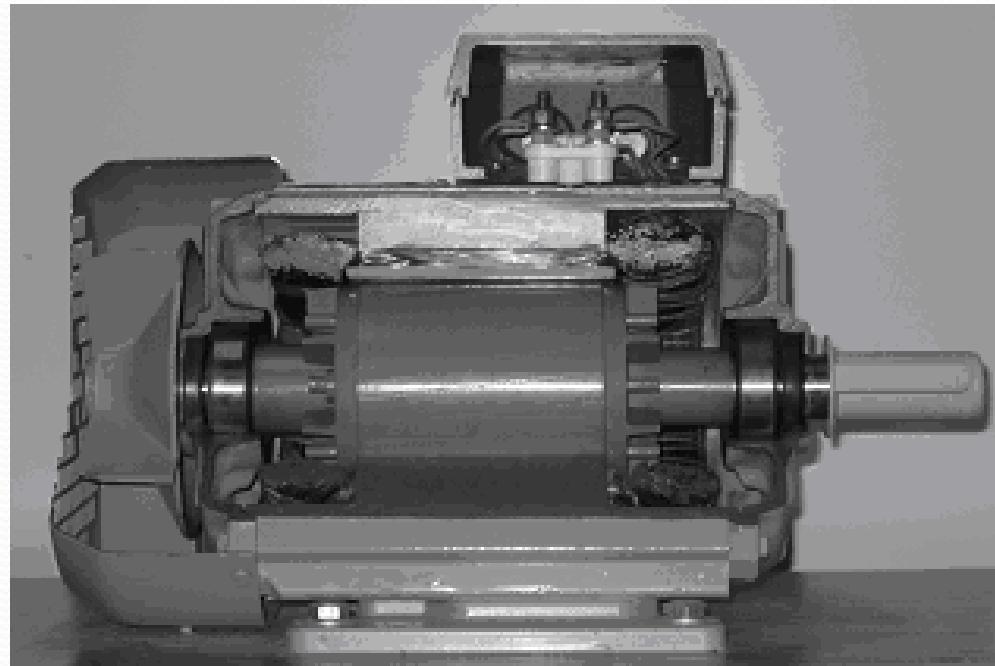


# EE 101

## Electrical Sciences



Department of Electronics & Electrical Engineering

# Lectures 17-19

**3-Phase Induction Motors  
Introduction to DC Machines and Synchronous Generators**

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# Electromechanical Energy Conversion

Two basic electromagnetic processes in electromechanical energy conversion are:

- A moving conductor in a magnetic field induces voltage. This is called **generator action**.
- A current carrying conductor in a magnetic field produces force or torque. This is called **motor action**.
- In all electric machines, both actions/processes take place simultaneously





# OPERATING PRINCIPLE – GENERATORS & MOTORS

## Generator

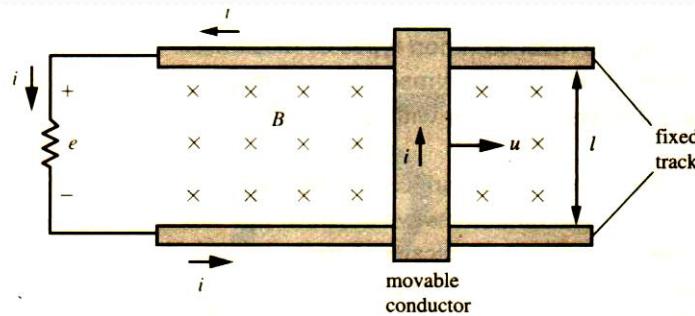


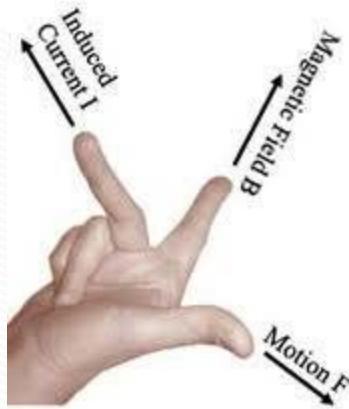
Fig. 15.1 Simple generator.

Input:

Field –  $B$

Movement –  $u$

(Force or Torque)



Output –  $e$

$$e = \frac{d\lambda}{dt} = Blu$$

## Motor

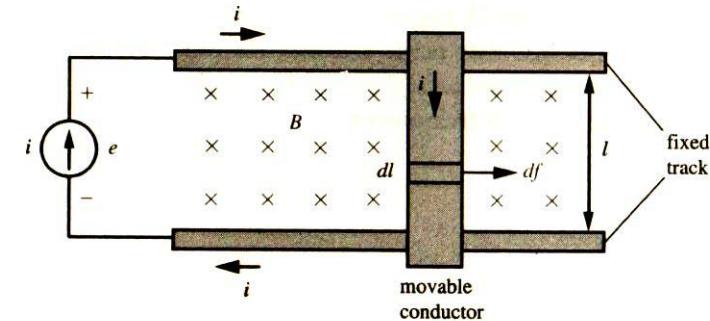


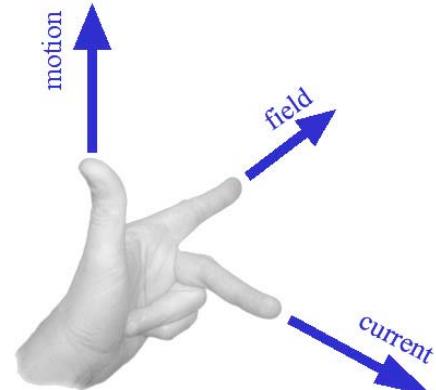
Fig. 15.2 Simple motor.

Input:

Field –  $B$

Current –  $I$

(Voltage)



Output –  $F$  or Torque

$$F = \int Bidl = Bil$$





# Three-Phase Induction Motors

- An induction motor is a singly-fed motor that converts AC electrical power into mechanical power
- Electrical power is feed to the stator and the mechanical power is obtained from the rotor
- No electrical source is connected to the rotor circuit. The rotor receives power from the stator by induction (**not** by conduction) and that is why it is called induction motor
- The rotor circuit of an induction motor is similar to the secondary circuit of a transformer which also receives power from the primary circuit by induction
- In transformers, both the primary and secondary windings are stationary but in induction motors, the rotor (or secondary) winding is not stationary but rotating
- An induction motor can be considered as a rotating transformer (with stationary primary and rotating secondary) in which the rotor winding receives power by induction while it rotates

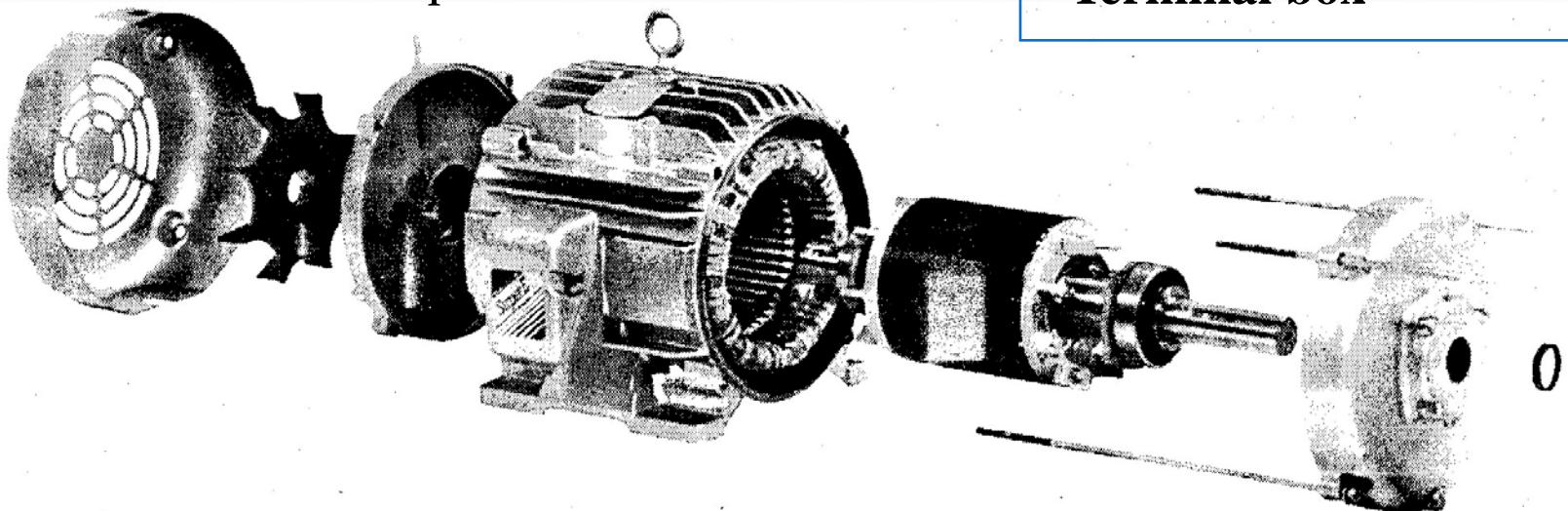




# General Features

## Two Basic Types of Induction Motors

- Single-phase induction motors
- Three-phase induction motors
  - Most widely used
  - Simple and robust construction
  - Low cost and reasonably good efficiency
  - Reliable and requires less maintenance



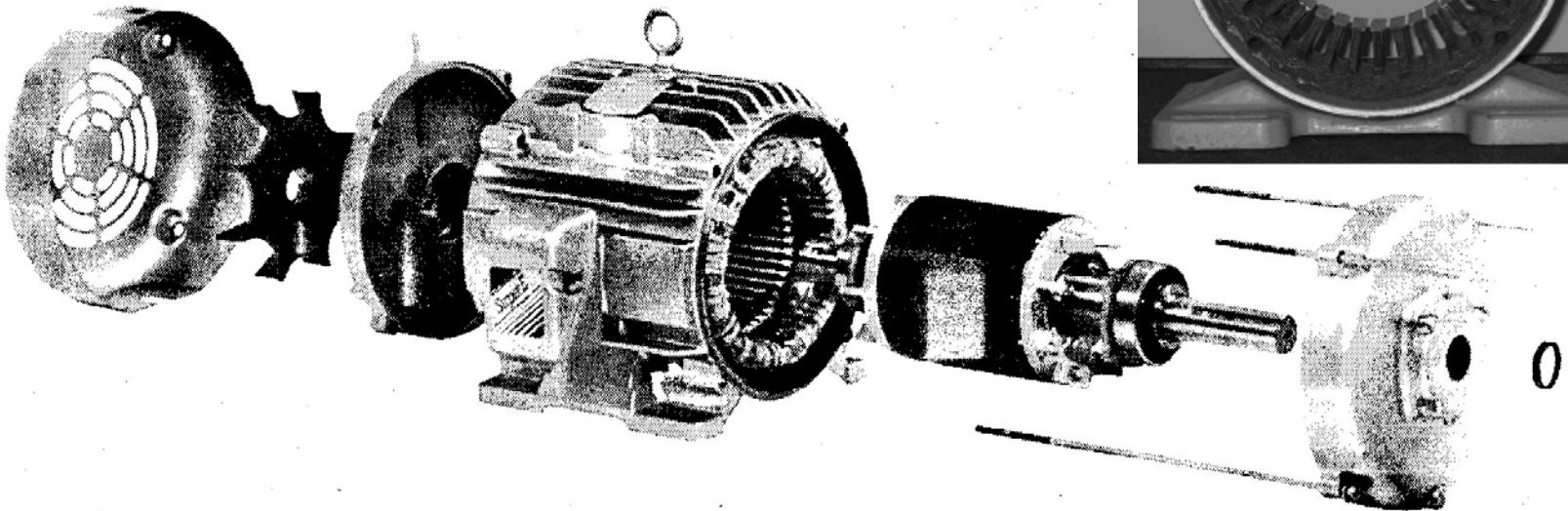
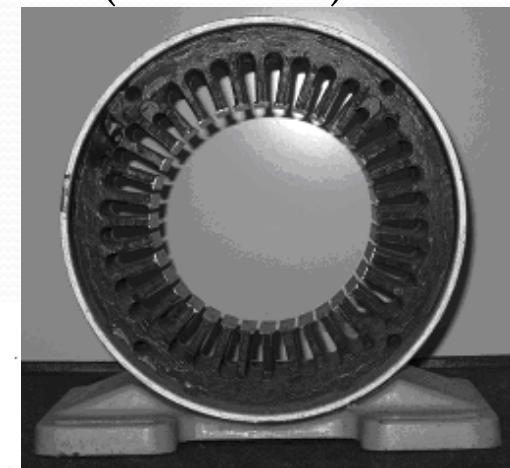
## Major Components

- Stator (stationary part) or armature
- Rotor (rotating part)
- Other mechanical fittings (bearing, fan, shaft extension, end-cover, etc.)
- Terminal box



# CONSTRUCTION - STATOR

- The outer (or stationary) part of an induction motor is called stator and is composed of laminated high-grade steel sheets
- Three-phase windings are placed in the slots cut on the inner surface of the stator frame. Phase windings are displaced by  $120^\circ$  (electrical) from others
- Winding ends are terminated to the terminal box. Windings can be connected in star (wye) or delta ( $\Delta$ ) configuration

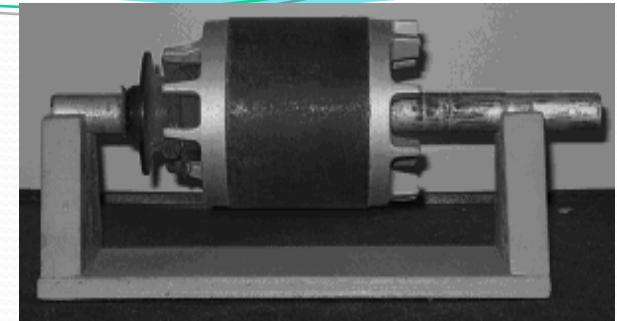




# CONSTRUCTION - ROTOR

- Rotor could be solid mild steel core

## Two Types of Rotors



### (a) Squirrel-cage rotor

- It is very commonly used. Rotor windings or bars are placed in rotor slots. Circular rings called **end-rings** short circuit the rotor bars on both ends of the rotor

### (b) Wound rotor

- Three-phase windings (with internal neutral) are placed in rotor slots. Three end terminals are connected to three slip-rings
- With brushes riding on slip-rings, the rotor terminals can be terminated at the terminal box
- Torque-speed characteristic of the motor can be controlled by changing the external rotor resistance





# OPERATING PRINCIPLE – ROTATING FIELD

- When the stator windings of a 3-phase induction motor are connected to a 3-phase supply, it draws 3-phase currents and produces three magnetic fields
- The resultant magnetic field is the sum (vector addition) of three magnetic fields. It can be shown that the resultant magnetic field is
  - constant in magnitude, and
  - rotates at a constant speed called **synchronous speed ( $N_s$ )**

Under linearity,

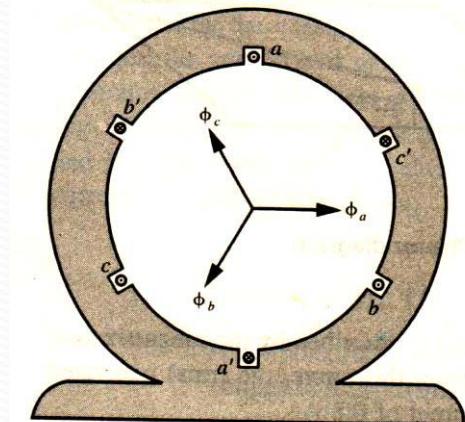
$$\Phi_a = ki_a e^{j0^\circ}, \quad \Phi_b = ki_b e^{-j120^\circ}, \quad \Phi_c = ki_c e^{j120^\circ},$$

and let,

$$i_a = I \cos \omega t, \quad i_b = I \cos(\omega t - 120^\circ), \quad i_c = I \cos(\omega t + 120^\circ)$$

Then it can be derived that,

$$\Phi = \Phi_a + \Phi_b + \Phi_c = \frac{3}{2} kI e^{-j\omega t}$$





# SYNCHRONOUS SPEED

- If balanced 3-phase currents of angular frequency  $\omega$  are applied to the three coiled spaced  $120^\circ$  from each other, the resultant flux is constant and rotates with the same angular speed, called synchronous speed.

$$\omega_s = f \text{ cycles/s} (= 2\pi f \text{ rad/s}) = f \text{ rps} = 60 f \text{ rpm}$$

where,  $f$  is the frequency of the power supply.

- For a machine with  $p$  number of poles, one mechanical rotation will be equivalent to  $p/2$  cycles, so that

$$\omega_s = f \text{ cycles/s} (= 2\pi f \text{ electrical rad/s}) = f/(p/2) \text{ rps} = 120 f/p \text{ rpm}$$

- The rotating magnetic field induces voltage in rotor windings or rotor bars
- The induced voltage causes rotor current (rotor bars or terminals are shorted directly or through resistances)
- The interaction of rotor current and rotating magnetic field produces a torque that tends to rotate the rotor





# ROTOR SPEED

- The rotor starts rotating in the direction of rotating magnetic field and ultimately reaches a steady-state speed which is very close to (but less than) synchronous speed 
- The rotor can never reach synchronous speed. At synchronous speed, the rotor appears stationary with respect to the rotating magnetic field and thus there will be no rotor induced voltage (and hence no rotor current or torque)
- The rotor speed is also called **motor speed** ( $N_m$  in rpm or  $\omega_m$  in rad/sec)
- The difference between the synchronous speed  $N_s$  and motor speed  $N_m$  is called **relative speed**  $N_r$

$$N_r = (N_s - N_m) \text{ rpm} \quad \text{or,} \quad \omega_r = (\omega_s - \omega_r) \text{ rad/sec}$$





# SLIP

- The relative speed  $N_r$  is also called **slip-speed**. This is the speed with which the rotor slipping behind the rotating magnetic field which is responsible for the production of torque
- The ratio of slip speed (or relative speed) to synchronous speed is called **slip (s)**

$$s = \frac{N_r}{N_s} = \frac{\omega_r}{\omega_s} = \frac{N_s - N_m}{N_s} = \frac{\omega_s - \omega_m}{\omega_s}$$

At stand still, motor speed

$N_m = 0 \Rightarrow \text{slip } s = 1$

At synchronous speed,

$N_m = N_s \Rightarrow \text{slip } s = 0$

In general,

$0 \leq N_m \leq N_s \Rightarrow 1 \geq s \geq 0$

- In terms of the synchronous speed ( $N_s$ ) and slip ( $s$ ), the motor speed ( $N_m$ ) can be written as

$$N_m = (1 - s)N_s \quad \text{or,} \quad \omega_m = (1 - s)\omega_s$$



# SLIP

- **At Stand Still (when the motor speed  $N_m = 0$ )**
  - The slip s becomes unity or 1
  - The rotor appears exactly the same as short-circuited secondary winding of a transformer
  - The frequency of the rotor induced voltage is the same as the stator frequency f
- **When the Rotor Rotates ( $0 < N_m < N_s$ )**
  - The relative speed  $N_r$  (or  $\omega_r$ ) is responsible to induce voltage in the rotor windings. Thus the frequency ( $f_r$ ) of rotor induced voltage is
$$f_r = \frac{PN_r}{120} = \frac{P(N_s - N_m)}{120} = \left[ \frac{N_s - N_m}{N_s} \right] \frac{PN_s}{120} = sf$$

  - The rotor frequency depends on slip (s) of the motor and stator frequency (f)





## EXAMPLE

A 240-V, 50-Hz, 4-pole, 3-phase induction motor has a full load speed of 1425 rpm. Calculate (a) the synchronous speed (b) the slip, and (c) the rotor frequency.

### Solution

(a) The synchronous speed  $N_s$  is

$$N_s = \frac{120f}{P} = \frac{120 \times 50}{4} = 1500 \text{ rpm}$$

$$\omega_s = \frac{2\pi N_s}{60} = \frac{4\pi f}{P} = 157 \text{ rad/sec}$$

(b) The slip  $s$  is

$$s = \frac{N_s - N_m}{N_s} = \frac{1500 - 1425}{1500} = 0.05 \text{ pu} = 5\%$$

(c) The rotor frequency  $f_r$  is

$$f_r = sf = 0.05 \times 50 = 2.5 \text{ Hz}$$





# DEVELOPMENT OF EQUIVALENT CIRCUIT

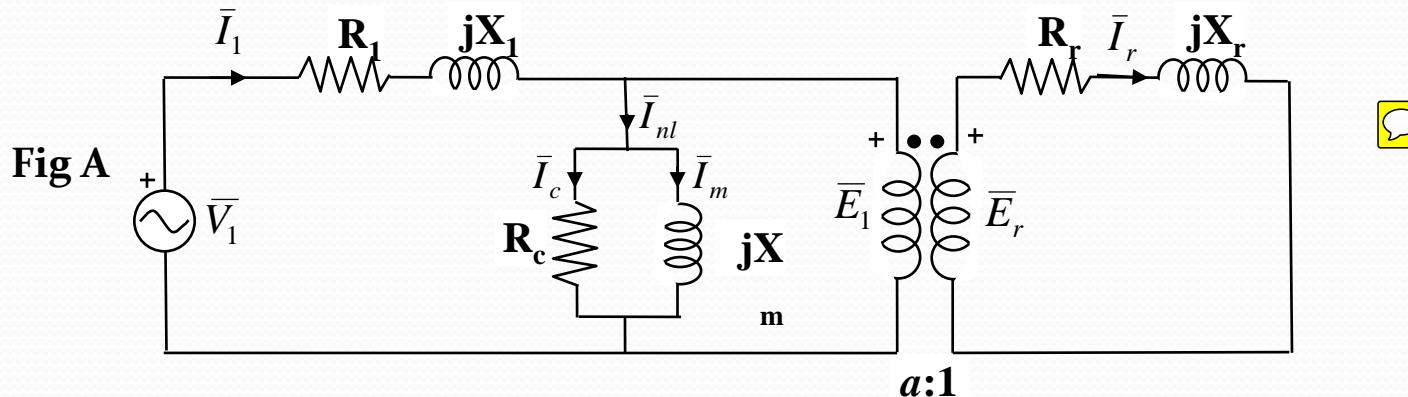
- When a 3-phase induction motor is connected to a balanced 3-phase supply, it draws a balanced 3-phase current (stator phase currents are equal in magnitude but shifted by  $120^\circ$  from others)
- A rotating magnetic field is created as explained earlier.
- At standstill (when  $N_m = 0$ , or  $s = 1$ ), an induction motor can be considered as a transformer with secondary short circuited.
- Balanced 3-phase voltages and therefore balanced 3-phase currents flow in the rotor.
- The rotating magnetic field and the rotor currents produce torque which makes the rotor rotate, but at a speed lower than synchronous speed. At synchronous speed, there is no induced emf, and so no rotor current and therefore no torque developed.
- The stator and rotor windings are coupled inductively and thus a 3-phase induction motor resembles a 3-phase transformer with rotating secondary windings
- The frequency of rotor current  $f_r$  is proportional to slip  $s$  ( $f_r = sf$ )





# DEVELOPMENT OF EQUIVALENT CIRCUIT

- The per phase equivalent circuit of a 3-phase induction motor is shown in Fig. a and is similar to the equivalent circuit of a transformer with secondary short-circuited



$V_1$  = per phase stator supply voltage

$R_1$  = per phase stator winding resistance

$X_1$  = per phase stator winding leakage reactance

$R_c$  = per phase equivalent core-loss resistance

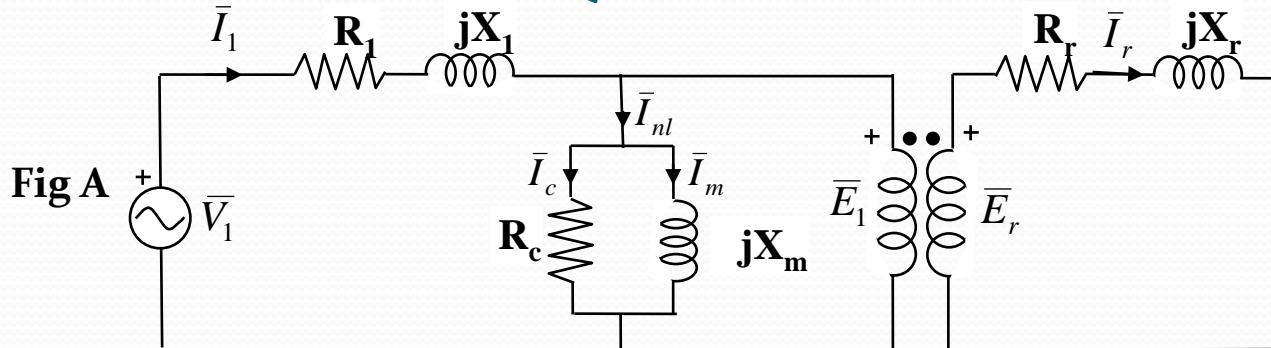
$X_m$  = per phase magnetizing reactance

$E_1 = 4.44 f N_1 k_{w1} \varphi_m$  = per phase stator induced voltage





# DEVELOPMENT OF EQUIVALENT CIRCUIT



$E_b = 4.44 f N_2 k_{w2} \varphi_m$  = per phase rotor induced voltage under **blocked** rotor condition ( $s = 1$ )



$E_r = s E_b$  = per phase rotor induced voltage at slip  $s$

$R_r$  = per phase rotor winding resistance

$X_b$  = per phase rotor winding leakage reactance under **blocked** rotor condition ( $s = 1$ )

$X_r = s X_b$  = per phase rotor winding leakage reactance at slip  $s$

$N_1$  and  $N_2$  are the number of turns in the stator and rotor windings

$k_{w1}$  and  $k_{w2}$  are the stator and rotor winding factors

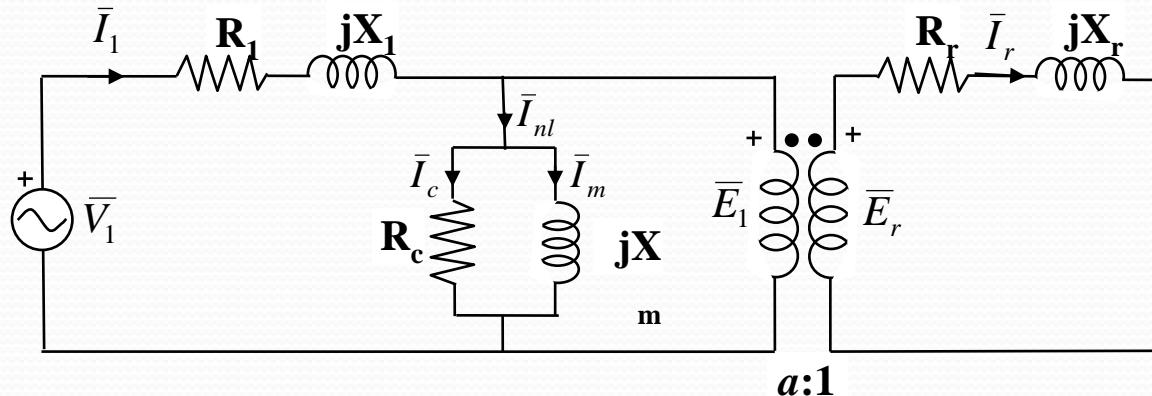
Note that  $E_r$  and  $X_r$  depend on frequency and hence slip  $s$





# DEVELOPMENT OF EQUIVALENT CIRCUIT

Fig A



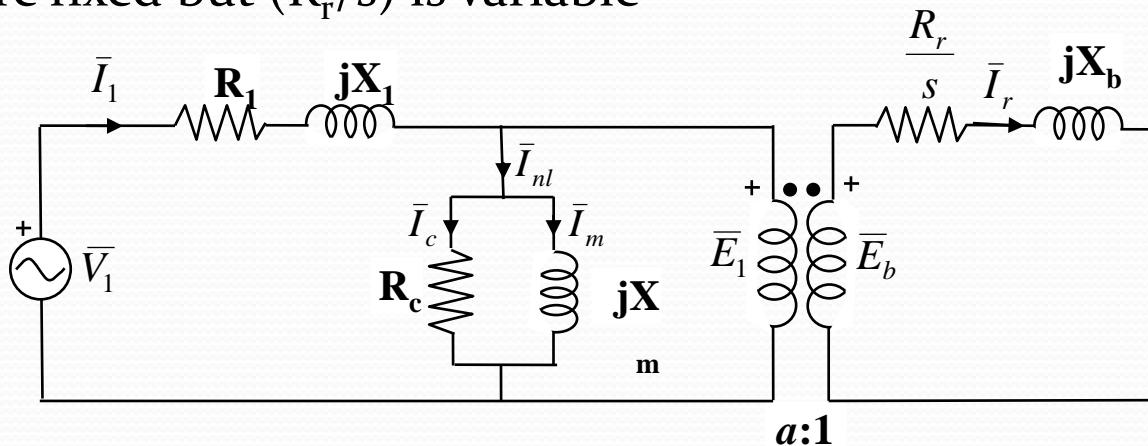
- The rotor current in the circuit is given by  $\bar{I}_r = \frac{\bar{E}_r}{R_r + jX_r}$
- Noting that  $\bar{E}_r = s\bar{E}_b$  and  $X_r = sX_b$ , the expression can be written as
$$\bar{I}_r = \frac{s\bar{E}_b}{R_r + jsX_b} = \frac{\bar{E}_b}{\frac{R_r}{s} + jX_b}$$
- Based on the above equation, a modified equivalent circuit (as shown in the Fig. B in the next page) of the motor can be developed



# DEVELOPMENT OF EQUIVALENT CIRCUIT

- In the first Fig. A,  $E_r$  and  $X_r$  are variable (depends on slip  $s$ ). In Fig. B,  $E_r$  and  $X_b$  are fixed but  $(R_r/s)$  is variable

**Fig B**



- The hypothetical resistance  $\frac{R_r}{s}$  in the rotor circuit is called **effective rotor resistance**
- At stand still (or blocked rotor condition),  $s = 1$  and thus the effective rotor resistance is the same as the actual rotor resistance  $R_r$
- At no load, the slip  $s$  approaches to zero and thus the effective rotor resistance approaches to infinity (very high)

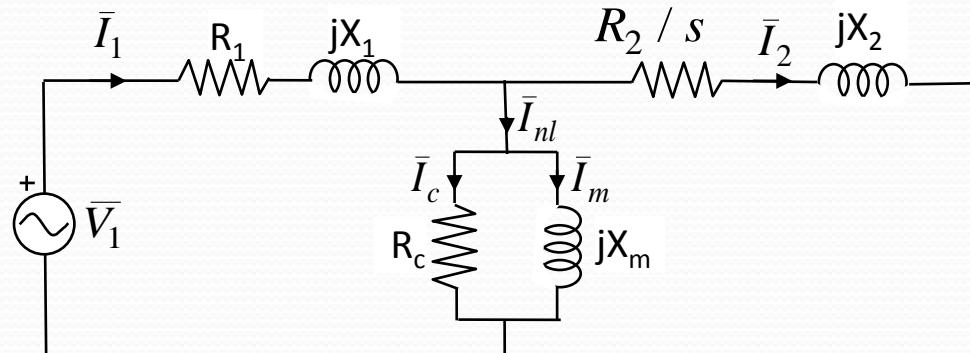


# DEVELOPMENT OF EQUIVALENT CIRCUIT

- Transfer the rotor quantities to the stator (similar to transformer) by using the effective turn ratio ‘ $a$ ’
- Let,  $R_2 = a^2 R_r$  and,  $X_2 = a^2 X_b$

Then, the per phase equivalent circuit of the motor referred to the stator becomes

Fig C1



- The above circuit shown in Fig C1 is called the **exact equivalent circuit** of an induction motor
- The effective rotor resistance  $R_2 / s$  (referred to the stator) in the above figure can be split into two components:

$$R_2 / s = R_2 + (1 - s)R_2 / s$$

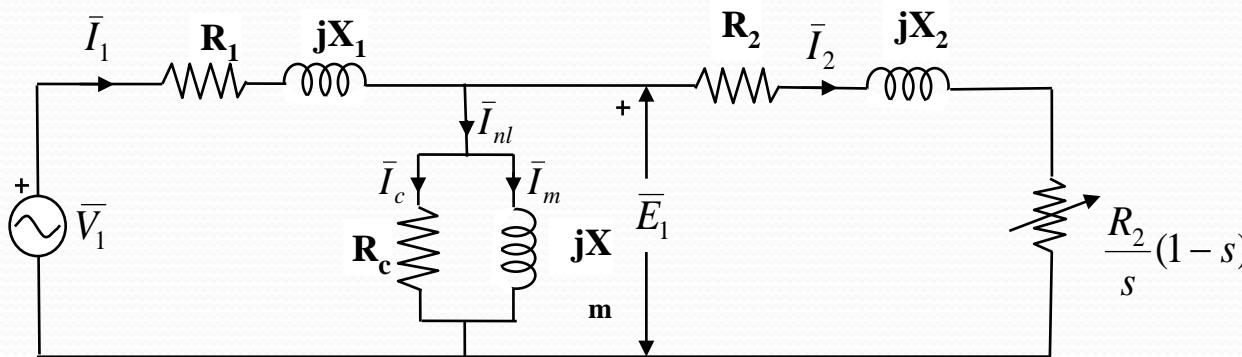




# DEVELOPMENT OF EQUIVALENT CIRCUIT

- The equivalent circuit of the motor showing two components of resistance is shown in Fig. C<sub>2</sub>

Fig C<sub>2</sub>



- Where:



$R_2$  is the actual rotor resistance of the rotor, and  
 $\frac{R_2}{s}(1-s)$  is the 'Fictitious' load resistance:

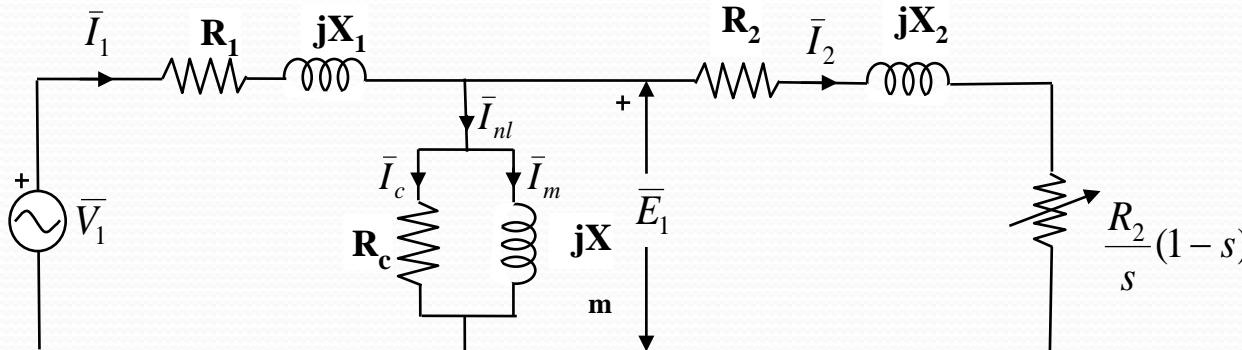
- Note that the sum of above two resistances is always  $R_2/s$
- The value of fictitious load resistance depends on slip (or motor speed) but the actual rotor resistance is independent of slip  $s$





# DEVELOPMENT OF EQUIVALENT CIRCUIT

Fig C2



- The fictitious load resistance in Fig. C emulates the **mechanical load** of the motor in electrical equivalent circuit
- The power absorbed by the load resistance represents the **mechanical power developed** ( $P_d$ ) by the motor. It is the power which is converted from electrical to mechanical

$$\therefore P_d = I_2^2 \frac{R_2}{s} (1-s) \text{ W}$$

- The above figure (Fig. C) is exactly the same as the exact equivalent circuit of a transformer delivering power to a load resistance of

$$\frac{R_2}{s} (1-s) \Omega$$





## Example

A 440-V, 50-Hz, Y-connected, 4-pole, 3-phase IM has  $R_r = 0.02 \Omega/\text{phase}$  and  $X_b = 0.06 \Omega/\text{phase}$  at stand still. The effective turn ratio 'a' is 5. Determine (a) the rotor resistance  $R_2$  referred to the stator, (b) the fictitious load resistance when the motor runs at 1450 rpm, at starting, and at synchronous speed.

### Solution

Here  $R_r = 0.02 \Omega/\text{phase}$ , and  $X_b = 0.06 \Omega/\text{phase}$

$$\text{Synchronous speed } N_s = \frac{120f}{P} = \frac{120 \times 50}{4} = 1500 \text{ rpm}$$

(a) The rotor resistance ( $R_2$ ) referred to the stator is

$$R_2 = a^2 R_r = 5^2 \times 0.02 = 0.50 \Omega/\text{phase}$$

(b) Slip  $s = \frac{N_s - N_m}{N_s}$  pu

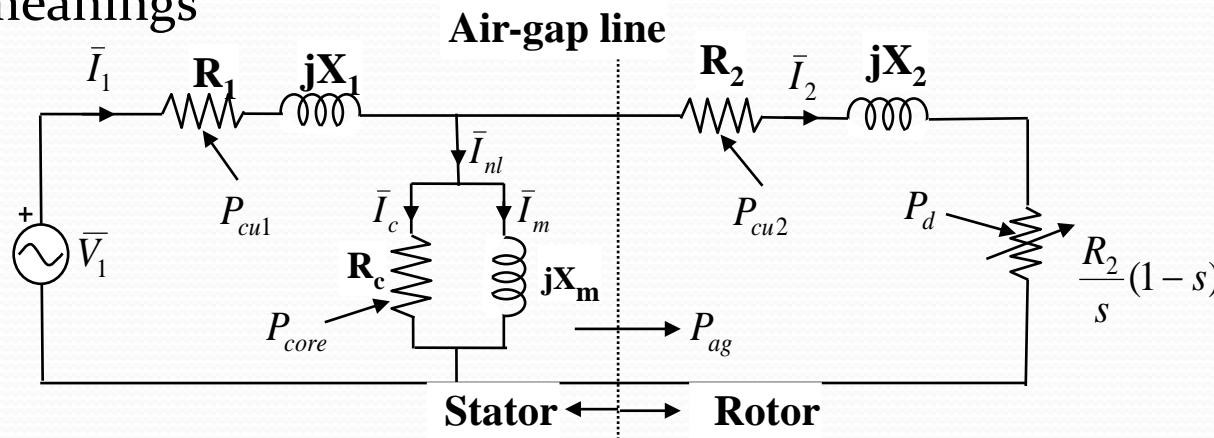
$$\text{Fictitious load resistance } R_{Load} = \frac{R_2}{s} (1-s) \Omega$$

$N_m$ (rpm)	1450	0 (Starting)	1500 (syn speed)
Slip $s$ (pu)	0.033333	1	0
$R_{Load}$ ( $\Omega$ )	14.5	0	$\infty$



# Power Associated with Various Resistances

- There are four resistances in the final equivalent circuit (Fig. C) of an induction motor and the power absorbed by these resistances has some special meanings

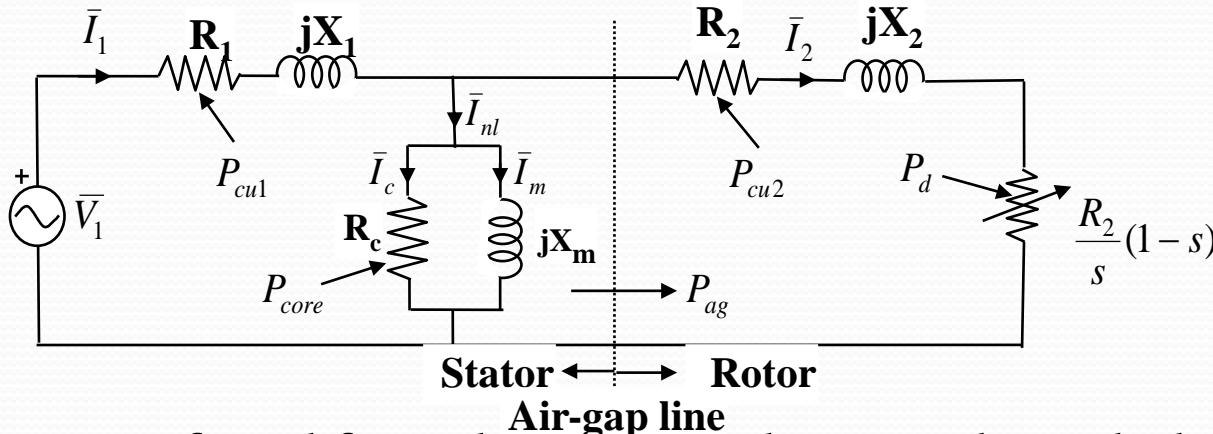


$I_1^2 R_1$	: Per phase stator cu-loss ( $P_{cu1}$ )
$I_c^2 R_c = E_1^2 / R_c$	: Per phase core loss ( $P_{core}$ )
$I_2^2 R_2$	: Per phase rotor cu-loss ( $P_{cu2}$ )
$I_2^2 \frac{R_2}{s} (1-s)$	: Per phase mechanical developed power ( $P_d$ )





# Power Associated with Various Resistances



- The power transferred from the stator to the rotor through the air-gap is called the 'Air-gap power'. So the air-gap power consists of the sum of rotor cu-loss ( $P_{cu2}$ ) and developed power ( $P_d$ ). Thus,

$I_2^2 R_2$	: Per phase rotor cu-loss ( $P_{cu2}$ )
$I_2^2 \frac{R_2}{s} (1-s)$	: Per phase developed mechanical power ( $P_d$ ) 
$I_2^2 \frac{R_2}{s}$	: Per phase air gap power ( $P_{ag}$ )

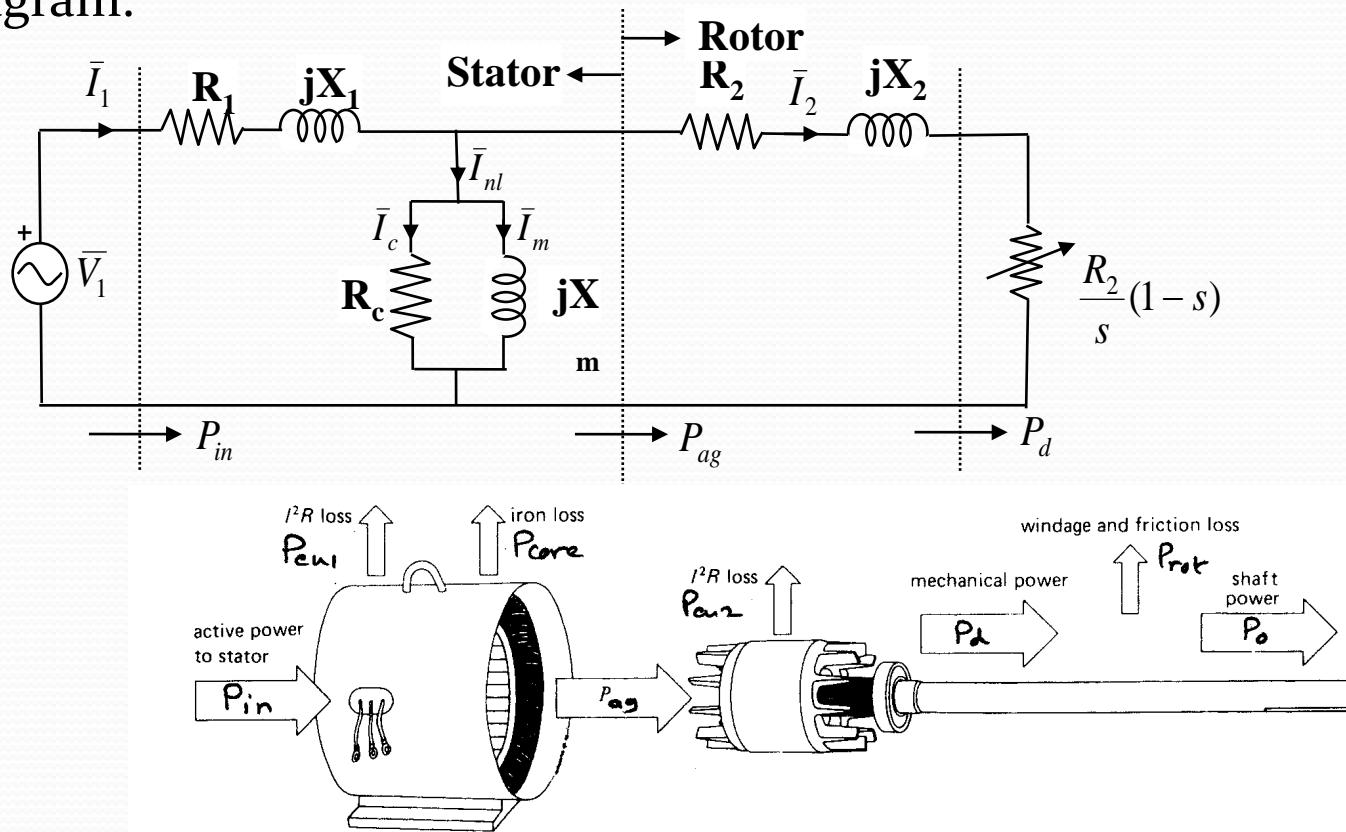
- Note that the above equivalent circuit is on per phase basis and proper relationships should be used to get the total power and line quantities.





# Power Flow Diagram

- The equivalent circuit enables us to understand the detailed behavior of an induction motor. However, it is easier to see how electrical energy (or power) is converted into mechanical energy (or power) in the power flow diagram.





## Example

A 10-hp, 4-pole, 440-V, 50-Hz, Y-connected, 3-phase induction motor runs at 1440 rpm on full load ( $P_{out} = 10 \text{ hp}$ ). The core loss is 200 W and rotational loss is 340 W. The stator copper loss at full load is 215 W. Determine the following quantities at full load: (a) developed power, (b) air-gap power, (c) rotor copper loss, (d) input power, (e) efficiency, and (f) shaft torque.

**Solution:** Output power  $P_{out} = 10 \text{ hp} = 7,460 \text{ W}$

Synchronous speed  $N_s = 120f/P = 1500 \text{ rpm; rad/sec}$

$$\text{Slip } s = \frac{N_s - N_m}{N_s} = \frac{1500 - 1440}{1500} = 0.04 \text{ pu} = 4\%$$

$$P_{core} = 200 \text{ W}, \quad P_{rot} = 340 \text{ W, and} \quad P_{cu1} = 215 \text{ W}$$

$$(a) \text{ Developed power: } P_d = P_{out} + P_{rot} = 7,460 + 340 = 7,800 \text{ W}$$

$$(b) \text{ Air-gap power: } P_{ag} = P_d / (1-s) = 7800 / 0.96 = 8,125 \text{ W}$$

$$(c) \text{ Rotor copper loss: } P_{cu2} = sP_{ag} = 0.04 \times 8,125 = 325 \text{ W}$$

$$(d) \text{ Input power: } P_{in} = (P_{ag} + P_{cu1} + P_{core}) = (8,125 + 215 + 200) = 8,540 \text{ W}$$

$$(e) \text{ Efficiency } \eta = \frac{P_{out}}{P_{in}} \times 100\% = \frac{7,460}{8,540} \times 100\% = 87.35\%$$

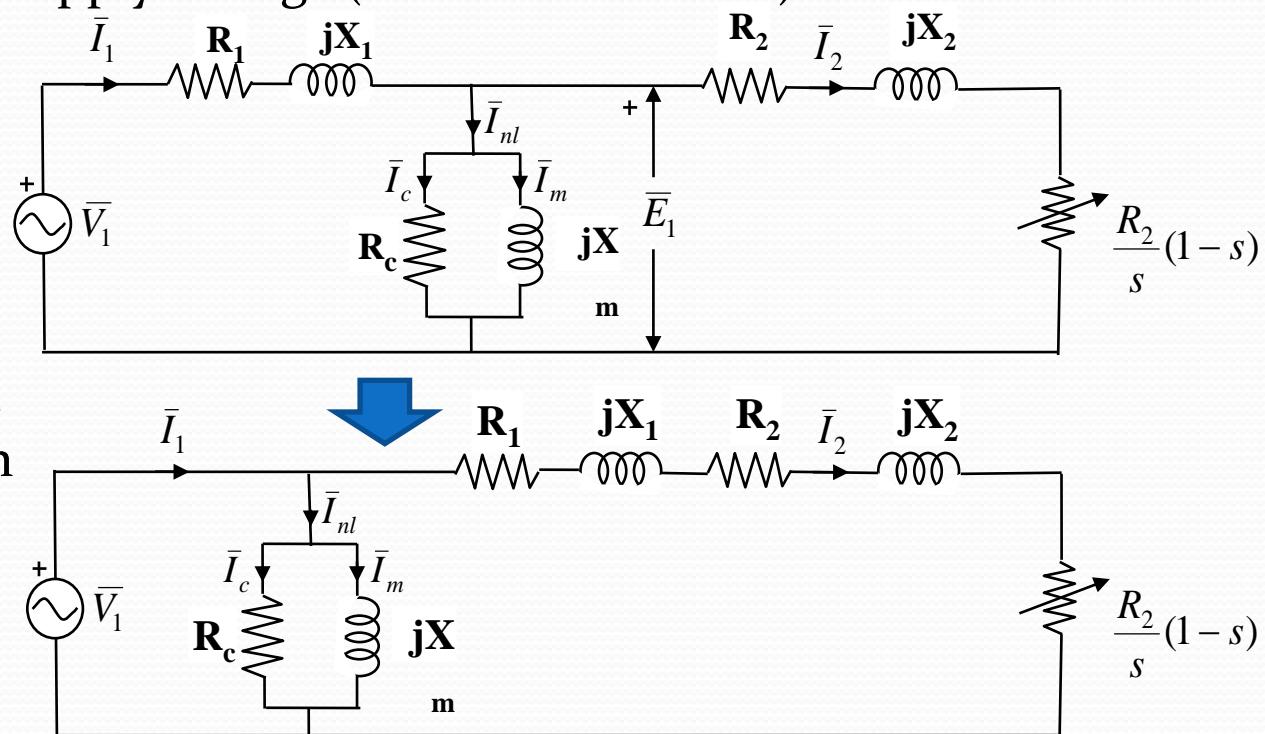
$$(f) \text{ Shaft torque = output torque } = T_s = T_{out} = \frac{P_{out}}{\omega_m} = \frac{7,460}{2\pi \times 1440 / 60} = 49.47 \text{ Nm}$$





# Approximate Equivalent Circuit

- The performance of an induction motor can be determined from its equivalent circuit – almost exactly the same way as for transformers.
- The approximate equivalent circuit is obtained by removing the shunt impedance ( $R_c$  in parallel with  $jX_m$ ) from middle of the exact circuit and placing it across the supply voltage (as in transformers).
- Determination of motor behaviors/ characteristics from approximate eq. circuit becomes much simpler and it provides results with reasonably small errors for well designed motors.





## Example

A 8-pole, 440-V, 50-Hz, Y-connected, 3-phase induction motor has the following parameters on a per phase basis:  $R_1 = 0.4 \Omega$ ,  $R_2 = 0.5 \Omega$ ,  $X_1 = 1.1 \Omega$ ,  $X_2 = 1.1 \Omega$ ,  $R_c = 350 \Omega$ , and  $X_m = 60 \Omega$ . The rotational loss is 250 W. Using the approximate equivalent circuit, determine the (a) input current, (b) power factor, (c) air-gap power, (d) developed torque, and (e) efficiency of the motor when it runs at a slip of 5%.

**Solution:**

Here

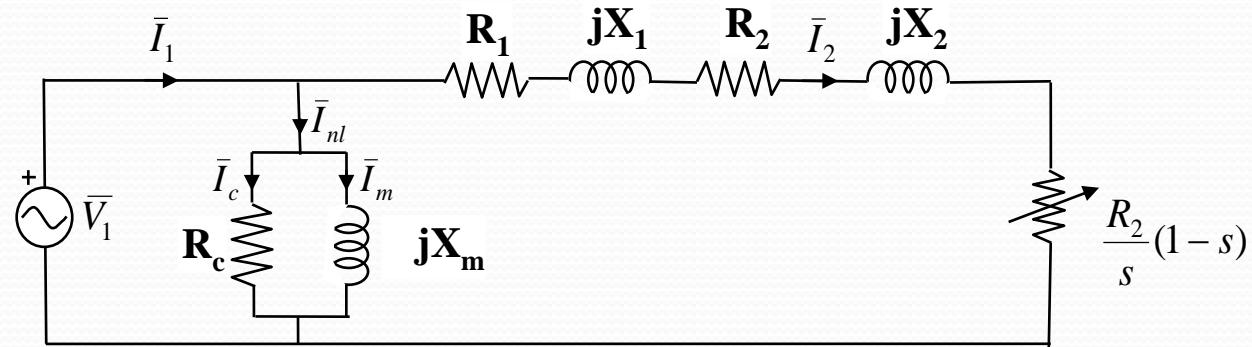
$$\begin{aligned} Z_1 &= (R_1 + jX_1) \\ &= (0.4 + j1.1) \Omega, \end{aligned}$$

$$Z_2 = (R_2/s + jX_2)$$

$$= (0.5/0.05 + j1.1) = (10 + j1.1) \Omega$$

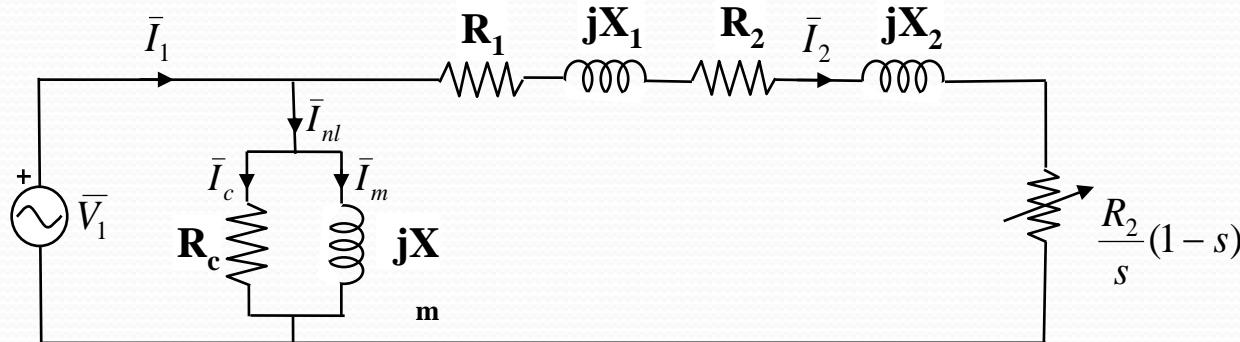
$$\bar{I}_2 = \frac{\bar{V}_1}{(\bar{Z}_1 + \bar{Z}_2)} = \frac{254 \angle 0^\circ}{(10.4 + j2.2)} = 23.89 \angle -11.944^\circ A$$

$$\bar{I}_{nl} = \left( \frac{\bar{V}_1}{R_c} + \frac{\bar{V}_1}{jX_m} \right) = (0.7257 - j4.233) A$$





## Example Solution:



- (a) Input current:  $\bar{I}_1 = (\bar{I}_{nl} + \bar{I}_2) = 25.786 \angle -20.85^\circ \text{ A}$
- (b) Power factor:  $pf = \cos(-20.85^\circ) = 0.934 \text{ (lagging)}$
- (c) Air-gap power:  $P_{ag} = 3I_2^2 \frac{R_2}{s} = 3 \times 23.89^2 \times \frac{0.5}{0.05} = 17.122 \text{ W}$
- (d) Developed torque:  $T_d = \frac{P_{ag}}{\omega_s} = \frac{17,122}{78.54} = 218 \text{ Nm}$
- (e) Developed power:  $P_d = (1-s)P_{ag} = 16.266 \text{ kW}$
- (f) Output power:  $P_{out} = (P_d - P_{rot}) = (16.266 - 0.25) = 16.02 \text{ kW}$
- (g) Input power:  $P_{in} = 3V_1 I_1 \cos\theta_1 = 3 \times 254 \times 25.786 \times \cos(-20.85) = 18.36 \text{ kW}$
- (h) Efficiency:  $\eta = \frac{P_{out}}{P_{in}} \times 100\% = \frac{16.02}{18.362} \times 100\% = 87.24\%$





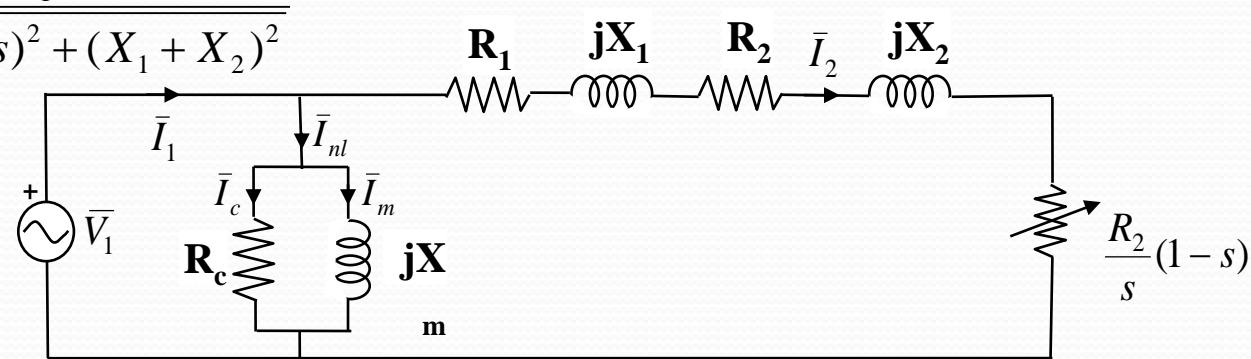
# Torque-Speed Characteristic

- Torque-speed characteristics showing the variation of torque with the speed of the motor is the most important characteristics of motors.
- Approximate equivalent can be used to for this purpose:

$$1. \quad I_2 = \frac{V_1}{\sqrt{(R_1 + R_2/s)^2 + (X_1 + X_2)^2}}$$

$$2. \quad P_{ag} = 3I_2^2 \frac{R_2}{s}$$

$$3. \quad T_d = \frac{P_{ag}}{\omega_s}$$



Thus the developed torque can be expressed as:

$$T_d = \frac{3}{\omega_s} \times \frac{V_1^2}{(R_1 + R_2/s)^2 + (X_1 + X_2)^2} \times \frac{R_2}{s} \text{ Nm}$$

which shows very non linear relationship between torque  $T_d$  and speed reflected in slip  $s$ .





# Torque-Speed Characteristic

- For small values  $s$ ,

$$T_d = \frac{3}{\omega_s} \times \frac{V_1^2}{(R_1 + R_2/s)^2 + (X_1 + X_2)^2} \times \frac{R_2}{s} \text{ Nm}$$

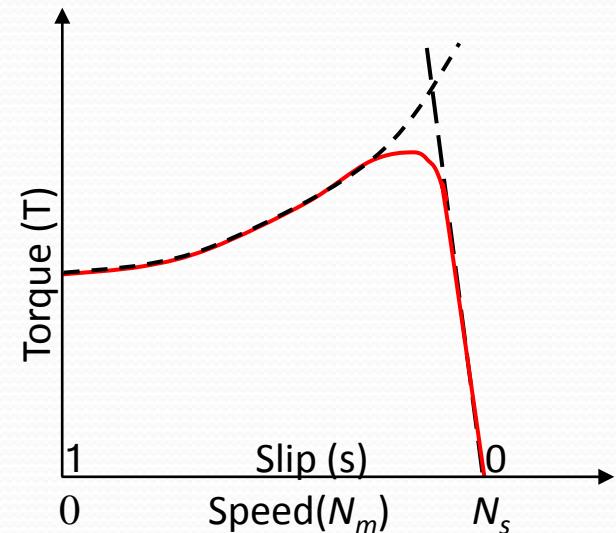
$$\approx \frac{3V_1^2}{\omega_s} \times \frac{1}{(R_2/s)^2 + (X_1 + X_2)^2} \times \frac{R_2}{s}$$

$$\approx \frac{3V_1^2}{\omega_s} \times \frac{1}{(R_2/s)^2} \times \frac{R_2}{s} = \frac{3V_1^2}{\omega_s} \times \frac{s}{R_2} \propto s$$

- For large values of  $s$ ,

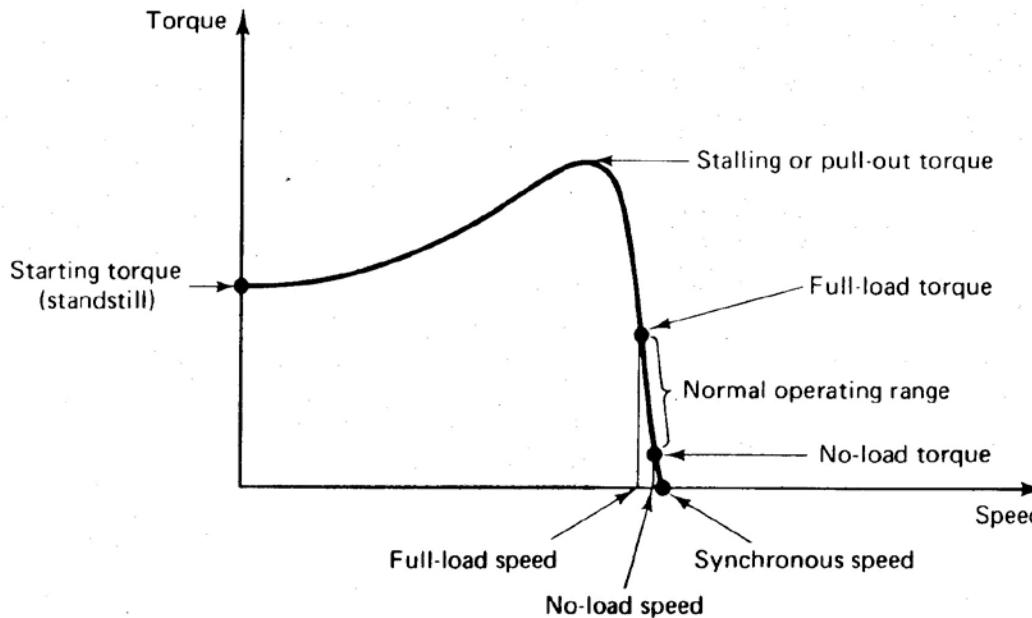
$$T_d = \frac{3}{\omega_s} \times \frac{V_1^2}{(R_1 + R_2/s)^2 + (X_1 + X_2)^2} \times \frac{R_2}{s} \text{ Nm}$$

$$\approx \frac{3}{\omega_s} \times \frac{V_1^2}{(X_1 + X_2)^2} \times \frac{R_2}{s} \propto \frac{1}{s}$$



# Torque-Speed Characteristic

- A typical torque-speed characteristic of an IM is shown below. Note that motor speed  $N_m = (1 - s)N_s$



- The important features of the characteristics are shown in the diagram.
- Starting Torque: at  $N_m = 0$  or  $s = 1$

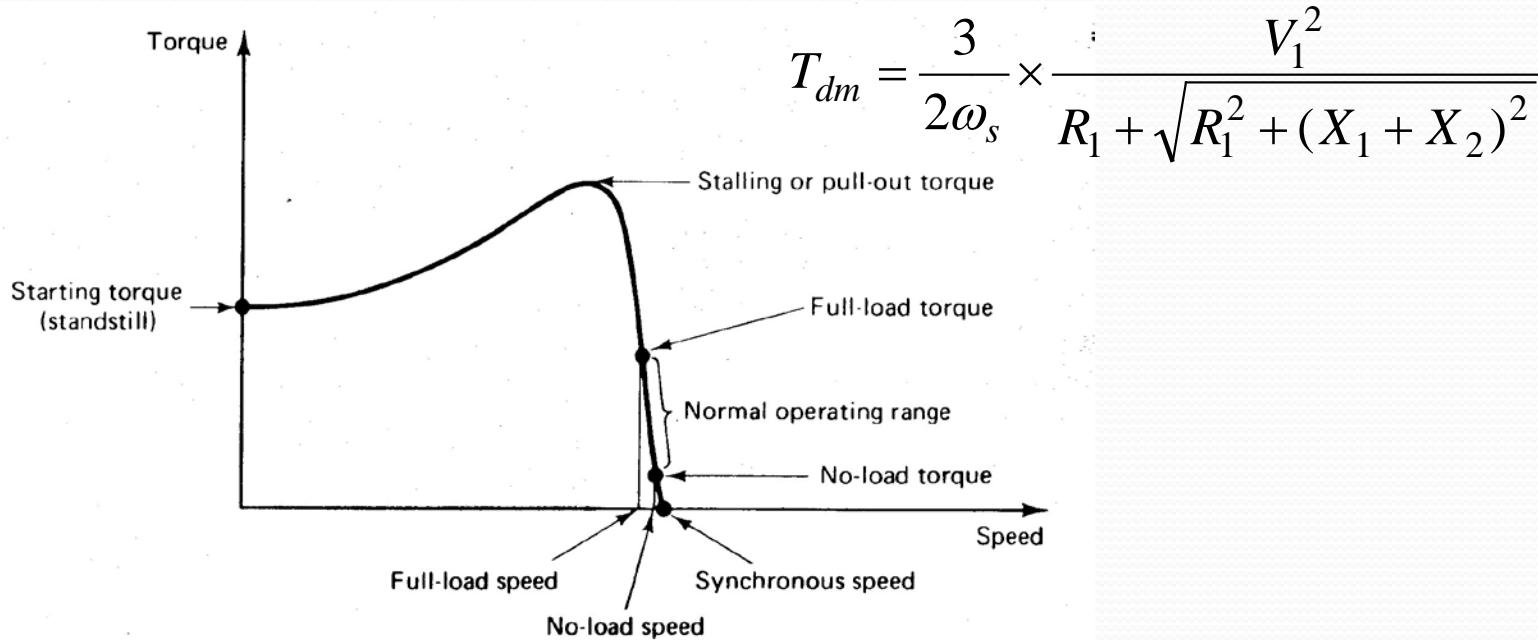
$$T_d = \frac{3}{\omega_s} \times \frac{V_1^2}{(R_1 + R_2)^2 + (X_1 + X_2)^2} \times R_2 \text{ Nm}$$

Important for motors which need to start under load.



# Important Features of T-Speed Characteristic

- Maximum Torque: (or pull out torque) can be shown to be:



- The motor will not operate beyond this load torque.
- The operating range of induction motors is very narrow. The speed can vary over a limited range. Constant speed motors.
- Methods of speed control is very important for induction motors.



# Determination of Equivalent Circuit Parameters

- The procedure of determining the equivalent circuit parameters of an induction motor is very similar to that of a transformer
- For an induction motor, usually the parameters of the exact equivalent circuit (instead of approximate equivalent circuit) are determined
- Two tests are conducted:
  - **Blocked-rotor Test**  
It is also called **locked-rotor test** and is very similar to the short circuit test of a transformer.
  - **No-load Test**  
Conducted at rated voltage without any load (disconnecting the load from the motor shaft) and is very similar to open circuit test of a transformer.
- Some extra measurements such as the stator resistance are also conducted.
- The calculation methods are very similar to that of transformer tests.





# Speed Control

- Motor speed  $N_m$  is given by

$$N_m = (1-s)N_s = (1-s) \times \frac{120f}{P} \Rightarrow N_m = \frac{120(1-s)f}{P}$$

- Possible Methods of Speed Control are:

- By changing supply frequency ( $f$ )
- By changing number of poles ( $P$ )
- By changing slip ( $s$ )

Changing the supply frequency is most commonly used

- Advantages

- Suitable for both squirrel-cage and wound-rotor motors
- Wide range of speed control is possible

- Disadvantages

Requires additional equipment (called inverter) to convert DC power into AC power of variable frequency. DC power can be obtained from normal AC supply by using a rectifier.

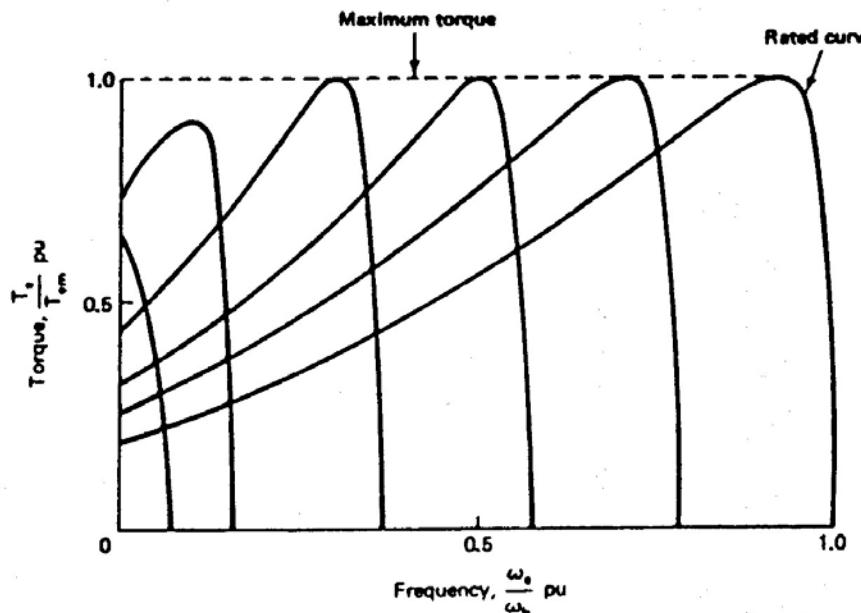




# Speed Control: Modes of operation

(a) Keeping  $V/f$  ratio constant

- Since  $E_1 \approx V_1$  (neglect stator leakage impedance voltage drop)
- When  $V/f$  ratio is kept constant, flux  $\phi_m$  also remains constant and it provides constant maximum torque capability. This technique is used when  $f < f_{rated}$



Motor torque-speed characteristics for constant  $V/f$  ratio

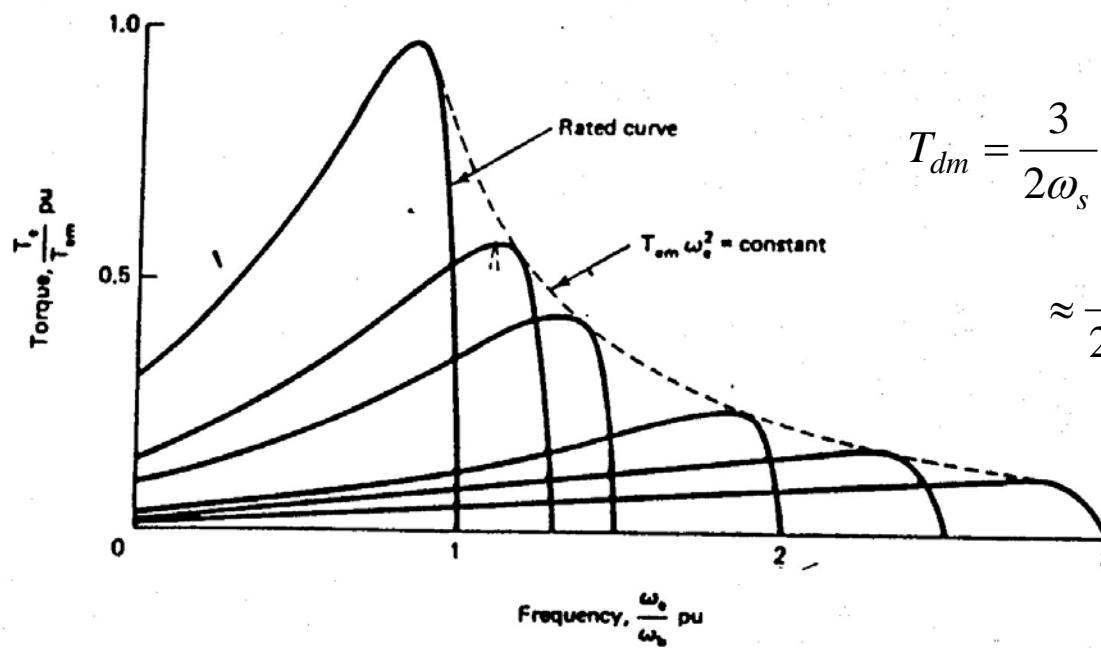
$$\begin{aligned}T_{dm} &= \frac{3}{2\omega_s} \times \frac{V_1^2}{R_1 + \sqrt{R_1^2 + (X_1 + X_2)^2}} \\ &\approx \frac{3}{2\omega_s} \times \frac{V_1^2}{(X_1 + X_2)}\end{aligned}$$



# Speed Control: Modes of operation

(a) Keeping V constant

- It is used when  $f > f_{rated}$
- At higher frequency ( $> f_{rated}$ ),  $\phi_m$  reduces for constant  $V_1$
- The maximum torque is also reduced



$$T_{dm} = \frac{3}{2\omega_s} \times \frac{V_1^2}{R_1 + \sqrt{R_1^2 + (X_1 + X_2)^2}}$$
$$\approx \frac{3}{2\omega_s} \times \frac{V_1^2}{(X_1 + X_2)}$$





## Example

A 440-V, 50-Hz, 4-pole, Y-connected, 3-phase induction motor has the following parameters on a per phase basis:  $R_1 = 0.3 \Omega$ ,  $R_2 = 0.6 \Omega$ ,  $X_1 = 0.9 \Omega$ ,  $X_2 = 0.9 \Omega$ ,  $R_c = 150 \Omega$ , and  $X_m = 60 \Omega$ . Using the approximate equivalent circuit, determine

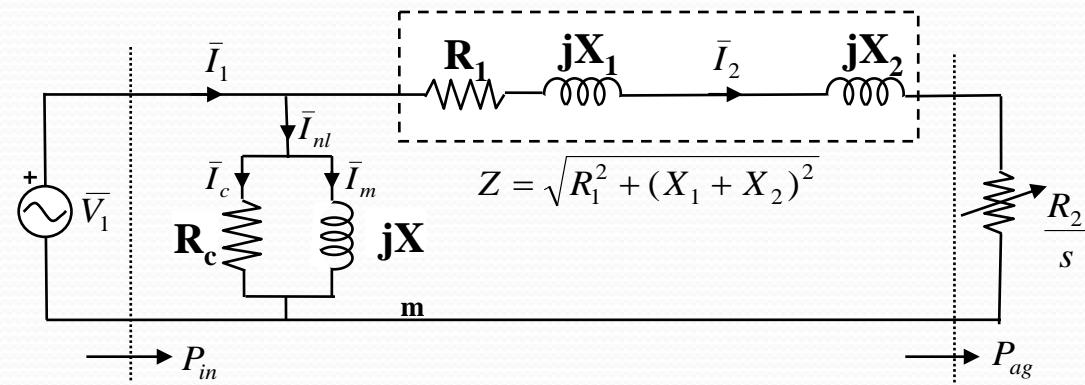
- the developed torque when the motor runs at 1450 rpm.
- the starting torque of the motor, and
- the slip and speed at which the motor develops the maximum torque, and therefore the value of maximum torque.

### Solution:

Synchronous speed

$$N_s = 120f/P = 1500 \text{ rpm};$$

$$\omega_s = 2\pi N_s / 60 = 157 \text{ rad/s}$$





## Example

(a) When  $N_m = 1450$  rpm, slip:  $s = \frac{N_s - N_m}{N_s} = \frac{1500 - 1450}{1500} = 0.0333$

Rotor current:

$$I_2 = \frac{V_1}{\sqrt{(R_1 + R_2 / s)^2 + (X_1 + X_2)^2}} = 13.82 \text{ A}$$

Air-gap power:

$$P_{ag} = 3I_2^2 \frac{R_2}{s} = 3 \times 12.82^2 \times \frac{0.6}{0.03333} = 10.31 \text{ kW}$$

Developed torque:

$$T_d = \frac{P_{ag}}{\omega_s} = \frac{10.31}{157} = 65.67 \text{ Nm}$$

(b) At starting,  $N_m = 0$  and hence  $s = 1$

Rotor current:

$$I_2 = \frac{V_1}{\sqrt{(R_1 + R_2 / s)^2 + (X_1 + X_2)^2}} = 126.24 \text{ A}$$

Air-gap power:

$$P_{ag} = 3I_2^2 \frac{R_2}{s} = 3 \times 218.64^2 \times \frac{0.6}{1} = 28.68 \text{ kW}$$

Developed torque:  $T_d = \frac{P_{ag}}{\omega_s} = \frac{28.68}{157} = 21.89 \text{ Nm}$

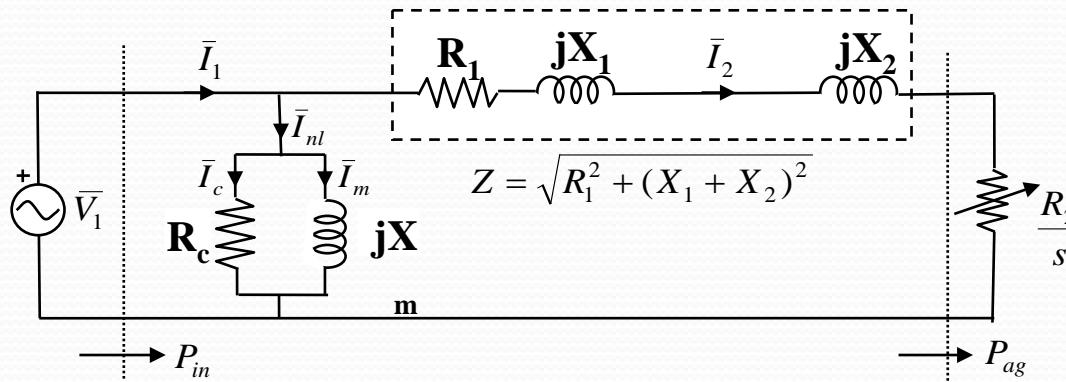




## Example:

(c) For maximum torque, it can be shown that:

$$\frac{R_2}{s_m} = \sqrt{R_1^2 + (X_1 + X_2)^2} \Rightarrow \frac{0.6}{s_m} = \sqrt{0.3^2 + (0.9 + 0.9)^2} \Rightarrow s_m = 0.3288 \text{ pu}$$



Corresponding motor speed  $N_m = (1 - s_m)N_s = 1006.8 \text{ rpm}$

When  $s = s_m = 0.3288$

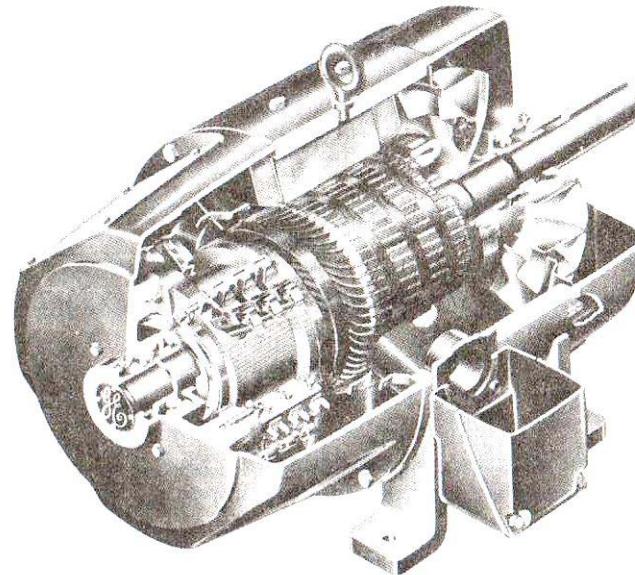
Rotor current:  $I_2 = \frac{V_1}{\sqrt{(R_1 + R_2/s)^2 + (X_1 + X_2)^2}} = 91.22 \text{ A}$

Air-gap power:  $P_{ag} = 3I_2^2 \frac{R_2}{s} = 3 \times 91.22^2 \times \frac{0.6}{0.3288} = 45.55 \text{ kW}$

Developed torque:  $T_d = \frac{P_{ag}}{\omega_s} = \frac{45.554}{157} = 290.17 \text{ Nm} = T_{dm}$



# **Introduction to Synchronous Generators and DC Machines**



**Dr. Govinda Bol Shrestha**  
**Visiting Professor**  
**Department of Electronics and Electrical Engineering**

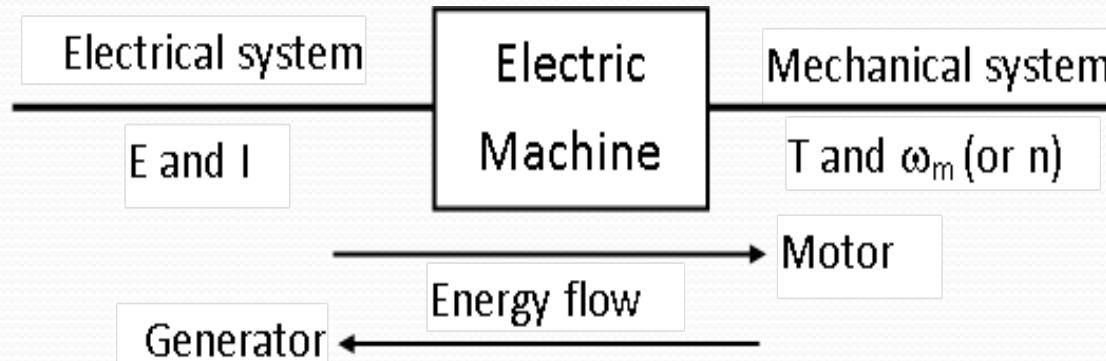




# Electric Machines

Generator: Converts mechanical energy into electrical energy

Motor: Converts electrical energy into mechanical energy



- AC Machines: Electrical system is AC
- DC Machines: Electrical system is DC

The coupling medium between the electrical and mechanical systems is magnetic field and is essential in all electromechanical energy conversion processes.





# Electromechanical Energy Conversion

Two basic electromagnetic processes in electromechanical energy conversion are:

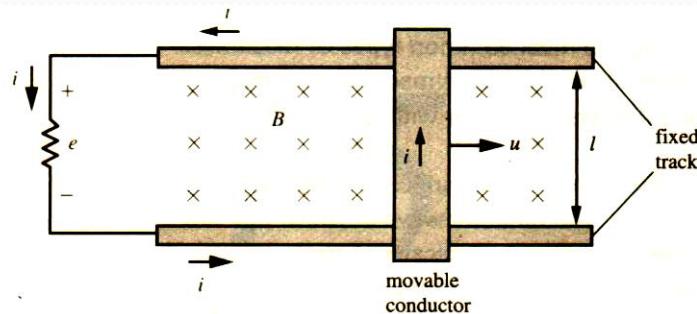
- A moving conductor in a magnetic field induces voltage. This is called **generator action**.
- A current carrying conductor in a magnetic field produces force or torque. This is called **motor action**.
- In all electric machines, both actions/processes take place simultaneously





# OPERATING PRINCIPLE – GENERATORS & MOTORS

## Generator



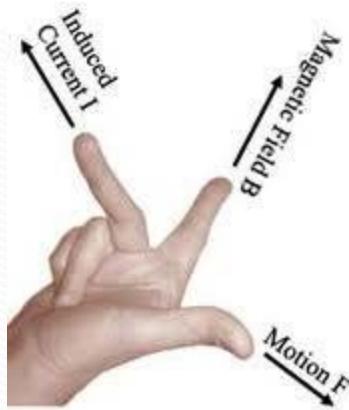
**Fig. 15.1** Simple generator.

Input:

Field –  $B$

Movement –  $u$

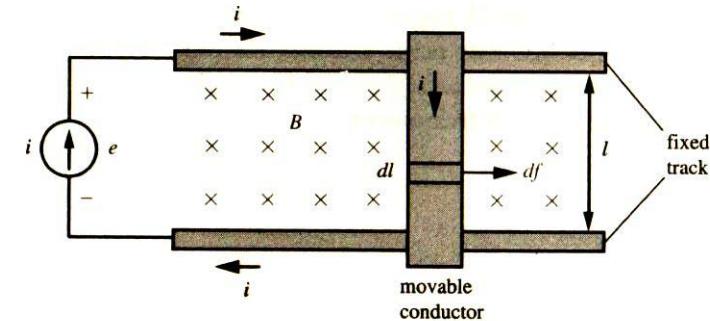
(Force or Torque)



Output –  $e$

$$e = \frac{d\lambda}{dt} = Blu$$

## Motor



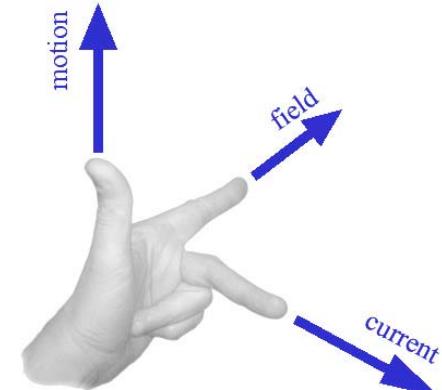
**Fig. 15.2** Simple motor.

Input:

Field –  $B$

Current –  $I$

(Voltage)

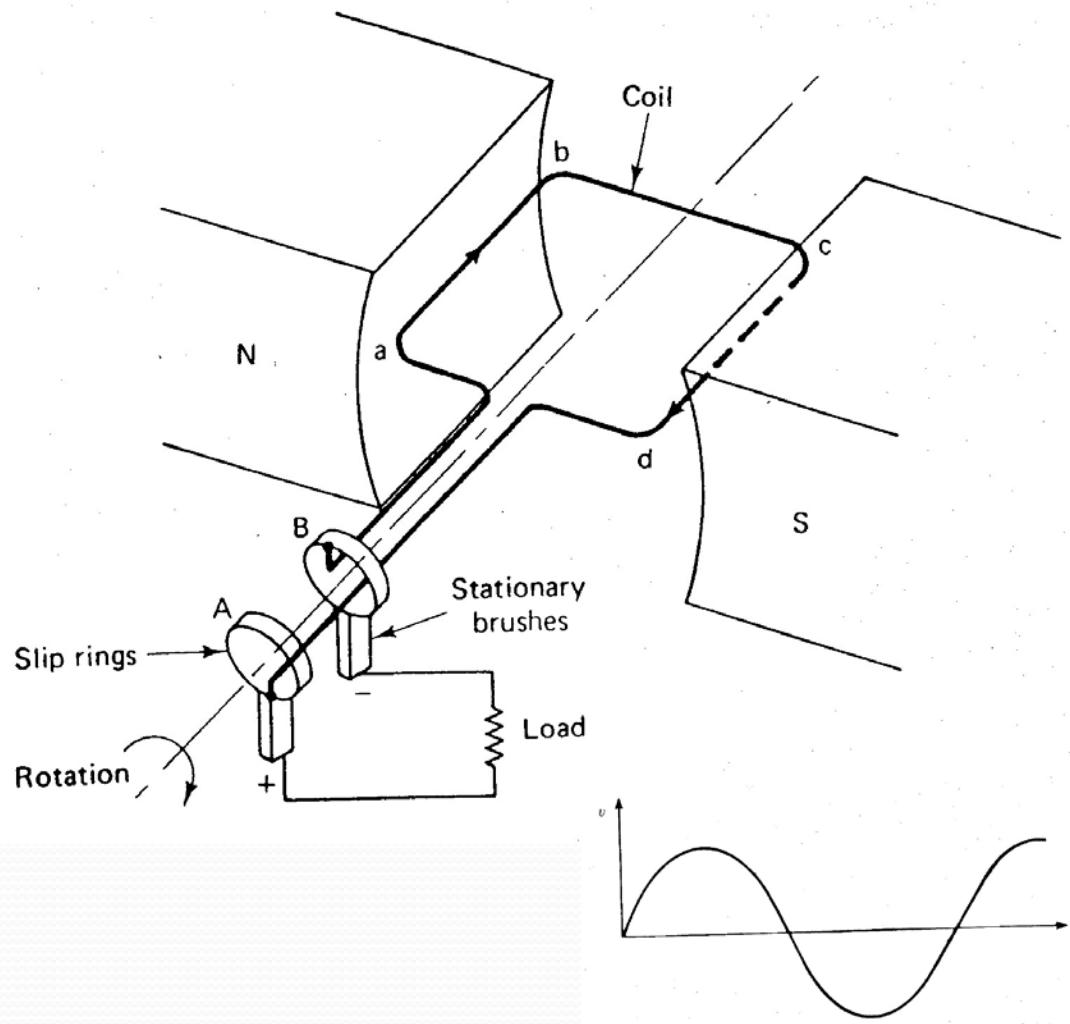


Output –  $F$  or Torque

$$F = \int Bidl = Bil$$

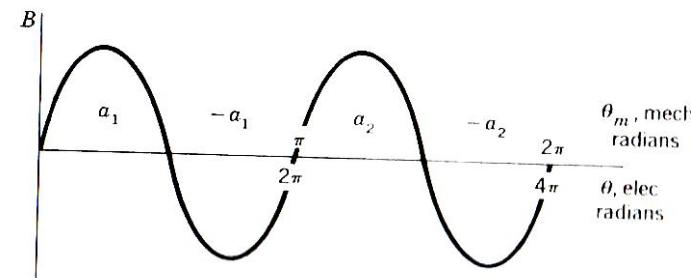
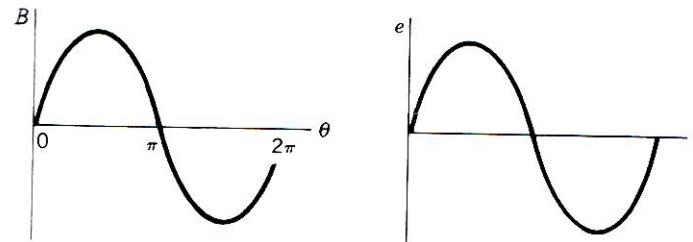
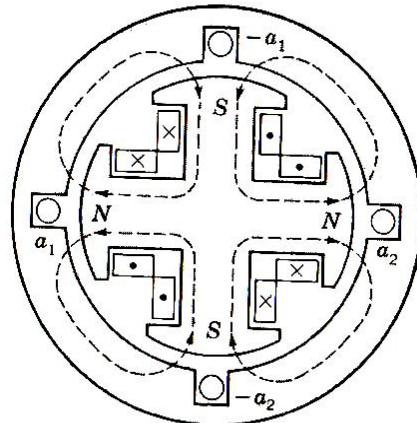
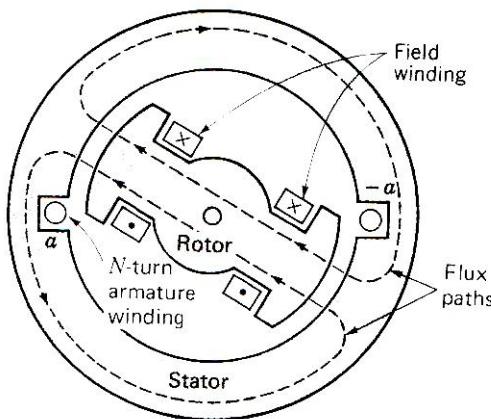


# A Simple Generator





# Synchronous Generators



# Synchronous Generators

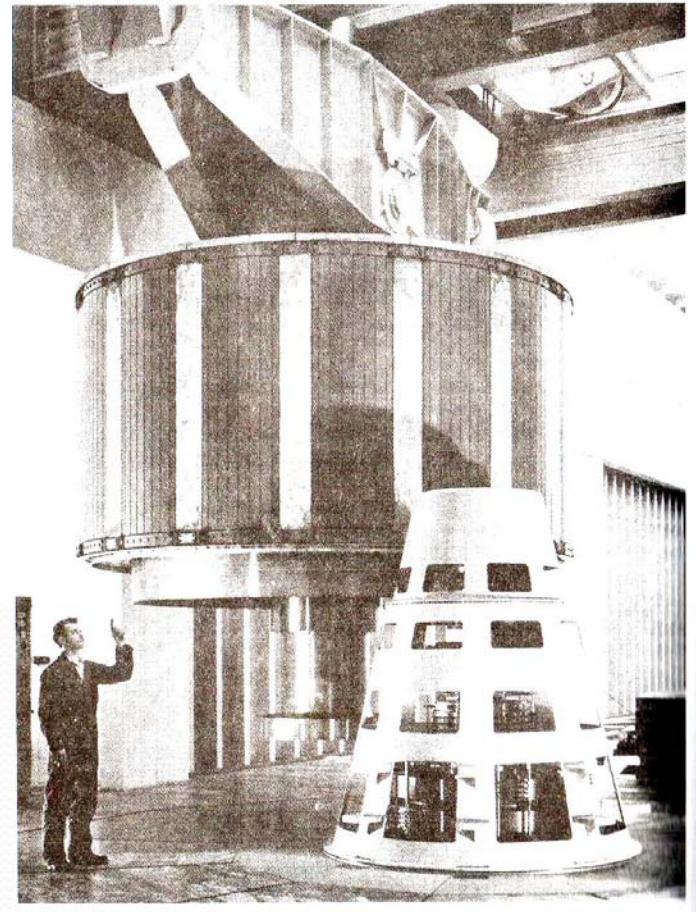
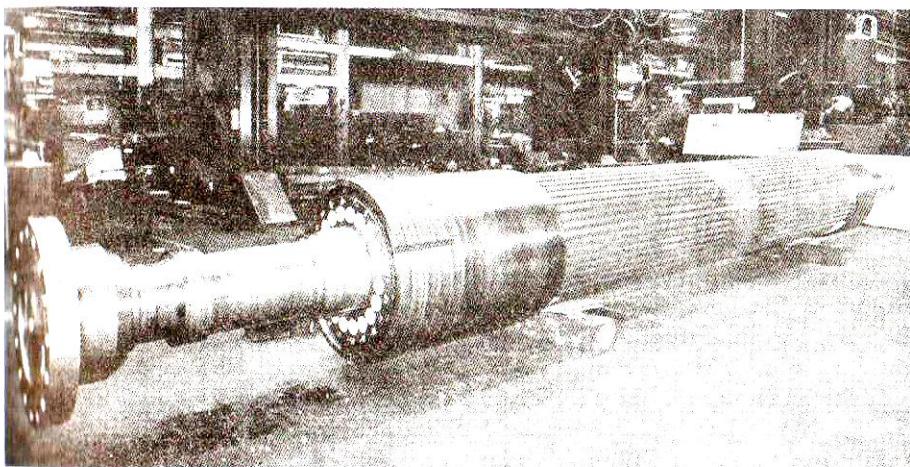
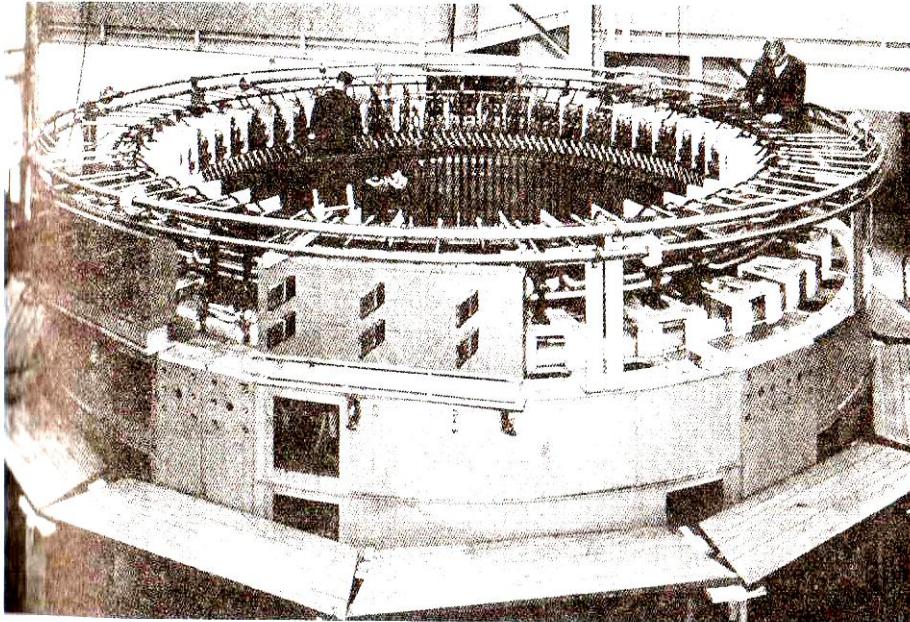
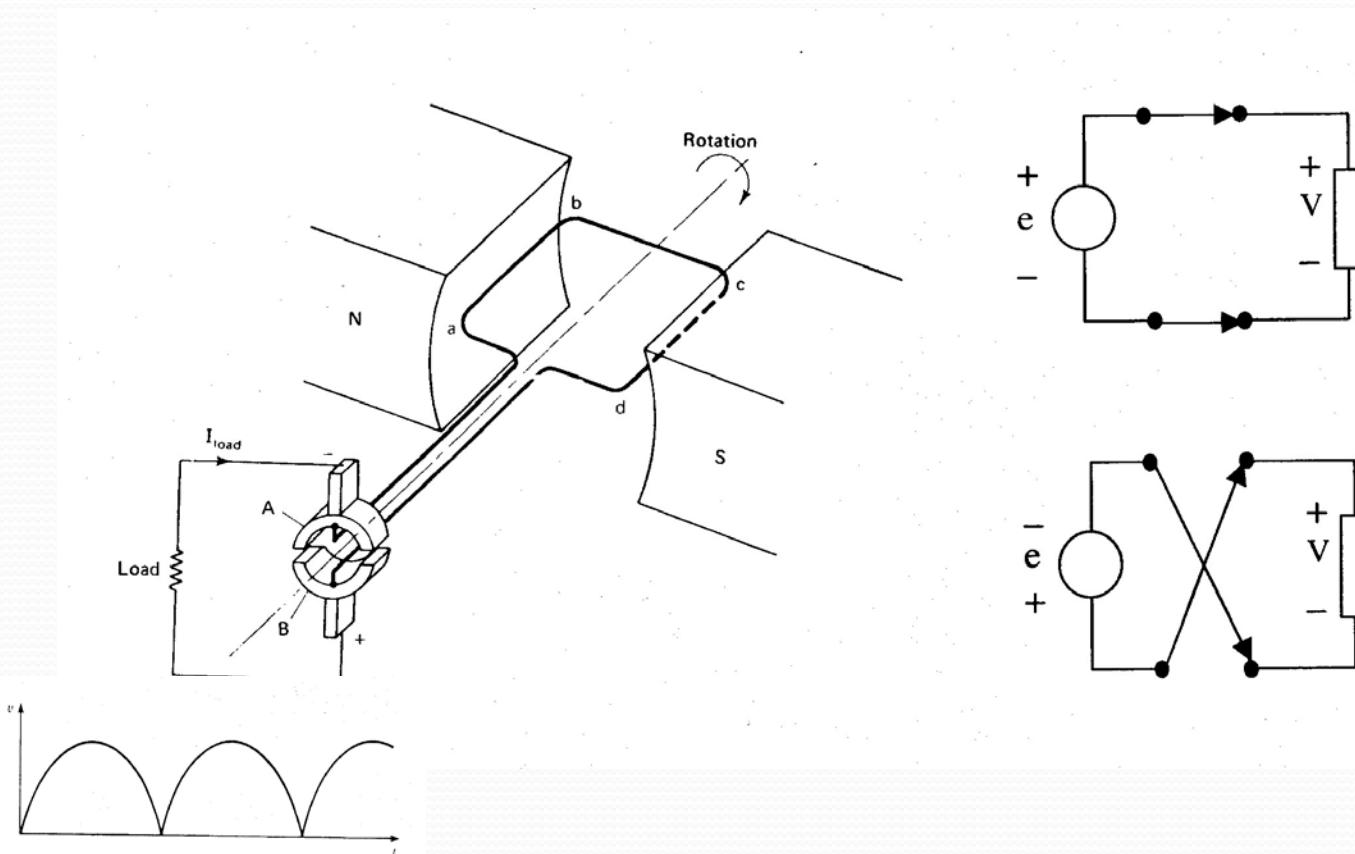


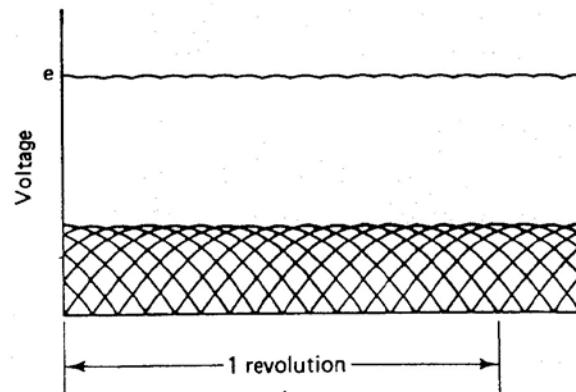
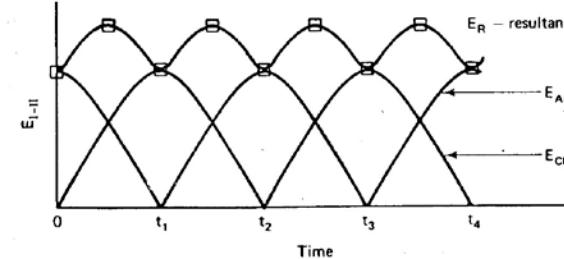
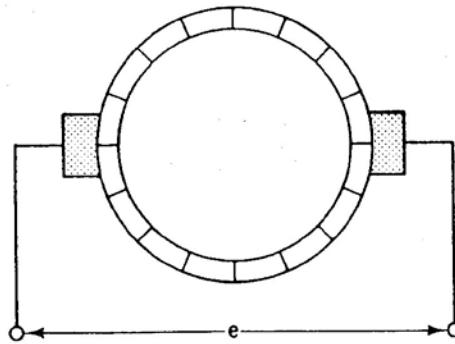
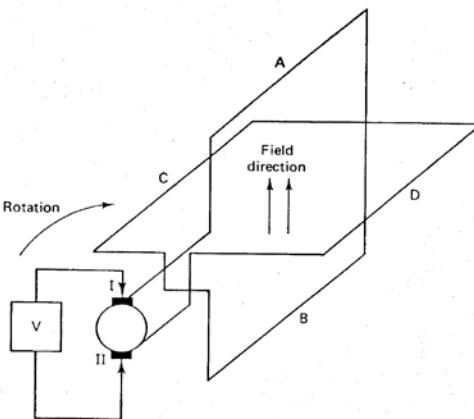
Fig. 10. Wärtsilä unit of the 100 MVA hydroelectric power plant at Kharai Dam



# Generation of Unidirectional Voltage



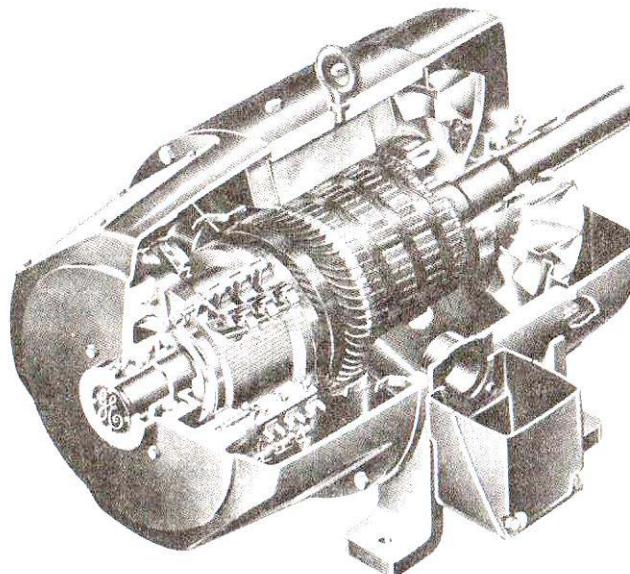
# Generation of DC Voltage



(c)

# DC machines

- **Stator:** - Provides the physical support and magnetic poles.
  - The magnetic poles are excited by coils, are commonly called the **Field** or the **Excitation**
- **Rotor:** - The main winding (where the voltage is induced) is placed in the rotor. The rotor is also called the **Armature**.  
**Commutator** is an important part of the rotor.





# BASIC OPERATING PRINCIPLES

- **Types of DC machines:**

is defined by the arrangement of the excitation or the field

- Shunt Machines

- Series Machines

- Compound Machines

- **AC Generators:**

$$E = k\phi\omega_m \text{ V}$$

Important Topics: Generation of rated voltage

Voltage regulation

Efficiency

- **DC Motors:**

$$T_d = k\phi I_a$$

Important Topics: Torque – Speed Characteristics

Speed control

Starting arrangements





# Thank you!

