# Equations Of Motion of Krang on Fixed Wheels

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March 26, 2015

In this report we attempt to find the dynamic model of Golem Krang with its wheels fixed. So it is reduced to a serial robot with a tree-structure (due to two arms branching out). Figure 1 shows the frames of references we will be using to determine the transforms and the coordinates on the robot. We denote these frames using symbol  $R_i$  where  $i \in \mathbb{F} = \{0, 1, 2, 3, 4l, 5l, 6l, 7l, 8l, 9l, 10l, 4r, 5r, 6r, 7r, 8r, 9r, 10r\}$ .  $R_0$  is the world frame fixed in the middle of the two wheels.  $R_1, R_2, R_3$  are fixed on the base, spine and torso with their rotations represented by  $q_{imu}$ ,  $q_w$  and  $q_{torso}$  respectively. Frames  $R_{4l}, ...R_{10l}$  are frames fixed on the links left 7-DOF arm with their motion represented by  $q_{1l}, ...q_{7l}$ . Similarly, frames  $R_{4r}, ...R_{10r}$  are frames fixed on the links right 7-DOF arm with their motion represented by  $q_{1r}, ...q_{7r}$ . All equations in the following text that do not show r or l in the subscript where they are supposed to, will mean that the respective equations are valid for both subscripts.

We will be using the Lagrange formulation with a systematic approach presented in [1] to derive the equations of motion.

## 1 Introduction to Lagrange Formulation

The Lagrange formulation describes the behavior of a dynamic system in terms of work and energy stored in the system. The Lagrange equations are commonly written in the form:

$$\Gamma_i = \frac{d}{dt} \frac{\partial L}{\partial \dot{q}_i} - \frac{\partial L}{\partial q_i} \quad fori \in \mathbb{F}$$
 (1)

where L is the Lagrangian of the robot defined as the difference between the kinetic energy E and potential energy U of the system:

$$L = E - U$$

#### 1.1 General Form of the Dynamic Equations

The kinetic energy of the system is a quadratic function in the joint velocities such that:

$$E = \frac{1}{2}\dot{\mathbf{q}}^{\mathbf{T}}\mathbf{A}\dot{\mathbf{q}} \tag{2}$$

where **A** is the  $n \times n$  symmetric and positive definite *inertia matrix* of the robot. Its elements are functions of the joint positions. The (i, j) element of **A** 

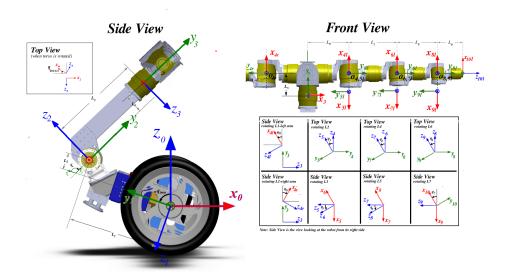


Figure 1: Frames of references on the robot

is denoted  $A_{ij}$ . Since the potential energy is a function of the joint positions, equation 1 leads to:

$$\Gamma = \mathbf{A}(\mathbf{q})\ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}} + \mathbf{Q}(\mathbf{q})$$
(3)

where:

- $\mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}}$  is the  $n \times 1$  vector of Coriolis and centrifugal torques, such that:  $\mathbf{C}\dot{\mathbf{q}} = \dot{\mathbf{A}}\dot{\mathbf{q}} \frac{\partial E}{\partial \mathbf{q}}$
- $\mathbf{Q} = \begin{bmatrix} Q_1 & Q_2 & Q_3 & Q_{4l} & \dots & Q_{10l} & Q_{4r} & \dots & Q_{10r} \end{bmatrix}^T$  is the vector of gravity torques

So the dynamic model of a tree-structured robot is described by n coupled and nonlinear second order differential equations. The elements of  $\mathbf{A}$ ,  $\mathbf{C}$  and  $\mathbf{Q}$  are functions of geometric and inertial parameters of the robot.

## 1.2 Computation of the elements of A, C and Q

To compute the elements of A, C and Q, we begin by symbollically computing the expressions of the kinetic and potential energies of all the links of the robot. Then we proceed as follows:

- the elements  $A_{ii}$  is equal to the coefficient of  $\left(\frac{\dot{q}_i^2}{2}\right)$  in the expression of the kinetic energy, while  $A_{ij}$ , for  $i \neq j$ , is equal to the coefficient of  $\dot{q}_i \dot{q}_j$
- for calculating the elements of  $\mathbf{C}$ , there exist several forms of the vector  $\mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}}$ . Using the *Christoffell symbols*  $c_{i,jk}$ , the (i,j) elements of the matrix  $\mathbf{C}$  can be written as:

$$\begin{cases}
C_{ij} = \sum_{k=1}^{n} c_{i,jk} \dot{q}_k \\
c_{i,jk} = \frac{1}{2} \left[ \frac{\partial A_{ij}}{\partial q_k} + \frac{\partial A_{ik}}{\partial q_j} - \frac{\partial A_{jk}}{\partial q_i} \right]
\end{cases}$$
(4)

• The  $Q_i$  element of the vector  $\mathbf{Q}$  is calculated according to:

$$Q_i = \frac{\partial U}{\partial q_i} \tag{5}$$

## 2 Finding A, C and Q for our robot

In this section we determine the symbolic expression for the total kinetic energy E of the robot.

### 2.1 Transformations

The transformation of frame  $R_i$  into frame  $R_j$  is represented by the homogeneous transformation matrix  ${}^iT_j$  such that.

$${}^{i}T_{j} = \begin{bmatrix} {}^{i}s_{j} & {}^{i}n_{j} & {}^{i}a_{j} & {}^{i}P_{j} \end{bmatrix} = \begin{bmatrix} {}^{i}A_{j} & {}^{i}P_{j} \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} s_{x} & n_{x} & a_{x} & P_{x} \\ s_{y} & n_{y} & a_{y} & P_{y} \\ s_{z} & n_{z} & a_{z} & P_{z} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
(6)

where  ${}^{i}s_{j}$ ,  ${}^{i}n_{j}$  and  ${}^{i}a_{j}$  contain the components of the unit vectors along the  $x_{j}$ ,  $y_{j}$  and  $z_{j}$  axes respectively expressed in frame  $R_{i}$ , and where  ${}^{i}P_{j}$  is the vector representing the coordinates of the origin of frame  $R_{j}$  expressed in frame  $R_{i}$ .

The transformation matrix  ${}^{i}T_{j}$  can be interpreted as: (a) the transformation from frame  $R_{i}$  to frame  $R_{j}$  and (b) the representation of frame  $R_{j}$  with respect to frame  $R_{i}$ . Using figure 1, we can write down these transformation matrices for our system as follows:

$${}^{0}T_{1} = \begin{bmatrix} 0 & sq_{imu} & -cq_{imu} & 0 \\ -1 & 0 & 0 & 0 & 0 \\ 0 & cq_{imu} & sq_{imu} & 0 \\ 0 & 0 & 0 & 0 & 1 \end{bmatrix}, {}^{1}T_{2} = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 \\ 0 & cq_{w} & sq_{w} & L_{1} \\ 0 & -sq_{w} & cq_{w} & -L_{2} \\ 0 & 0 & 0 & 1 \end{bmatrix}, {}^{2}T_{3} = \begin{bmatrix} -cq_{torso} & 0 & sq_{torso} & 0 \\ 0 & 1 & 0 & L_{3} \\ -sq_{torso} & 0 & -cq_{torso} & L_{4} \\ 0 & 0 & 0 & 1 \end{bmatrix}, {}^{2}T_{3} = \begin{bmatrix} -cq_{torso} & 0 & sq_{torso} & 0 \\ 0 & 1 & 0 & L_{3} \\ -sq_{torso} & 0 & -cq_{torso} & L_{4} \\ 0 & 0 & 0 & 1 \end{bmatrix}, {}^{2}T_{3} = \begin{bmatrix} -cq_{torso} & 0 & sq_{torso} & 0 \\ 0 & 1 & 0 & L_{3} \\ -sq_{torso} & 0 & -cq_{torso} & L_{4} \\ 0 & 0 & 0 & 1 \end{bmatrix}, {}^{2}T_{3} = \begin{bmatrix} -cq_{torso} & 0 & sq_{torso} & 0 \\ 0 & 1 & 0 & L_{3} \\ -sq_{torso} & 0 & -cq_{torso} & L_{4} \\ 0 & 0 & 0 & 1 \end{bmatrix}, {}^{2}T_{3} = \begin{bmatrix} -cq_{torso} & 0 & sq_{torso} & 0 \\ 0 & 1 & 0 & L_{3} \\ -sq_{torso} & 0 & -cq_{torso} & L_{4} \\ 0 & 0 & 0 & 1 \end{bmatrix}, {}^{2}T_{3} = \begin{bmatrix} -cq_{torso} & 0 & sq_{torso} & 0 \\ 0 & 1 & 0 & L_{3} \\ -sq_{torso} & 0 & -cq_{torso} & L_{4} \\ 0 & 0 & 0 & 1 \end{bmatrix}, {}^{2}T_{3} = \begin{bmatrix} -cq_{torso} & 0 & sq_{torso} & 0 \\ 0 & 1 & 0 & L_{3} \\ -sq_{torso} & 0 & -cq_{torso} & L_{4} \\ 0 & 0 & 0 & 1 \end{bmatrix}, {}^{2}T_{3} = \begin{bmatrix} -cq_{torso} & 0 & sq_{torso} & 0 \\ 0 & 1 & 0 & L_{3} \\ -sq_{torso} & 0 & -cq_{torso} & L_{4} \\ 0 & 0 & 0 & 1 \end{bmatrix}, {}^{2}T_{3} = \begin{bmatrix} -cq_{torso} & 0 & sq_{torso} & 0 \\ 0 & 1 & 0 & L_{3} \\ -sq_{torso} & 0 & -cq_{torso} & L_{4} \\ 0 & 0 & 0 & 1 \end{bmatrix}, {}^{2}T_{3} = \begin{bmatrix} -cq_{torso} & 0 & sq_{torso} & 0 \\ -cq_{torso} & 0 & -cq_{torso} & 0 \\ -cq_{torso} & 0 & -cq_{torso} & 0 \\ -cq_{torso} & 0 & -cq_{torso} &$$

$${}^{3}T_{4l} = \begin{bmatrix} 0 & 1 & 0 & L_6 \\ cq_{1l} & 0 & -sq_{1l} & L_5 \\ -sq_{1l} & 0 & -cq_{1l} & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, {}^{3}T_{4r} = \begin{bmatrix} 0 & -1 & 0 & -L_6 \\ cq_{1r} & 0 & -sq_{1r} & L_5 \\ sq_{1r} & 0 & cq_{1r} & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, {}^{4}T_5 = \begin{bmatrix} -1 & 0 & 0 & 0 \\ 0 & -cq_2 & -sq_2 & 0 \\ 0 & -sq_2 & cq_2 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix},$$

$${}^{5}T_{6} = \begin{bmatrix} -cq_{3} & 0 & sq_{3} & 0 \\ 0 & -1 & 0 & -L_{7} \\ sq_{3} & 0 & cq_{3} & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, {}^{6}T_{7} = \begin{bmatrix} -1 & 0 & 0 & 0 \\ 0 & -cq_{4} & -sq_{4} & 0 \\ 0 & -sq_{4} & cq_{4} & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, {}^{7}T_{8} = \begin{bmatrix} -cq_{5} & 0 & sq_{5} & 0 \\ 0 & -1 & 0 & -L_{8} \\ sq_{5} & 0 & cq_{5} & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix},$$

$${}^{8}T_{9} = \begin{bmatrix} -1 & 0 & 0 & 0 \\ 0 & -cq_{6} & -sq_{6} & 0 \\ 0 & -sq_{6} & cq_{6} & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, {}^{9}T_{10} = \begin{bmatrix} -cq_{7} & -sq_{7} & 0 & 0 \\ 0 & 0 & -1 & -L_{9} \\ sq_{7} & -cq_{7} & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

### 2.2 Angular and Linear Velocities of Frames

The angular and linear velocities of the frames can be calculated using the recursive formulation:

$${}^{j}\omega_{j} = {}^{j}A_{i}{}^{i}\omega_{i} + {}^{j}e_{j}\dot{q}_{j} \tag{7}$$

$${}^{j}V_{j} = {}^{j}A_{i}\left({}^{i}V_{i} + {}^{i}\omega_{i} \times {}^{i}P_{j}\right) \tag{8}$$

where  ${}^{i}\omega_{j}$  and  ${}^{i}V_{j}$  denote the angular and linear velocities repectively of frame j measured with respect to the world frame and represented in frame i.  ${}^{j}e_{j}$  denotes the direction of local angular velocity of frame j represented in frame j.  $i, j \in \mathbb{F}$  identify the frames and i identifies the antecedent frame of j. So, the rotation  ${}^{j}A_{i}$  and the translation  ${}^{j}P_{i}$  that appear in these equations can not be directly deduced from the transformations listed in the previous section, as the they all represent  ${}^{i}T_{j}$  (note the position of i and j). Rather, we need to use following expressions to deduce our matrices:

$$j A_i = {}^i A_j^T$$
  
$$j P_i = -{}^i A_j^T {}^i P_j$$

Since frame  $R_0$  is fixed  ${}^0\omega_0$  and  ${}^0V_0$  are both  $\begin{bmatrix} 0 & 0 & 0 \end{bmatrix}^T$ . We can deduce directions of local angular velocities of the frames using figure 1 as follows.

$$\begin{split} ^{1}e_{1} &= \begin{bmatrix} -1 & 0 & 0 \end{bmatrix}^{T}, ^{2}e_{2} = \begin{bmatrix} -1 & 0 & 0 \end{bmatrix}^{T}, ^{3}e_{3} = \begin{bmatrix} 0 & -1 & 0 \end{bmatrix}^{T}, ^{4}e_{4} = \begin{bmatrix} 0 & -1 & 0 \end{bmatrix}^{T}, \\ ^{5}e_{5} &= \begin{bmatrix} -1 & 0 & 0 \end{bmatrix}^{T}, ^{6}e_{6} = \begin{bmatrix} 0 & -1 & 0 \end{bmatrix}^{T}, ^{7}e_{7} = \begin{bmatrix} -1 & 0 & 0 \end{bmatrix}^{T}, ^{8}e_{8} = \begin{bmatrix} 0 & -1 & 0 \end{bmatrix}^{T}, \\ ^{9}e_{9} &= \begin{bmatrix} -1 & 0 & 0 \end{bmatrix}^{T}, ^{10}e_{10} = \begin{bmatrix} 0 & 0 & -1 \end{bmatrix}^{T} \end{split}$$

This information can now be used to derive expressions for the angular and linear velocities of the frames.

#### 2.3 Kinetic Energy

The kinetic energy of the robot is given as:

$$E = \sum_{j \in \mathbb{F}} E_j \tag{9}$$

where  $E_j$  denotes the kinetic energy of link j, which can be computed by

$$E_{j} = \frac{1}{2} (\omega_{j}^{T} I_{Gj} \omega_{j} + M_{j} V_{Gj}^{T} V_{Gj})$$
(10)

where the velocity of the center of mass can be expressed as:

$$V_{Gj} = V_j + \omega_j \times S_j$$

and since:

$$J_j = I_{Gj} - M_j \hat{S}_j \hat{S}_j$$

equation 10 becomes:

$$E_j = \frac{1}{2} (\omega_j^T J_{Gj} \omega_j + M_j V_j^T V_j + 2\mathbf{M} \mathbf{S}_j^T (V_j \times \omega_j))$$
(11)

See section A in the appendix to know the details of the derivation.

### 2.4 Potential Energy

The total potential energy U of the robot is given by:

$$U = \sum_{j \in \mathbb{F}} U_j = \sum_{j \in \mathbb{F}} -M_j \mathbf{g}^T (L_{0,j} + S_j)$$
(12)

where  $L_{0,j}$  is the position vector from the origin  $O_0$  to  $O_j$  and  $\mathbf{g}$  is the gravitational acceleration. Projecting the vectors appearing in 12 into frame  $R_0$ , we obtain:

$$U_{j} = -M_{j} {}^{0}\mathbf{g}^{T} ({}^{0}P_{j} + {}^{0}A_{j} {}^{j}S_{j})$$
(13)

$$= -{}^{0}\mathbf{g}^{T}(M_{j}{}^{0}P_{j} + {}^{0}A_{j}{}^{j}\mathbf{MS}_{j})$$
(14)

$$= -\begin{bmatrix} {}^{0}\mathbf{g}^{T} & 0 \end{bmatrix} {}^{0}T_{j} \begin{bmatrix} {}^{j}\mathbf{M}\mathbf{S}_{j} \\ M_{j} \end{bmatrix}$$
 (15)

Given the frames defined in figure 1,  ${}^{0}\mathbf{g} = \begin{bmatrix} 0 & 0 & -g \end{bmatrix}^{T}$ .

## 3 Effects of forces and torques on the end effectors

The well known relationship between joint torques and end effector forces on a simple serial robot is:

$$\mathbf{\Gamma} = \mathbb{J}_n^T \mathbb{f}_{e@n}$$

where

- $\Gamma$  is the vector of torques of the individual joints in the chain
- $\mathbb{f}_{e@n} = \begin{bmatrix} f_{e@n} \\ \tau_{e@n} \end{bmatrix}$  is the wrench applied by the robot at the origin of the *n*th frame (i.e. the last link in the chain which has the end-effector mounted on it). This wrench is usually represented in frame  $R_n$  or in the world frame  $R_0$  denoted as  ${}^n\mathbb{f}_{e@n}$  or  ${}^0\mathbb{f}_{e@n}$  respectively.
- $\mathbb{J}_n$  is  $6 \times n$  Jacobian matrix of the robot calculated using:

$$\mathbb{J}_n = \begin{bmatrix} e_1 \times L_{1,n} & \dots & e_n \times L_{n,n} \\ e_1 & \dots & e_n \end{bmatrix}$$

where  $e_j$  denotes the unit vectors along the local angular velocities of the frame j and  $L_{j,n}$  is the position vector from  $O_j$  to  $O_n$ . These vectors are expressed in the same frame as the wrench  $\mathbb{f}_{e@n}$ . So for  ${}^0\mathbb{f}_{e@n}$  all vectors in the Jacobian matrix will be expressed in frame 0 and the Jacobian will be denoted as  ${}^0\mathbb{J}_n$ . Similarly for  ${}^n\mathbb{f}_{e@n}$  the Jacobian will be denoted  ${}^n\mathbb{J}_n$ .

### 3.1 Jacobians for the two-armed robot

For the case of krang, we will have two wrenches  $f_{el@10l}$  and  $f_{er@10r}$  applied at two end-effectors on the right and the left arms respectively. As previously el and er are identifying the wrench and 10l and 10r are idenfying the frames

at whose origin the wrenches are being applied. The joint torques will now be calculated using the equation:

$$\Gamma = \mathbb{J}_{10l}^T \mathbb{I}_{el@10l} + \mathbb{J}_{10r}^T \mathbb{I}_{er@10r}$$

$$\tag{16}$$

where

- $\bullet \ \ \Gamma = \begin{bmatrix} \tau_1 & \tau_2 & \tau_3 & \tau_{4l} & \dots & \tau_{10l} & \tau_{4r} & \dots & \tau_{10r} \end{bmatrix}^T$
- $\bullet \quad \mathbb{J}_{10l} = \begin{bmatrix} e_1 \times L_{1,10l} & e_2 \times L_{2,10l} & e_3 \times L_{3,10l} & e_{4l} \times L_{4l,10l} & \dots & e_{10l} \times L_{10l,10l} & O_{3 \times 7} \\ e_1 & e_2 & e_3 & e_{4l} & \dots & e_{10l} & O_{3 \times 7} \end{bmatrix}$
- $\bullet \quad \mathbb{J}_{10r} = \begin{bmatrix} e_1 \times L_{1,10r} & e_2 \times L_{2,10r} & e_3 \times L_{3,10r} & O_{3 \times 7} & e_{4r} \times L_{4r,10r} & \dots & e_{10r} \times L_{10r,10r} \\ e_1 & e_2 & e_3 & O_{3 \times 7} & e_{4r} & \dots & e_{10r} \end{bmatrix}$

## 4 Other terms in the Lagrange Equations

### 4.1 Considering Friction

The most often employed model for friction is composed of Coulomb friction together with viscous friction. Therefor, the friction torque at joint i is written as:

$$\Gamma_{fi} = F_{ci} sign(\dot{q}_i) + F_{vi} \dot{q}_i$$

To take into account the friction in the dynamic model of a robot we add the vector  $\Gamma_f$  to the right side of the Lagrange equation (i.e. the vector of generalized forces), such that:

$$\Gamma_f = \operatorname{diag}(\dot{\mathbf{q}})\mathbf{F_v} + \operatorname{diag}[\operatorname{sign}(\dot{\mathbf{q}})\mathbf{F_c}]$$
(17)

where

- $\bullet \ \mathbf{F}_v = \begin{bmatrix} F_{v1} & F_{v2} & F_{v3} & F_{v4l} & \dots & F_{v10l} & F_{v4r} & \dots & F_{v10r} \end{bmatrix}^T$
- $\mathbf{F}_c = \begin{bmatrix} F_{c1} & F_{c2} & F_{c3} & F_{c4l} & \dots & F_{c10l} & F_{c4r} & \dots & F_{c10r} \end{bmatrix}^T$
- $\mathbf{diag}(\dot{\mathbf{q}}) is the diagonal matrix whose elements are the components of \dot{\mathbf{q}}$

#### 4.2 Considering rotor inertia

The kinetic energy of the rotor (and transmission system) and actuator j, is given by the expression  $\frac{1}{2}I_{aj}\dot{q}_j^2$ . The inertial parameter  $I_{aj}$  denotes the equivalent inertia referred to the joint velocity. It is given by:

$$I_{aj} = N_j^2 J_{mj} (18)$$

where  $J_{mj}$  is the moment of inertia of the rotor and transmissions of actuator j,  $N_j$  is the transmission ratio of the joint axis, equal to  $\frac{\dot{q}_{mj}}{\dot{q}_j}$  where  $\dot{q}_{mj}$  denotes the rotor velocity of actuator j. In the case of a prismatic joint,  $I_{aj}$  is an equivalent mass.

In order to consider the rotor inertia in the dynamic model of the robot, we add the inertia (or mass)  $I_{aj}$  to the  $A_{jj}$  element of the matrix **A**.

### 5 MATLAB code

The dynamic model is generated using a script dynamicModel.m found in the folder stableForceInteraction/Implementation/1-ForceControlWhileBalancing/1-ControlProblem1/1-DynamicModeling/2-DynamicModelOfTreeStructuredRobot/2-matlab/Lagrange. The function populates the frame information in a map container using getKrangFrames(), then calculates the total kinetic energy, total potential energy, then the matrices A, C and Q using functions totalKE(), totalPE(), findA(), findC() and findQ(). The resulting matrices are saved in the symbolic variables AA, CC and QQ which can be loaded in the workspace by loading the mat file Lagrange.mat.

### 5.1 Map Container for all the Frame Information

The function getKrangFrames() populates the information in a map container f. A map container is a data structure in MATLAB that stores a list of data that is retrievable using a key. We store a frame structure in each cell of the map and use strings  $s \in \mathbf{S} = \{ \ '0', \ '1', \ '2', \ '3', \ '41', \ '51', \ '61', \ '71', \ '81', \ '91', \ '101', \ '4r', \ '5r', \ '6r', \ '7r', \ '8r', \ '9r', \ '10r' \}$  as a key to retrieve information. The frame structure stores the following elements:

- x the unit vector along x-axis represented in the antecedent frame
- y the unit vector along y-axis represented in the antecedent frame
- z the unit vector along z-axis represented in the antecedent frame
- P the position of the origin frame represented in the antecedent frame
- e the unit vector along direction of positive rotation of the frame represented in the local frame
- a the string  $\in \mathbf{S}$  (defined above) that is the key that maps to the antecedent frame
- ${\tt q}$  the symbolic variable used for representing the generalized position q associated with this frame
- ${\tt dq}$  the symbolic variable used for representing the generalized speed  $\dot{q}$  associated with this frame
- ddq the symbolic variable used for representing the generalized acceleration  $\ddot{q}$  associated with this frame
  - o the row number in the inertia matrix  ${\bf A}$  (i.e. in the final dynamic model  ${\bf A}\ddot{{\bf q}}+{\bf C}\dot{{\bf q}}+{\bf Q}={\bf F})$  that corresponds to the current joint

param array of ten symbolic variables used to represent the inertial parameters of the joint [m] MX MY MZ XX YY ZZ XY XZ YZ $]^T$ 

### 5.2 Functions associated with the Map Container

There are a number of functions that take the map container **f** as the input argument and construct a useful information as an output. Here is a list of those functions:

- isBefore(f, key1, key2) returns true if frame 1 (identified by key1) is before frame 2 (identified by key2) in the tree structure of the robot
  - Rot(f, key1, key2) returns rotation transform  ${}^{j}A_{i}$  i.e. represention of frame i (identified by key1) in frame j (identified by key2)
  - Tf(f, key1, key2) returns rotation transform  ${}^{j}T_{i}$  i.e. represention of frame i (identified by key1) in frame j (identified by key2)
    - qVec(f) generates the vector  $\mathbf{q}$  containing generalized positions of all frames
    - dqVec(f) generates the vector  $\dot{\mathbf{q}}$  containing generalized speeds of all frames
    - mass(f, key) returns the mass of the frame identified by the key
    - mcom(f, key) returns the mass times COM  $(MS = [MX \ MY \ MZ]^T)$  of the joint identified by the key represented in the local frame
  - $\begin{array}{ll} \text{inertiaMat(f, key)} & \text{returns the inertia matrix } \left( \mathbf{J} = \begin{bmatrix} \mathbf{XX} & \mathbf{XY} & \mathbf{XZ} \\ \mathbf{XY} & \mathbf{YY} & \mathbf{YZ} \\ \mathbf{XZ} & \mathbf{YZ} & \mathbf{ZZ} \end{bmatrix} \right) \text{ of the joint indentified by } \\ \text{key represented in the local frame} \\ \end{aligned}$ 
    - angVel(f, key) returns the symbolic expression for the angular velocity  $(\bar{\omega})$  of the joint represented in local frame calculated recursively using eq. 7
    - linVel(f, key) returns the symbolic expression for the linear velocity  $(\bar{v})$  of the joint represented in local frame calculated recursively using eq. 8

#### 5.3 Main functions

The main functions that are used in the script to find the dynamic model are briefly explained here:

- totalKE() Finds the symbolic expression for the total kinetic energy of the system. This is done by calling function KE() for every joint which in turn uses the eq.11. The quantities such as inertia, velocities etc. needed for evaluating the kinetic energy expression are supplied by the helper functions dicussed in the previous section
- totalPE() Finds the symbolic expression for the total potential energy of the system.

  This is done by calling function PE() for every joint which in turn uses the eq.15 to find out the potential energy
  - findA() This function uses the method as described in section 1.2 to find the A. The elements  $A_{ii}$  is equal to the coefficient of  $\left(\frac{\dot{q}_i^2}{2}\right)$  in the expression of the kinetic energy, while  $A_{ij}$ , for  $i \neq j$ , is equal to the coefficient of  $\dot{q}_i \dot{q}_j$
  - findC() This function uses the equation 4 to evaluate the symbolic expressions for the elements of C matrix

findQ() This function uses the equation 5 to evaluate the symbolic expressions for the elements of  $\mathbf{Q}$  matrix

## References

[1] Wisama Khalil and Etienne Dombre. *Modeling, identification and control of robots*. Butterworth-Heinemann, 2004.

## A Expression for Kinetic Energy

We show here how the equation 11 was derived from 10. Equation 10 is:

$$E_{j} = \frac{1}{2} (\omega_{j}^{T} I_{Gj} \omega_{j} + M_{j} V_{Gj}^{T} V_{Gj})$$
(19)

where the velocity of the center of mass can be expressed as:

$$V_{Gj} = V_j + \omega_j \times S_j$$

and since:

$$J_j = I_{Gj} - M_j \hat{S}_j \hat{S}_i^T$$

So equation 19 becomes:

$$E_j = \frac{1}{2} (\omega_j^T (J_j + M_j \hat{S}_j \hat{S}_j) \omega_j + M_j (V_j + \omega_j \times S_j)^T (V_j + \omega_j \times S_j))$$

$$E_j = \frac{1}{2} (\omega_j^T J_j \omega_j + M_j V_j^T V_j + \omega_j^T M_j \hat{S}_j \hat{S}_j \omega_j + M_j V_j^T (\omega_j \times S_j)$$

$$+ M_j (\omega_j \times S_j)^T V_j + M_j (\omega_j \times S_j)^T (\omega_j \times S_j))$$

Noting that the last term:

$$\begin{aligned} M_j(\omega_j \times S_j)^T(\omega_j \times S_j) &= (-)(-)M_j(S_j \times \omega_j)^T(S_j \times \omega_j) \\ &= M_j(\hat{S}_j\omega_j)^T(\hat{S}_j\omega_j) \\ &= M_j\omega_j^T \hat{S}_j^T \hat{S}_j\omega_j \\ &= -M_j\omega_j^T \hat{S}_j \hat{S}_j\omega_j \end{aligned}$$

cancels out the third term. And noting that the fourth and fifth terms are equal, we are left with:

$$E_j = \frac{1}{2} (\omega_j^T J_j \omega_j + M_j V_j^T V_j + 2M_j (\omega_j \times S_j)^T V_j)$$

The last term in the above expression can be simplified as follows:

$$M_{j}(\omega_{j} \times S_{j})^{T} V_{j} = M_{j}(\hat{\omega}_{j} S_{j})^{T} V_{j}$$

$$= M_{j} S_{j}^{T} \hat{\omega}_{j}^{T} V_{j}$$

$$= -M_{j} S_{j}^{T} \hat{\omega}_{j} V_{j}$$

$$= -M_{j} S_{j}^{T} (\omega_{j} \times V_{j})$$

$$= \mathbf{MS}_{j}^{T} (V_{j} \times \omega_{j})$$

so we end up with:

$$E_j = \frac{1}{2} (\omega_j^T J_{Gj} \omega_j + M_j V_j^T V_j + 2\mathbf{MS}_j^T (V_j \times \omega_j))$$

## B MATLAB Code Listings

In this section we present the code for the MATLAB functions discussed in the report.

### B.1 dynamicModel.m

```
% author: Mnzir Zafar
% cate: Aug 2, 2014
% brief: Finding the dynamic model of krang

5     f = getKrangFrames(17);
    E = total KE(f);
    A = findA(f, E);
    C = findC(f, A);

10     Q = findQ(f, U);
```

### **B.2** getKrangFrames()

```
function f = getKrangFrames(nFrame)

% This first incorperates amps. The keys to the maps are string literals
% in 1' 1' 1' 2' 3' 3' 4' 1' 5' 1' 1' 10' 1' 4t', '5t', ... '10t')

% and the values are structs that have members associated with the
% respective joints of the rubt.
% respective joints
```

```
% f('1') = frame;
F{2} = frame;
                  frame.x = sym([1; 0; 0]); frame.y = [0; cos(q_w); -sin(q_w)]; frame.z = [0; sin(q_w); cos(q_w)]; frame.P = [0; L1; -L2]; frame.e = [-1; 0; 0]; frame.a = '1'; frame.q = q_w; frame.dq = dq_w; frame.ddq = ddq_w; frame.o = 2; frame.para = [m_2 MX_2 MY_2 MZ_2 XX_2 XY_2 XZ_2 YY_2 YZ_2 ZZ_2]; % f(Z) = frame; F(3) = frame;
  70
                   frame.x = [-cos(q_torso); 0; -sin(q_torso)]; frame.y = sym([0; 1; 0]); frame.z = [sin(q_torso); 0; -cos(q_torso)]; frame.P = [0; L3; L4]; frame.e = [0; -1; 0]; frame.a = '2'; frame.q = q_torso; frame.dq = dq_torso; frame.o = 3; frame.param = [m_3 MX_3 MY_3 MZ_3 XX_3 XY_3 XZ_3 YY_3 YZ_3 ZZ_3]; % ff'# = frame; F{4} = frame;
                   frame.x = [0; cos(q_11); -sin(q_11)]; frame.y = sym([1; 0; 0]); frame.z = [0; -sin(q_11); -cos(q_11)]; frame.P = sym([L6; L5; 0]); frame.e = [0; -1; 0]; frame.a = '3'; frame.q = q_11; frame.dq = dq_11; frame.ddq = ddq_11; frame.o = 4; frame.param = [m_41 MX_41 MY_41 MZ_41 XX_41 XY_41 XZ_41 YY_41 YZ_41 ZZ_41]; % f(\(\alpha \) = frame;
  85
                  frame.x = [-cos(q_31); 0; sin(q_31)]; frame.y = sym([0; -1; 0]); frame.z = [sin(q_31); 0; cos(q_31)]; frame.P = sym([0; -L7; 0]); frame.e = [0; -1; 0]; frame.a = '51'; frame.o = 6; frame.q = q_31; frame.dq = dq_31; frame.ddq = ddq_31; frame.param = [m_61 MX_61 MY_61 MZ_61 XX_61 XY_61 XZ_61 YY_61 YZ_61 ZZ_61]; % f(01') = frame;
                   frame.x = sym([-1; 0; 0]); frame.y = [0; -cos(q_41); -sin(q_41)]; frame.z = [0; -sin(q_41); cos(q_41)]; frame.P = sym([0; 0; 0]); frame.e = [-1; 0; 0]; frame.a = '61'; frame.o = 7; frame.q = q_41; frame.dq = dq_41; frame.dq = dq_41; frame.param = [m_71 MX_71 MY_71 MZ_71 XX_71 XY_71 XZ_71 YY_71 YZ_71 ZZ_71]; % f(Tl') = frame; F{8} = frame;
110
                   125
                   F{10} = frame;
                   frame.x = [-cos(q_71); 0; sin(q_71)]; frame.y = [-sin(q_71); 0; -cos(q_71)];
frame.z = sym([0; -1; 0]); frame.P = [0; -L9; 0];
frame.e = [0; 0; -1]; frame.a = '91';
frame.q = q_71; frame.dq = dq_71; frame.ddq = ddq_71; frame.o = 10;
frame.parm = [m_101 MX_101 MY_101 MZ_101 XX_101 XY_101 XZ_101 YY_101 YZ_101 ZZ_101];
                   % f('101') = frame;
F{11} = frame;
                   frame.x = [0; cos(q_1r); sin(q_1r)]; frame.y = sym([-1; 0; 0]); frame.z = [0; -sin(q_1r); cos(q_1r)]; frame.P = [-L6; L5; 0]; frame.e = [0; -1; 0]; frame.a = '3'; frame.q = q_1r; frame.dq = dq_1r; frame.ddq = ddq_1r; frame.o = 11; frame.para = [m_4r MX_4r MY_4r MZ_4r XX_4r XY_4r XZ_4r YY_4r YZ_4r ZZ_4r]; % f('4r') = frame; F(12) = frame;
145
                   frame.x = sym([-1; 0; 0]); frame.y = [0; -cos(q_2r); -sin(q_2r)]; frame.z = [0; -sin(q_2r); cos(q_2r)]; frame.P = sym([0; 0; 0]); frame.e = [-1; 0; 0]; frame.a = '4r'; frame.q = q_2r; frame.dq = dq_2r; frame.ddq = ddq_2r; frame.o = 12; frame.param = [m_5r MX_5r MY_5r MZ_5r XX_5r XY_5r XZ_5r YY_5r YZ_5r ZZ_5r]; % f('5r') = frame; frame; frame;
150
                   frame.x = [-cos(q_3r); 0; sin(q_3r)]; frame.y = sym([0; -1; 0]);
frame.z = [sin(q_3r); 0; cos(q_3r)]; frame.P = sym([0; -L7; 0]);
frame.e = [0; -1; 0]; frame.a = '5r';
frame.q = q_3r; frame.dq = dq_3r; frame.ddq = ddq_3r; frame.o = 13;
frame.param = [m_6r MX_6r MY_6r MZ_6r XX_6r XY_6r XZ_6r YY_6r YZ_6r ZZ_6r];
```

```
8 f('a') = frame;

frame.x = sym([-1; 0; 0]); frame.y = [0; -cos(q_4r); -sin(q_4r)];
frame.z = [0; -sin(q_4r); cos(q_4r)]; frame.P = sym([0; 0; 0]);
frame.e = [-1; 0; 0]; frame.a = '6r'; frame.o = 14;
frame.param = [m_7r MX_7r MY_7r MZ_7r XX_7r XY_7r XZ_7r YY_7r YZ_7r ZZ_7r];
8 f('A') = frame;

170

frame.x = [-cos(q_5r); 0; sin(q_5r)]; frame.y = sym([0; -1; 0]);
frame.z = (sin(q_5r); 0; cos(q_5r)); frame.P = sym([0; -1: 0]);
frame.z = (sin(q_5r); 0; cos(q_5r)); frame.P = sym([0; -1: 0]);
frame.a = [0; -1; 0]; frame.a = '7r'; frame.o = 15;
frame.q = q_5r; frame.dq = dq_5r; frame.ddq = ddq_5r; frame.o = 15;
frame.param = [n_5r MX_5r MY_6r MZ_6r XX_8r XX_8r XZ_6r YY_8r YZ_8r ZZ_8r];

8 f('8') = frame;

frame.z = sym([-1; 0; 0]); frame.y = [0; -cos(q_6r); -sin(q_6r)];
frame.z = (0; -sin(q_6r); cos(q_6r)]; frame.P = sym([0; 0; 0]);

frame.z = (0; -sin(q_6r); cos(q_6r)]; frame.P = sym([0; 0; 0]);

frame.a = q_6r; frame.dq = dq_6r; frame.dd = ddq_6r; frame.o = 16;
frame.param = [n_9r MX_9r MY_9r MZ_9r XX_9r XY_9r XZ_9r YY_9r YZ_9r ZZ_9r];

8 f('9') = frame;

frame.x = [-cos(q_7r); 0; sin(q_7r)]; frame.y = [-sin(q_7r); 0; -cos(q_7r)];
frame.z = sym([0; -1; 0]); frame.P = [0; -L9; 0];
frame.z = sym([0; -1; 0]); frame.e = [0; -1];
frame.x = [-cos(q_7r); frame.ed = dq_7r; frame.o = 17;
frame.x = [-cos(q_7r); frame.ed = dq_7r; frame.o = 17;
frame.x = [-cos(q_7r); frame.ed = dq_7r; frame.dd = ddq_7r; frame.o = 17;
frame.x = [-cos(q_7r); frame.ed = dq_7r; frame.dd = ddq_7r; frame.o = 17;
frame.a = [-cos(q_7r); frame.ed = dq_7r; frame.dd = ddq_7r; frame.o = 17;
frame.q = q_7r; frame.dq = dq_7r; frame.dd = ddq_7r; frame.o = 17;
frame.q = q_7r; frame.dq = dq_7r; frame.dd = ddq_7r; frame.o = 17;
frame.q = q_7r; frame.dq = dq_7r; frame.dd = ddq_7r; frame.o = 17;
frame.q = [-cos(q_7r); frame.ed = dq_7r; frame.dd = ddq_7r; frame.o = 17;
frame.q = q_7r; frame.dq = dq_7r; frame.dd = ddq_7r; frame.de = 17;
frame.q = [-cos(q_7r); frame.ed = 17; frame.dd = 17;
frame.q = [-cos(q_7r); frame.ed = 17; frame.dd = 17;
frame.q = [-cos(q_7r);
```

### B.3 totalKE()

#### B.4 totalPE()

#### $B.5 \quad findA()$

### $B.6 \quad findC()$

### $B.7 \quad findQ()$

```
function Q = findQ(f, U)

% Campute the symbolic expression for Q

g = qVec(f);
Q = sym(zeros(length(q), 1));
for i=1:length(q)
Q(i) = diff(U, q(i));
end
```

## B.8 angVel()

```
if(isequal(f(key).a, *0*)) % if it's the first link in the chain
w = Rot(f, f(key).a, key) * w0 * f(key).e*f(key).dq;
else % rearsive call if the frame is not the first link in the chain
w = Rot(f, f(key).a, key) * angVel(f, f(key).a) * f(key).e*f(key).dq;
end
```

### B.9 linVel()

```
function V = linVel(f, key, varargin)

% Calculate linear velocity of the current frame measured in the world
% frame represented in the current frame

8 'f' is the map container containing the information of the frames of
% the robot
% 'key' is this fies the current frame
% chical anguents
% 'W' is the angular velocity of the base frame

10 % 'VO' is the linear velocity of the base frame

if (nargin == 2)
    wo = [0;0;01;
    vo = [0;0;01;
    vo = varargin(1);
    yo = varargin(2);
end

20 if (is equal (f(key).a, 'o')) % if it's the first link in the chain
    V = Rot(f, f(key).a, key) * (VO + cross(wO, f(key).P));
else % if it's same other link
    V = Rot(f, f(key).a, key) * (linVel(f, f(key).a) + ...
    cross(angVel(f, f(key).a), f(key).P));
end
```

### B.10 Rot()

```
function A = Rot(f, key1, key2)

% Findtherotation transform of a frame
% for death empocartainer that contains information of the frames.

5 % key1 ichtifies the frame1 that is being represented
% key2 ichtifies frame2 in which frame1 is being represented
% This function assumes frame1 immediately follows frame2 or frame2
% immerdiately follows frame1

if (isequal(f(key1).a, key1)) % if frame2 is the antecedent of frame1

A = [f(key1).x f(key1).y f(key1).z];
elseif (isequal(f(key2).a, key1)) % if frame1 is the antecedent of frame2

A = [f(key2).x'; f(key2).y'; f(key2).z'];
end
```

### B.11 Tf()

```
function T = Tf(f, key1, key2)
% Findthetransformof a frame
% f chrotesthemap container that contains information of the frames.
% key1 icartifies the frame1 that is being represented
% key2 icartifies frame2 in which frame1 is being represented

if(isBefore(f, key2, key1)) % if frame2 is before frame1 in the chain
    T = [f(key1).x f(key1).y f(key1).z f(key1).P; 0 0 0 0 1];
    key = f(key1).a;
    while('isaqual(key, key2))
        T = [f(key).x f(key).y f(key).z f(key).P; 0 0 0 0 1] * T;
        key = f(key).a;
end

15 elseif(isBefore(f, key1, key2)) % if frame1 is before frame2 in the chain
    T = [f(key2).x' - f(key2).x'**f(key2).P; ...
        f(key2).z' - f(key2).z'**f(key2).P; ...
        0 0 0 0 1];
key = f(key2).a;
while('isaqual(key, key1))
    T = T * ff(key).x' - f(key).x'**f(key).P; ...
        f(key).y' - f(key).x'**f(key).P; ...
        f(key).y' - f(key).y'**f(key).P; ...
        f(key).y' - f(key).y'**f(key).P; ...
```

```
f(key).z' -f(key).z'*f(key).P; ...
0 0 0 11;
key = f(key).a;
end
end
```

## B.12 mass()

```
function m = mass(f, key)
param = f(key).param;
m = param(1);
```

### $B.13 \quad mCOM()$

```
function MS = mCOM(f, key)
param = f(key).param;
MS = param(2:4);
```

## B.14 inertiaMat()

```
function J = inertiaMat(f, key)
param = f(key).param;
J = param([5 6 7; 6 8 9; 7 9 10]);
```

## B.15 qVec()

## B.16 dqVec()

```
function dq = dqVec(f)

% Generate dqvector in the order defined by member 'd' of the frames
% contained in 'f'

key = keys(f);
n = length(key)-1;
dq = sym(zeros(n, 1));
for i=f:length(key)

if (isequal(key(i), '0')); continue; end
dq(f(key(i)).o) = f(key(i)).dq;
end
```

# B.17 getcoeff()

```
function c = getcoeff(P, x, a)

[C, T] = coeffs(P, x);
n=length(C);
exists = 0;
for i=1:n
    if(isequal(T(i),x^a));
    exists = 1;
    break;
end

if(exists)
    c = C(i);
else
    c = 0;
end
```