

"2nd Order" Step Responses

$$\ddot{y}(t) + \alpha_1 \dot{y}(t) + \alpha_0 y(t) = \beta_0 u(t) \Rightarrow G(s) = \frac{\beta_0}{s^2 + \alpha_1 s + \alpha_0}$$

2 poles, both stable if $\alpha_1 > 0, \alpha_0 > 0$.

3 possibilities for poles:

- ① $\alpha_1^2 < 4\alpha_0 \Rightarrow p_1, p_2$ complex conjugates
- ② $\alpha_1^2 = 4\alpha_0 \Rightarrow p_1 = p_2$ repeated real
- ③ $\alpha_1^2 > 4\alpha_0 \Rightarrow p_1, p_2$ real, non-repeated

Case ① is most interesting (and complicated)
tackle this after the other two

Useful Observation (Case 1)

$$p_1 = \sigma + j\omega_d \quad \omega_d = \text{Im}\{p_1\}$$

Note slight change of notation! $\omega \rightarrow \omega_d$

$$s^2 + \alpha_1 s + \alpha_0 = (s - p_1)(s - \bar{p}_1)$$

$$= s^2 - (p_1 + \bar{p}_1)s + p_1 \bar{p}_1$$

$$= s^2 - 2\text{Re}\{p_1\}s + |p_1|^2$$

$$= s^2 - 2\sigma s + (\sigma^2 + \omega_d^2)$$

Hence:

$$\alpha_1 = -2\sigma = -2\text{Re}\{p_1\}$$

$$\alpha_0 = \sigma^2 + \omega_d^2 = |p_1|^2$$

Rapidly identify pole location from coefs.

2nd Order Response, Case 1:

$$Y(s) = \frac{\beta_0}{s(s-p_1)(s-\bar{p}_1)} = \frac{A_1}{s} + \frac{A_2}{(s-p_1)} + \frac{\bar{A}_2}{(s-\bar{p}_1)}$$

$$A_1 = [sY(s)]_{s=0} = \frac{\beta_0}{p_1 \bar{p}_1} = \frac{\beta_0}{\alpha_0} = G(0)$$

$$A_2 = [(s-p_1)Y(s)]_{s=p_1} = \frac{\beta_0}{p_1(p_1-\bar{p}_1)} = \frac{\beta_0}{(\sigma+j\omega_d)(2j\omega_d)}$$

$$\frac{1}{2}G(0) = \left(\frac{\beta_0}{2\alpha_0}\right) \left(\frac{\alpha_0}{(\sigma+j\omega_d)(j\omega_d)}\right) - B$$

So:

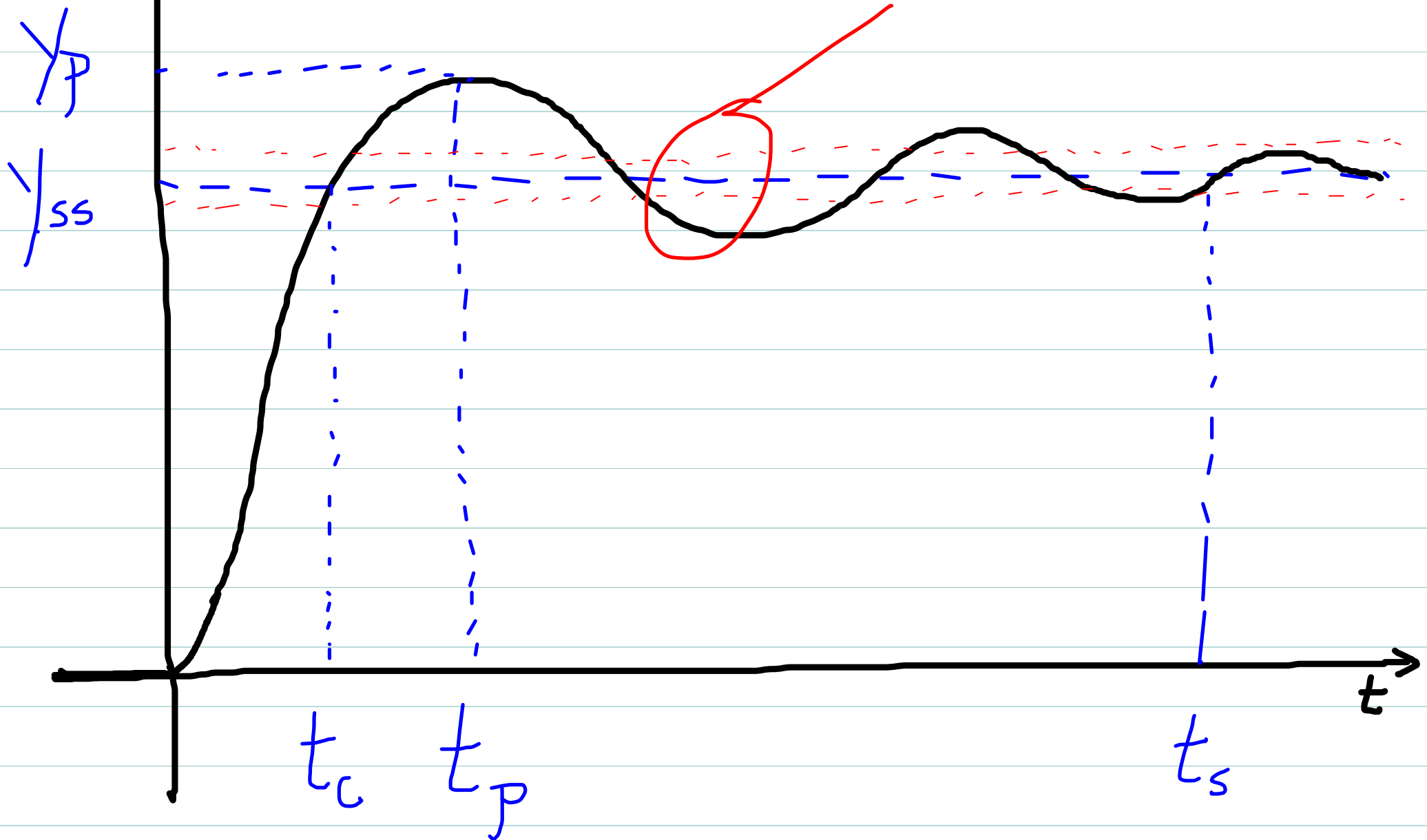
$$y(t) = G(0) + 2|A_2| e^{\sigma t} \cos(\omega_d t + \angle A_2)$$

OR:

$$y(t) = G(0) [1 + |B| e^{\sigma t} \cos(\omega_d t + \angle B)]$$

$y(t)$

$\pm 2\%$ of y_{ss}



General Observations

- (1) $y(t)$ continually oscillates about its steady-state value $y_{ss} = G(\phi)$
 - (2) t_c = time steady-state is first crossed
 - (3) 1st oscillation is largest, and creates an initial overshoot past the steady-state.
 - (4) This initial overshoot has peak value y_p , and occurs at time t_p
 - (5) Settling time t_s defined where response enters $\pm 2\%$ tolerance band and remains within it for times thereafter
- Must learn to rapidly quantify these!!

$$y(t) = G(0) [1 + |B| e^{\sigma t} \cos(\omega_d t + \angle B)]$$

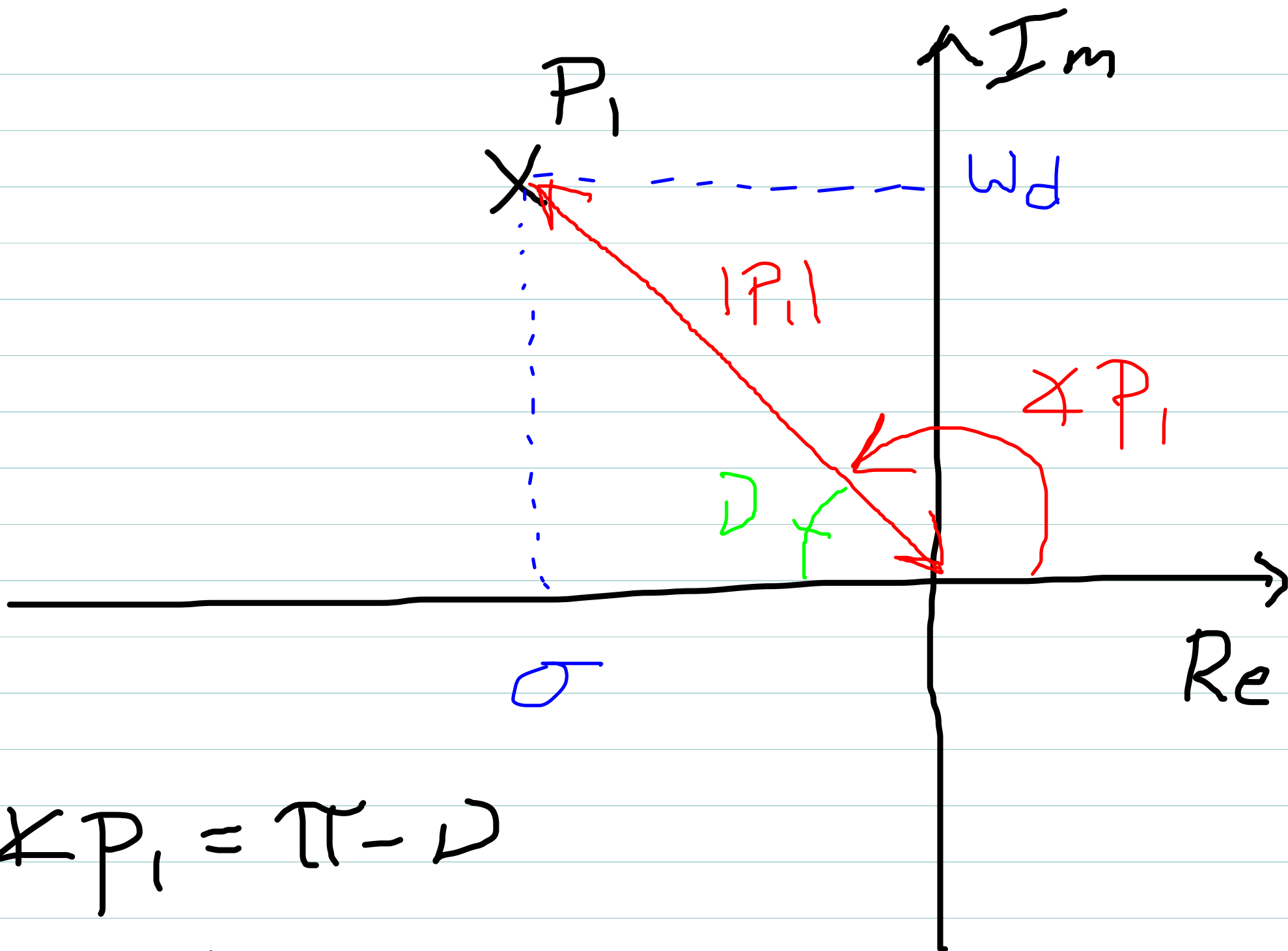
where: $B = \frac{\alpha_0}{(j\omega_d)(\sigma + j\omega_d)} = \frac{|P_1|^2}{(j\omega_d) P_1}$

\Rightarrow Transient features completely determined by location of pole $P_1 = \sigma + j\omega_d$ in complex plane

$$|B| = \frac{|P_1|^2}{|j\omega_d| \cdot |P_1|} = \frac{|P_1|}{\omega_d}$$

$$\angle B = \cancel{\angle |P_1|^2} - (\angle(j\omega_d) + \angle P_1)$$

$$= -\left(\frac{\pi}{2} + \angle P_1\right) \text{ — must quantify this!}$$



$$\angle P_1 = \pi - \nu$$

Note: $\nu > \phi$ is supplement of $\angle P_1$

So:

$$\angle B = -\left(\frac{\pi}{2} + \angle P_1\right) = -\left(\frac{\pi}{2} + (\pi - \nu)\right) \\ = -\frac{3\pi}{2} + \nu$$

and thus:

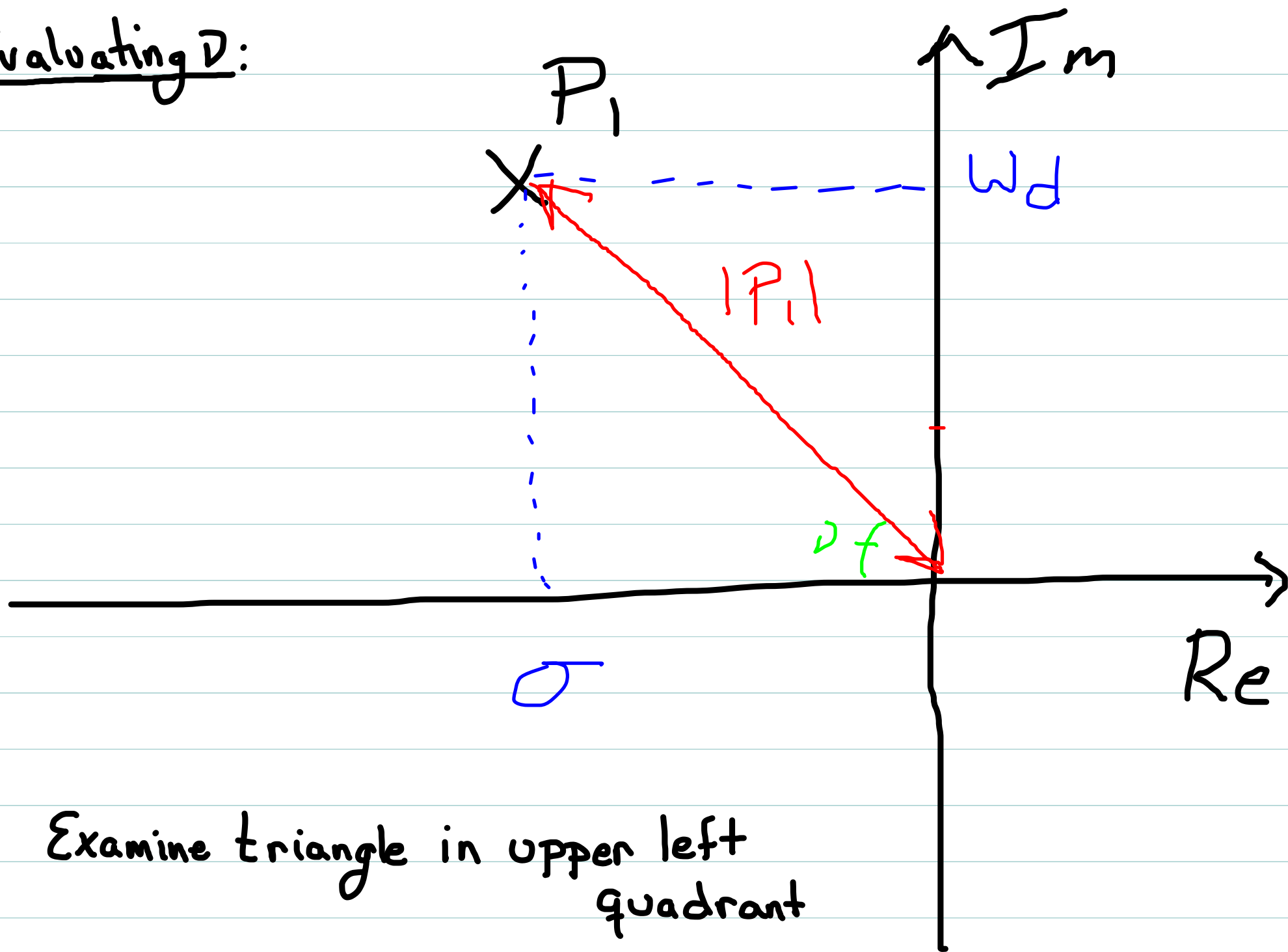
$$y(t) = G(0) \left[1 + \left(\frac{|P_1|}{\omega_d}\right) e^{\sigma t} \cos(\omega_d t - \frac{3\pi}{2} + \nu) \right]$$

so:

$$y(t) = G(0) \left[1 - \left(\frac{|P_1|}{\omega_d}\right) e^{\sigma t} \sin(\omega_d t + \nu) \right]$$

Need to understand how ν depends on P_1

Evaluating D :



Examine triangle in upper left quadrant

Two Useful Parameters

Define: $\omega_n = |p_1| = \sqrt{\sigma^2 + \omega_d^2}$ "natural" frequency

\Rightarrow purely theoretical! ω_d is physical frequency of transient oscillations

Define: $\xi = \frac{|\sigma|}{\omega_n} = \frac{|\sigma|}{\sqrt{\sigma^2 + \omega_d^2}}$

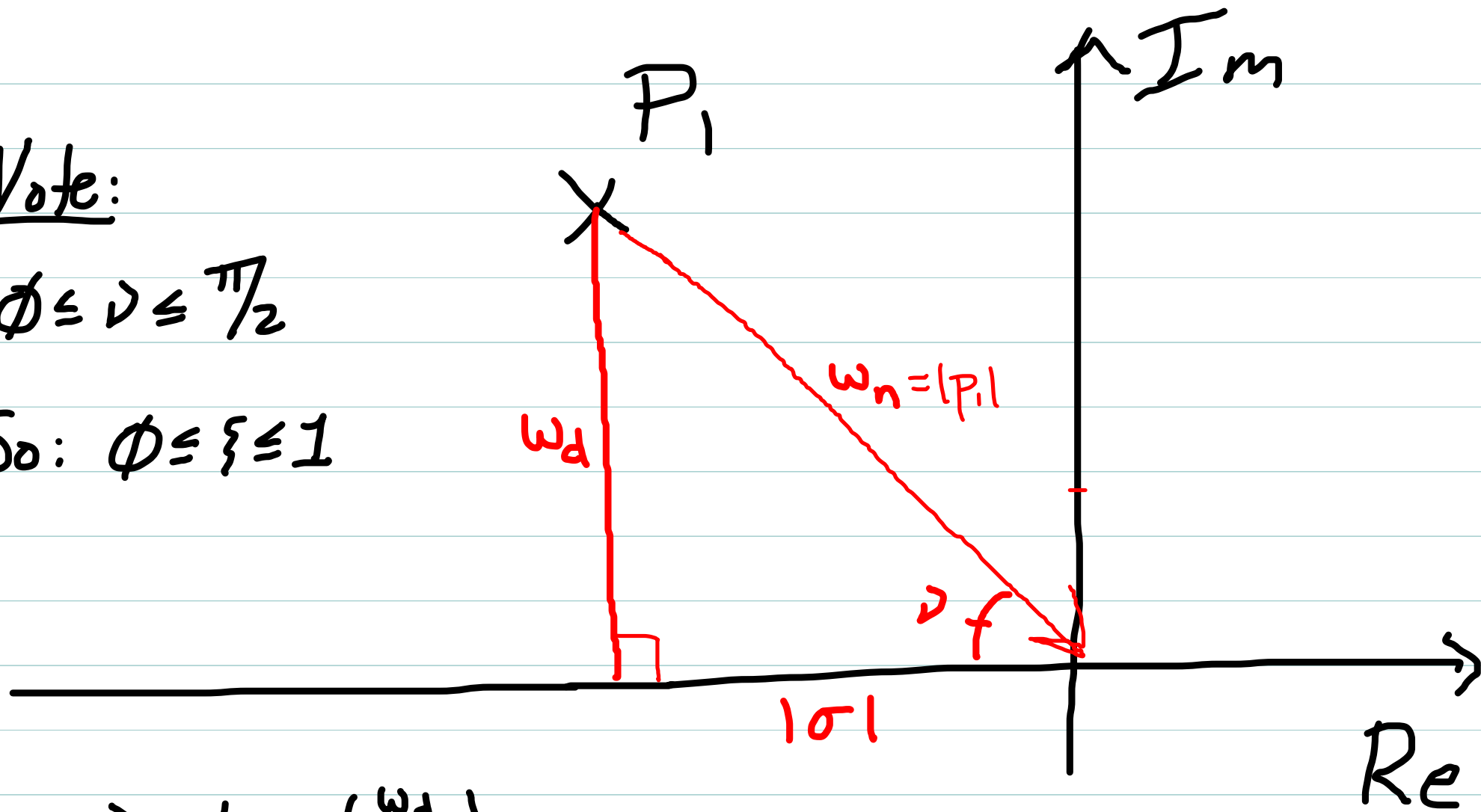
"Damping ratio"

\Rightarrow A normalized measure of the number of transient oscillations observed before amplitude becomes negligible

Note:

$$\phi \leq \nu \leq \pi/2$$

$$\text{So: } \phi \leq \xi \leq 1$$



$$\nu = \tan^{-1}\left(\frac{\omega_d}{|\sigma|}\right)$$

$$\nu = \sin^{-1}\left(\frac{\omega_d}{\omega_n}\right)$$

$$\nu = \cos^{-1}\left(\frac{|\sigma|}{\omega_n}\right) = \cos^{-1} \xi \leftarrow \text{very useful!}$$

A few more observations

$$\xi = \frac{|\sigma|}{\omega_n} \Rightarrow \boxed{\sigma = -\xi \omega_n} \quad \left(\begin{array}{l} \text{Stable} \\ \text{System} \\ \text{Assumed} \end{array} \right)$$

$$\omega_n = \sqrt{\sigma^2 + \omega_d^2}$$

$$\Rightarrow \omega_d^2 = \omega_n^2 - \sigma^2 = \omega_n^2 - (-\xi \omega_n)^2 = \omega_n^2(1 - \xi^2)$$

$$\text{So: } \boxed{\omega_d = \omega_n \sqrt{1 - \xi^2}}$$

Then note:

$$\begin{aligned} s^2 + \alpha_1 s + \alpha_0 &= (s - p)(s - \bar{p}) \\ &= s^2 - 2\sigma s + (\sigma^2 + \omega_d^2) \\ &= s^2 + 2\xi\omega_n s + \omega_n^2 \end{aligned}$$

all
equivalent \Leftarrow

Note:

The three possible cases for 2nd order

Step responses can be categorized by ξ :

Case 1 (Complex poles): $0 \leq \xi < 1$

$$\alpha_1^2 < 4\alpha_0 \Rightarrow (2\xi\omega_n)^2 < 4\omega_n^2 \quad \checkmark$$

Case 2 (repeated real poles): $\xi = 1$

$$\alpha_1^2 = 4\alpha_0 \Rightarrow (2\xi\omega_n)^2 = 4\omega_n^2 \quad \checkmark$$

Case 3 (distinct real poles): $\xi > 1$

$$\alpha_1^2 > 4\alpha_0 \Rightarrow 4\xi^2\omega_n^2 > 4\omega_n^2 \quad \checkmark$$

Thus finally, the Case 1 step response is:

$$\rightarrow y(t) = G(0) \left[1 - \left(\frac{\omega_n}{\omega_d} \right) e^{\sigma t} \sin(\omega_d t + \cos^{-1} \xi) \right]$$

We can now solve for important transient parameters

$\Rightarrow \underline{t_c}$: Solve for first $t > 0$ such that

$$y(t) = y_{ss}(t) = G(0)$$

$$\Rightarrow \sin(\omega_d t + \cos^{-1} \xi) = 0$$

$$\Rightarrow t_c = \frac{\pi - \cos^{-1} \xi}{\omega_d}$$

or:

$$t_c = \frac{\pi - \nu}{\omega_d}$$

\Rightarrow For t_p, y_p

Solve for first $t > 0$ such that

$$\dot{y}(t) = 0$$

$$\Rightarrow t_p = \frac{\pi}{\omega_d}$$

Substituting:

$$y_p = y(t_p) = G(0) [1 + e^{(\sigma\pi/\omega_d)}]$$

Define:

$$M_p = e^{(\sigma\pi/\omega_d)}$$

then:

$$y_p = G(0) [1 + M_p]$$

Peak Overshoot

⇒ M_p is the Normalized peak overshoot

$$y_p = G(0)[1 + M_p] \Rightarrow M_p = \frac{y_p - G(0)}{G(0)} = \frac{y_p - y_{ss}}{y_{ss}}$$

⇒ M_p is entirely determined by damping ratio ξ

$$M_p = \exp\left[\frac{\sigma\pi}{\omega_d}\right]$$

$$= \exp\left[\frac{(-\xi\omega_n)\pi}{\omega_n\sqrt{1-\xi^2}}\right]$$

OR

$$M_p = \exp\left[\frac{-\xi\pi}{\sqrt{1-\xi^2}}\right]$$

$$\%OS = 100 \times M_p$$

Settling Time

As usual, we can use the approximation

$$t_s \approx \frac{4}{|\operatorname{Re}\{\rho, \beta\}|} = \frac{4}{|\sigma|}$$

But t_s is actually a function of ξ also here:

$$t_s = \frac{C(\xi)}{|\sigma|}$$

with $3 \leq C(\xi) \leq 5$ for most $0 \leq \xi < 0.9$

so 4 is an "average" value for $C(\xi)$

However for $0.95 \leq \xi \leq 1$ a better approximation is:

$$t_s \approx \frac{6}{|\sigma|}$$

Summary: Case I step response; $P_1 = \sigma + j\omega_d$

"Natural" frequency: $\omega_n = \sqrt{\sigma^2 + \omega_d^2} = |P_1|$

Damping ratio: $\xi = \frac{|\sigma|}{\omega_n}$

1st crossing: $t_c = \frac{\pi - \cos^{-1}\xi}{\omega_d} = \frac{\pi - \nu}{\omega_d}$, $\xi = \cos \nu$

1st peak: $t_p = \frac{\pi}{\omega_d}$

Normalized overshoot: $M_p = \exp\left[\frac{\sigma\pi}{\omega_d}\right] = \exp\left[\frac{-\xi\pi}{\sqrt{1-\xi^2}}\right]$

$$M_p = \left[\frac{y_p - y_{ss}}{y_{ss}} \right]$$

Peak response: $y_p = y_{ss} [1 + M_p]$ $y_{ss} = G(\phi)$ for unit step

Limiting case: $\xi \rightarrow 0$

$\xi \rightarrow 0 \Rightarrow \sigma = -\xi\omega_n \rightarrow 0 \Rightarrow p_1 = j\omega_d$ (pure imaginary)

Overshoot $M_p = e^{(\sigma\pi/\omega_d)} \rightarrow 1$ (100% OS)

Peak: $y_p = G(0)[1 + M_p]$

or $y_p = 2y_{ss}$

Settling time: $t_s \approx \frac{4}{|\sigma|} = \infty$

Never settles!

Response oscillates infinitely between 0 and $2G(0)$
with frequency $\omega_d = \omega_n \sqrt{1 - \xi^2} = \omega_n$

"Undamped"

$y(t)$

$\xi = 0$
Oscillates continually

frequency $\omega_d = \text{Im}\{p_1\} = \omega_n$ here

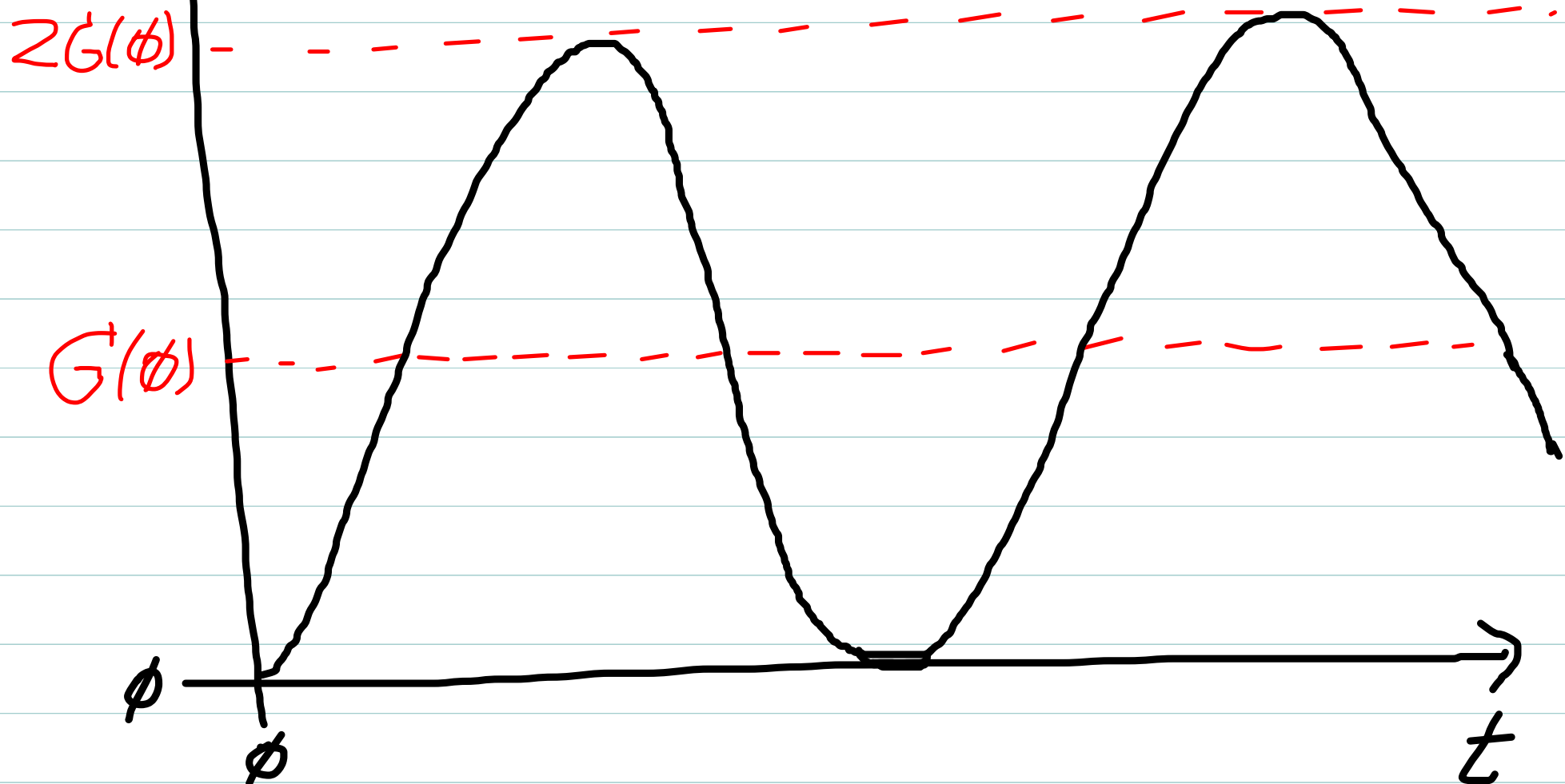
$2G(\phi)$

$G'(\phi)$

ϕ

ϕ

t



Limiting Case, $\xi \rightarrow 1$

$$\xi \rightarrow 1 \Rightarrow \sigma = -\xi \omega_n \rightarrow -\omega_n$$

$$\omega_d = \omega_n \sqrt{1 - \xi^2} \rightarrow 0$$

Response does not oscillate!

Overhoot: $M_p = e^{(\sigma \pi / \omega_d)} = e^{-\omega_n \pi / 0} = 0$

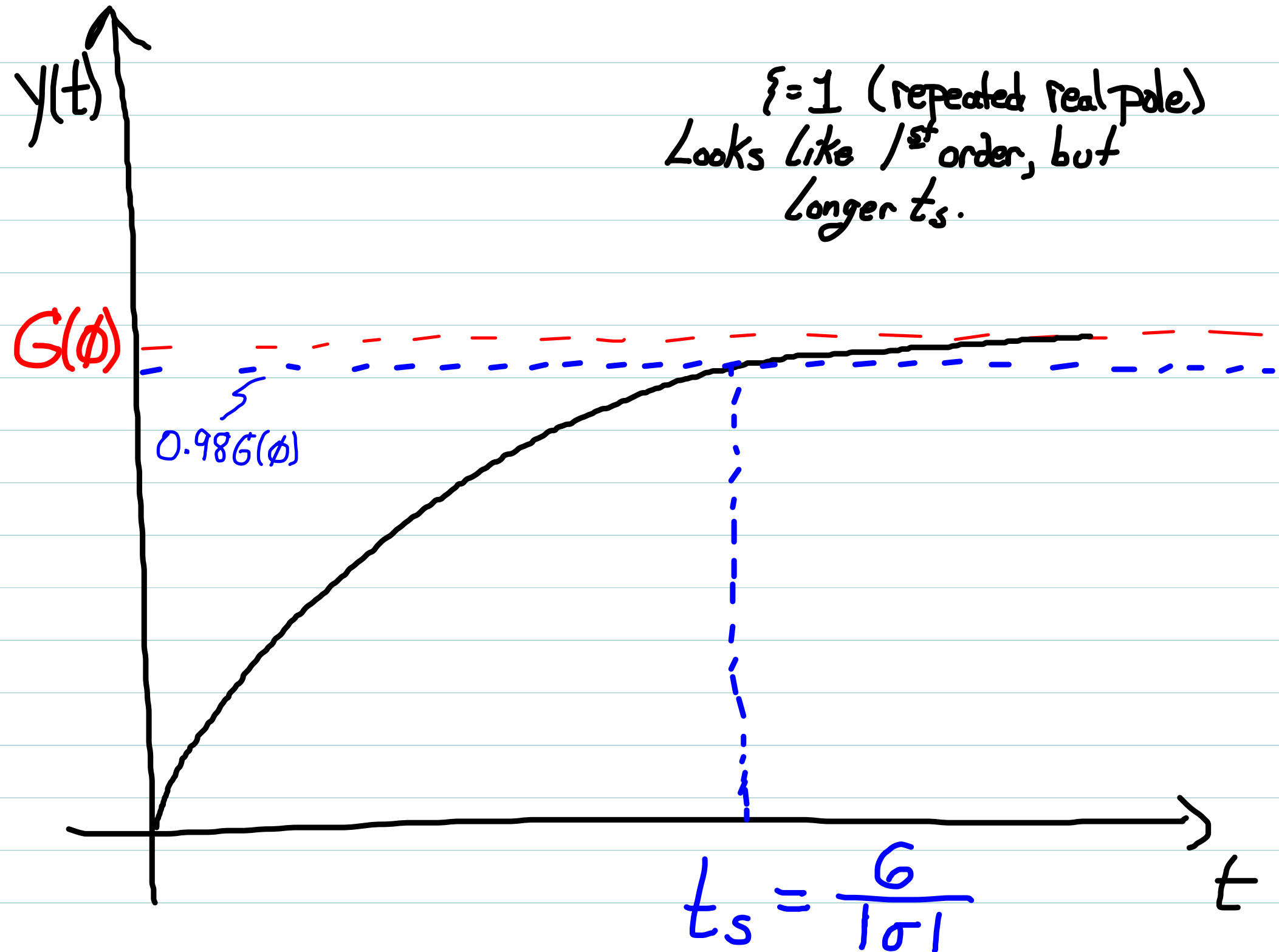
No overshoot

1st crossing: $t_c = \frac{\pi - \cos^{-1} \xi}{\omega_d} = \pi/2 / 0 = \infty$

\Rightarrow response asymptotes to y_{ss} from below

Settling: $t_s \approx \frac{6}{|\sigma|}$ use 6 here

$\zeta = 1$ (repeated real pole)
Looks like 1st order, but
longer t_s .

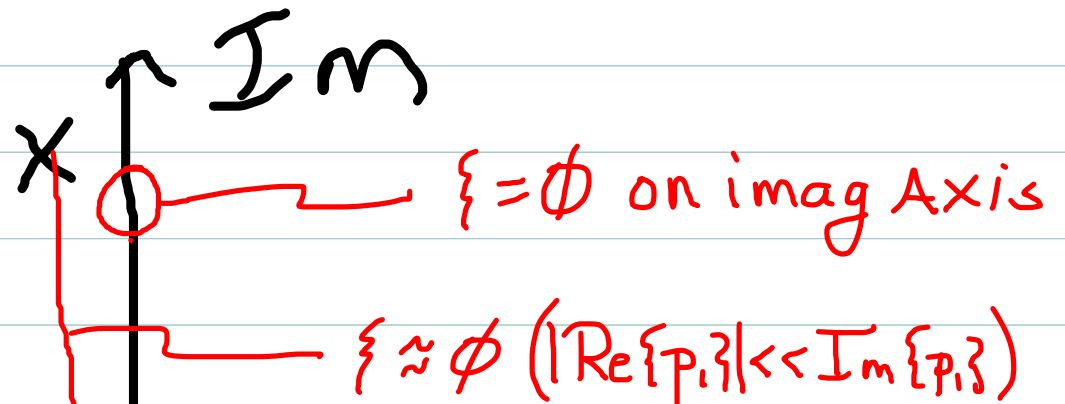
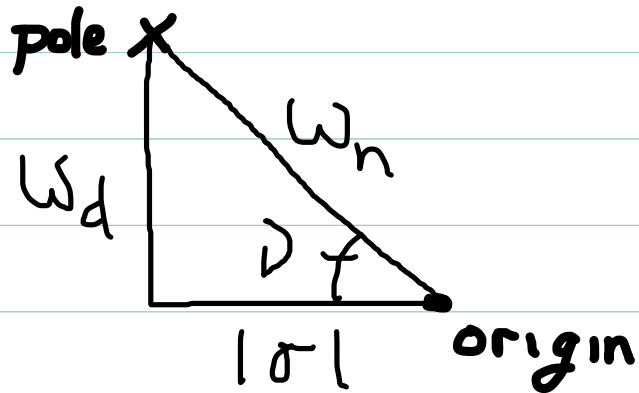


Graphical Interpretation of ξ :

$$\xi = \cos \nu :$$

$$\xi \rightarrow 0 \Rightarrow \nu \rightarrow \pi/2$$

$$\xi \rightarrow 1 \Rightarrow \nu \rightarrow 0$$



$$\xi \approx 1 \quad (|\text{Re}\{p,3\}| \gg \text{Im}\{p,3\})$$

$$\xi = 1 \text{ for repeated real Pole}$$

Lines of constant ξ lie on rays in upper left quadrant of complex plane:

