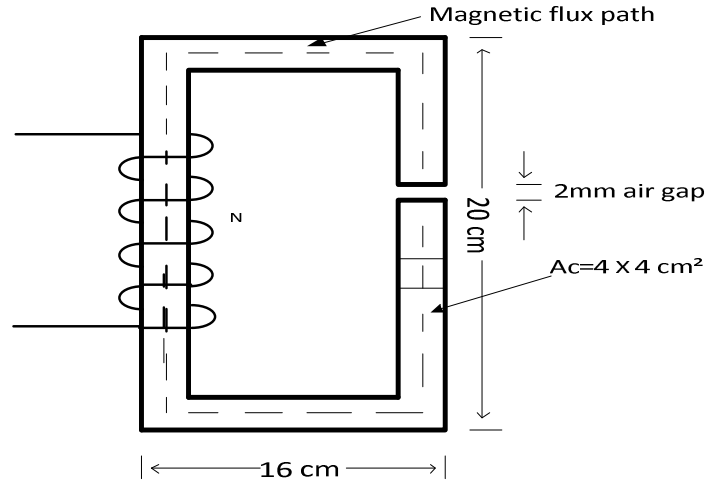


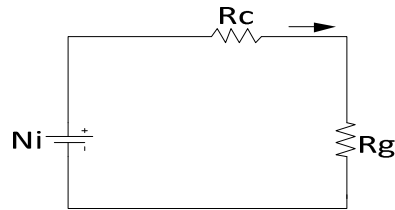
## **Tutorial-9 (Solutions)**

### 1. (Pre-tutorial question)

Fig. 1(a) shows a rectangular magnetic core with an air gap. Find the exciting current needed to cause a flux density of  $B_g = 1.2T$  in the air gap. Given  $N = 400 \text{ turns}$  and  $\mu_r(\text{iron}) = 4000$ .



### **Solution:**



It is a simple series magnetic circuit with its analog shown in Fig. 1(b).

$$\text{Core length, } l_c = 2[(20 - 4) + (16 - 4)] - 0.2 = 55.8 \text{ cm}$$

$$\text{Cross-sectional area of core, } A_c = 16 \text{ cm}^2$$

$$\text{Core reluctance, } \mathfrak{R}_c = \frac{l_c}{\mu_r \mu_0 A_c} = \frac{55.8 \times 10^{-2}}{4000 \times 4\pi \times 10^{-7} \times 16 \times 10^{-4}} = 0.694 \times 10^5$$

$$\text{Air gap length, } l_g = 0.2 \text{ cm}$$

$$\text{Area of air gap, } A_g = 16 \text{ cm}^2$$

$$\text{Air gap reluctance, } \mathfrak{R}_g = \frac{l_g}{\mu_0 A_g} = \frac{2 \times 10^{-3}}{4\pi \times 10^{-7} \times 16 \times 10^{-4}}$$

$$\text{Total, } \mathfrak{R} = \mathfrak{R}_c + \mathfrak{R}_g = 10.64 \times 10^5 \text{ AT/Wb}$$

$$\text{Flux in the magnetic circuit, } \Phi = BA = 1.2 \times 16 \times 10^{-4} = 1.92 \text{ mWb}$$

$$\text{Now, } Ni = \Phi(\mathfrak{R}_c + \mathfrak{R}_g) = \Phi \mathfrak{R} = 1.92 \times 10^{-3} \times 10.64 \times 10^5 = 2043 \text{ AT}$$

$$\text{So Exciting current, } i = \frac{\Phi \mathfrak{R}}{N} = \frac{2043}{400} = \mathbf{5.11 \text{ A}}$$

2. Derive the output voltage expression for the following circuit.

**Solution**

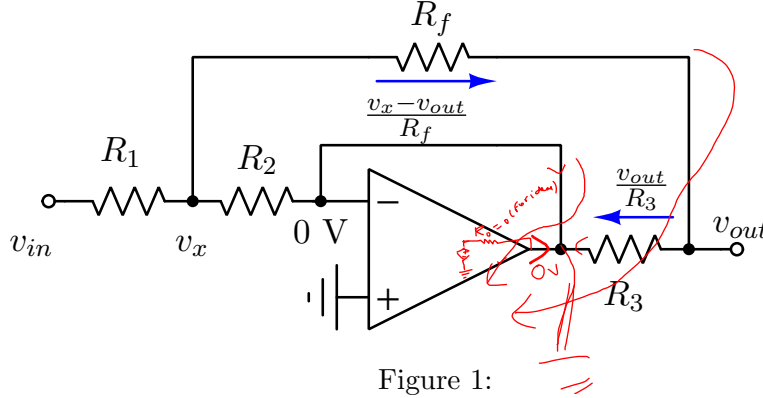


Figure 1:

If we assume a virtual short at the opamp input terminals and write the KCL at the intermediate node,

$$\frac{v_{in} - v_x}{R_1} = \frac{v_x}{R_2} + \frac{v_x - v_{out}}{R_f}.$$

**Important points:**

- (i) Even though there is no real ground at the opamp negative input terminal, there exists a low impedance path for the current to flow (unity feedback connection). Hence  $v_x$  is not equal to zero.
- (ii) Due to the unity feedback, opamp output terminal is at 0 V.
- (iii)  $\frac{v_x}{R_2} \neq \frac{-v_{out}}{R_3}$ . An ideal opamp (a VCVS) can supply any amount of current at the output.

The second equation we have is,

$$\frac{v_x - v_{out}}{R_f} = \frac{v_{out}}{R_3}$$

Solving the above two equations will give  $v_{in} = v_{out} \left[ \frac{R_1}{R_3} + \frac{(R_f + R_3)(R_1 + R_2)}{R_2 R_3} \right]$ .

3. In the circuit shown in fig. 3, find the average power absorbed by (a) the source, (b) each of the two resistors, (c) each of the inductance, (d) mutual inductance.

## Tutorial-9 (Solutions)

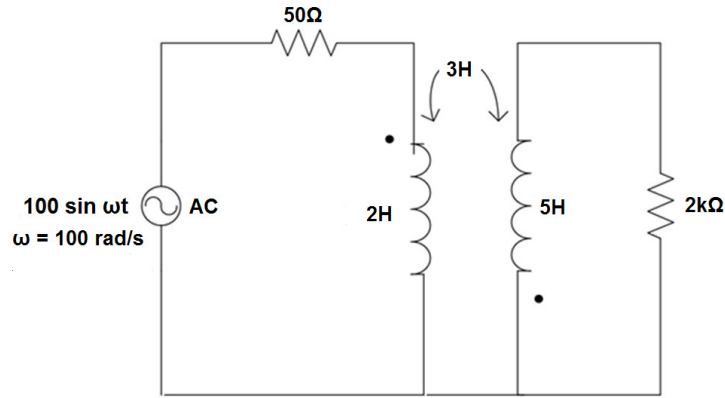


Fig. 3

### Solution:

#### KVL in the loop – 1:

$$100 - I_1(50 + j200) - j300I_2 = 0$$

$$\Rightarrow I_1(5 + j20) + j30I_2 = 10 \text{ ----- (1)}$$

#### KVL in the loop – 2:

$$-j\omega 5I_2 - 2000I_2 - j\omega 3I_1 = 0$$

$$\Rightarrow j3I_1 + I_2(20 + j5) = 0 \text{ ----- (2)}$$

Solving equation (1) & (2)

$$I_2 = 0.069 \angle -168.04^\circ \text{ A}, I_1 = 0.475 \angle 64.04^\circ \text{ A}$$

a) Power absorbed the source =  $V_{eff} I_{eff} \cos \phi = -\frac{100}{\sqrt{2}} \times \frac{0.475}{\sqrt{2}} \cos(64.04^\circ)$   
 $= -10.40 \text{ W}$  (-ve sign indicates power delivered)

b)  $P_{50} = I_{1eff}^2 \times 50 = 5.64 \text{ W}$ ,  $P_{2K} = I_{2eff}^2 \times 2K = 4.76 \text{ W}$

c) & d) Power absorbed by each inductance and mutual inductance is **zero**.

4. Find the equivalent inductances seen at terminals 1 and 2 in the network of Fig. 4 if the following terminals are connected together: (a) none, (b) A to B, (c) A to C.

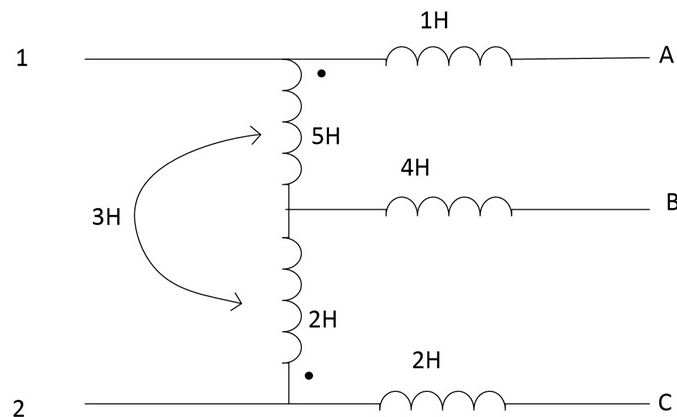
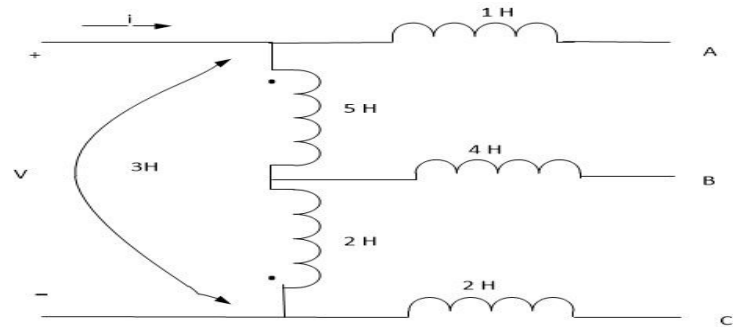


Fig. 4

## Tutorial-9 (Solutions)

Solution:

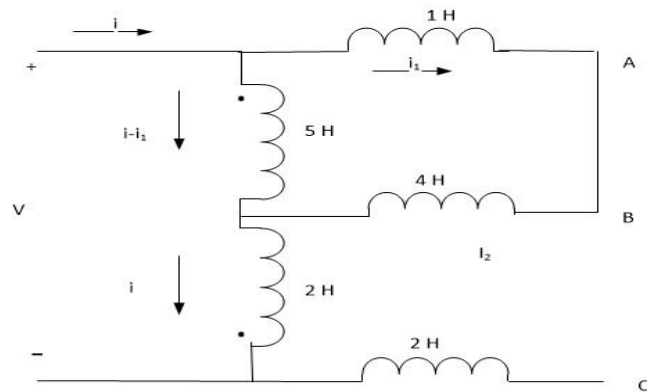
a)



$$V - \left(5 \frac{di}{dt} - 3 \frac{di}{dt}\right) - \left(2 \frac{di}{dt} - 3 \frac{di}{dt}\right) = 0 \Rightarrow v - \frac{di}{dt} = 0$$

$$L_{eq} = 1 \text{ H}$$

b)



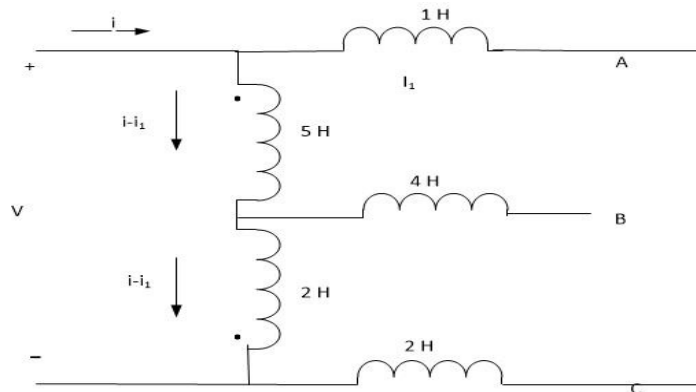
$$V - 5 \frac{d(i-i_1)}{dt} + 3 \frac{di}{dt} - 2 \frac{di}{dt} + 3 \frac{d(i-i_1)}{dt} = 0 \Rightarrow V - \frac{di}{dt} + 2 \frac{di_1}{dt} = 0 \quad (1)$$

$$-1 \frac{di_1}{dt} - 4 \frac{di_1}{dt} + 5 \frac{d(i-i_1)}{dt} - 3 \frac{di}{dt} = 0 \Rightarrow \frac{di_1}{dt} = \frac{1}{5} \frac{di}{dt} \quad (2)$$

Replacing the value of  $\frac{di_1}{dt}$  from (2) in equation (1)

$$V - \frac{di}{dt} \left(1 - \frac{2}{5}\right) = 0 \Rightarrow L_{eq} = \frac{3}{5} \text{ H}$$

c)



## **Tutorial-9 (Solutions)**

$$V - \left( 5 \frac{d(i-i_1)}{dt} - 3 \frac{d(i-i_1)}{dt} \right) - \left( 2 \frac{d(i-i_1)}{dt} - 3 \frac{d(i-i_1)}{dt} \right) = 0$$

$$V - \frac{di}{dt} + \frac{di_1}{dt} = 0 \text{ ----- (1)}$$

$$-\frac{di_1}{dt} - 2 \frac{di_1}{dt} + 2 \frac{d(i-i_1)}{dt} - 3 \frac{d(i-i_1)}{dt} + 5 \frac{d(i-i_1)}{dt} - 3 \frac{d(i-i_1)}{dt} = 0$$

$$\Rightarrow \frac{di_1}{dt} = \frac{1}{4} \frac{di}{dt} \text{ ----- (2)}$$

$$V - \frac{di}{dt} \left( 1 - \frac{1}{4} \right) = 0 \Rightarrow \mathbf{L_{eq} = \frac{3}{4} H}$$