

Power

Amplifiers

## Power Transistors:

- Are capable of dissipating larger power (say  $> 1W$  typically)
- Usually require a heat sink
- Usually have lower  $\beta$

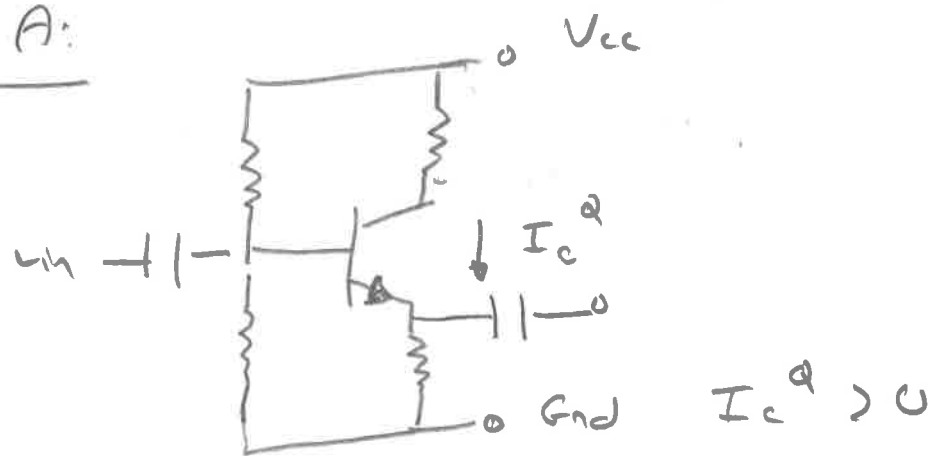
eg. BD 139:

$$P = 1.25W \quad \text{w/o heat sink}$$

$$P = 12.5W \quad \text{w/ heat sink}$$

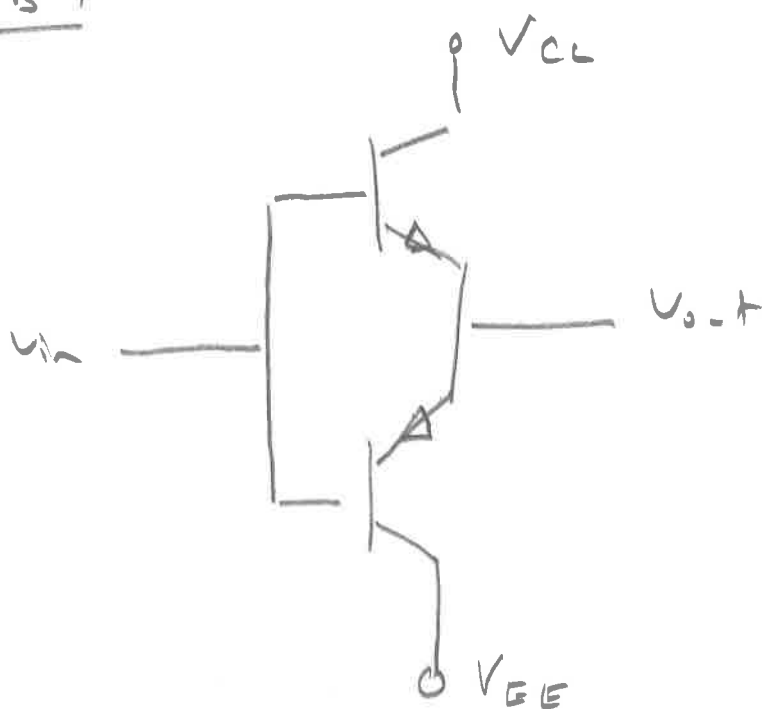
$$\beta > 40 \quad \text{at} \quad I_C = 0.15A$$

## Class A:



Problem:  $I_c^Q > 0$  wastes energy!  
Not suitable for power amplifiers!

## Class B:

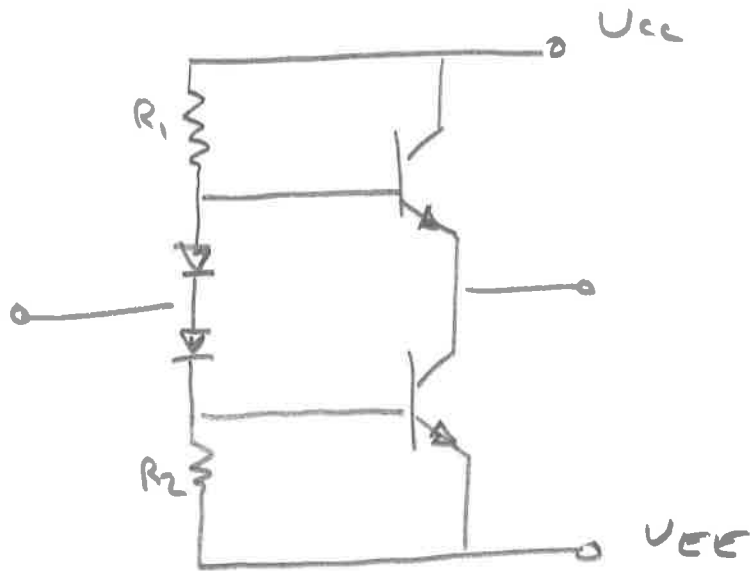


Each active device on for  $\sim 180^\circ$

No  $I_c^Q$  ---

Problem: Crossover Distortion.

# Class AB Amplifier



Choose  $R_1$  and  $R_2$  to ensure enough  
base current at peak output

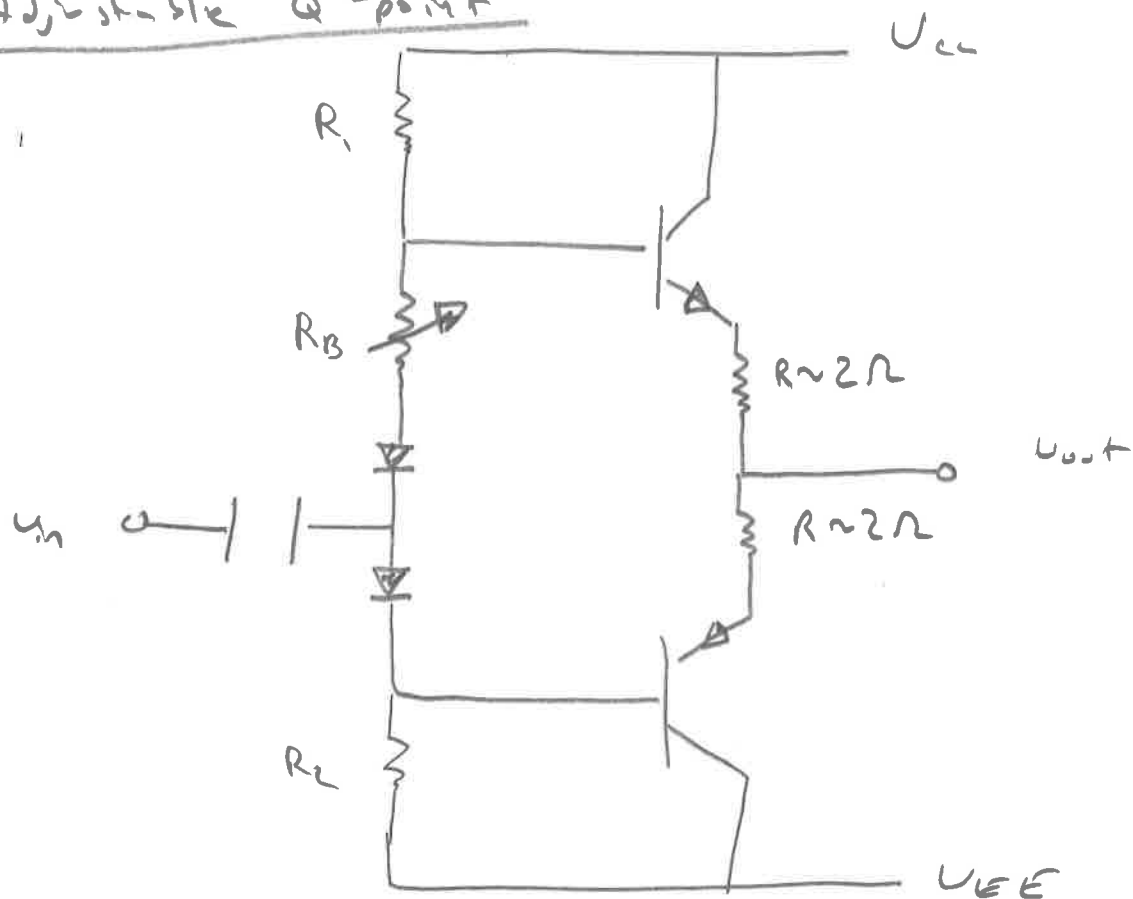
$$P_{max} = \frac{\left(\frac{1}{2}(V_{CC} - V_{EE})\right)^2}{R_L} = \frac{V_{CC}^2}{R_L}$$

$$I_{max} = \frac{V_{CC}}{R_L} = \beta \frac{V_{CC}}{R_1}$$

$$R_1 \sim \beta R_L$$

1st Problem:  $T$  instability ... Power transistors  
heat up more than diodes, Q-point  
moves ...

# Adjustable Q-point



Now bias point can be adjusted

with  $R_B$  so that

$$V_{out}^Q = 0$$

## Real Example:

$$P_{\max} = 12.5 \text{ W}, \quad V_{CC} = 10 \text{ V}, \quad R_L = 8 \Omega, \quad \beta = 40$$

$$R_1 = \beta R_L = 320 \Omega$$

$$P_R = \frac{V^2}{R} = \frac{100 \text{ V}^2}{320 \Omega} > \frac{1}{4} \text{ W}$$

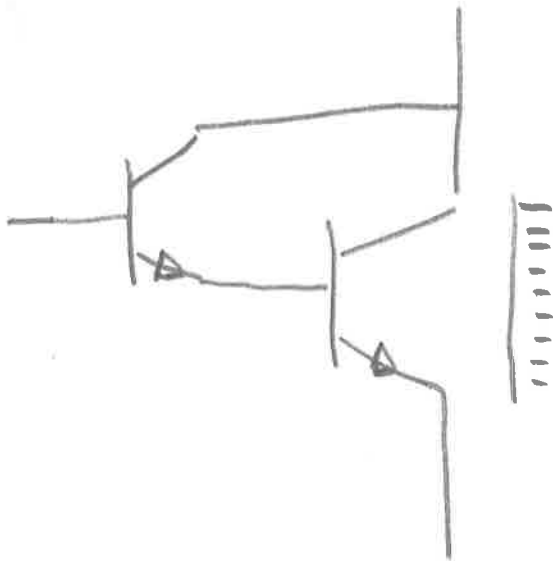
Solution:

Get power  $\sqrt{R}$ !

$\beta$ -boosting

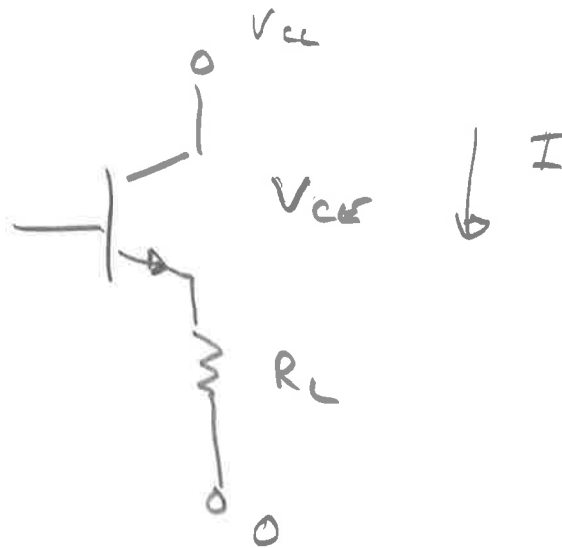
Darlington

Transistor



$$\beta = \beta_1 \times \beta_2$$

## Power Limitations:



$$P_T = V_{ce} \cdot I$$
$$= V_{ce} \frac{(V_{cc} - V_{ce})}{R_L}$$

$$\frac{dP_T}{dV_{ce}} = \frac{V_{cc} - 2V_{ce}}{R_L} = 0 \Rightarrow \boxed{V_{ce} = \frac{1}{2} V_{cc}}$$

$$P_T^{\max} = \left(\frac{1}{2} V_{cc}\right)^2 / R_L$$

$$V_{cc}^{\max} = 2 \cdot (P_T^{\max} R_L)^{\frac{1}{2}}$$

e.g.  $12.5 \text{ W}$ ,  $8 \Omega \Rightarrow$

$$V_{cc}^{\max} = 2 \cdot (12.5 \times 8)^{\frac{1}{2}} \text{ V}$$

$$V_{cc}^{\max} = 20 \text{ V} \quad (\text{or } +10 \text{ V}, -10 \text{ V})!$$

(40 W speakers :(!)

# Feed back !

