## ONSAS v.0.1.10 analysis report Problem: StaticTower

This is an ONSAS automatically-generated report with part of the results obtained after the analysis. The user can access other magnitudes and results through the GNU-Octave/MATLAB console. The code is provided AS IS **WITHOUT WARRANTY of any kind**, express or implied.

## **Analysis results**

#t	$\lambda(t)$	its	RHS	$\ \Delta u\ $	flagExit	npos	nneg
1	0.00e+00	0			0	0	0
		1	6.13e+02	5.01e-02			
		2	6.11e-02	6.16e-05			
		3	1.97e-05	2.80e-09			
2	2.00e+00	$-\frac{1}{3}$		. – – – –	<u>-</u>	10	
		1	5.33e+02	3.89e-02			
		2	2.58e-02	4.03e-05			
3	4.00e+00	$-\frac{1}{2}$			<u>-</u>	10	0
		1	5.35e+02	3.89e-02			
		2	2.95e-02	4.26e-05			
4	6.00e+00	$-\frac{1}{2}$			<u>-</u>	10	
		1	5.36e+02	3.90e-02			
		2	3.38e-02	4.51e-05			
· 5	8.00e+00				1	10	
·		1	5.37e+02	3.90e-02	-	_ ~	-
		2	3.88e-02	4.79e-05			
	1.00e+01	$-\frac{2}{2}$			 1	10	
O	1.000 101	1	5.39e+02	3.90e-02	•	10	U
		2	4.47e-02	5.09e-05			
<sub>7</sub>	1.20e+01	$-\frac{2}{2}$			 1	- 10	
,	1.200 101	1	5.41e+02	3.90e-02	1	10	U
		2	5.41e+02 5.17e-02	5.43e-05			
	1.40e+01	$-\frac{2}{2}$		J.43E-03	 1		
0	1.400+01	1	F 44a + 00	2.01 - 02	1	10	U
			5.44e+02	3.91e-02			
		$-\frac{2}{3}$	6.00e-02	5.80e-05			
9	1.60e+01	2	<b>5</b> 46 00	0.04.00	1	10	0
		1	5.46e+02	3.91e-02			
		$-\frac{2}{3}$	6.99e-02	6.21e-05		·	
10	1.80e+01				1	10	0
		1	5.49e+02	3.92e-02			
		_ 2 _	8.18e-02	6.67e-05			
11	2.00e+01				1	10	0
		1	5.53e+02	3.92e-02			
		_ 2 _	9.60e-02	7.18e-05			
12	2.20e+01	2			1	10	0
		1	5.58e+02	3.93e-02			
		_ 2 _	1.13e-01	7.75e-05			
13	2.40e+01				1	10	0
		1	5.64e+02	3.93e-02			
		2	1.34e-01	8.38e-05			
14	2.60e+01				1	10	0
		1	5.71e+02	3.94e-02			
		2	1.59e-01	9.09e-05			
15	2.80e+01	$-\frac{1}{2}$			1	10	0
		1	5.80e+02	3.94e-02			
		2	1.90e-01	9.89e-05			
16	3.00e+01				<u>-</u>	10	
		1	5.91e+02	3.95e-02			
		2	2.29e-01	1.08e-04			

$\frac{\#t}{17}$	$\lambda(t)$ 3.20e+01	its 2	RHS	$\ \Delta u\ $	flagExit	npos	nneg 0
17	3.200+01	1 2	6.06e+02 2.76e-01	3.96e-02 1.18e-04	1	10	U
18	3.40e+01	$-\frac{1}{2}$	6.24e+02	3.96e-02	1	10	0
		2	3.35e-01	1.30e-02			
19	3.60e+01				1	10	0
		1 2	6.47e+02 4.09e-01	3.97e-02 1.43e-04			
20	3.80e+01	$-\frac{2}{2}$			<sub>1</sub>	10	
		1 2	6.76e+02 5.02e-01	3.98e-02 1.58e-04			
21	4.00e+01	$-\frac{2}{2}$		1.56e-04	<sub>-</sub>	- <del>-</del>	
		1	7.14e+02	4.00e-02			
	4.20e+01	$-\frac{2}{2}$	6.19e-01	1.75e-04	<sub>-</sub>	- <del>-</del>	
22	1.200 101	1	7.63e+02	4.01e-02	1	10	O
		$-\frac{2}{2}$	7.69e-01	1.95e-04	,		
23	4.40e+01	2 1	8.26e+02	4.02e-02	1	10	0
		2	9.61e-01	2.18e-04			
		$-\frac{3}{3}$	_1.96e-05	7.76e-08			
24	4.60e+01	3 1	9.07e+02	4.04e-02	1	10	0
		2	1.21e+00	2.45e-04			
25	4.80e+01	$-\frac{3}{3}$	1.49e-05	1.04e-07	<sub>1</sub>		
23	4.000 101	1	1.01e+03	4.06e-02	1	10	O
		2	1.53e+00	2.75e-04			
26	5.00e+01	$-\frac{3}{3}$	2.37e-05	1.41e-07	<sub>1</sub>	- <del>-</del>	
		1	1.14e+03	4.08e-02			
		2 3	1.95e+00 2.09e-05	3.11e-04 1.94e-07			
27	5.20e+01	$-\frac{3}{3}$		1.946-07	 1	- <del>-</del>	
		1	1.31e+03	4.11e-02			
		2 3	2.49e+00 1.64e-05	3.52e-04 2.70e-07			
28	5.40e+01	$-\frac{3}{3}$		2.700 07	1	10	
		1	1.52e+03	4.14e-02			
		2 3	3.19e+00 1.81e-05	4.00e-04 3.78e-07			
29	5.60e+01				1	- 10	0
		1 2	1.80e+03 4.11e+00	4.18e-02 4.56e-04			
		3	1.69e-05	5.36e-07			
30	5.80e+01				1	10	0
		1 2	2.14e+03 5.30e+00	4.23e-02 5.20e-04			
		3_	2.38e-05	7.66e-07			
31	6.00e+01	3	2.502.02	4.20 - 02	1	10	0
		1 2	2.58e+03 6.81e+00	4.28e-02 5.93e-04			
		_ 3 _	2.88e-05	1.10e-06			
32	6.20e+01	3 1	3.13e+03	4.35e-02	1	10	0
		2	8.69e+00	4.33e-02 6.76e-04			
:		$-\frac{3}{2}$	5.06e-05	1.59e-06			
33	6.40e+01	3			1	10	0

_#t	$\lambda(t)$	its	RHS	$\ \Delta u\ $	flagExit	npos	nneg
		1	3.82e+03	4.43e-02			
		2	1.09e+01	7.67e-04			
		$-\frac{3}{2}$	9.86e-05	2.29e-06			
34	6.60e+01	3	4.6000	4.50 00	1	10	0
		1	4.69e+03	4.53e-02			
		2	1.35e+01	8.64e-04			
	6.80e+01	$-\frac{3}{2}$	2.08e-04	3.27e-06			
35	6.80e+01	3	F 77 a . 02	1 ( 1 = 0 2	1	10	0
		1 2	5.77e+03	4.64e-02 9.62e-04			
		3	1.61e+01	9.62e-04 4.60e-06			
36	7.00e+01	$-\frac{3}{3}$	4.11e-04	4.000-00	1		
30	7.000+01	3 1	7.07e+03	4.78e-02	1	10	U
		2	1.84e+01	1.05e-03			
		3	7.66e-04	6.29e-06			
37	7.20e+01	$-\frac{3}{3}$		0.270 00	<sub>-</sub>	- <del>-</del>	
37	7.200101	1	8.61e+03	4.94e-02	1	10	O
		2	1.98e+01	1.13e-03			
		3	1.31e-03	8.26e-06			
38	7.40e+01	$-\frac{3}{3}$			<sub>1</sub>		
30	,.100,01	1	1.04e+04	5.12e-02	•	10	J
		2	1.96e+01	1.17e-03			
		3	1.99e-03	1.02e-05			
39	7.60e+01	$-\frac{3}{3}$			<sub>1</sub>		
		1	1.23e+04	5.31e-02			
		2	1.76e+01	1.18e-03			
		3	2.58e-03	1.18e-05			
40	7.80e+01			. – – – –	<sub>1</sub>	- <del>-</del>	0
		1	1.42e+04	5.51e-02			
		2	1.41e+01	1.15e-03			
		3	2.79e-03	1.24e-05			
41	8.00e+01				<u>-</u>	10	0
		1	1.60e+04	5.71e-02			
		2	9.97e+00	1.08e-03			
		3	2.47e-03	1.20e-05			
42	8.20e+01	$-\frac{1}{3}$			1	10	0
		1	1.76e+04	5.90e-02			
		2	6.31e+00	1.01e-03			
		3	1.90e-03	1.13e-05			
43	8.40e+01					10	0
		1	1.88e+04	6.08e-02			
		2	3.87e+00	9.70e-04			
		_ 3 _	1.93e-03	1.51e-05			
44	8.60e+01	3			1	10	0
		1	1.96e+04	6.23e-02			
		2	3.15e+00	1.06e-03			
		_ 3 _	9.29e-03	4.49e-05			
45	8.80e+01	3			1	10	0
		1	2.01e+04	6.38e-02			
		2	1.18e+01	1.97e-03			
		$-\frac{3}{2}$	3.53e-01	2.97e-04			
46	9.00e+01	3	0.06 - 0.4	(FF 00	1	10	0
		1	2.06e+04	6.55e-02			
		2	1.02e+03	1.75e-02			
		3	1.07e+03	1.74e-02			
		4	3.86e+00	1.05e-03			
	0.202.01	$-\frac{5}{2}$	1.66e-02	6.85e-05			
47	9.20e+01	5 1	2.420+05	252201	1	10	0
		1	2.42e+05	2.53e-01			

	1 (1)		DII G	II <b>A</b> II	0 D 1		
#t	$\lambda(t)$	its	$\ RHS\ $	$\ \Delta u\ $	flagExit	npos	nneg
		2	3.98e+04	1.28e-01			
		3	5.81e+06	1.38e+00			
		4	5.34e+04	1.93e-01			
		5	2.73e+07	3.09e+00			
		6	7.55e+05	8.56e-01			
		7	1.02e+07	2.92e+00			
		8	2.16e+05	3.96e-01			
		9	3.57e+07	1.02e+00			
		10	2.23e+06	1.26e+00			
		11	9.84e+05	1.70e+00			
		12	5.40e+06	2.54e+00			
		13	9.91e+04	3.07e-01			
		14	6.67e+06	3.16e+00			
		15	9.30e+04	1.95e-01			
		16	1.68e+05	5.96e-01			
		17	1.07e+05	3.20e-01			
		18	6.95e+04	2.61e-01			
		19	1.34e+04	1.11e-01			
		20	6.29e+02	2.58e-02			
		_ 21 _	1.18e+00	1.03e-03		·	
48	9.40e+01	21			1	10	0
		1	9.37e+05	9.74e-01			
		2	1.58e+04	4.56e-02			
		3	5.25e+04	2.02e-01			
		4	1.57e+02	7.19e-03			
		5	2.35e+00	1.41e-03			
		_ 6 _	2.02e-05	4.23e-07			
49	9.60e+01	6			1	10	0
		1	5.42e+05	6.67e-01			
		2	2.82e+07	4.42e+00			
		3	6.09e+05	8.88e-01			
		4	4.50e+06	2.65e+00			
		5	1.13e+05	1.89e-01			
		6	4.97e+06	7.46e-01			
		7	7.18e+04	2.95e-01			
		8	3.37e+06	1.11e+00			
		9	2.10e+04	1.13e-01			
		10	1.75e+05	2.67e-01			
		11	5.09e+04	1.34e-01			
		12	5.86e+04	1.50e-01			
		13	6.54e+03	5.03e-02			
		14	5.46e+02	1.45e-02			
		_ 15 _	_5.40e-01	4.54e-04			
50	9.80e+01	15			1	10	0
		1	2.47e+04	7.94e-02			
		2	5.18e+02	1.73e-02			
		3	4.78e+00	1.50e-03			
		_ 4 _	3.84e-05	4.24e-06			
51	1.00e+02	4			1	10	0

Table 1: Output of incremental analysis.