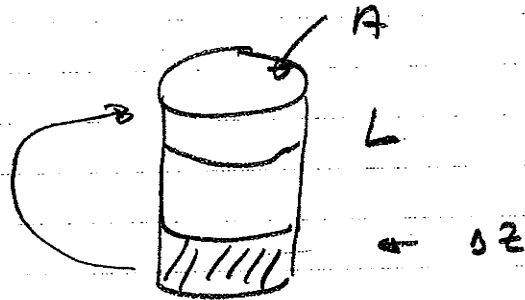


## Proof of Archimedes principles



$$\Delta U = \Delta m g L = (A \cdot \Delta z \rho) g \cdot L$$

$$\frac{\Delta U}{\Delta z} = \rho g L \cdot A$$

$$F = \rho g \cdot L \cdot A = W_{\text{water}}$$

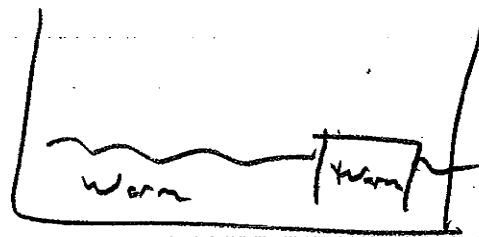
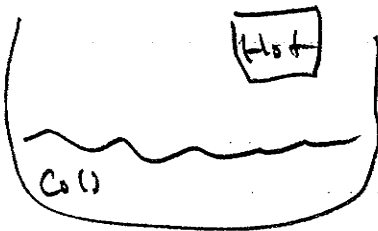
Goal: Define temperature

Problem: We don't yet have the understanding to do it properly yet... a state we're often (maybe always) in...

So we proceed empirically at first. We notice things.

Thing 1:

When hot and cold are in contact, the hot gets colder and the cold gets hotter, until they stop.



Q: What do we mean by thermal contact?

For now: touching!

(Will find more ways,)

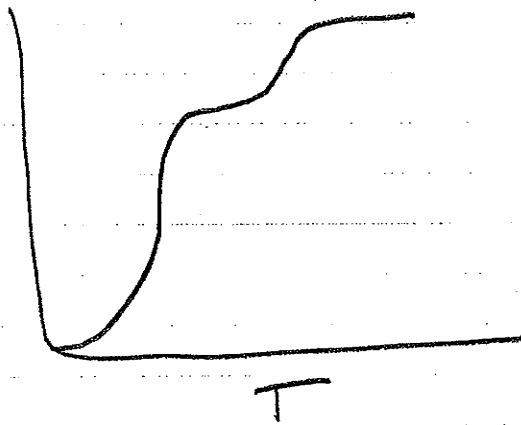
TIT4

Thing 2: Many phenomenon has a  
functional relationship with  
hotness or coldness!

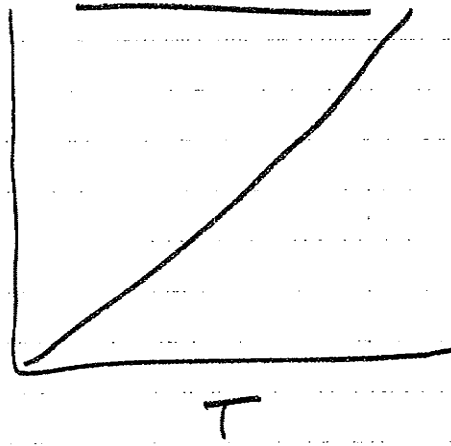
→ resistances increase with hotness

→ pressure of a gas increases

Thermoscope



Thermometer



We don't know enough yet to define  
a standard thermometer, but for  
now we only need a thermoscope  
to notice

T1 S.2

$$T \rightarrow -T$$

$$\Rightarrow \frac{dU}{dT} = mc$$

$$\rightarrow \frac{dU}{dT} = mc$$

Heat capacities would be  
negative ---

$$m v_x^2 = k_B T$$

$$\rightarrow m v_x^2 = -k_B T$$

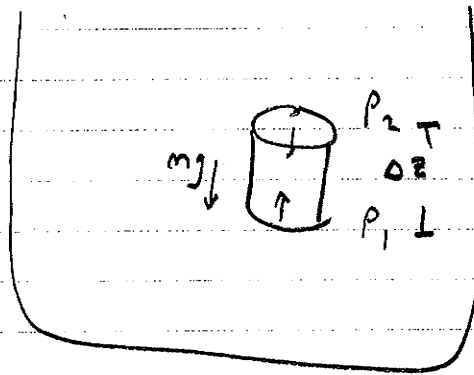
T1 S. 3

$$0 = mg + P_2 \cdot A - P_1 \cdot A$$

$$\Rightarrow P_1 - P_2 = \frac{mg}{A}$$

$$= \frac{m}{A \Delta z} \cdot \Delta z \cdot g = \frac{m}{V} \Delta z g$$

$$P_1 - P_2 = \rho \Delta z g$$



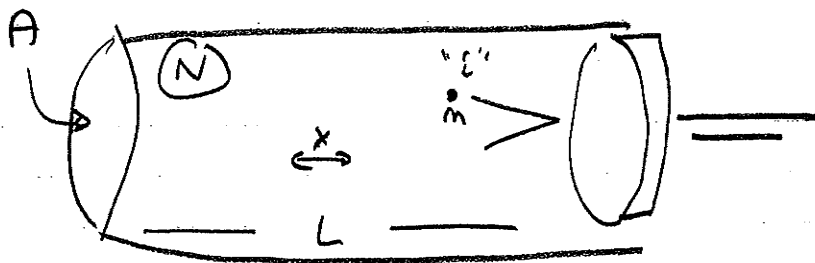
Ideal Gas Model:

- 1)  $N \gg 1$
- 2) molecules are point-like.
- 3) molecules obey Newton's laws  
(definitely not true)
- 4) Molecules don't interact with  
one another
- 5) Collisions with wall are elastic
- 6) Motion of molecules is entirely  
random.

We need to make a lot of  
unnecessary assumptions here to  
make the math easier.

Nowadays, you can write a  
computer simulation to verify this  
model. If you know how  
to program, and are interested,  
I will help you write a  
model.

(No Extra Credit  $\rightarrow$  But Very Fun)



$$\Delta \vec{p}_i = \Delta p_{i, \text{final}} - \Delta p_{i, \text{initial}}$$

$$\Delta p_y = \Delta p_z = 0$$

$$\Delta p_x = -m |u_{ix}| - m |u_{ix}|$$

$$= -2m |u_{ix}|$$

On piston:  $\Delta p_x = \underline{\underline{+2m |u_{ix}|}}$

$$\Delta t = 2L / u_{ix}$$

$$F_i = \frac{\Delta p_x}{\Delta t} = \frac{2m u_{ix}}{2L / u_{ix}} = \frac{m u_{ix}^2}{L}$$

$$p_i = \frac{F_i}{A} = \frac{m u_{ix}^2}{A \cdot L} = \frac{m u_{ix}^2}{V}$$

$$p_{\text{TOT}} = \sum_i \frac{m_i u_{ix}^2}{V} = \frac{N}{V} \left( \frac{1}{N} \sum_i m_i u_{ix}^2 \right)$$

$$p = \frac{N}{V} [m u_x^2]_{\text{avg}}$$

Q: Why  $u_x^2$  (one factor  $\Delta p$ , one factor  $\Delta t$ )

Now our definition of  $T$  in terms of a gas thermometer can be seen to be new light.

$$P = CT$$

$$+ P = \frac{N}{V} [m u_x^2]$$

$$\Rightarrow m u_x^2 = \left( \frac{V}{N} C \right) \cdot T$$

$$m u_x^2 = C' T$$

Now at this stage,  $C'$  can depend on  $V, N$ , type of gas, --

But what if it didn't.

**BIG CLUE** we are on the right path.

$$C' = k_b = 1.38 \times 10^{-23} \text{ J/K}$$

$$P = \frac{N}{V} k_b T$$



T2 S. 2

Boyle's Law

$$P \sim \frac{1}{V} \quad \text{at const } N$$

Gay-Lussac's Law

$$V \sim T \quad \text{at const } P$$

Average

$$V \sim N \quad \text{at const } P \text{ and } T$$

$$B: PV = N k_B T \Rightarrow PV = \text{const} \quad \text{at const } N, T$$

$$\Rightarrow P \sim \frac{1}{V}$$

$$G.L.: PV = N k_B T$$

$$\Rightarrow P = \left( \frac{N k_B}{V} \right) T$$

$$P \sim T \quad \text{at const } N, V$$

Average 1

$$V = N \left( \frac{k_B T}{P} \right)$$

## Temperature and Energy

Randomness:

$$[m v_x^2]_{avg} = [m v_y^2]_{avg} = [m v_z^2]_{avg} \\ = k_B T$$

$$3 k_B T = [m v_x^2]_{avg} + [m v_y^2]_{avg} + [m v_z^2]_{avg} \\ = \frac{1}{N} \sum_i m (v_x^2 + v_y^2 + v_z^2) \\ = 2 \cdot K_{avg}$$

$$\Rightarrow \boxed{K_{avg} = \frac{3}{2} k_B T}$$

WOW! We are definitely on the right path.

→  $T$  is proportional to average kinetic energy of molecule in a gas.

## Heat Capacity of a gas

$$\Delta U = m c \Delta T$$

$$U = \frac{3}{2} N k_b T$$

$$\frac{dU}{dT} = \frac{3}{2} N k_b \quad (\equiv m c)$$

$$\left( c = \frac{3}{2} \left( \frac{N}{m} \right) k_b \right)$$

## Non-Ideal Gases:

$$U = \frac{F}{2} N k_b T$$

$F = 3$  for monatomic gases

$F = 5$  for diatomic gases

$F > 6$  for poly-atomic gases

Those Pesky Chemists...

$$PV = N k_B T$$

$$\rightarrow PV = \frac{N}{N_A} (N_A \cdot k_B) T$$

$$= n R T$$

$$\left( n \equiv \frac{N}{N_A} \right)$$

$$n = \frac{M}{M_A} \quad \leftarrow \text{mass of sample}$$

$$M_A \quad \leftarrow \text{mass of } N_A \text{ molecules,} \\ (M_A / N_A)$$

$$\left( n = \frac{M / m}{N_A} \right) \quad (\text{Conceptually})$$

### T2S.3

a) Assume for simplicity  $m_i = m$

$$\langle x \rangle = \frac{\sum m_i x_i}{\sum m_i} = \frac{1}{N} \sum_i x_i$$

$$\frac{d\langle x \rangle}{dt} = 0 \Rightarrow \frac{d}{dt} \sum_i x_i = \frac{1}{N} \sum_i v_i$$

$$\Rightarrow \boxed{\langle v \rangle = 0}$$

b) Simple example: if every particle  
has a duplicate with  $v \rightarrow -v$

$$\langle v \rangle = \frac{1}{2N} \left( \sum_i v_i + (-v_i) \right)$$

$$\langle v^2 \rangle = \frac{1}{2N} \sum_i v_i^2 + (-v_i)^2$$

$$> 0$$

T2 S4



$$\Delta p = 2m u_0$$

$$N = r \cdot \Delta t \cdot A \quad (\text{defines "r"})$$

$$P = N \frac{\Delta p}{\Delta t} \frac{1}{A} = \left( \frac{N}{\Delta t A} \right) \Delta p = \boxed{r 2m u_0}$$

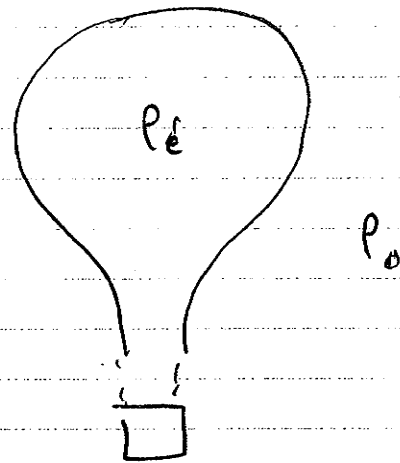
T2 S.5

Boyant Force is

$$F = \rho_o \cdot V \cdot g$$

Gravity is

$$F = -\rho_i V \cdot g - Mg$$



Floating is

$$\rho_o V g + (-\rho_i V g) - Mg = 0$$

$$\Rightarrow \boxed{\rho_o - \rho_i = \frac{M}{V}}$$

$$b) \quad \rho = \frac{N \cdot m}{V} \quad m = \frac{M_A}{N_A}$$

$$= \frac{N}{N_A} \cdot \frac{M_A}{V} = \frac{n}{V} M_A$$

$$PV = nRT \quad \Rightarrow \quad \frac{P}{V} = \frac{P}{RT}$$

$\Rightarrow$

$$\rho = \frac{P M_A}{R T}$$



$$c) \quad p_0 - p_L = \frac{M}{U}$$

$$\Rightarrow U = \frac{M}{(p_0 - p_L)}$$

$$= \frac{M}{p_0} \frac{1}{(1 - p_L/p_0)}$$

$$\text{From (b)} \quad p \sim \frac{1}{T}$$

$$V = \frac{M}{p_0} \frac{1}{(1 - T_0/T_L)}$$

## Lecture T3

### Review Reading

$$\Delta U = Q + W$$

Heat  
(Flow due to  $\Delta T$ )

Everything Else

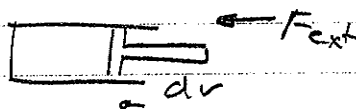
$$dW = -P dV$$

Why?

$$W = F \cdot dr$$
$$= \frac{F}{A} \cdot dr \cdot A$$

$$W = -P \cdot dV$$

Q: ? Why Negative



Does Positive work, but  $dV < 0$

$P, V, T, U, M, N$

$$N = \frac{M}{M_A}$$

$$PV = N k_B T$$

$$U = \frac{5}{2} N k_B T$$

$\Rightarrow$  3 independent state variables only  
If 1 held constant (e.g.  $N$ )

value of  $PV$  uniquely defines state.

## Computing Work

Iso baric

$$W = - \int_{V_I}^{V_F} p dV = - p(V_F - V_I)$$

Iso thermal

$$p = \frac{NkT}{V} = \frac{p_I V_I}{V}$$

$$W = -NkT \int \frac{dV}{V} = -NkT \log(V_F/V_I)$$

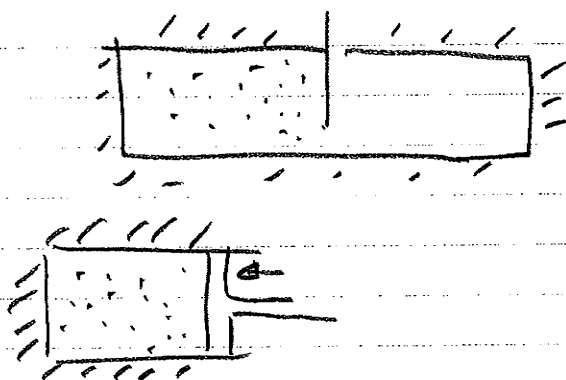
$$= -p_I V_I \log(V_F/V_I)$$

Iso choric

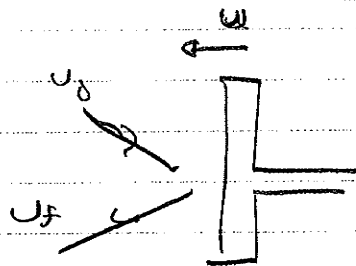
$$W = 0$$

Adiabatic?

Introduce



## Work on Adiabatic Compression of Gas



$$1) u_f = |u_i| + 2u \quad (\text{why?})$$

$$2) \Delta K = \frac{1}{2} m (|u_i| + 2u)^2 - \frac{1}{2} m u_{ix}^2 \\ \sim 2m |u_i| u$$

$$3) \frac{dK_i}{dt} = \frac{2m |u_i| u}{2L/|u_i|} = \frac{m u_{ix}^2 u}{L}$$

$$4) \frac{dU}{dt} = \sum_i \frac{dK_i}{dt} = \frac{(\sum m u_{ix}^2) \cdot u}{L}$$

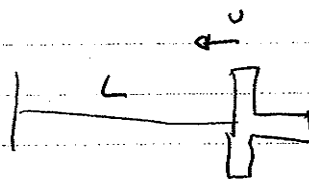
$$\boxed{\frac{dU}{dt} = \frac{(N k T) \cdot u}{L}}$$

$$5) U = \frac{f}{2} N k T$$

$$\frac{dU}{dt} = \frac{f}{2} N k \frac{dT}{dt} = \frac{N k T \cdot U}{L}$$

$$\boxed{\frac{1}{T} \frac{dT}{dt} = \frac{2}{f} \frac{U}{L}}$$

$$6) U = - \frac{dL}{dt}$$



$$\Rightarrow \frac{U}{L} = - \frac{1}{L} \frac{dL}{dt} = - \frac{1}{L \cdot A} \frac{d(LA)}{dt} = - \frac{1}{V} \frac{dV}{dt}$$

$$7) \boxed{\frac{1}{T} \frac{dT}{dt} = - \frac{2}{f} \frac{1}{V} \frac{dV}{dt}}$$

Differential Equation!

(See Better Solution)

8) How to solve without magic

$$\frac{1}{T} \frac{dT}{dt} + \frac{2}{f} \frac{1}{V} \frac{dV}{dt} = 0$$

Goal: Write as

$$\frac{1}{(?)^{\alpha}} \frac{d(?)^{\alpha}}{dt} = 0$$

Why?  $\Rightarrow (?)^{\alpha} = \text{const}$

How: Looks like a chain rule...

$$X = TV \quad \frac{1}{X} \frac{dX}{dt} = \frac{1}{T} \frac{dT}{dt} + \frac{1}{V} \frac{dV}{dt}$$

$$X = TV^{\alpha}$$

missing a factor!

$$\frac{1}{X} \frac{dX}{dt} = \frac{1}{T} \frac{dT}{dt} + \alpha \cdot \frac{V^{\alpha-1}}{V^{\alpha}} \frac{dV}{dt}$$

$$= \frac{1}{T} \frac{dT}{dt} + \alpha \frac{1}{V} \frac{dV}{dt}$$

$$\alpha = \frac{2}{f}$$

$$\frac{1}{TV^{2/f}} \frac{d}{dt} (TV^{2/f}) = \frac{1}{T} \frac{dT}{dt} + \frac{2}{f} \frac{1}{V} \frac{dV}{dt}$$

$$= 0$$

$$a) \quad \frac{d}{dt} (T V^{2/5}) = 0$$

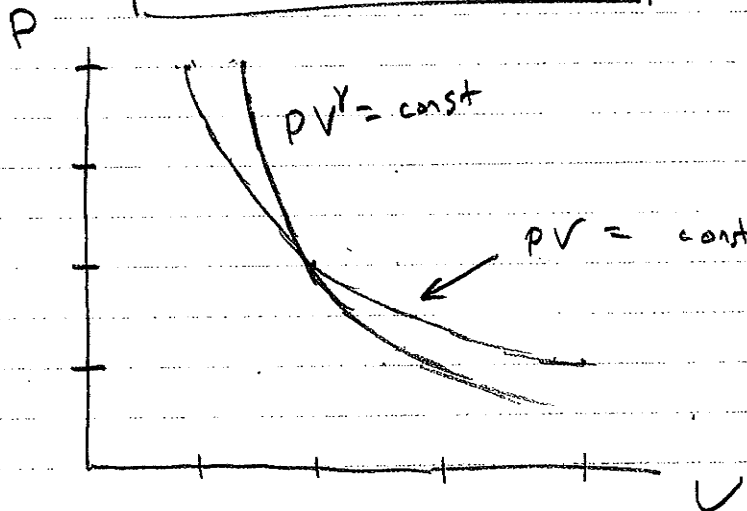
means?  $T V^{2/5} = \text{const}$

$$10) \quad T \sim PV$$

$$\Rightarrow P V^{1+2/5} = \text{const}$$

Define  $\gamma = 1 + 2/5$

$$\begin{aligned} P V^\gamma &= \text{const} \\ T V^{\gamma-1} &= \text{const} \end{aligned}$$



(Better solution to ~~DIFF EQ~~)

$$0 = \frac{1}{T} \frac{dT}{dt} + \frac{2}{f} \frac{1}{V} \frac{dV}{dt}$$

$$-\frac{1}{T} \frac{dT}{dt} = \frac{2}{f} \frac{1}{V} \frac{dV}{dt}$$

Integrate both sides wrt  $t$

$$-\int \frac{1}{T} \frac{dT}{dt} dt = \frac{2}{f} \int \frac{1}{V} \frac{dV}{dt} dt$$

$$-\int \frac{1}{T} dT = \frac{2}{f} \int \frac{dV}{V}$$

$$-\log T + C = \frac{2}{f} \log V$$

$$C = \log V^{2/f} \cdot T$$

$$\exp(C) = \text{const} = V^{2/f} T \quad !!!$$



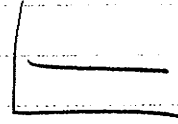
Have Students  
Do it...

## P-V Diagrams

Draw Process going through

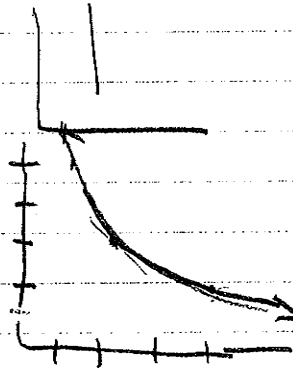
$$P = 8 \text{ kPa} \quad U = 8 \text{ m}^3$$

- isochoric (const  $V$ )

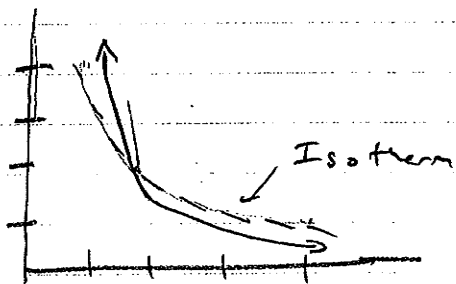


- isobaric (const  $P$ )

- isothermal (const  $T$ )



- adiabatic ( $Q = 0$ )



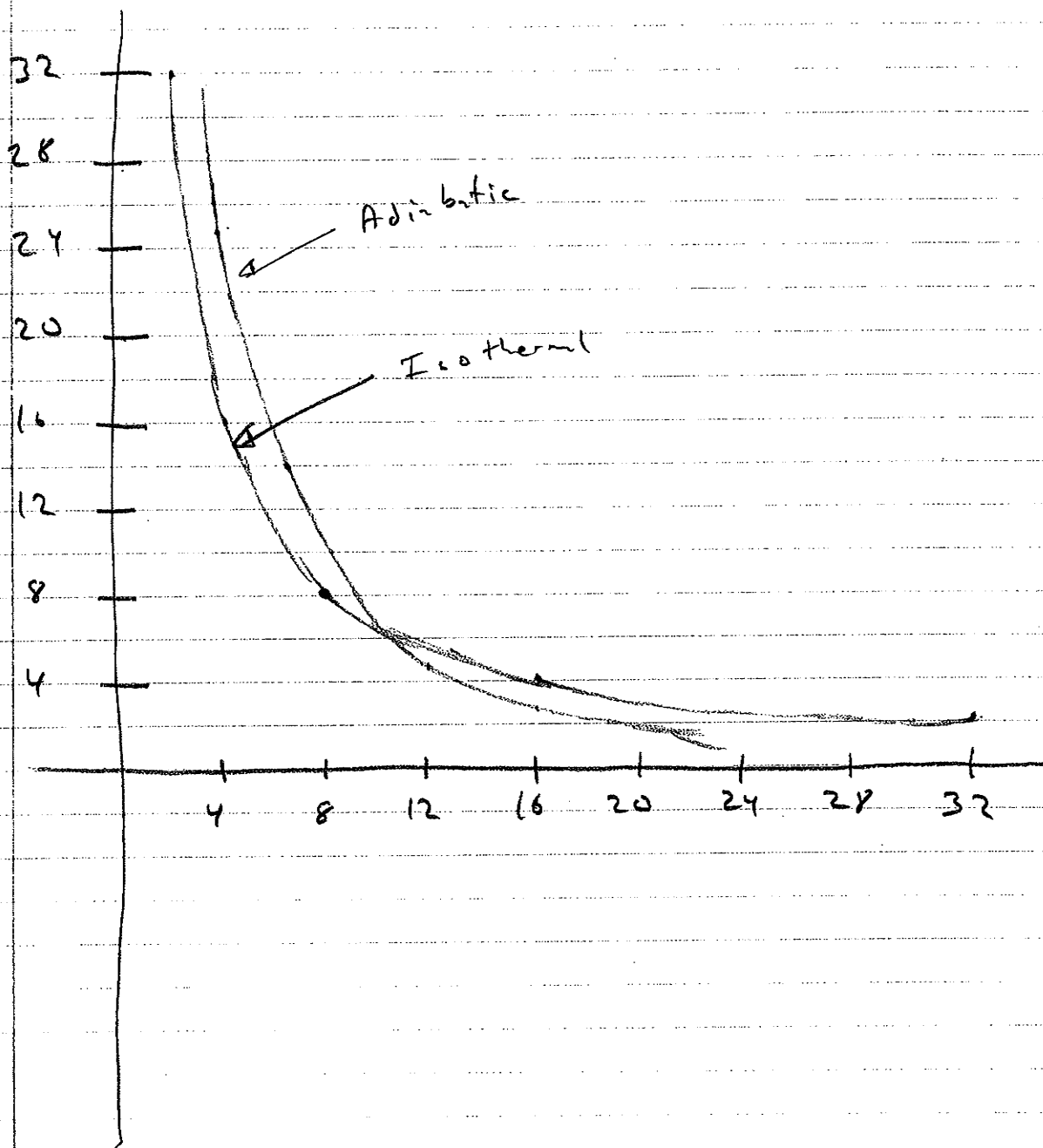
Explicit E.g. computing AdS<sub>2</sub> / D11

$V$	$P \sim \frac{1}{V}$	$P \sim \frac{1}{V^{5/3}}$
8	8 ( $\equiv$ )	8 ( $\equiv$ )
6	10	13
4	16	25
2	32	80
1	64	256

Calc:  $P = \frac{8 \cdot 8}{V} = \frac{64}{V}$

$P = \frac{8 \cdot 8^{5/3}}{V^{5/3}} = \frac{256}{V^{5/3}}$

10	6.4	5.5
12	5.3	4.1
14	4.6	3.1
16	4	2.5
32	2	0.8



# IW CLASS

T3 S. 4

A  $\rightarrow$  B

B  $\rightarrow$  C

C  $\rightarrow$  A

Q	W	$\Delta U$
+	-	+
+	0	+
-	+	-

A  $\rightarrow$  B:

$$W = - \int P dV = - P \Delta V < 0$$

$$PV = NkT \Rightarrow V \sim T$$

$$\Rightarrow T_F > T_I \Rightarrow U_F > U_I \Rightarrow \Delta U > 0$$

Since  $\Delta U = Q + W$ , and  $\Delta U > 0$  but  $W < 0$   
 $Q > 0$

B  $\rightarrow$  C

$$W = 0$$

$$PV = NkT \Rightarrow P \sim T$$

$$P_F > P_I \Rightarrow T_F > T_I \Rightarrow U_F > U_I$$

$$\Rightarrow \Delta U > 0$$

C → A

$\Delta U$  for the cycle must be 0,  
so  $\Delta U = -$ .

$W$  is negative. In fact,

$$|W_{C \rightarrow A}| > |W_{A \rightarrow B}|$$

Implying that  $W$  for the entire cycle is +.

Since  $\Delta U = 0 = Q + W$  for the whole cycle,  $Q$  for the cycle must be negative. But  $Q$  for  $A \rightarrow B$ ,  $B \rightarrow C$  is positive, so  $Q$  for  $C \rightarrow A$  must be negative.

Alternate:

$$P_I V_I > P_F V_F \quad \text{for } C \rightarrow A$$

$$\Rightarrow T_I > T_F \Rightarrow \boxed{\Delta U < 0}$$

$$\text{As } \Delta U < 0, \quad \boxed{W > 0}$$

$$\text{Since } \Delta U < 0 \text{ and } W > 0, \quad \boxed{Q < 0}$$

(HW)

T3 S.5

A → B

$$W = -\int p dV < 0$$

Adiabatic  $\Rightarrow Q = 0$

Hence  $\Delta U = W < 0$

A → B

B → C

C → D

	Q	W	$\Delta U$
A → B	0	-	-
B → C	-	+	0
C → D	+	0	+

Alternative:

Since  $T_B = T_C$ ,  $T_A > T_B \Rightarrow U_A > U_B$

∴

$$\Rightarrow \Delta U < 0$$

B → C

Isothermal  $\Rightarrow T = \text{const} \Rightarrow U = \text{const} \Rightarrow \Delta U = 0$

$$W = -\int p dV > 0$$

$$\Delta U = Q + W = 0 \Rightarrow Q = -W$$

C → A

$$W = 0$$

Since  $V = \text{const}$ , and  $pV = NkT$ ,  $T_A > T_C$

So  $U_A > U_C \Rightarrow \Delta U > 0$ .

Alternatively: Since  $\Delta U$  for cycle = 0,  $\Delta U > 0$ ,

Since  $W = 0$ ,  $\Delta U = Q$ ,  $Q > 0$

T35.6  $T \uparrow$ , so  $\Delta U > 0$

$V = \text{const} \Rightarrow W = 0$ , so  $Q = \Delta U > 0$

$PV \Rightarrow NkT \Rightarrow P \sim T$

$\frac{T_F}{T_i} = \frac{P_F}{P_i} \Rightarrow T_F = \frac{P_F}{P_i} T_i = \frac{50}{30} 290 \text{ K}$

From

$PV = NkT \Rightarrow N = \frac{P_i V_i}{k T_i} \left( = \frac{(30 \text{ kPa})(1 \text{ m}^3)}{k 290 \text{ K}} \right)$

$dU = \frac{3}{2} N k dT$

$= \frac{3}{2} \frac{P_i V_i}{T_i} (T_F - T_i)$

T3 S.7

$$TV^{\gamma-1} = \text{const}$$

$$PV^{\gamma} = \text{const}$$

$$P_i V_i^{\gamma} = P_f V_f^{\gamma}$$

$$\frac{V_i^{\gamma}}{V_f^{\gamma}} = \frac{P_f}{P_i}$$

$$\frac{V_i}{V_f} = \left( \frac{P_f}{P_i} \right)^{\frac{1}{\gamma}}$$

$$T_i V_i^{\gamma-1} = T_f V_f^{\gamma-1}$$

$$\Rightarrow T_f = \left( \frac{V_i}{V_f} \right)^{\gamma-1} \cdot T_i$$

$$= \left( \frac{P_f}{P_i} \right)^{\frac{\gamma-1}{\gamma}} \cdot T_i$$

$$= \left( \frac{1}{3} \right)^{\frac{\gamma-1}{\gamma}} T_i$$

For air  $\gamma \sim 1.4$



T3 S.8       $\gamma \sim 1.4$

$$T V^{\gamma-1} = \text{const}$$

$$P V^{\gamma} = \text{const}$$

We are given  $P_F / P_C \sim 0.045$

$$P_C V_C^{\gamma} = P_F V_F^{\gamma}$$

$$\Rightarrow V_F / V_C = \left( P_C / P_F \right)^{1/\gamma}$$

$$T_C V_C^{\gamma-1} = T_F V_F^{\gamma-1}$$

$$T_F = T_C \left( \frac{V_C}{V_F} \right)^{\gamma-1}$$

$$= T_C \left( \frac{P_F}{P_C} \right)^{\frac{\gamma-1}{\gamma}}$$

T3 S.9

For adiabatic process:

$$TV^{\gamma-1} = \text{const}$$

$$PV^{\gamma} = \text{const}$$

$$\Rightarrow P = P_I V_I^{\gamma} V^{-\gamma}$$

$$W = - \int P dV = - P_I V_I^{\gamma} \int_{V_I}^{V_F} V^{-\gamma} dV$$
$$= - \frac{P_I V_I^{\gamma}}{1-\gamma} V^{1-\gamma} \Big|_{V_I}^{V_F}$$

$$= \frac{P_I V_I^{\gamma}}{\gamma-1} (V_F^{1-\gamma} - V_I^{1-\gamma})$$

$$= \frac{P_I V_I}{\gamma-1} \left( \frac{V_I^{\gamma-1}}{V_F^{\gamma-1}} - 1 \right)$$

$$= \frac{NkT_I}{\gamma-1} \left( \frac{T_F}{T_I} - 1 \right)$$

$$= \left( \frac{1}{\gamma-1} \right) Nk (T_F - T_I)$$

$$= \frac{f}{2} Nk dT$$

T3 S10

a)  $PV = NkT$

$$P \frac{dV}{dT} + V \frac{dP}{dT} = Nk$$

$$P dV + V dP = Nk dT$$

b) For adiabatic process,  $Q = 0$ ,  
so

$$\Delta U = Q + W \Rightarrow \Delta U = W$$

$$\text{But } dW = -P dV$$

$$A) dU = \frac{f}{2} Nk dT$$

$$\Rightarrow P dV = -\frac{f}{2} Nk dT$$

$$c) Nk dT = -\frac{2}{f} P dV$$

$$\Rightarrow P dV + V dP = -\frac{2}{f} P dV$$

$$V dP + P \left(1 + \frac{2}{f}\right) dV = 0$$

$$V dP + \gamma P dV = 0 \quad \gamma \equiv 1 + \frac{2}{f}$$

$$\frac{dP}{dV} + \gamma \frac{P}{V} = 0$$

$$d) \frac{d}{dV} V^\gamma = \gamma V^{\gamma-1}$$

So, as we have a term

$$\gamma \frac{p}{V} \rightarrow \gamma V^{\gamma-1} \cdot p \rightarrow p \frac{d}{dV} (V^\gamma)$$

So multiply above by  $V^\gamma$

$$V^\gamma \frac{dp}{dV} + \gamma p V^{\gamma-1} = 0$$

$$V^\gamma \frac{dp}{dV} + p \frac{d}{dV} V^\gamma = 0$$

$$\frac{d}{dV} (p V^\gamma) = 0$$

$$\Rightarrow \boxed{p V^\gamma = \text{const}}$$

### T3 S.2 I, Class:

Let's say you are clever:

$$Q = 0 \Rightarrow dU = W$$

$$U = \frac{f}{2} N k T$$

$$dU = \frac{f}{2} N k dT$$

$$W = \Delta U = \frac{f}{2} N k \Delta T = \frac{f}{2} N k (T_F - T_I)$$

(HW solution!)

Now imagine you aren't smart:

$$W = - \int P dV$$

$$P V^\gamma = \text{const} = P_I V_I^\gamma$$

$$\Rightarrow P = P_I V_I^\gamma V^{-\gamma}$$

$$W = - \int_{V_I}^{V_F} P dV = - P_I V_I^\gamma \int_{V_I}^{V_F} V^{-\gamma} dV$$

$$= \frac{P_I V_I^\gamma}{(\gamma-1)} \left( \frac{1}{V_F^{\gamma-1}} - \frac{1}{V_I^{\gamma-1}} \right)$$

We also know:

$$T V^{\gamma-1}$$

$$\Rightarrow T_I V_I^{\gamma-1} = T_F V_F^{\gamma-1}$$

$$\Rightarrow \frac{V_{\pm}^{\gamma-1}}{V_F^{\gamma-1}} = \frac{T_F}{T_{\pm}}$$

$$W = \frac{P_I V_I}{\gamma - 1} \left( \frac{T_F}{T_I} - 1 \right)$$

$$p_I V_I = N k T_I$$

$$W = \frac{Nk}{\gamma - 1} (T_F - T_I)$$

$$\frac{1}{Y-1} = \frac{1}{1 + 2/F - 1} = \frac{F}{2}$$

$$W = \frac{5}{2} N k (T_F - T_I)$$

111

Easy Way

T3 S.2

$$Q = 0 \Rightarrow dU = W$$

$$U = \frac{f}{2} N k T$$

$$\Rightarrow dU = \frac{f}{2} N k dT$$

$$W = \Delta U = \frac{f}{2} N k (T_f - T_i)$$

## HARD WAY !!!

T3 S.2

Work done during an adiabatic change in volume is:

$$W = - \int P dV$$

$$P V^\gamma = \text{const} = P_I V_I^\gamma$$

$$\Rightarrow P = P_I V_I^\gamma V^{-\gamma}$$

$$W = - \int_{V_I}^{V_F} P dV = - P_I V_I^\gamma \int_{V_I}^{V_F} V^{-\gamma} dV$$

$$= - P_I V_I^\gamma \left. \frac{V^{1-\gamma}}{1-\gamma} \right|_{V_I}^{V_F}$$

$$= \frac{P_I V_I^\gamma}{(\gamma-1)} \left( \frac{1}{V_F^{\gamma-1}} - \frac{1}{V_I^{\gamma-1}} \right)$$

$$W = \frac{P_I V_I}{(\gamma-1)} \left( \frac{V_I^{\gamma-1}}{V_F^{\gamma-1}} - 1 \right)$$

Cont. —



T3 S2 ... cont. ....

$$T/V^{\gamma-1} = \text{const}$$

$$\Rightarrow T_I V_I^{\gamma-1} = T_F V_F^{\gamma-1}$$

$$\Rightarrow V_I^{\gamma-1} / V_F^{\gamma-1} = T_F / T_I$$

$$W = \frac{p_I V_I}{(\gamma-1)} \left( \frac{T_F}{T_I} - 1 \right)$$

$$W = \frac{N k T_I}{(\gamma-1)} \left( \frac{T_F}{T_I} - 1 \right)$$

$$\frac{1}{\gamma-1} = \frac{1}{1 + \frac{2}{f} - 1} = \boxed{\frac{f}{2}}$$

$$W = \frac{f}{2} N k (T_F - T_I)$$

T3 S.3

(1-1w)

\*\*\* Isothermal process for an ideal gas  
at constant  $N$  is has:  $U = NkT = \text{const} \Rightarrow \Delta U = 0$ .

$$\Delta U = 0 \quad \text{and} \quad U = \frac{f}{2} NkT \quad ***$$

$$\Delta U = Q + W$$

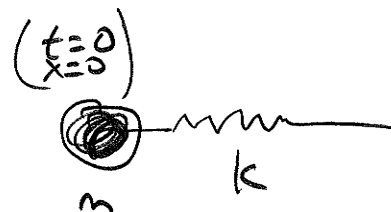
$$\Rightarrow \boxed{Q = -W = + NkT \ln \frac{V_f}{V_i}}$$

# Classical Mass on Spring

T4

$$F = -kx = ma = m \frac{d^2x}{dt^2}$$

$$\frac{d^2x}{dt^2} = -\frac{k}{m}x$$



How solution:  $x = A \sin \omega t + B \cos \omega t$

But  $x = 0$  at  $t=0 \Rightarrow B=0$

$$x = A \sin \omega t$$

$$\frac{dx}{dt} = \omega A \cos \omega t$$

$$\frac{d^2x}{dt^2} = -\omega^2 A \sin \omega t = -\frac{k}{m}x$$

$$\text{if } \omega = \sqrt{\frac{k}{m}}$$

Energy of spring?

Quick solution: potential energy = 0 at  $x=0$

$$\frac{dx}{dt} = \omega A \cos \omega t = \omega A \text{ at } x=0$$

$$K = \frac{1}{2} m \left( \frac{dx}{dt} \right)^2 = \frac{1}{2} m \omega^2 A^2 = \boxed{\frac{1}{2} k A^2}$$

Note:

$$U = \frac{1}{2} k x^2 = \frac{1}{2} k A^2 \text{ when } \frac{dx}{dt} = 0 \text{ and } x \text{ is max}$$

Classically, that's it, we can choose any value of  $A$ , and therefore system energy can take any value (at least until spring break!!!)

System  $E$ :

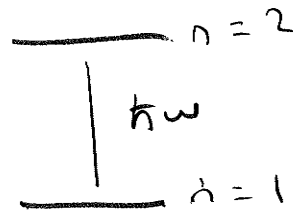
\* Q.M. the system energy is in discrete units

$$E = \hbar \omega \left( n + \frac{1}{2} \right)$$

↑  
planck's constant    ↑  
Quantum Number

—

—

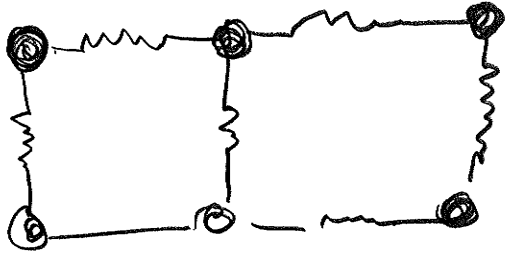


—  $n=0$

— 0

\* For our purposes

## Einstein model for a Solid,



Each atom can oscillate in  $x, y,$  or  $z$  dimensions  $\Rightarrow$  3 quantum numbers for each atom

$$U_{\text{solid}} = \sum_{i=1}^{3N} \epsilon \left( n_i + \cancel{\frac{1}{2}} \right) = \sum_{i=1}^{3N} \epsilon n_i$$

$\uparrow$   
Not accessible

T 458:

M oscillators with total energy  $E = \epsilon_v q$

$(q = 0, 1, 2, \dots)$

say  $m = 4$   $q = 7$

3 0 4 0

0 0 0 | | 0 0 0 0 |

2 2 2 1

4 3 0 0

1 1 1 4

Need  $q$  marbles and  $M-1$  notches

$$\Omega = \frac{(q + m - 1)!}{q! (m-1)!}$$

For Einstein solid.  $M = 3N$

$$\Omega = \frac{(3N + q - 1)!}{q! (3N-1)!}$$

$$q = E/\epsilon$$

745.1

$\Omega_A$  for  $U_A = 4\epsilon$ ,  $N=3$

1	2	3
4	0	0
0	4	0
0	0	4
3	1	0
3	0	1
0	3	1
1	3	0
1	0	3
0	1	3
2	2	0
2	0	2
0	2	2
2	1	1
1	2	1
1	1	2

15

$U_A = 7\epsilon$

1	2	3
7	0	0
0	7	0
0	0	7
6	1	0
6	0	1
0	6	1
1	6	0
1	0	6
0	1	6
5	2	0
5	0	2
0	5	2
2	5	0
2	0	5
0	2	5

5	1	1
1	5	1
1	1	5
4	3	0
4	0	3
0	4	3
3	4	0
3	0	4
0	3	4

3	3	1
3	1	3
1	3	3
3	2	2
2	3	2
2	2	3
4	2	1
4	1	2
1	4	2
2	4	1
2	1	4
1	2	4

TYS.2

(HW)

a)

$$\begin{array}{cccccc} 1 & 2 & 3 & 4 & 5 & 6 \\ 2 & 0 & 0 & 0 & 0 & 0 \end{array}$$

$$\begin{array}{cccccc} 0 & 0 & 0 & 0 & 0 & 2 \end{array}$$

6

$$\begin{array}{cccccc} 1 & 1 & 0 & 0 & 0 & 0 \end{array}$$

$$\begin{array}{cccccc} 1 & 0 & 0 & 0 & 0 & 1 \end{array}$$

5

$$\begin{array}{cccccc} 0 & 1 & 1 & 0 & 0 & 0 \end{array}$$

$$\begin{array}{cccccc} 0 & 1 & 0 & 0 & 0 & 1 \end{array}$$

4

$$n_B = 6 + 5 + 4 + 3 + 2 + 1$$

$$= 21$$

$$b) \quad n(N, U) = \frac{(q + 3N - 1)!}{2! (3N - 1)!}$$

$$U_B = 6 \text{ e}$$

$$U_D = 9 \text{ e}$$

$$3N = 6$$

$$\frac{(6 + 6 - 1)!}{6! 5!}$$

$$\frac{11!}{6! 5!}$$

$$\frac{11!}{6! 5!}$$

$$\frac{11!}{6! 5!}$$

$$\frac{11 \cdot 10 \cdot 9 \cdot 8 \cdot 7}{5 \cdot 4 \cdot 3 \cdot 2 \cdot 1}$$

$$66 \cdot 7 = 462$$

$$66 \cdot 7 = 462$$

$$\frac{(9 + 6 - 1)!}{9! 5!}$$

$$\frac{14!}{9! 5!}$$

$$\frac{14!}{9! 5!}$$

$$\frac{14!}{9! 5!}$$

$$\frac{14 \cdot 13 \cdot 12 \cdot 11 \cdot 10}{5 \cdot 4 \cdot 3 \cdot 2}$$

$$5432$$

$$5432$$

$$\frac{14!}{9! 5!}$$

$$\frac{14!}{9! 5!}$$

$$\frac{14!}{9! 5!}$$

$$\frac{14!}{9! 5!}$$

$$\frac{14!}{9! 5!}$$

$$\frac{14!}{9! 5!}$$

$$\frac{14!}{9! 5!}$$

$$\frac{14!}{9! 5!}$$



T4S.3

(1-4W)

a)	(1) $U_A$	(2) $U_B$	$\Omega_A$	$\Omega_B$	$\Omega_{AB}$
	6	0	28	1	28
	5	1	21	6	126
	4	2	15	21	315
	3	3	10	56	560
	2	4	6	126	756
	1	5	3	252	756
	0	6	1	462	462

b)  $U_A = 1$   $U_B = 5$

$\frac{U_A}{N_A} = 1$   $\frac{U_B}{N_B} = 2.5$

$U_A = 2$   $U_B = 4$

$\frac{U_A}{N_A} = 2$   $\frac{U_B}{N_B} = 2$

+45.4

<u><math>V_A</math></u>	<u><math>V_B</math></u>	<u><math>N_A</math></u>	<u><math>N_B</math></u>	<u><math>N_{AB}</math></u>
9	0	55	1	55
8	1	45	6	270
7	2	36	21	756
6	3	28	56	1568
5	4	21	126	2646
4	5	15	252	3780
3	6	10	462	4620
2	7	6	792	4752
1	8	3	1287	3861
0	9	1	2002	2002

$$\frac{V_A}{N_A} = 2$$

$$\frac{V_B}{N_B} = \frac{7}{2} = 3.5$$

+45.5

a)	<u>U<sub>A</sub></u>	<u>U<sub>B</sub></u>	<u>Ω<sub>A</sub></u>	<u>Ω<sub>B</sub></u>	<u>Ω<sub>AB</sub></u>
	9	0	2002	1	2002
	8	1	1287	6	7722
	7	2	792	21	16632
	6	3	462	86	25872
	5	4	252	126	31752
	4	5	126	252	31752
	3	6	56	462	25872
	2	7	21	792	16632
	1	8	6	1287	7722
	0	9	1	2002	2002

b)  $\frac{5}{2} = 2.5$        $\frac{4}{2} = 2$

45.6

(HW)

- a)
- (1)  $2.828 \times 10^{13}$
  - (2) 10, 10  $3.447 \times 10^{12}$
  - (3) 2 and 2
  - (4) 0.3 ~ 0.7

- b)
- (1)  $3 \times 10^{144}$
  - (2) 100, 100  $1.3 \times 10^{143}$
  - (3) 2, 2
  - (4) 0.45 - 0.55

- c)
- # states increases,
  - # states become more concentrated toward

TY S. 7

a)  $U_A / N_A = U_B / N_B$

Not Always, -- eg 39/20

b) Hold true

# Recap w/ Stat Mech

$N_A$	$N_B$	$U_A$	$U_B$
2	3	3	5

$$\Omega_A = \frac{(3 \cdot 2 + 3 - 1)!}{(3 \cdot 2 - 1)! (3!)} = \frac{8!}{5! 3!}$$

$$= \frac{8 \cdot 7 \cdot 6}{3 \cdot 2} = \boxed{56}$$

$$\Omega_B = \frac{(3 \cdot 3 + 5 - 1)!}{(3 \cdot 3 - 1)! 5!} = \frac{13!}{8! 5!}$$

$$= \frac{13 \cdot 12 \cdot 11 \cdot 10 \cdot 9}{8 \cdot 7 \cdot 6 \cdot 5 \cdot 4}$$

$$= 13 \cdot 11 \cdot 9$$

2
99
1 13
297
990
<div style="border: 1px solid black; padding: 2px;">1287</div>

$N_A$	$N_B$	$U$
<u>10</u>	<u>10</u>	<u>10</u>

→ Notice that equal "shares" of energy are most probable...

→ Show effect gets more dramatic as  $N \rightarrow \infty$  (10, 100, 100)

<p>2nd Law of Thermodynamics</p> <hr/> <p>The entropy of an isolated system never <u>decreases</u>.</p>
---

### Interesting Cases

→ Small # Atoms, lots of energy  
5 5 1000

→ Not Narrow

→ Large # Atoms, limited energy  
1000, 1000, 10

# Lecture T5 + T6

Caused  
Confusion -  
What is  
A vs B?  
Micro  
or  
meso

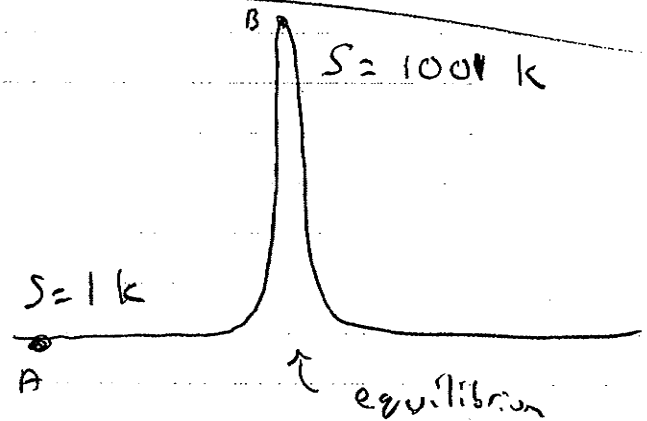
$$S = k \log \Omega$$

$$\Rightarrow S_{AB} = S_A + S_B$$

$$\boxed{Q:} \frac{P_{\text{prob}}(A)}{P_{\text{prob}}(B)} = \frac{\Omega_A}{\Omega_B} = \frac{\exp(S_A/k)}{\exp(S_B/k)} = \exp\left(\frac{S_A - S_B}{k}\right)$$

Irreversibility

$$\frac{P(A)}{P(B)} = \exp(-1000)$$



At later time, much much much more likely to observe is state B than A...

2nd Law:

The entropy of an isolated system never decreases.



What is Entropy?

$$S = k \ln \Omega$$

Order vs Disorder

1 2 3 4 5 6 7 8

$$\Omega = 1 \quad S = 0$$

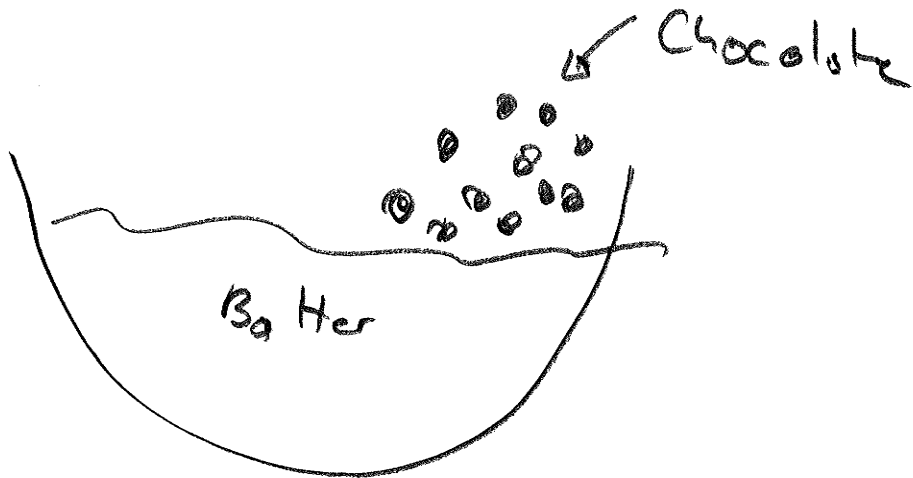
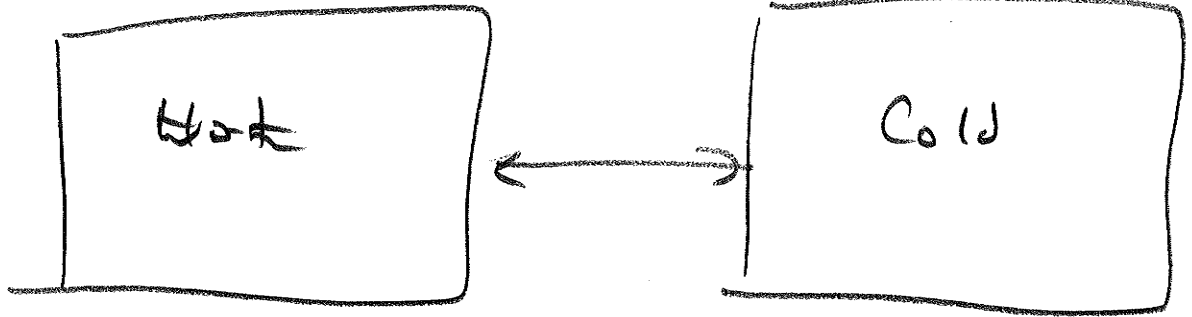
1 2 3 4 5 6 7 8

$$\Omega = 8 \quad S \sim 2k$$

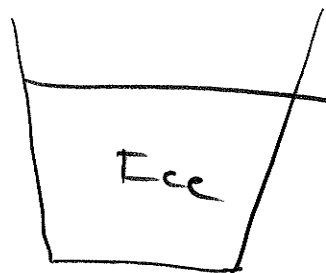
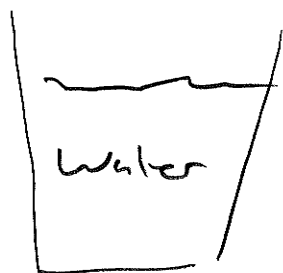
2 5 1 4 3 6 7

$$S \gg 1$$

# Examples



Which has higher Entropy?



Answers):

- (1) One must add  $Q$  to ice in order to make water. . .  
More energy generally  $\Rightarrow$  more  $S$

(2)  $\frac{1}{T} = \frac{\partial S}{\partial U} \Rightarrow \Delta S = T_{\text{freeze}} \cdot \Delta Q$

Q2:

Does answer depend on  $T$ ?

A:

Entropy of system ( $G + \text{Reservoir}$ )  
Entropy of water . . .  $T_{\text{freeze}}$  No!

T6

## Temperature and Entropy

New definition:

Equilibrium system, maximizes entropy at  
i.e.

$$\frac{dS_{AB}}{dU_A} = 0$$

$$S_{AB} = S_A + S_B$$

$$\Rightarrow 0 = \frac{dS_A}{dU_A} + \frac{dS_B}{dU_A}$$

$$U_A + U_B = \text{const} \Rightarrow dU_A = -dU_B$$

$$0 = \frac{dS_A}{dU_A} - \frac{dS_B}{dU_B}$$

$$\Rightarrow \boxed{\frac{dS_A}{dU_A} = \frac{dS_B}{dU_B}}$$

\* The quantity

$\frac{dS}{dU}$  is the same for A + B

at equilibrium.

Q What else is the same?  $T$  !!!

Pick

$$\frac{1}{T} = \frac{dS}{dU}$$

Is consistent  $\rightarrow$  higher temps, higher energy

(Will show later for ideal gas)

~~For  $E_{avg}$  look at  $S$  vs  $E$  graph~~

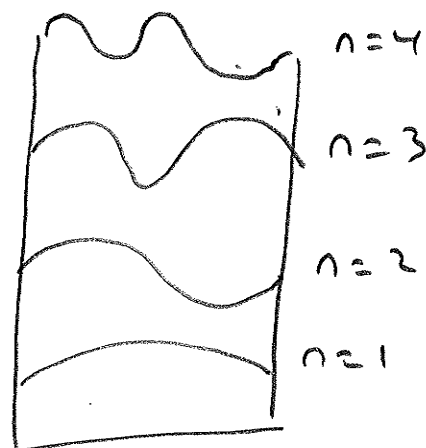
# Particle in a Box $\rightarrow$ Ideal Gas

Recall: (Don't show to students they don't have QM yet...)

$$\lambda = \frac{h}{p}$$

$$\lambda = \frac{2L}{n} = \frac{h}{p}$$

$$n \sim p \Rightarrow U \sim p^2 \sim n^2$$



What we say:

QM tells us for particle constrained in a volume

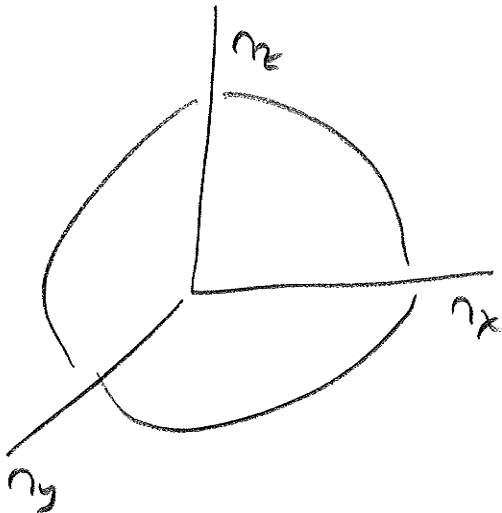
$$U = \sum \left( n_x^2 + n_y^2 + n_z^2 \right)$$

Quantum Numbers which enumerate microstates.

For now just assume this is true.

So

$$\frac{U}{\epsilon} = n_x^2 + n_y^2 + n_z^2 \equiv n^2 \Rightarrow n \sim \sqrt{\frac{U}{\epsilon}}$$



Consider 1 particle of a gas with Energy  $U$ . This particle can occupy any state from those with  $n=0$  to  $n=\sqrt{\frac{U}{\epsilon}}$

i.e.  $\Omega_1 \sim n^3 \sim \left(\frac{U}{\epsilon}\right)^{3/2}$

$$\Omega_N \sim \left(\frac{U}{\epsilon}\right)^{3/2 N}$$

$$S = k \log \Omega_N \sim k \log U^{3/2 N} \\ \sim \frac{3}{2} N k \log \left(\frac{U}{\epsilon}\right)$$

$$\frac{1}{T} \equiv \frac{\partial S}{\partial U} = \frac{3}{2} N k \frac{(1/\epsilon)}{(U/\epsilon)} = \frac{3}{2} N k \frac{1}{U}$$

$$\Rightarrow U = \frac{3}{2} N k T$$

(Temperature of Einstein Solids)

Gong ping's Trick

(Gongping Niu)

$$\Omega = \frac{(3N-1+q)!}{(3N-1)! q!}$$

$$\log \Omega = \log (3N-1+q)! - \log q! - \log (3N-1)!$$

To use Stirling's Approximation, we only need  $q \gg 1$   
(the last term is just a constant)

$$\log \Omega = (3N-1+q) \log (3N-1+q) - q \log q + \text{Const}$$

Gong ping's trick:

$$= (3N-1) \log (3N-1+q) + q \log (3N-1+q) - q \log q + \text{Const}$$

$$= (3N-1) \log (3N-1+q) + \log \left( \frac{3N-1+q}{q} \right)^q$$

$$\lim_{q \rightarrow \infty} \left( \frac{3N-1+q}{q} \right)^q = \lim_{q \rightarrow \infty} \left( 1 + \frac{3N-1}{q} \right)^q \\ = \exp(3N-1)$$

Hence:

$$\log \Omega = (3N-1) \log (3N-1+q) + \text{Const}$$



$$\frac{1}{T} = \frac{k}{\varepsilon} \frac{\partial}{\partial q} \log \Omega$$

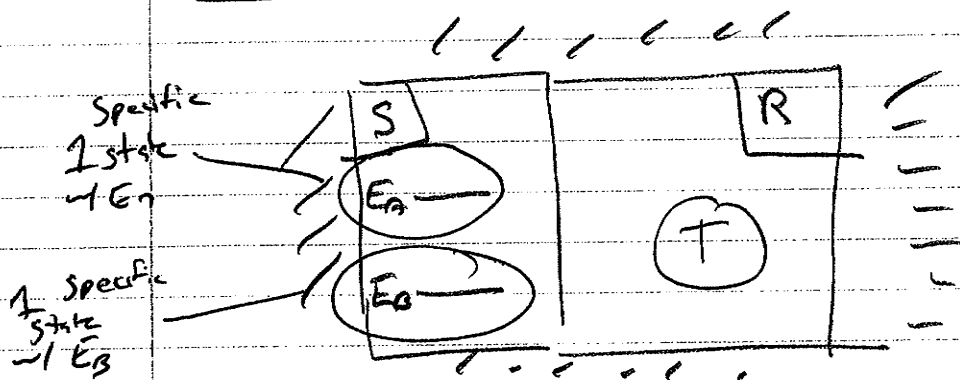
$$= \frac{k}{\varepsilon} \frac{3N-1}{3N-1+2} = \frac{k}{\varepsilon q} \cdot \frac{3N-1}{1 + \left(\frac{3N-1}{q}\right)}$$

$$\boxed{\frac{1}{T} = \frac{k}{U} (3N-1)}$$

(True for both  
large and small  
 $N$ , large  $\varepsilon$ !)

For large  $N$  this is

## Boltzmann Factor



$$\rightarrow P(A) / P(B) = ?$$

$\rightarrow$  In thermal contact w/ reservoir at  $T$

$\rightarrow$  Isolated

$\rightarrow$  Reservoir:

- large system

-  $T$  is constant, even if heat flows in/out of reservoir.

$$\frac{P(A)}{P(B)} = \frac{\Omega_{A}^{S+R}}{\Omega_{B}^{S+R}} = \frac{\Omega_{A}^S}{\Omega_{B}^S} \cdot \frac{\Omega_{A}^R}{\Omega_{B}^R} = \frac{\Omega_{A}^R}{\Omega_{B}^R}$$

$$\Omega_A^S / \Omega_B^S = 1/1 = 1 \text{ (by construction!)} \quad \Omega_A^R / \Omega_B^R = \frac{\Omega_A^R}{\Omega_B^R}$$

$$\frac{P(A)}{P(B)} = \frac{\exp(S_A^R / k)}{\exp(S_B^R / k)} = \exp\left(\frac{S_A^R - S_B^R}{k}\right)$$

Discuss!

rel prob of  
2 configs  
of S

Entropy difference  
of R

For the reservoir

$$\frac{\partial S}{\partial U} = \frac{1}{T} = \underline{\text{const.}}$$

$$\Rightarrow \Delta S^R = \Delta U^R / T$$

$$S_A^R - S_B^R = (U_A^R - U_B^R) / T$$

Isolated sys

$$E_A + U_A^R = E_B + U_B^R$$

$$\Rightarrow U_A^R - U_B^R = -(E_A - E_B)$$

Finally:

$$\boxed{\frac{p(A)}{p(B)} = \exp\left(\frac{-(E_A - E_B)}{kT}\right)}$$

Not possible to overstate the importance...

Normalization

$$P(E_i) = C \cdot \exp(-E_i/kT)$$

$$\frac{P(E_A)}{P(E_B)} = \frac{C \cdot \exp(-E_A/kT)}{C \cdot \exp(-E_B/kT)}$$

$$= \exp\left(\frac{-(E_A - E_B)}{kT}\right) \quad \checkmark$$

But what is  $C$ ?

$$\sum_i P(E_i) = 1$$

$$\sum_i C \cdot \exp(-E_i/kT) = 1$$

$$\frac{1}{C} = \sum_i \exp(-E_i/kT) \equiv Z$$

$$P(E_i) = \frac{1}{Z} \exp(-E_i/kT)$$

$$Z = \sum_i \exp(-E_i/kT)$$

## Alternate Solution to TGS.9

Define ground state by all protons  
(lowest energy configuration)

The energy of a state with  $N_n$  protons  
is therefore:

$$U = \varepsilon N_n \Rightarrow N_n = \frac{U}{\varepsilon}$$

We also must have

$$N = N_n + N_p \Rightarrow N_p = \left(N - \frac{U}{\varepsilon}\right)$$

The multiplicity of states is

$$\Omega = \frac{(N_n + N_p)!}{N_n! N_p!}$$

$$S = k \log \Omega = k \log (N_n + N_p)! - k \log N_n! - k \log N_p!$$

Use Stirling's approximation:

$$N! = N \log N - N \quad (\text{for large } N)$$

$$S = k(N_n + N_p) \log(N_n + N_p) - kN_n - kN_p \\ - kN_n \log N_n + kN_n - kN_p \log N_p + kN_p$$

The first term is constant, since  $N = N_n + N_p$  is conserved. So we can write as

$$S = S_0 - kN_n \log N_n - kN_p \log N_p$$

$$\text{Using } N_n = \frac{U}{\varepsilon} \quad N_p = N - \frac{U}{\varepsilon}$$

$$S = S_0 - k \frac{U}{\varepsilon} \log \frac{U}{\varepsilon} - \left(N - \frac{U}{\varepsilon}\right) k \log \left(N - \frac{U}{\varepsilon}\right)$$

$$\frac{\partial S}{\partial U} = -\frac{k}{\varepsilon} \log \frac{U}{\varepsilon} + \frac{k}{\varepsilon} \log \left(N - \frac{U}{\varepsilon}\right)$$

$$= -k \frac{U}{\varepsilon} \frac{1}{\left(\frac{U}{\varepsilon}\right)} - k \left(N - \frac{U}{\varepsilon}\right) \frac{(-1)}{\left(N - \frac{U}{\varepsilon}\right)}$$

$$\frac{1}{T} = \frac{\partial S}{\partial U} = \frac{k}{\varepsilon} \log \left( \frac{N - \frac{U}{\varepsilon}}{\frac{U}{\varepsilon}} \right) + 1$$

$$\boxed{\frac{\varepsilon}{kT} = \log \left( \frac{N_p}{N_n} \right)}$$

## Stirling's Approximation

$$\log(n!) = \log(1) + \log(2) + \dots + \log(n)$$

Trick: RHS looks like an integral  
except coefficients of  $\log(1)$  and  $\log(2)$ ...

$$\log(n!) - \frac{1}{2} \log(1) - \frac{1}{2} \log(n) \quad \log n \ll n$$

$$= \frac{\log(1) + \log(2)}{2} + \frac{\log(2) + \log(3)}{2} + \dots + \frac{\log(n-1) + \log(n)}{2}$$

$$\approx \int_1^n \log x \, dx$$

What is  $\int \log x \, dx$ ?

Integration by parts:

skip!

$$(uv)' = u'v + v'u$$

$$d(uv) = duv + vdu$$

$$u dv = uv - v du$$

$$u = \ln x \quad du = dx$$

$$dv = \frac{1}{x} dx \quad v = x$$

$$\int \log x \, dx = x \ln x - \int x \frac{1}{x} \cdot dx = x \log x - x$$

$$\Rightarrow \boxed{\log(n!) = n \log n - n}$$

Other Useful trick

$\exp(x)$  where  $x = \text{big number} \dots$

Trick: IF find  $y$  s.t.  $x = y \log 10$

then  $x = \log 10^y$

$$\exp(x) = \exp(\log 10^y) = 10^y$$

So, given  $x$ , calculate  $y = x / \log 10$

$$\boxed{\exp(x) = 10^{x / \log 10}}$$



# Maxwell - Boltzmann Distribution

T7

Consider a particle to be small system in equilibrium with reservoir at temperature  $T$  (the temperature of the gas)

$P_r$  (one particular microstate with speed  $u$ )

$$\propto e^{-E/kT} = e^{-\frac{mu^2}{2kT}}$$

$$\sqrt{\frac{2kT}{m}} = u_p$$

$$P_r(u) \propto e^{-u^2/u_p^2}$$

But there might be a different number of microstates at each value of  $u$ ,

What to do?

Recall: Confined particle has

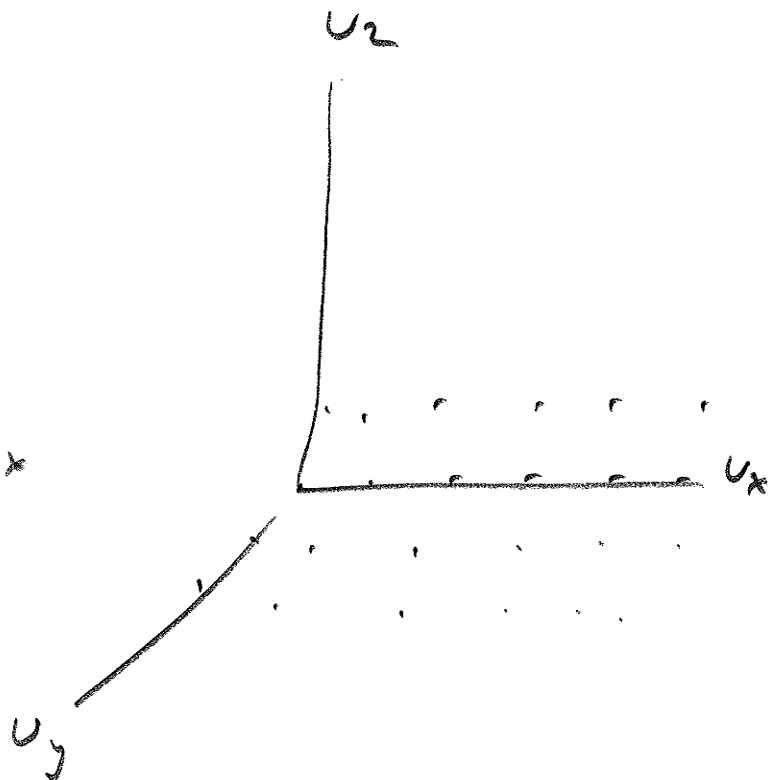
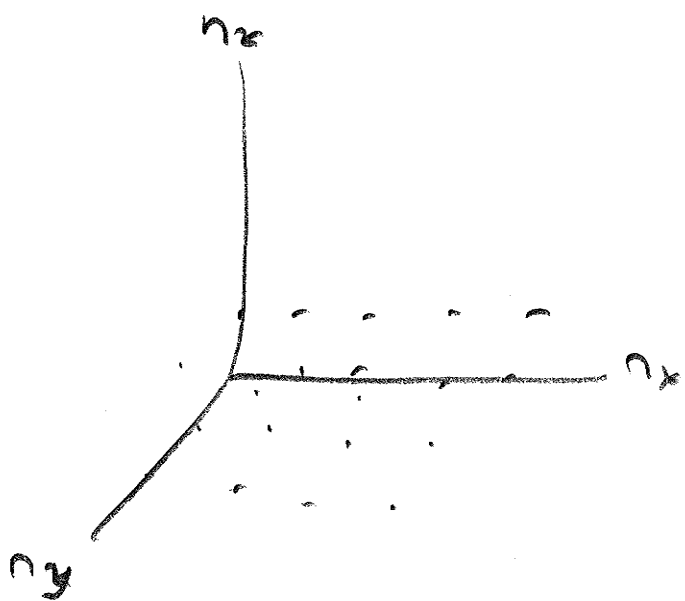
$$E = \varepsilon(n_x^2 + n_y^2 + n_z^2) = \frac{1}{2} m (v_x^2 + v_y^2 + v_z^2)$$

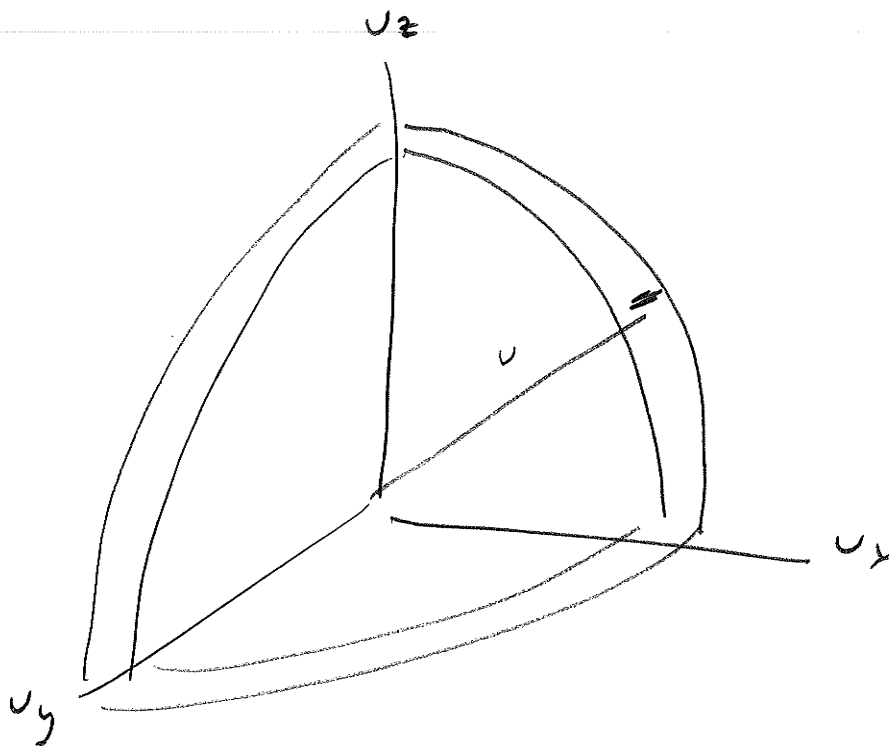
It turns out that in fact

$$|v_x| \propto n_x \quad |v_y| \propto n_y \quad |v_z| \propto n_z$$

Important point:

Microstates are uniform in  
velocity space





( # states  $\propto 4\pi u^2 du$

(Book says  $\frac{1}{8} \cdot 4\pi u^2 du$  since  $|u_x| > 0$ , etc)

But all we need is

$$n(u) \propto u^2 du \propto \left(\frac{u}{u_p}\right)^2 \frac{du}{u_p}$$

So Finally:

$$D(v) = N \cdot \left(\frac{v}{v_p}\right)^2 \frac{dv}{v_p} \exp\left(-\left(\frac{v}{v_p}\right)^2\right)$$

$$1 \equiv \int_0^{\infty} D(v) dv = N \cdot \int x^2 dx \exp(-x^2) \\ = N \cdot \frac{\sqrt{\pi}}{4}$$

$$\Rightarrow N = \frac{4}{\sqrt{\pi}}$$

$$Pr(v) = \frac{4}{\sqrt{\pi}} \left(\frac{v}{v_p}\right)^2 \left(\frac{dv}{v_p}\right) \exp\left(-\left(\frac{v}{v_p}\right)^2\right)$$

$$v_p \cdot \frac{dP}{dv} = \frac{4}{\sqrt{\pi}} \left(\frac{v}{v_p}\right)^2 \exp\left(-\left(\frac{v}{v_p}\right)^2\right)$$

↑ To get probabilities you have to either integrate over some range or approximate

$$P = \frac{dP}{dv} \cdot \Delta v$$

$$1) \quad I = \int x e^{-x^2} dx$$

$$\text{Let } y = x^2 \quad dy = 2x dx$$

$$I = \frac{1}{2} \int 2x dx e^{-x^2} = \frac{1}{2} \int dy e^{-y}$$

$$= -\frac{1}{2} e^{-y} = -\frac{1}{2} e^{-x^2}$$

$$\boxed{\int x e^{-x^2} dx = -\frac{1}{2} e^{-x^2}}$$

$$2) \quad I = \int_{-\infty}^{\infty} e^{-x^2} dx$$

$$I^2 = \int_{-\infty}^{\infty} e^{-x^2} dx \int_{-\infty}^{\infty} e^{-y^2} dy$$

$$= \iint e^{-(x^2+y^2)} dx dy$$

$$= \iint e^{-r^2} r dr d\theta$$

$$= \left. -\frac{1}{2} e^{-r^2} \right|_0^{\infty} \cdot 2\pi$$

$$= \pi$$

$$\Rightarrow I = \sqrt{\pi} = \int_{-\infty}^{\infty} e^{-x^2} dx$$

$$\text{So } \int_0^{\infty} e^{-x^2} dx = \frac{\sqrt{\pi}}{2}$$

$$3) \quad I = \int_0^{\infty} x^2 e^{-x^2} dx$$

$$u = x$$

$$du = dx$$

$$du = x e^{-x^2} dx$$

$$u = -\frac{1}{2} e^{-x^2}$$

$$\int_0^{\infty} x^2 e^{-x^2} = x \left( -\frac{1}{2} e^{-x^2} \right) \Big|_0^{\infty} + \frac{1}{2} \int_0^{\infty} e^{-x^2} dx$$

$$= 0 + \frac{1}{2} \cdot \frac{\sqrt{\pi}}{2} = \frac{\sqrt{\pi}}{4}$$

$$\int_0^{\infty} x^2 e^{-x^2} dx = \frac{\sqrt{\pi}}{4}$$

# Calculating Entropy Changes T8

$$\frac{1}{T} \equiv \frac{\partial S}{\partial U} \quad (\text{constant } V, W)$$

$$\Rightarrow dS = \frac{dU}{T} \quad (\text{at constant } V, W)$$

Easy cases:

1)  $\Delta T$  for ideal gas (constant  $V, W$ )

$$U = \frac{f}{2} N k T$$

$$dU = \frac{f}{2} N k dT$$

$$dS = \frac{f}{2} N k \frac{dT}{T}$$

$$S = \frac{f}{2} N k \int_{T_1}^{T_2} \frac{dT}{T} = \frac{f}{2} N k \ln\left(\frac{T_2}{T_1}\right)$$

2)  $dU = mc dT$

$$S = mc \ln\left(\frac{T_2}{T_1}\right)$$

Recall:  $\Delta U = Q + W$

Essentially, we've calculated  $\Delta S$

in case where  $W = 0$ ,

Now let's consider

$$Q = 0 \quad W \neq 0$$

But to make life easier, let's  
look at quasistatic work first  
(work done slowly, so system  
in equilibrium at every point.)

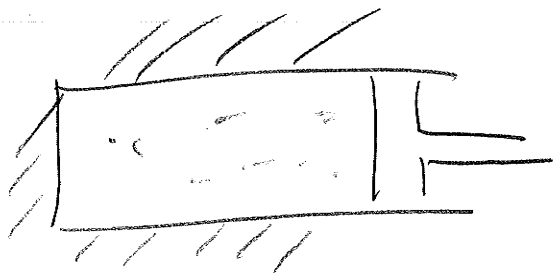
$$\Delta U = \cancel{Q} + W_{qs} + \cancel{W_{nqs}} \\ (Q=0) \quad (W_{nqs}=0)$$



**T8**

Quasistatic Adiabatic

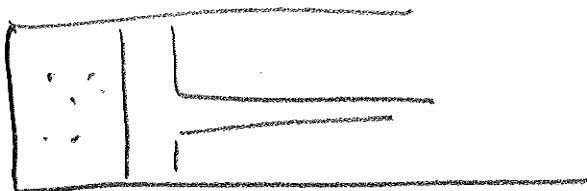
(I)



$$T_1, V_1$$

$$\leftarrow W_1$$

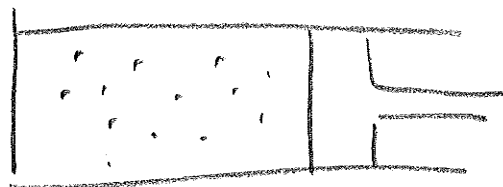
(II)



$$T_2, V_2$$

$$\leftarrow W_2$$

(III)



Return to  $V_1, T_3$

Q: What is  $T_2$ ?  $T_1 V_1^{\gamma-1} = T_2 V_2^{\gamma-1}$

$$\Rightarrow T_2 = T_1 \left( \frac{V_1}{V_2} \right)^{\gamma-1}$$

Q: What is  $T_3$ ?  $T_1 V_1^{\gamma-1} = T_3 V_1^{\gamma-1}$

$$\Rightarrow \boxed{T_1 = T_3}$$

$$\Delta U = 0$$

$$\Rightarrow W_1 + W_2 = 0$$

Reversible: Can return to original state with zero net work!

For monatomic gas

(T 8.7)

$$S \sim \ln V^{2/3} U$$

$$\sim \ln V^{2/3} T$$

During adiabatic compression of a

gas  $V^{2/3} T = \text{const}$

i.e.,  $\Delta S = 0$  during adiabatic

compression, expansion of a gas!!!

Is there a more general  
argument?

1st Try:

I  $\longrightarrow$  II reversible

I  $\rightarrow$  II  $\rightarrow$  I possible

$$\Delta S (I \rightarrow II \rightarrow I) = 0$$

$$\Delta S (I \rightarrow II) > 0$$

$$\Delta S (II \rightarrow I) < 0 \quad (\text{violates 2nd Law ???})$$

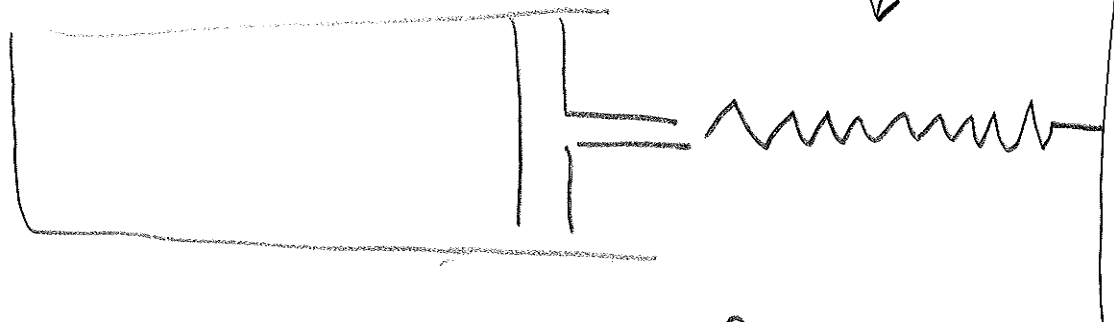
$\therefore \Delta S = 0$  for reversible processes.

Not quite so easy, because we can have work during

$$I \xrightarrow{w_1} II \xrightarrow{w_2} I$$

i.e. Not An isolated system !!!

# Patch-up Job:



Does it have  
Entropy?

$$\text{For } U_{\text{spring}} = \frac{1}{2} k x^2$$

there is only one  
state of spring:

$$\Omega = 1$$

$$S = 0 \quad \therefore$$

So patch up our  
argument


I  $\rightarrow$  II

w / work

beats  
(original system)

Spring System ( $S=0$ )

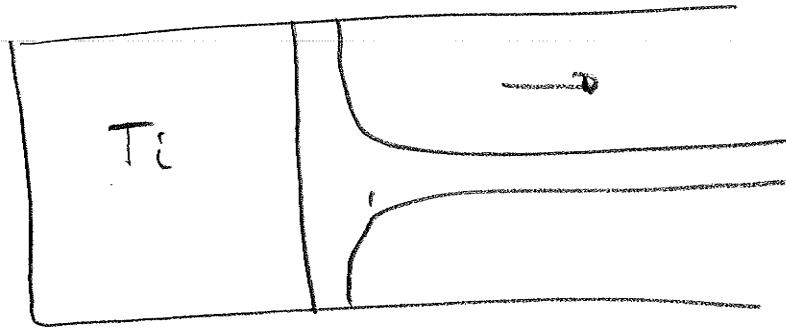
I  $\rightarrow$  II

+  

II  $\rightarrow$  I

+  

3)



Adiabatic Quasistatic Expansion, then heat!

$$TV^{2/5} = \text{const}$$

$$T_1 V_1^{2/5} = T_2 V_2^{2/5}$$

$$T_1 V^{2/5} = T_2 (2V)^{2/5}$$

$$\left(\frac{1}{2}\right)^{2/5} T_1 = T_2$$



$$\Delta S = \int \frac{dU}{T} = \int_{T_2}^{T_1} \frac{\frac{5}{2} N k dT}{T}$$

$$= \frac{5}{2} N k \ln(T_1/T_2)$$

$$T_1/T_2 = 2^{2/5}$$

$$= \boxed{N k \ln 2}$$

## Problems

T8B4       $\Delta S = \frac{Q}{T} = \frac{-35 \text{ J}}{(273 + 22) \text{ K}} = -0.12 \text{ J/K}$

T8B7       $\Delta Q = mL$

$$\Delta S = \frac{\Delta Q}{T} = \frac{mL}{T} = \frac{(0.125 \text{ kg})(2256 \text{ kJ/kg})}{(273 + 100) \text{ K}}$$
$$= 760 \text{ J/K}$$

T8S9      If this were done quasistatically,

$$\Delta T = 0, \quad \Delta S = 0$$

In this case, you would work harder to compress the gas, as the particle density would be higher near the cylinder.

So  $\Delta U = |W_1| - |W_2|$  where  $|W_1| > |W_2|$

So  $\Delta U > 0$ , so  $\boxed{\Delta T > 0}$ .

This is consistent with  $\boxed{\Delta S > 0}$