

Beam Resonance Problem

Question:

A special 2 m long beam is composed of three materials; Aluminum bronze ($E = 120 \text{ GPa}$, $\nu = 0.316$, density = 7640 kg/m^3), Gold ($E = 74 \text{ GPa}$, $\nu = 0.415$, density = 19320 kg/m^3) and Tin ($E = 47 \text{ GPa}$, $\nu = 0.36$, density = 7310 kg/m^3) all comprising $1/3^{\text{rd}}$ of the beams thickness. The beam is 0.4 m wide and 0.2 m thick. The beam is suspended such that its left end is supported by a pin whereas its right end is fixed. This only allows for rotation about an axis parallel to the width direction axis.

- Determine the flexural rigidity of the beam for bending in the direction about an axis parallel to the width direction axis.
- Use Maple to determine the first three resonant frequencies in the thickness direction. Make a plot of what the mode shapes (displacement vs. x-position) look like
- Use FlexPDE to find *any one* of the first three resonant modes & frequencies this beam has in the thickness direction. Show a deformed shape plot and state the resonant frequency you found correct to the nearest 1 rad/s

Solution:

a) We start off our question by defining the thickness varying material properties as piecewise functions in Maple. We can then proceed to find Zbar and in turn our flexural rigidity EI.

Maple Code:

restart:

L:=2: B:=.4: h:=.2:

E:=piecewise(z<h*0.3333, 120e9, z<h*0.6666, 74e9, z>h*0.6666, 47e9):

rho:=piecewise(z<h*0.3333, 7640, z<h*0.6666, 19320, z>h*0.6666, 7310):

mu:=int(rho, z=0..h)*B;

Zbar:=int(int(z*E, z=0..h), y=0..B)/int(int(E, z=0..h), y=0..B);

EI:=int(int(E*(z-Zbar)^2, z=0..h), y=0..B);

$\mu := 913.833760$

$Zbar := 0.07980541398$

$EI := 1.955172042 \cdot 10^7$

b) Using the dynamic beam equation, $\frac{\partial^2 v}{\partial t^2} = -\frac{EI}{\mu} \frac{\partial^4 v}{\partial z^4}$ and knowing that $v(z,t) = \hat{v}(z) \cos(\omega t + \phi)$, we can obtain the simplified equation $\omega^2 \hat{v}(z) = \frac{EI}{\mu} \hat{v}''''(z)$. The solution to this 4th order differential equation is $\hat{v}(z) = c_1 \cos \beta z + c_2 \sin \beta z + c_3 \cosh \beta z + c_4 \sinh \beta z$, where $\omega = \beta^2 \sqrt{\frac{EI}{\mu}}$. Since the beam is supported by a pin at $z=0$, the BC's will be: $\hat{v}(0) = 0$, $\hat{v}''(0) = 0$ and $\hat{v}(Lz) = 0$, $\hat{v}''(Lz) = 0$. We know that by solving this, we will obtain an infinite number of

values for beta that satisfy the equation and each value corresponds to a different mode. We need to find the first three resonant frequencies in the thickness direction and plot their mode shapes. We first solve for our first three beta values and then by substituting the beta values found previously into the original differential equation, we can plot all the modes.

Maple Code:

```
restart;
L:=2: B:=.4: h:=.2:
E:=piecewise(z<h*0.3333, 120e9, z<h*0.6666, 74e9, z>h*0.6666, 47e9):
rho:=piecewise(z<h*0.3333, 7640, z<h*0.6666, 19320, z>h*0.6666, 7310):
mu:=int(rho, z=0..h)*B;
Zbar:=int(int(z*E, z=0..h), y=0..B)/int(int(E, z=0..h), y=0..B);
EI:=int(int(E*(z-Zbar)^2, z=0..h), y=0..B);
bv:=c1*cos(beta*z)+c2*sin(beta*z)+c3*cosh(beta*z)+c4*sinh(beta*z);
bvp:=diff(bv,z);
bvpp:=diff(bvp,z);
bvppp:=diff(bvpp,z);
c1:=solve(simplify(subs(z=0, bv)), c1);
simplify(subs(z=0, bvpp));
c3:=0;
bv;
c4:=solve(subs(z=L, bv), c4);
bv;
c2:=1;
GenFn:=simplify(subs(z=L, bvp/beta));
plot(GenFn, beta=0..8);
beta1:=fsolve(GenFn, beta=1..3);
beta2:=fsolve(GenFn, beta=3..5);
beta3:=fsolve(GenFn, beta=5..7);
bv1:=subs(beta=beta1, bv);
bv2:=subs(beta=beta2, bv);
bv3:=subs(beta=beta3, bv);
plot([bv1, bv2, bv3], z=0..L, legend=['FirstMode', 'SecondMode', 'ThirdMode']);
omega1:=beta1^2*sqrt(EI/mu);
omega2:=beta2^2*sqrt(EI/mu);
omega3:=beta3^2*sqrt(EI/mu);
```

$$bv := c1 \cos(\beta z) + c2 \sin(\beta z) + c3 \cosh(\beta z) + c4 \sinh(\beta z)$$

$$c1 := -c3$$

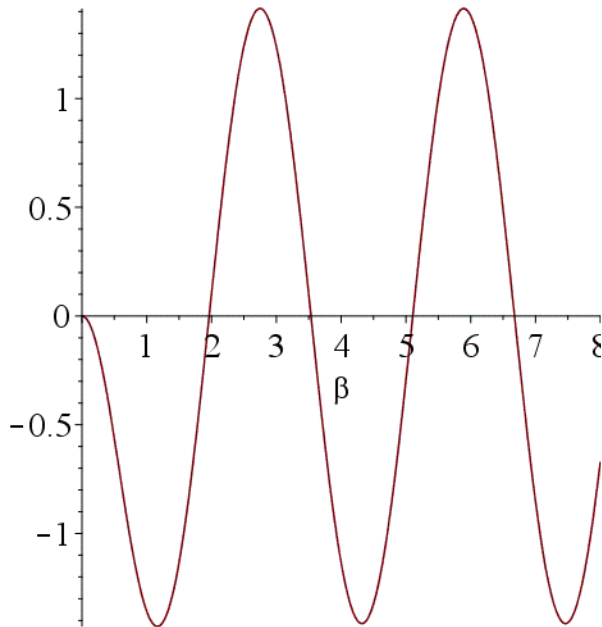
$$2 c3 \beta^2$$

$$c2 \sin(\beta z) + c4 \sinh(\beta z)$$

$$c4 := -\frac{c2 \sin(2 \beta)}{\sinh(2 \beta)}$$

$$c2 \sin(\beta z) - \frac{c2 \sin(2 \beta) \sinh(\beta z)}{\sinh(2 \beta)}$$

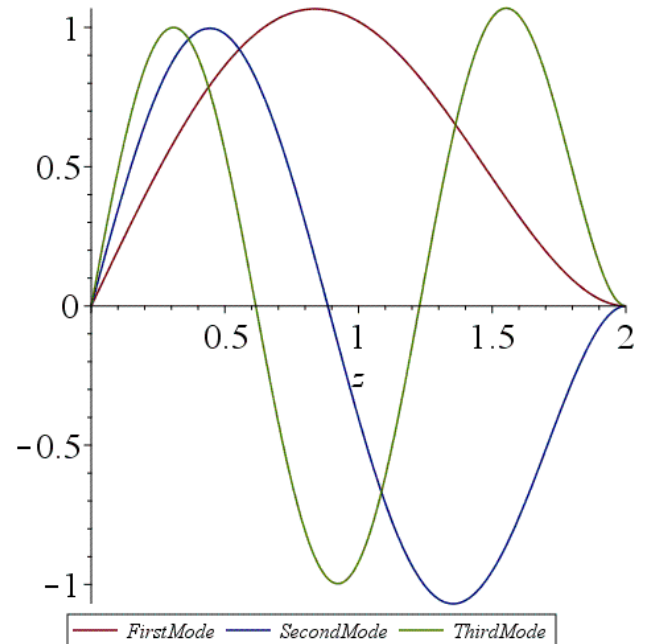
$$GenFn := \frac{1}{\sinh(2 \beta)} (\cos(2 \beta) \sinh(2 \beta) - \cosh(2 \beta) \sin(2 \beta))$$



$$\beta_1 := 1.963301156$$

$$\beta_2 := 3.534291373$$

$$\beta_3 := 5.105088061$$



$$\omega_1 := 563.8099486$$

$$\omega_2 := 1827.105359$$

$$\omega_3 := 3812.109492$$

c) We will now use FlexPDE to find our first resonant mode and its plot along with its corresponding angular frequency to confirm our answer obtained with Maple

FlexPDE code:

```
TITLE
'H10.2 hussam43'
COORDINATES
cartesian3
SELECT
errlim=1e-4
ngrid=15
spectral_colors
stages = 10
v !Displacement in y
w !Displacement in z
DEFINITIONS
mag=1000
x
!Displacement in
Lx=2
```

```

Ly=.4                                gxy = dy(u) + dx(v)                                surface 'top'

Lz=.2                                load(u)=0

E=if z<0.3333*Lz then                !!Stress via Hooke's law                                load(v)=0
120e9 else if
z<0.6666*Lz then 74e9                !Axial Stress                                load(w)=0
else 47e9
sx =
C11*ex+C12*ey+C13*ez                                REGION 1
nu=if z<0.3333*Lz then                sy =                                START(0,0) !y=0
0.316 else if                        C21*ex+C22*ey+C23*ez                                surface:
z<0.6666*Lz then 0.415
else 0.36                                sz =                                load(u)=0
rho=if z<0.3333*Lz then                C31*ex+C32*ey+C33*ez                                load(v)=0
7640 else if z<0.6666*Lz
then 19320 else 7310                !Shear stress                                load(w)=0
G=E/(2*(1+nu))                        sxy=G*gxy
sxz=G*gxz                                LINE TO (Lx,0)
omaga = 565+0.1*stage                syz=G*gyz                                !x=Lx surface
                                        value(u)=0
                                        load(v)=0
                                        value(w)=0
C11 =E*(1-nu)/(1+nu)/(1-2*nu)        EQUATIONS
C22 = C11                                !FNet = 0
C33 = C11                                u:                                LINE TO
                                        dx(sx)+dy(sxy)+dz                                (Lx,Ly) !y=Ly surface
                                        (sxz)= -rho*omaga^2*u                                load(u)=0
                                        v:                                load(v)=0
                                        dx(sxy)+dy(sy)+dz                                load(w)=0
                                        (syz) =-rho*omaga^2*v
                                        w:                                LINE TO
                                        dx(sxz)+dy(syz)+d                                (0,Ly) !x=0 surface
                                        z(sz) -rho*9.81=-                                load(u)=0
                                        rho*omaga^2*w !gravity                                load(v)=0
                                        in thickness direction                                value(w)=0
                                        is really just to get it
                                        started
                                        LINE TO
                                        CLOSE
!! Strain                                EXTRUSION
!Axial Strain                                surface 'bottom' z=0
ex=dx(u)                                surface 'top' z=Lz
ey=dy(v)                                MONITORS
ez=dz(w)                                !contour(u) painted on
!Engineering Shear                                x=0
Strain                                load(u)=0
gyz = dz(v) + dy(w)                                load(v)=0
gxz = dz(u) + dx(w)                                load(w)=0
!contour(v) painted on
x=0
!contour(w) painted on
x=0

```

```

!grid(x+u,y+v,z+w)
                                elevation(w) from
                                (0,Ly/2,Lz/2)
                                to(Lx,Ly/2,Lz/2)
                                report
                                val(v,Lx,Ly,Lz)

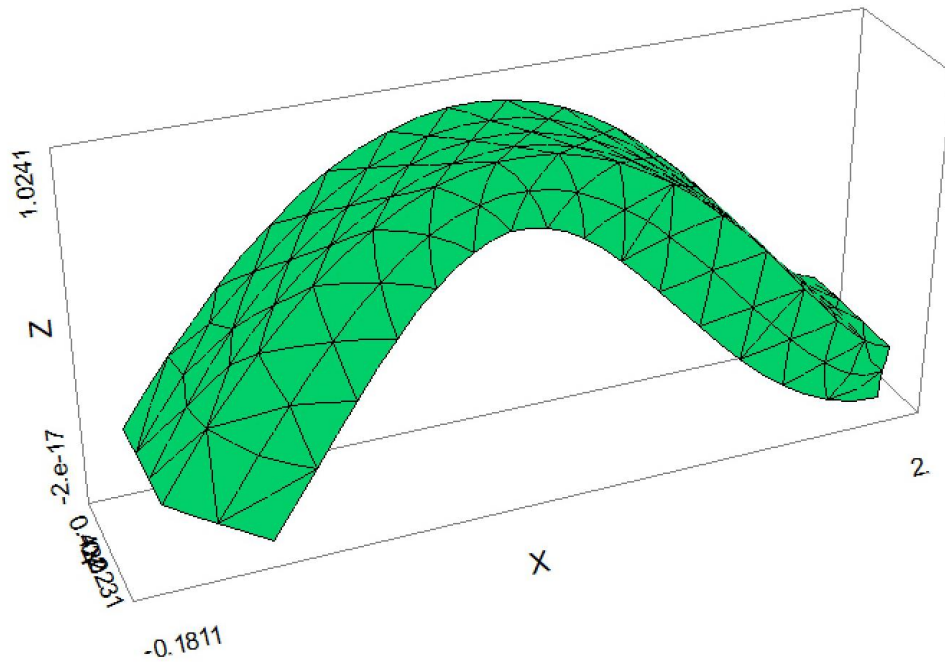
PLOTS
                                history(w) at
                                (Lx/2,Ly/2,Lz/2) !the
                                middle will show a lot
                                of displacement
                                report
                                val(w,Lx,Ly,Lz)
                                report
                                val(w,Lx/2,Ly/2,Lz)
                                end

                                contour(sxz) on
                                surface z=Lz

                                elevation(sx,sy,s
                                z,syz,sxz,sxy) from
                                (0,0,0) to (0,0,Lz)
                                summary
                                report
                                val(u,Lx,Ly,Lz)

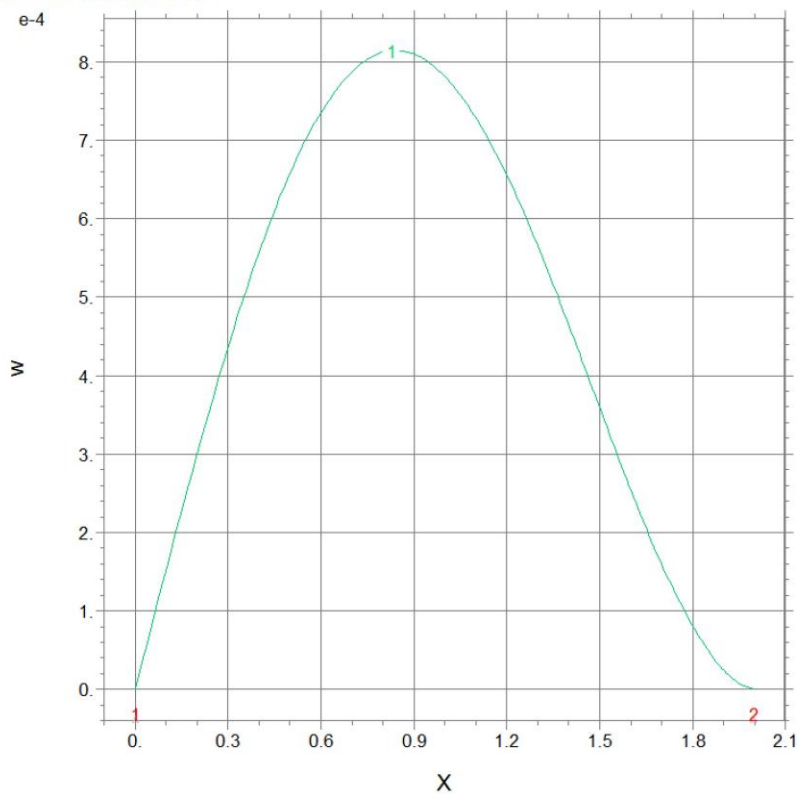
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The approximate value for omega obtained from FlexPDE is 565 rad/s compared to 563.8 obtained from Maple which is extremely accurate. The depiction of the beam and the plot of the first mode is:



H10.2 hussam43

19:37:15 11/29/20
FlexPDE Student 6.36s/W32



w
from (0,Ly/2,Lz/2)
to(Lx,Ly/2,Lz/2)

1: w

