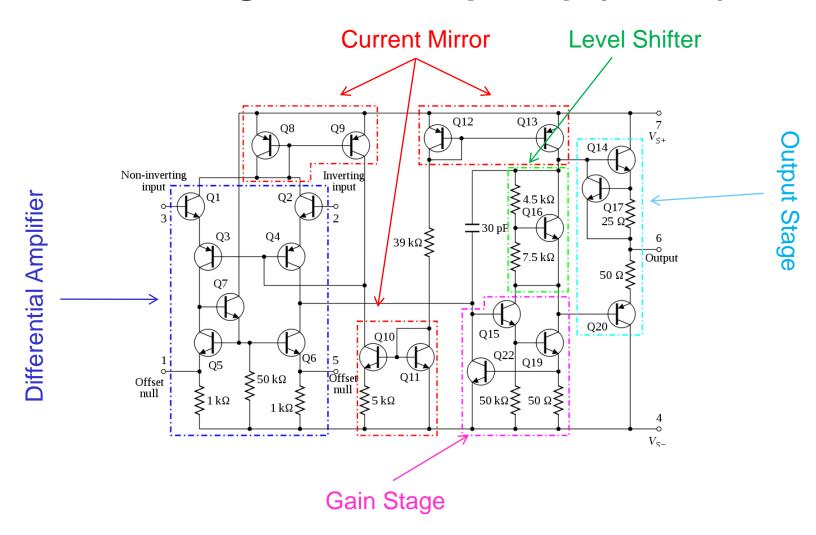
# Operational Amplifier (Op-Amp)

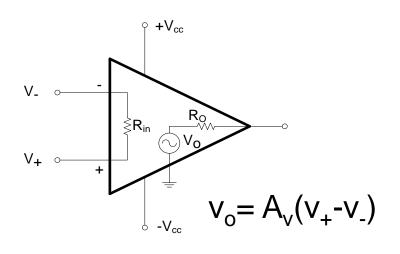
# Circuit Diagram of an Op-Amp (IC 741)

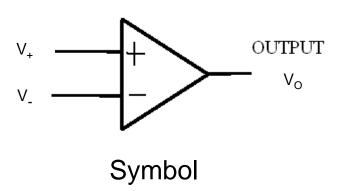


# **Operational Amplifier (Op-Amp)**

- An Op-Amp is a very high gain amplifier having a number of differential amplifier stages
- It has high input impedance (typically a few Megaohm)
- It has a low output impedance (less than  $100\Omega$ )

# **Op-Amp Model**





# In a good Op-Amp

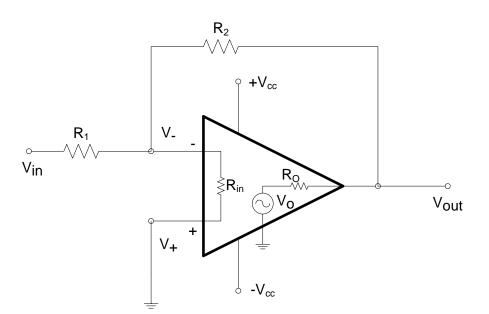
$$A_{V} \rightarrow \infty$$

$$\mathsf{R}_{\mathsf{in}} o \infty$$

$$R_0 \rightarrow 0$$

If  $v_+$  is even slightly higher than  $v_-$ ,  $v_o = +V_{cc}$ If  $v_+$  is even slightly lower than  $v_-$ ,  $v_o = -V_{cc}$  Cannot be used as an amplifier by itself!

#### Consider the circuit shown below



$$v_{+} = 0 \quad v_{o} = -A_{v}v_{-}$$

$$\frac{v_{in} - v_{-}}{R_{1}} + \frac{v_{o} - v_{-}}{R_{2} + R_{o}} = \frac{v_{-}}{R_{in}}$$

$$v_{-} \left[ \frac{1}{R_{2} + R_{o}} + \frac{1}{R_{1}} + \frac{1}{R_{in}} \right] - \frac{v_{o}}{R_{2} + R_{o}} = \frac{1}{R_{1}}v_{in}$$

$$- \frac{v_{o}}{A_{v}} \left[ \frac{1}{R_{2} + R_{o}} + \frac{1}{R_{1}} + \frac{1}{R_{in}} \right] - \frac{v_{o}}{R_{2} + R_{o}} = \frac{1}{R_{1}}v_{in}$$

For 
$$A_v \rightarrow \infty$$
, we get

$$\left| v_o \right| - \frac{1}{R_2 + R_O} \left| = \frac{v_{in}}{R_1} \right|$$

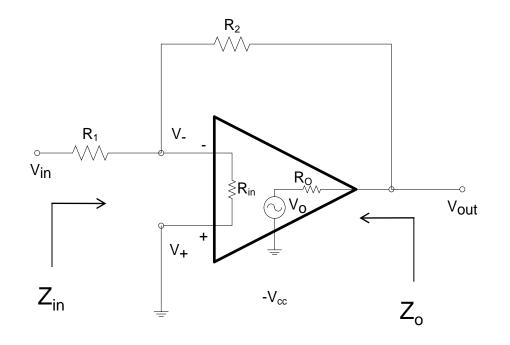
$$\left[\frac{v_0}{R_0 + R_2}\right] R_2 = v_{out}$$

$$\frac{v_{out}}{v_{in}} = -\frac{R_2}{R_1}$$

For 
$$A_{V} \rightarrow \infty$$
, we get  $v_{o} \left[ -\frac{1}{R_{2} + R_{o}} \right] = \frac{v_{in}}{R_{1}}$  and  $v_{-} = -\frac{v_{o}}{A_{V}} \rightarrow 0$ 

 $\left| \frac{v_0}{R_1 + R_2} \right| R_2 = v_{out}$  The (-) terminal is effectively at ground. This is referred to as "Virtual Ground"

## **Interesting Points**



With 
$$A_v \rightarrow \infty$$
,

Gain = 
$$-R_2/R_1$$
  
(does not depend on  $A_v$ )

- (+) is at Ground
- (-) is at Virtual Ground

$$Z_{\text{in}} = R_1$$
  
 $Z_{\text{out}} = R_0 || R_2 \approx R_0$ 

## **Concept of Virtual Ground**

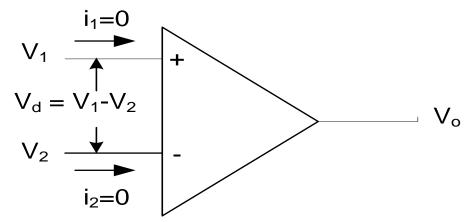
- 1. V<sub>-</sub>≈ 0 V (-) terminal is at ground potential
- 2. No Current Enters the (-) terminal of the Op-Amp Valid only when there is feedback connection between the output and the (-) terminal.

6

## Characteristics of an ideal OP-Amp

- Input Resistance R<sub>i</sub> = ∞
- Output Resistance R<sub>o</sub>= 0
- Voltage Gain A<sub>v</sub> = ∞
- Bandwidth = ∞ (i.e. can work over a wide range of frequencies)
- Perfect balance i.e  $v_0 = 0$  when  $v_1 = v_2$
- Characteristics do not drift with temperature

# Ideal Op-Amp analysis



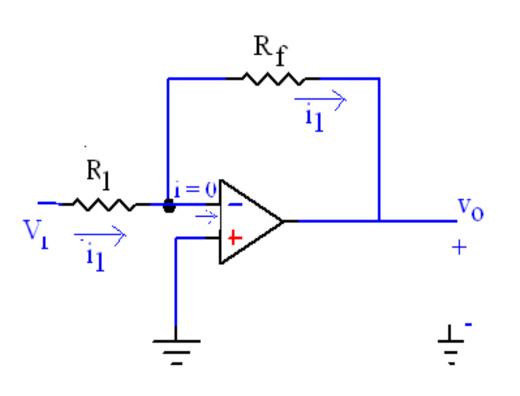
i) R<sub>i</sub> = ∞,
 No current enters into op-amp

Voltage Gain  $A_v = \infty$  or,  $v_o/v_d = \infty$  or,  $v_d = v_o/\infty = 0$  [since  $v_o$  is finite] Therefore,  $v_1 - v_2 = 0$  or,

ii) 
$$V_1 = V_2$$

# **Simple OP-AMP Circuits**

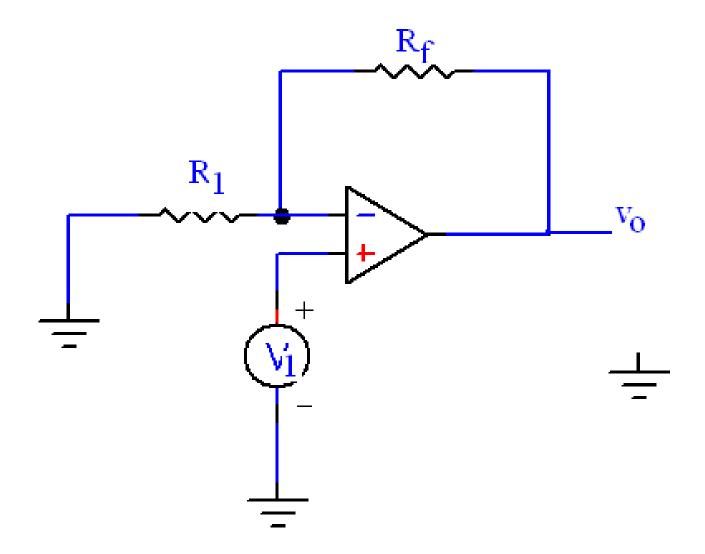
# 1. Inverting Amplifier



Using KVL,  

$$v_1 - i_1R_1 = 0$$
  
 $\Rightarrow i_1 = v_1/R_1$   
&  
 $0 - i_1R_f - v_o = 0$   
or,  $v_o = -i_1R_f = -v_1R_f/R_1$   
 $v_0/v_1 = -R_f/R_1$ 

# 2. Non Inverting Amplifier

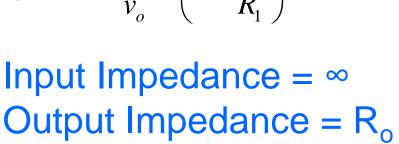


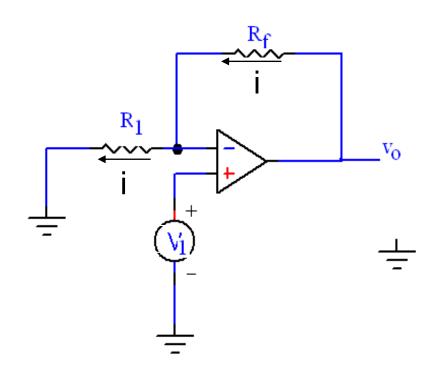
$$v_{-} = v_{+} = v_{1}$$

$$i = \frac{v_{1}}{R_{1}} = \frac{v_{o} - v_{1}}{R_{f}}$$

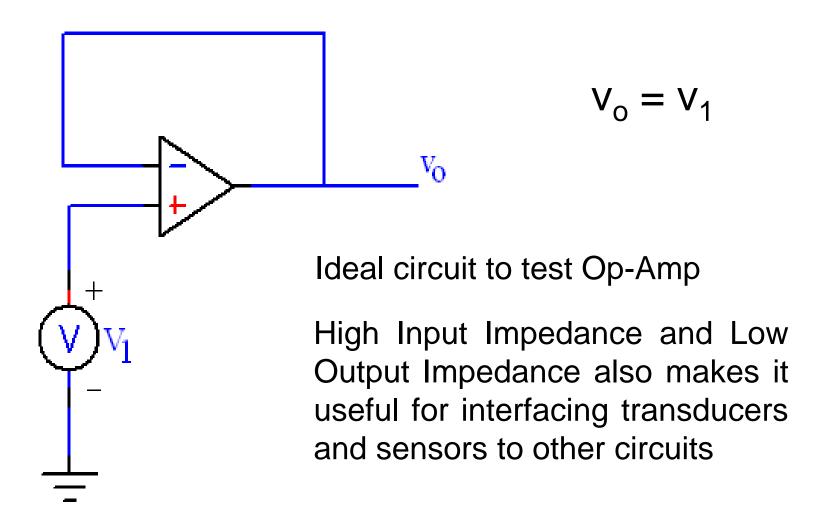
$$v_{o} = R_{f} \left[ \frac{1}{R_{1}} + \frac{1}{R_{f}} \right] v_{1}$$

$$\frac{v_{o}}{v_{o}} = \left( 1 + \frac{R_{f}}{R_{1}} \right)$$





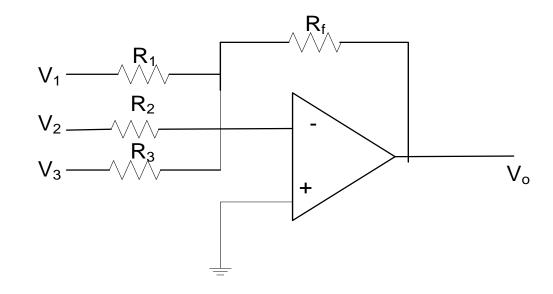
# 3. Voltage Follower



# 4. Summing Amplifier

Use superposition (i.e. consider one source at a time and add their respective outputs)

Can also be done directly



$$v_o = -\left[\frac{R_f}{R_1}v_1 + \frac{R_f}{R_2}v_2 + \frac{R_f}{R_3}v_3\right]$$

# Difference Amplifier (or Voltage Subtractor)

### **Use Superposition**

(can also be done directly) R<sub>1</sub>

If 
$$v_2=0$$
,  $v_{o1}=-\frac{R_2}{R_1}v_1$ 

If 
$$v_1=0$$
,  $v_{o2} = v_2 \left[ \frac{R_2}{R_1 + R_2} \right] \left[ 1 + \frac{R_2}{R_1} \right]$ 
$$= v_2 \frac{R_2}{R_1}$$

Therefore, 
$$v_o = v_{o1} + v_{o2} = \frac{R_2}{R_1}(v_2 - v_1)$$

Difference Gain =  $R_2/R_1$ 

#### **Tutorial Problem**

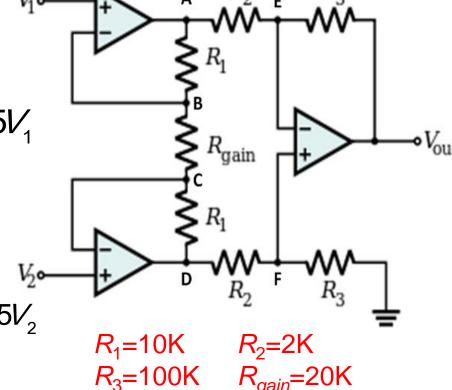
(Instrumentation Amplifier)

$$V_B = V_1$$
  $V_C = V_2$   $V_D = 1.5V_2 - 0.5V_1$ 

$$V_A = 1.5V_1 - 0.5V_2$$

$$V_E = V_F = 1.4706V_2 - 0.4902V_1$$

$$V_{out} = 75.006V_2 - 25.002V_1 - 75V_1 + 25V_2$$
$$= 100.006V_2 - 100.002V_1$$
$$= 100.004 V_2 - V_1) + 0.002 V_2 + V_1)$$



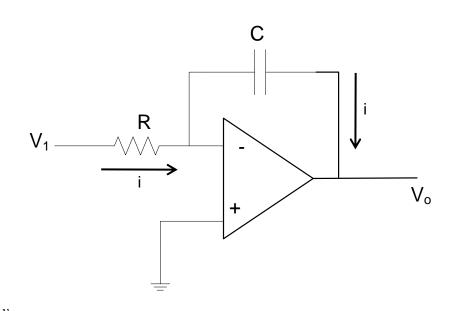
$$\frac{V_{out}}{V_2 - V_1} = \left(1 + \frac{2R_1}{R_{gain}}\right) \frac{R_3}{R_2}$$
 Gain can be varied by just changing one resistor,  $R_{gain}$ 

# Integrator

$$i = \frac{v_1}{R}$$
  $v_o = -\frac{1}{C} \int_0^t i dt$  with  $v_o(0) = 0$   $v_1$ 

Therefore,

$$v_o = -\frac{1}{RC} \int_0^t v_1 dt$$
 with  $v_o(0) = 0$ 

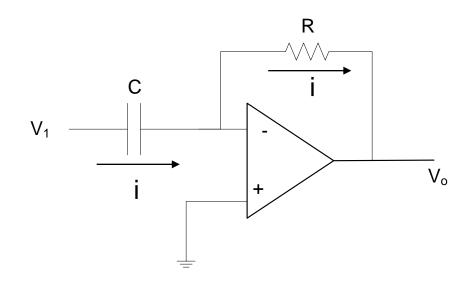


#### **Differentiator**

$$v_1 = \frac{1}{C} \int_0^t i dt \quad \text{with } v_1(0) = 0$$

$$v_0 = -iR$$

Therefore, 
$$v_1 = -\frac{1}{RC} \int_0^t v_o dt$$
 or 
$$v_o = -RC \frac{dv_1}{dt}$$



# **Example**

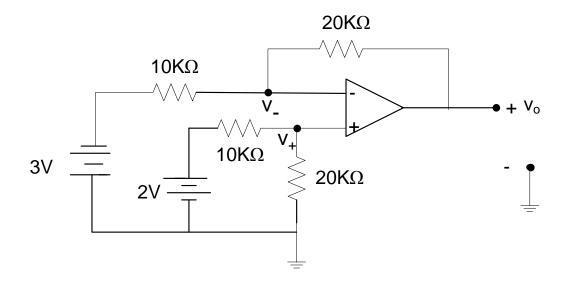
Find v<sub>o</sub> in the given circuit.

$$v_{-} = v_{+} = 2 \times \frac{20}{30} = \frac{4}{3}$$

$$\frac{v_{o} - v_{-}}{20} = \frac{v_{-} - (-3)}{10}$$

$$\frac{v_{o}}{20} = v_{-} \left(\frac{1}{10} + \frac{1}{20}\right) + \frac{3}{10}$$

$$v_{0} = 3v_{-} + 6 = 10 \text{ V}$$



# **Example**

Find the gain  $v_o/v_i$  in the given circuit.

$$v_{-} = v_{+} = 0$$
 Virtual Ground at (-)

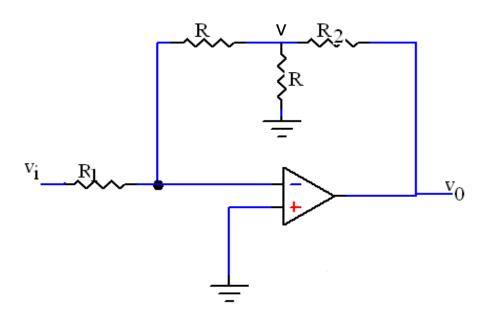
$$\frac{v_i}{R_1} = -\frac{v}{R} \qquad \Rightarrow \quad v = -\frac{R}{R_1} v_i$$

$$\frac{v_o - v}{R_2} = \frac{v}{R} + \frac{v}{R} = \frac{2v}{R}$$

$$v_o = v \left[ 1 + \frac{2R_2}{R} \right]$$

$$= -\left[ \frac{R}{R_1} \right] \left[ 1 + \frac{2R_2}{R} \right] v_i$$

$$= -\left( \frac{R + 2R_2}{R_1} \right) v_i$$



Gain 
$$A_V = \frac{v_o}{v_i} = -\left(\frac{R + 2R_2}{R_1}\right)$$

## **Voltage Controlled Current Source**

(with grounded load)

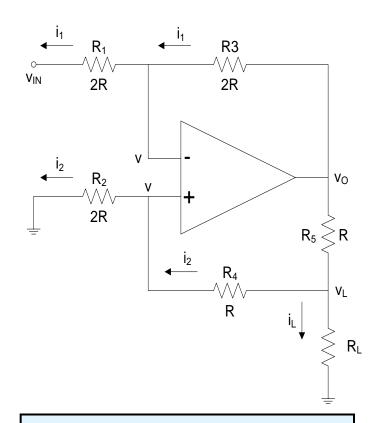
$$i_{1} = \frac{v - v_{IN}}{2R} = \frac{v_{O} - v}{2R} \implies 2v - v_{O} = v_{IN}$$

$$i_{2} = \frac{v}{2R} = \frac{v_{L} - v}{R} \implies v_{L} = \frac{3}{2}v$$

$$i_{L} = \frac{v_{O} - v_{L}}{R} - \frac{v_{L} - v}{R} = \frac{v_{O} - 3v + v}{R} = \frac{v_{O} - 2v}{R}$$

Therefore, 
$$i_L = -\frac{v_{IN}}{R}$$

Note that i<sub>L</sub> does not depend on R<sub>L</sub>, implying that we have got a current source!

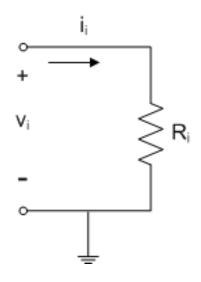


#### **General Condition:**

$$R_1 = R_2 \& R_3 = R_4 + R_5$$

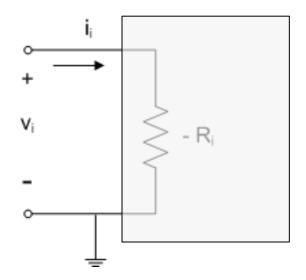
# Creating an effectively "Negative Resistance"

What is "Negative Resistance"?



Normal Resistance

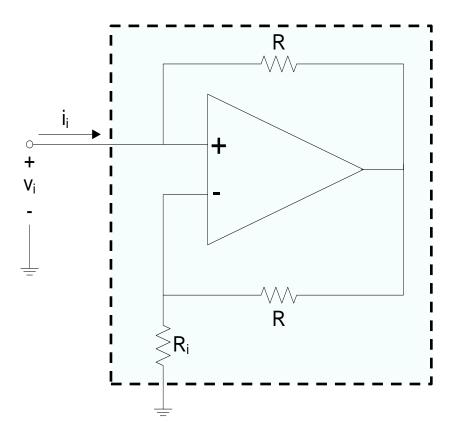
$$\frac{v_i}{i_i} = R_i$$



Negative  $\frac{v_i}{i_i} = -R_i$ 

$$\frac{v_i}{i_i} = -R_i$$

# Creating an effectively "Negative Resistance"



Let  $v_0 = \text{opamp output voltage}$ and  $v_+=v_-=v_i$ 

$$\frac{v_i}{R_i} = \frac{v_O - v_i}{R} \implies v_O = v_i \left( 1 + \frac{R}{R_i} \right)$$

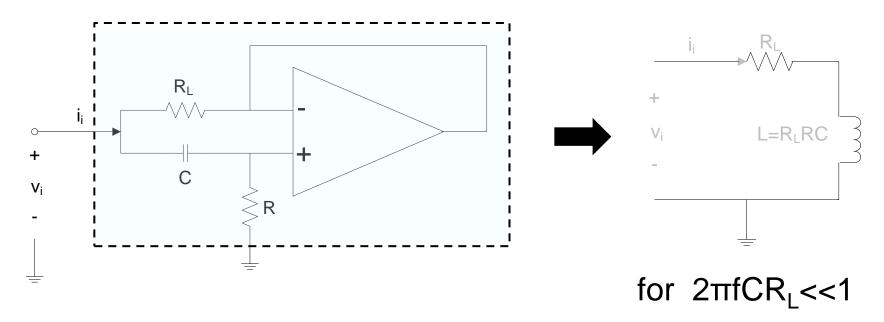
$$i_i = \frac{v_i - v_O}{R} = -\frac{v_i}{R_i}$$

Therefore, 
$$\frac{v_i}{i_i} = -R_i$$

$$\frac{v_i}{i_i} = -R_i$$
 Negative Resistance

# **Using Capacitors to make Inductors**

(practical to do only small values of inductances)



Using phasors, show that

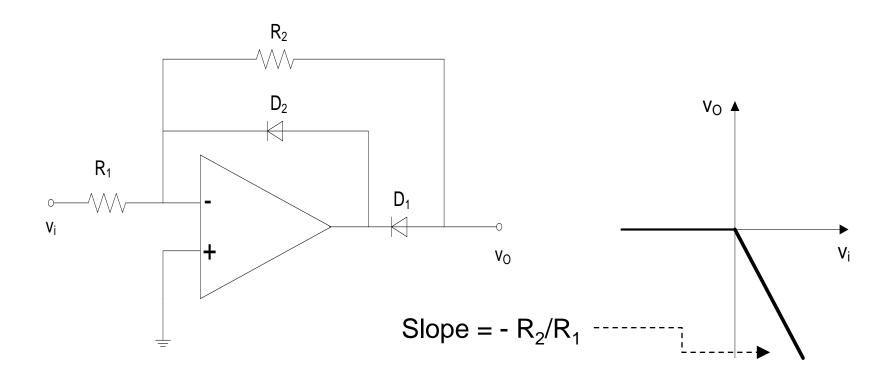
$$\frac{v_i}{i_i} = \frac{R_L + j\varpi RCR_L}{(1 + j\varpi CR_L)} = R_L + j\varpi RCR_L$$

#### **Precision Rectifier**

The simple half-wave and full-wave rectifiers we saw earlier have one big drawback – They do not work for small voltages (say a few millivolts). The input voltage must cross the threshold which forward biases the diode for rectification to occur.

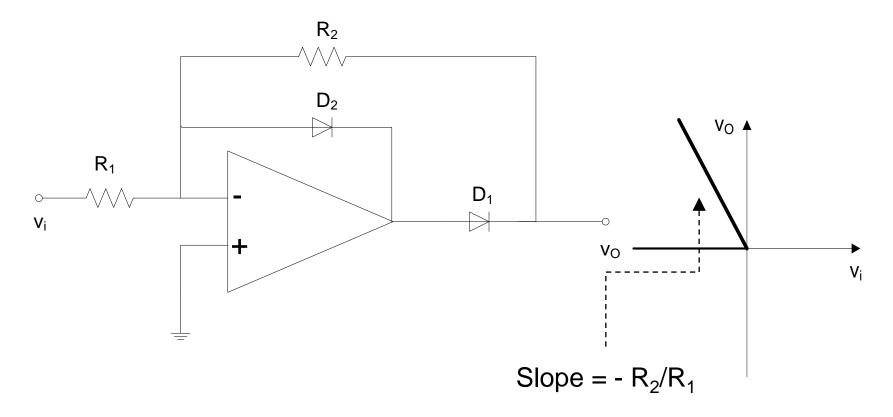
Using Op-Amps, we can design rectifiers which do not have this disadvantage.

#### Half-Wave Precision Rectifier



You will be making this circuit in EC102 Lab next semester

#### What happens when you reverse the diodes?



Build a full wave rectifier using these two half-wave rectifiers and a difference amplifier – needs three opamps!

#### **Full-Wave Precision Rectifier**

