## 1st flow Brace along line A

Assume: braco only comes lateral loads windward force: (3,5 kpa) (7(5) m) (6m) = 367.5 kN W= 2.5 kPa leeward P= (2.5 kPa) (7(5) m) 2 m) = 87.5 kN P3 = (2.5 KPG)(7(5) m)(4m) = 175 KN Top flour: 367.5 87.5 87.5 TOP flour: 367.5 Middle: \$\frac{1}{175} = 0 \Rightarrow \frac{7}{165} = 0 \Rightarrow \frac{7}{165} = 130. 95 KN T/C ZFX= 4(130.95)=+175-4F2/65=0 = 181.32 KN T/C 175 EFX = 4(181.32)(7/155) +175-463 7/65 = 0 = 231.60 W >1.4 (231.69) >  $T_f = C_f = 324.37$ W250x49 350W 640.20/21 Fy=350MPa E=200000 MPa 6=77000 MPa, WCG A= 6260 mm2 Ix = 70.6(106) mm4 Iy=15.1(106) mm4 rx=106 mm ry=49.2 mm J= 241 (103) mm4 (w= 211(109) mm 6 d= 247 mm 6= 202 mm += 11 mm w= 7,4 mm Paraces are oriented so they buckle about strong axis if they buckle in the plane of the frame. By \$10.3.15. Hength = 565 m = 8062.26 mm = Lx = Ly (no lateral bracing). And ideal conditions are assumed - \$10.3.1, k=1.0. Check standerness, kx=ky=1.0 \$10.4.2.1 kxLx = 76.06 \le 200 and kyly = (1.0)(8062.26) 163.87 = 200 Check local buckling (13.3.1.1 (Table 1)  $\frac{\text{Ueb:}}{W} = \frac{247 - 2(11)}{7.4} = 30.405 = \frac{670}{\sqrt{f_4}} = \frac{670}{\sqrt{350}} = 35.8 \times \frac{15/2}{7} = \frac{202/2}{11} = 9.18 < 10.69 = \frac{200}{\sqrt{f_4}}$  $C_{T} = \frac{4ATy}{(1+\lambda^{2n})^{\frac{1}{n}}} = \frac{\phi = 0.9 \text{ $413.1}}{A = 1.34} = \sqrt{\frac{Fy}{Fe}} = \frac{\pi^{2}E}{(\pi_{x}L_{x})^{2}} = \frac{\pi^{2}E}{(76.06)^{2}} = 341.2 \quad Tey = \frac{\pi^{2}E}{(163.87)^{2}} = 73.51$ Check compression \$13.3.1.1 f=min(Fexifey, Feq) = fey = 73.51 Fez = (T2E(W +6J) = 292.02  $1 = \sqrt{\frac{350}{73.51}} = 2.18$  $\frac{C_{f}}{(1+2.18)^{2(1.34)})^{1.54}} \cdot \frac{1}{1000N} = \frac{379.67 \text{ kN}}{(1+2.18)^{2(1.34)})^{1.54}} \cdot \frac{1}{1000N} = \frac{379.67 \text{ kN}}{(1+2.18)^{2(1.34)}} \cdot \frac{1}{1000N} = \frac{379.67 \text{ kN}}{(1+2.$ £13.2 Tensian Tr = 9AFy = (0.9×6260)(350) = 1971.9 KN, doesn't govern.