

WEEK 9

giovedì 6 febbraio 2020 11:31

TASK 1

Use a weather forecast website, and utilize the psychrometric chart and the formula we went through in the class to determine the absolute humidity, the wet-bulb temperature and the mass of water vapour in the air in Classroom A (Aula A) of Piacenza campus in the moment that you are solving this exercise (provide the inputs that you utilized)

$$A = 10 \times 25 \times 5 = 1250 \text{ m}^2$$

$$T = 11^\circ\text{C} = 284 \text{ K}$$

$$P = 102.9 \text{ kPa} \sim 101.325 \text{ kPa} = 1 \text{ atm}$$

$$\Phi = 30\%$$

$$? = \omega - T_{wb} - m_v$$

FORMULAS

$$\Phi = m_v / m_g = P_v / P_g$$

$$P_g = P_{\text{sat}@11^\circ\text{C}} = 1.2276 \text{ kPa (value found in steam tables for } P_{\text{sat}@10^\circ\text{C}})$$

$$P_v = \Phi \times P_g = 0.3 \times 1.2276 \text{ kPa} = 0.36828 \text{ kPa}$$

$$P = P_a + P_v$$

$$P_a = P - P_v = 102.9 \text{ kPa} - 0.37 \text{ kPa} = 102.35 \text{ kPa}$$

$$\omega = 0.622 P_v / P_a = (0.622 \times 0.37 \text{ kPa}) / 102.35 \text{ kPa} = 0.00225 \text{ kg}_v/\text{kg}_a$$

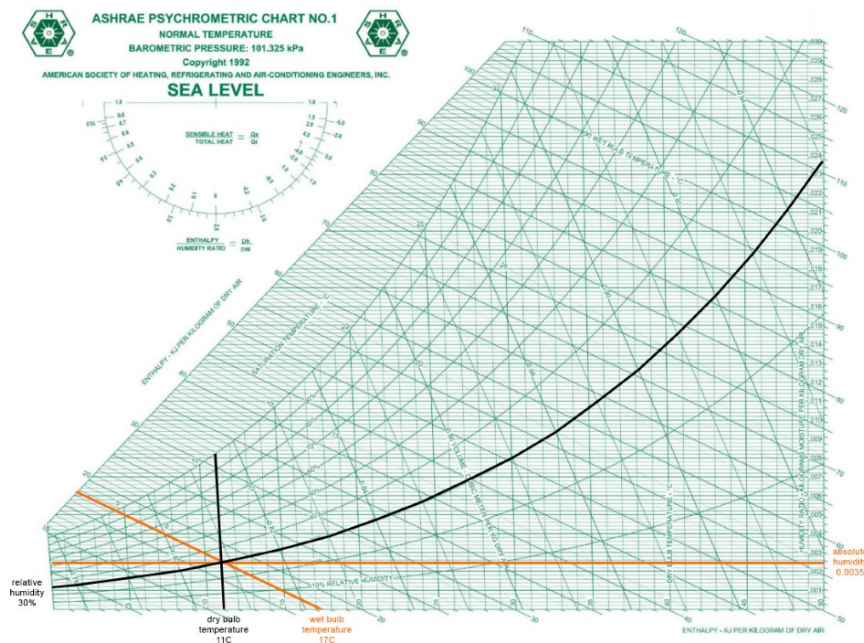
HP: for temperatures below 50°C we treat dry air and water vapour as ideal gasses ($m = PV/R_{\text{SPECIFIC}}T_{\text{inK}}$)

$$m_v = P_v V_v / R_v T$$

$$R_v = 0.4615 \text{ (found in tables)}$$

$$m_v = (0.37 \text{ kPa} \times 1250 \text{ m}^2) / (0.4615 \times 284 \text{ K}) = 3.53 \text{ kg}$$

PSYCHROMETRIC CHART



TASK 2

Utilize the same methodology we went through in the class and determine the sensible and latent load corresponding to internal gains, the ventilation, and the infiltration in a house with a good construction quality and with the same geometry as that of the example which is located in Brindisi, Italy.

EXAMPLE: A building with a height of 2.5 m and an average construction quality, is located in Piacenza, considering two occupants and one bedroom calculate, and a conditioned floor area of 200 m² and wall area is 144 m², calculate the internal gains, infiltration, and ventilation loads.

$$Q_{\text{igsensible}} = 136 + 2.2 A_{\text{cf}} + 22 N_{\text{oc}} = 136 + 2.2 \times 200 \text{ m}^2 + 22 \times 2 = 620 \text{ W}$$

$$Q_{\text{iglatent}} = 20 + 0.22 A_{\text{cf}} + 12 N_{\text{oc}} = 20 + 0.22 \times 200 \text{ m}^2 + 12 \times 2 = 88 \text{ W}$$

To find the infiltration I must know how much is the max flowrate of air

Table 3 Unit Leakage Areas

Construction	Description	A_{ul} , cm ² /m ²
Tight	Construction supervised by air-sealing specialist	0.7
Good	Carefully sealed construction by knowledgeable builder	1.4
Average	Typical current production housing	2.8
Leaky	Typical pre-1970 houses	5.6
Very leaky	Old houses in original condition	10.4

$$A_{ul} = 1.4 \text{ cm}^2/\text{m}^2$$

Exposed surfaces (wall + roof)

$$A_{\text{ex}} = 200 \text{ m}^2 + 144 \text{ m}^2 = 344 \text{ m}^2$$

$$A_L = A_{\text{ex}} \times A_{ul} = 344 \text{ m}^2 \times 1.4 \text{ cm}^2/\text{m}^2 = 481.6 \text{ cm}^2$$

INFILTRATION DRIVING FORCE

Table 5 Typical IDF Values, L/(s·cm²)

H , m	Heating Design Temperature, °C					Cooling Design Temperature, °C				
	-40	-30	-20	-10	0	10	30	35	40	
2.5	0.10	0.095	0.086	0.077	0.069	0.060	0.031	0.035	0.040	
3	0.11	0.10	0.093	0.083	0.072	0.061	0.032	0.038	0.043	
4	0.14	0.12	0.11	0.093	0.079	0.065	0.034	0.042	0.049	
5	0.16	0.14	0.12	0.10	0.086	0.069	0.036	0.046	0.055	
6	0.18	0.16	0.14	0.11	0.093	0.072	0.039	0.050	0.061	
7	0.20	0.17	0.15	0.12	0.10	0.075	0.041	0.051	0.068	
8	0.22	0.19	0.16	0.14	0.11	0.079	0.043	0.058	0.074	

$$\text{IDF}_{\text{heating}} = 0.073 \text{ L/s} \cdot \text{cm}^2$$

$$\text{IDF}_{\text{cooling}} = 0.033 \text{ L/s} \cdot \text{cm}^2$$

$$V_{\text{infiltrationH}} = A_L \times \text{IDF}_{\text{heating}} = 481.6 \text{ cm}^2 \times 0.073 \text{ L/s} \cdot \text{cm}^2 = 35.16 \text{ L/s}$$

$$V_{\text{infiltrationC}} = A_L \times \text{IDF}_{\text{cooling}} = 481.6 \text{ cm}^2 \times 0.033 \text{ L/s} \cdot \text{cm}^2 = 15.89 \text{ L/s}$$

$$V_{\text{ventilation}} = 0.05 A_{\text{cf}} + 3.5 (N_{\text{br}} + 1) = 0.05 \times 200 \text{ m}^2 + 3.5 \times (1 + 1) = 17 \text{ L/s}$$

$$V_{\text{ventilation-infiltrationH}} = 35.16 \text{ L/s} + 17 \text{ L/s} = 52.16 \text{ L/s}$$

$$V_{\text{ventilation-infiltrationC}} = 15.98 \text{ L/s} + 17 \text{ L/s} = 32.89 \text{ L/s}$$

BRINDISI, Italy

WMO#: 163200

Lat: 40.65N Long: 17.95E Elev: 10 StdP: 101.2 Time Zone: 1.00 (EUW) Period: 86-10 WBAN: 99999

Annual Heating and Humidification Design Conditions

Coldest Month	Heating DB		Humidification DP/MCDB and HR						Coldest month WS/MCDB				MCWS/PCWD to 99.6% DB	
			99.6%			99%			0.4%		1%			
	99.6%	99%	DP	HR	MCDB	DP	HR	MCDB	WS	MCDB	WS	MCDB	MCWS	PCWD
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)
(1) 2	2.9	4.1	-5.1	2.5	7.2	-3.0	3.0	7.4	13.4	10.2	12.4	10.6	3.4	250

Annual Cooling, Dehumidification, and Enthalpy Design Conditions

(2)	Hottest Month	Hottest Month DB Range		Cooling DB/MCWB						Evaporation WB/MCDB						MCWS/PCWD to 0.4% DB	
				0.4%		1%		2%		0.4%		1%		2%			
		DB	MCWB	DB	MCWB	DB	MCWB	WB	MCDB	WB	MCDB	WB	MCDB	MCWS	PCWD		
	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	
	8	7.1	32.8	23.6	31.1	24.3	29.9	24.3	27.2	29.7	26.3	29.0	25.6	28.3	4.2	180	
Dehumidification DP/MCDB and HR																	
(3)													Enthalpy/MCDB		Hours 8 to 4 & 12.8/20.6		
	0.4%			1%			2%			0.4%							
	DP	HR	MCDB	DP	HR	MCDB	DP	HR	MCDB	Enth	MCDB	Enth	MCDB	Enth		MCDB	
	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	
	26.3	21.8	29.2	25.4	20.7	28.5	24.7	19.7	27.9	86.0	30.1	82.2	29.1	78.5	28.3	1236	
(3)																	

Extreme Annual Design Conditions

Extreme Annual WS			Extreme Max WB	Extreme Annual DB				n-Year Return Period Values of Extreme DB									
				Mean	Standard deviation			n=5 years		n=10 years		n=20 years		n=50 years			
1%	2.5%	5%		Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max		
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)		
(4) 11.3	9.9	8.7	31.4	0.4	37.3	1.4	3.0	-0.6	39.4	-1.4	41.1	-2.2	42.8	-3.2	44.9		

$$C_{\text{sensible}} = 1.23$$

$$C_{\text{latent}} = 3010$$

Based on ASHRAE Standard 55: cooling = 24°C – heating = 20°C

$$Q_{\text{sensibleC}} = C_{\text{sensible}} V_{\text{ventilation-infiltration}} \Delta T_{\text{cooling}}$$

$$Q_{\text{sensibleC}} = 1.23 * 32.89 \text{ L/s} * (31.1 - 24) ^\circ\text{C} = 287.23 \text{ W}$$

$$Q_{\text{sensibleH}} = C_{\text{sensible}} V_{\text{ventilation-infiltration}} \Delta T_{\text{heating}}$$

$$Q_{\text{sensibleH}} = 1.23 * 52.16 \text{ L/s} * (20 - 4.1) ^\circ\text{C} = 1020.09 \text{ W}$$

$$Q_{\text{latentC}} = C_{\text{latent}} V_{\text{ventilation-infiltration}} \Delta \omega_{\text{cooling}}$$

$$Q_{\text{latentC}} = 3010 * 32.89 \text{ L/s} * 0.017 = 1682.98 \text{ W}$$

$$\Delta \omega_{\text{cooling}} = 0.017 \text{ (found with the psychrometric chart knowing the dry and wet bulb temperatures)}$$