## Rotational Equations of Motion

$$\begin{split} I_{xx}\dot{\omega}_{x} - I_{xy}\big(\dot{\omega}_{y} - \omega_{x}\omega_{z}\big) - I_{xz}\big(\dot{\omega}_{z} + \omega_{x}\omega_{y}\big) - \big(I_{yy} - I_{zz}\big)\omega_{y}\omega_{z} - I_{yz}\big(\omega_{y}^{2} - \omega_{z}^{2}\big) &= M_{x} \\ I_{yy}\dot{\omega}_{y} - I_{yz}\big(\dot{\omega}_{z} - \omega_{x}\omega_{y}\big) - I_{xy}\big(\dot{\omega}_{x} + \omega_{y}\omega_{z}\big) - \big(I_{zz} - I_{xx}\big)\omega_{x}\omega_{z} - I_{xz}(\omega_{z}^{2} - \omega_{x}^{2}\big) &= M_{y} \\ I_{zz}\dot{\omega}_{z} - I_{xz}\big(\dot{\omega}_{x} - \omega_{y}\omega_{z}\big) - I_{yz}\big(\dot{\omega}_{y} + \omega_{x}\omega_{z}\big) - \big(I_{xx} - I_{yy}\big)\omega_{x}\omega_{y} - I_{xy}\big(\omega_{x}^{2} - \omega_{y}^{2}\big) &= M_{z} \end{split}$$

Three 1<sup>st</sup>-order EOMs in terms of angular velocities, not in terms of angles → We can't use them to solve for the orientation/attitude of a body!

## **Euler Angle Sequences**

- · Orientation/attitude/angles specified using three sequential rotations
- For example, we could use a "3-1-3" sequence:
  - Start with an inertial "a" frame
  - Rotate about the "3" axis by  $\phi$  to get a primed frame
  - Rotate about the primed "1" axis by heta to get a double primed frame
  - Rotate about the double primed "3" axis by  $\psi$  to get the body-fixed "b" frame

$$\begin{bmatrix} b_1 \\ b_2 \\ b_3 \end{bmatrix} = [R_3(\psi)][R_1(\theta)][R_3(\phi)]\begin{bmatrix} a_1 \\ a_2 \\ a_3 \end{bmatrix} = [R]\begin{bmatrix} a_1 \\ a_2 \\ a_3 \end{bmatrix}$$

$$\mathbf{1}^{\text{st}}$$

## Angular Velocity and Euler Angle Rates

- $\phi, \theta, \psi \rightarrow$  "Euler angles" (about individual axes)
- $\dot{\phi}$ ,  $\dot{\theta}$ ,  $\dot{\psi} \rightarrow$  "Euler Angle rates" (about individual axes)
- $\omega_1, \omega_2, \omega_3 \rightarrow$  "Angular velocities" (about body-fixed axes)
- We can write the angular velocity of the body in terms of  $\dot{\phi}$ ,  $\dot{\theta}$ ,  $\dot{\psi}$ :

$$\vec{\omega} = \dot{\phi}\hat{a}_3 + \dot{\theta}\hat{a}_1' + \dot{\psi}\hat{a}_3''$$

· Written in the body frame:

 $\vec{\omega} = (\dot{\phi}\sin\theta\sin\psi + \dot{\theta}\cos\psi)\hat{b}_1 + (\dot{\phi}\sin\theta\cos\psi - \dot{\theta}\sin\psi)\hat{b}_2 + (\dot{\phi}\cos\theta + \dot{\psi})\hat{b}_3$ 

$$\begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix} = \begin{bmatrix} \sin\theta \sin\psi & \cos\psi & 0 \\ \sin\theta \cos\psi & -\sin\psi & 0 \\ \cos\theta & 0 & 1 \end{bmatrix} \begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = [B] \begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix}$$

#### Three More Rotational EOMs

$$\begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix} = [B] \begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix}$$

· Solve for the Euler Angle rates:

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = [B]^{-1} \begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix}$$

$$\dot{\phi} = \frac{1}{s \theta} (\omega_x s \psi + \omega_y c \psi)$$

$$\dot{\theta} = \omega_x c \psi - \omega_y s \psi$$

$$\dot{\psi} = \frac{1}{s \theta} (-\omega_x c \theta s \psi - \omega_y c \theta c \psi) + \omega_z$$

## Six 1st-Order Rotational EOMs

$$\begin{split} I_{xx}\dot{\omega}_x - I_{xy}\big(\dot{\omega}_y - \omega_x\omega_z\big) - I_{xz}\big(\dot{\omega}_z + \omega_x\omega_y\big) - \big(I_{yy} - I_{zz}\big)\omega_y\omega_z - I_{yz}\big(\omega_y^2 - \omega_z^2\big) &= M_x \\ I_{yy}\dot{\omega}_y - I_{yz}\big(\dot{\omega}_z - \omega_x\omega_y\big) - I_{xy}\big(\dot{\omega}_x + \omega_y\omega_z\big) - \big(I_{zz} - I_{xx}\big)\omega_x\omega_z - I_{xz}\big(\omega_z^2 - \omega_x^2\big) &= M_y \\ I_{zz}\dot{\omega}_z - I_{xz}\big(\dot{\omega}_x - \omega_y\omega_z\big) - I_{yz}\big(\dot{\omega}_y + \omega_x\omega_z\big) - \big(I_{xx} - I_{yy}\big)\omega_x\omega_y - I_{xy}\big(\omega_x^2 - \omega_y^2\big) &= M_z \\ \dot{\phi} &= \frac{1}{s\,\theta}\big(\omega_x\,s\,\psi + \,\omega_y\,c\,\psi\big) \\ \dot{\theta} &= \omega_x\,c\,\psi - \omega_y\,s\,\psi \\ \dot{\psi} &= \frac{1}{s\,\theta}\big(-\omega_x\,c\,\theta\,s\,\psi - \,\omega_y\,c\,\theta\,c\,\psi\big) + \omega_z \end{split}$$
 Or  $\{\dot{\omega}\} = [I]^{-1}\{F\}$  and  $\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = [B]^{-1}\{\omega\}$ 

• Solve these six EOMs simultaneously (numerically) for body-fixed angular velocity ( $\omega_x$ ,  $\omega_y$ ,  $\omega_z$ ) and Euler angles ( $\phi$ ,  $\theta$ ,  $\psi$ )

#### Three 2<sup>nd</sup>-Order Rotational EOMs

$$\begin{split} I_{xx}\dot{\omega}_{x} - I_{xy}\big(\dot{\omega}_{y} - \omega_{x}\omega_{z}\big) - I_{xz}\big(\dot{\omega}_{z} + \omega_{x}\omega_{y}\big) - \big(I_{yy} - I_{zz}\big)\omega_{y}\omega_{z} - I_{yz}\big(\omega_{y}^{2} - \omega_{z}^{2}\big) &= M_{x} \\ I_{yy}\dot{\omega}_{y} - I_{yz}\big(\dot{\omega}_{z} - \omega_{x}\omega_{y}\big) - I_{xy}\big(\dot{\omega}_{x} + \omega_{y}\omega_{z}\big) - \big(I_{zz} - I_{xx}\big)\omega_{x}\omega_{z} - I_{xz}\big(\omega_{z}^{2} - \omega_{x}^{2}\big) &= M_{y} \\ I_{zz}\dot{\omega}_{z} - I_{xz}\big(\dot{\omega}_{x} - \omega_{y}\omega_{z}\big) - I_{yz}\big(\dot{\omega}_{y} + \omega_{x}\omega_{z}\big) - \big(I_{xx} - I_{yy}\big)\omega_{x}\omega_{y} - I_{xy}\big(\omega_{x}^{2} - \omega_{y}^{2}\big) &= M_{z} \\ \vec{\omega} &= (\dot{\phi}\sin\theta\sin\psi + \dot{\theta}\cos\psi)\hat{b}_{1} + (\dot{\phi}\sin\theta\cos\psi - \dot{\theta}\sin\psi)\hat{b}_{2} + (\dot{\phi}\cos\theta + \dot{\psi})\hat{b}_{3} \\ \vec{\omega} &= (...)\hat{b}_{1} + (...)\hat{b}_{2} + (...)\hat{b}_{3} \end{split}$$

- Plug three components of  $\vec{\omega}$  and  $\dot{\vec{\omega}}$  into equations of motion above  $\rightarrow$  Three 2<sup>nd</sup>-order ODEs in terms of  $\ddot{\theta}$ ,  $\ddot{\phi}$ ,  $\ddot{\psi}$ ,  $\dot{\theta}$ ,  $\dot{\phi}$ ,  $\dot{\psi}$ ,  $\theta$ ,  $\phi$ ,  $\psi$
- Define six state variables  $x_1 \dots x_6$
- Solve six state equations simultaneously (numerically) for  $heta(t), \phi(t), \psi(t)$

### Singularities

- There's a problem....
- Look at the case where  $\theta = 0$  (the middle rotation)
  - It's now like having a "3" rotation followed by another "3" rotation
  - We can't distinguish the 1st rotation from the 3rd rotation
- The problem shows up when we look at the [B] matrix:

$$\begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix} = [B] \begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix}$$

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = [B]^{-1} \begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix}$$

## Singularities

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = [B]^{-1} \begin{bmatrix} \omega_{\chi} \\ \omega_{y} \\ \omega_{z} \end{bmatrix}$$

- · When doesn't this work?
  - When  $[B]^{-1}$  doesn't exist  $\rightarrow$  when [B] is "singular"

$$[B] = \begin{bmatrix} \sin \theta \sin \psi & \cos \psi & 0 \\ \sin \theta \cos \psi & -\sin \psi & 0 \\ \cos \theta & 0 & 1 \end{bmatrix} \rightarrow [B]^{-1} = \begin{bmatrix} \frac{\sin \psi}{\sin \theta} & \frac{\cos \psi}{\sin \theta} & 0 \\ \cos \psi & -\sin \psi & 0 \\ \frac{-\sin \psi}{\tan \theta} & \frac{-\cos \psi}{\tan \theta} & 1 \end{bmatrix}$$

•  $[B]^{-1}$  breaks down when  $\theta=0,\pm\pi,\pm2\pi,...$ 

## Singularities

Could also see this from the determinant of [B]:

$$|B| = -\sin\theta \sin^2\psi - \sin\theta \cos^2\psi = -\sin\theta = 0$$
 
$$\to \theta = 0, \pm \pi, \pm 2\pi, \dots$$

## **Euler Angle Sequences**

• There are 12 possible Euler Angle sequences:

1-2-1	2-1-2	3-1-2	
1-2-3	2-1-3	3-1-3	
1-3-1	2-3-1	3-2-1	
1-3-2	2-3-2	3-2-3	

• Each sequence has different [R], [B], and singularities

		*	
$\begin{bmatrix} \frac{1}{\tau} + (\phi z \theta s + \omega z \theta s + \omega z \theta c \phi) + \omega z \theta e \phi + \omega z e \phi e$	$\begin{bmatrix} \varepsilon_{tm} + (\phi s \theta ) z_{tm} - \phi ) \theta s \tau_{tm} \\ \phi ) z_{tm} + \phi s \tau_{tm} \\ (\phi s z_{tm} + \phi ) \frac{\theta s}{\tau} \end{bmatrix} = \begin{bmatrix} \phi \\ \theta \\ \phi \end{bmatrix}$	$\begin{bmatrix} \varepsilon_{\mathcal{O}} + (\phi \circ \theta \circ z_{\mathcal{O}} - \phi \circ \theta \circ \tau_{\mathcal{O}} -) \frac{\theta}{\tau} \\ \phi \circ z_{\mathcal{O}} - \phi \circ \tau_{\mathcal{O}} \\ (\phi \circ \tau_{\mathcal{O}} + \phi \circ \tau_{\mathcal{O}}) \frac{\theta}{\tau} \end{bmatrix} = \begin{bmatrix} \phi \\ \theta \\ \phi \end{bmatrix}$	seteR elgnR relui to smre of neulanA selocitles
$\begin{bmatrix} \phi \circ \theta - \phi \circ \theta \circ \phi \\ \phi \circ \theta + \phi \circ \theta \circ \phi \\ \phi + \theta \circ \phi - \end{bmatrix} = \begin{bmatrix} \varepsilon_{00} \\ \varepsilon_{00} \\ \varepsilon_{00} \end{bmatrix}$	down the [B] matrix	$\begin{bmatrix} \psi + \theta \circ \phi \\ \psi \circ \phi + \psi \circ \theta \circ \phi \\ \psi \circ \phi + \psi \circ \phi \circ \phi \end{bmatrix} = \begin{bmatrix} \varepsilon \omega \\ \varepsilon \omega \\ \varepsilon \omega \end{bmatrix}$	Angular Velocities in Terms of Euler Angle Rates
$Z/\mu \mp = \theta$	Where it all breaks	$\pi \pm 0 = \theta$	Singularities
$\begin{bmatrix} 0 & \phi s - \phi s \theta s \\ 0 & \phi s - \phi s \theta s \\ 0 & \phi s & \phi s \theta s \end{bmatrix} = [g]$	$\begin{bmatrix} 0 & \phi \circ & \phi \circ \phi \circ \\ 0 & \phi \circ & \phi \circ \theta \circ - \end{bmatrix} = [a]$	$\begin{bmatrix} 1 & 0 & \theta \\ 0 & \phi s - \phi s \theta \\ 0 & \phi s & \phi s \theta \end{bmatrix} = \begin{bmatrix} B \end{bmatrix}$	xinteM [8]
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		Combined Combined Tanastion [R]
$3_{iq} : [B^3] = \begin{bmatrix} \phi & \phi$	Relates angular  2º Velocity to Euler angle rates	$3u_{2} : [R_{3}] = \begin{bmatrix} R_{3} \\ R_{3} \end{bmatrix} = \begin{bmatrix} R_{$	Transformation Matrices
[0 φs φο]	səlpoq Bullior to grimmide	celestial mechanics; spinning or rolling bodies	Application
<ul> <li>ψ (heading/yaw), θ (attitude/pitch), φ (bank/roll)</li> <li>γ (heading/yaw), ε (attitude dynamics)</li> </ul>	Relates body frame to inertial frame	$\phi$ (brecession), $\theta$ (nutation), $\psi$ (spin)	Sequence of salanA
3-2-1 (NASA Standard Airplane)	ard Aerospace)	3-1-3 (Historically Significant)	

I-	From	-

$\begin{bmatrix} \iota_{m} + (\phi \circ \theta s \varepsilon_{m} + \phi s \theta s z_{m}) \frac{\theta \circ}{1} \\ \phi s \varepsilon_{m} - \phi \circ z_{m} \\ (\phi \circ z_{m} + \phi s z_{m}) \frac{\theta \circ}{1} \end{bmatrix} = \begin{bmatrix} \phi \\ \theta \\ \phi \end{bmatrix}$	$\begin{bmatrix} \varepsilon_{m} + (\phi s \theta s \varepsilon_{m} - \phi s \theta s \tau_{m}) \frac{\theta s}{\tau} \\ \phi s \varepsilon_{m} + \phi s \tau_{m} \\ (\phi s \varepsilon_{m} + \phi s \tau_{m} -) \frac{\theta s}{\tau} \end{bmatrix} = \begin{bmatrix} \phi \\ \theta \\ \phi \end{bmatrix}$	$\begin{bmatrix} \varepsilon \omega + (\psi \circ \theta \circ \varphi \circ - \psi \circ \theta \circ \psi - \varphi \circ \varphi$	sets Angle Rates for Terms of Angle Rates Angle Rates Angle Rates
$\begin{bmatrix} \phi \circ \theta - \phi \circ \theta \circ \phi \\ \phi \circ \theta + \phi \circ \theta \circ \phi \\ \phi + \theta \circ \phi - \end{bmatrix} = \begin{bmatrix} s_{00} \\ t_{00} \end{bmatrix}$	$\begin{bmatrix} \phi + \theta \circ \phi \\ \phi \circ \phi + \phi \circ \theta \circ \phi \\ \phi \circ \theta + \phi \circ \theta \circ \phi - \end{bmatrix} = \begin{bmatrix} s_{co} \\ t_{co} \end{bmatrix}$	$\begin{bmatrix} \phi + \theta \circ \phi \\ \phi \circ \phi + \phi \circ \phi \circ \phi \\ \phi \circ \phi + \phi \circ \phi \circ \phi \end{bmatrix} = \begin{bmatrix} \varepsilon_{00} \\ \varepsilon_{00} \\ \vdots \\ 0 \end{bmatrix}$	Angular Velocities in Terms of Euler Terms of Stes
$Z/u \mp = \theta$	$\pi \pm 0 = \theta$	$ \mu \pm 0 = \theta $	Singularities
$\begin{bmatrix} 0 & \phi s - \phi s \theta o \\ 0 & \phi s - \phi s \theta o \\ 0 & \phi s - \phi s \theta o \end{bmatrix} = \begin{bmatrix} g \\ g \end{bmatrix}$	$\begin{bmatrix} \mathbf{I} & 0 & \theta \\ 0 & \phi 3 & \phi 5 \theta \\ 0 & \phi 5 & \phi 3 \theta 5 \end{bmatrix} = [\mathbf{g}]$	$\begin{bmatrix} t & \theta \\ 0 & hs - \phi \\ 0 & hs & \phi \\ s\theta s \end{bmatrix} = [g]$	xinteM [8]
$ \begin{bmatrix} \phi_{\partial}\theta_{\partial} & \phi_{\partial}\theta_{\beta} + \phi_{\beta}\phi_{\beta} - \phi_{\beta}\phi_{\beta} + \phi_{\beta}\phi_{\beta} \\ \phi_{\beta}\theta_{\partial} & \phi_{\beta}\theta_{\beta} + \phi_{\beta}\phi_{\beta} + \phi_{\beta}\phi_{\beta} \\ \theta_{\beta}\theta_{\beta} & \phi_{\beta}\theta_{\beta}\phi_{\beta} + \phi_{\beta}\phi_{\beta} \\ \theta_{\beta}\phi_{\beta} & \phi_{\beta}\phi_{\beta}\phi_{\beta} \\ \theta_{\beta}\phi_{\beta} & \phi_{\beta}\phi_{\beta} \\ \phi_{\beta}\phi_{\beta} & \phi_{\beta}\phi_{\beta} $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		Combined Transformation Matrix [R]
$\begin{bmatrix} \phi \circ & \phi s - 0 \\ \phi s & \phi \circ & 0 \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} xy \end{bmatrix} :_{\varphi x} $ $\begin{bmatrix} \phi \circ & \phi s - 0 \\ 0 & 0 & \theta s \end{bmatrix} = \begin{bmatrix} zy \end{bmatrix} :_{\varphi x} $ $\begin{bmatrix} \theta \circ & 0 & \theta s \\ 0 & 1 & 0 \end{bmatrix} = \begin{bmatrix} zy \end{bmatrix} :_{\varphi x} $ $\begin{bmatrix} 1 & 0 & 0 \\ \theta s - 0 & \theta s \end{bmatrix} = \begin{bmatrix} xy \end{bmatrix} :_{\varphi x} $ $\begin{bmatrix} 1 & 0 & 0 \\ 0 & \phi s & \phi s \end{bmatrix} = \begin{bmatrix} xy \end{bmatrix} :_{\varphi x} $	$\begin{bmatrix} 0 & \psi_2 & \psi & \text{albbim ant to sau} \\ 1 & 0 & \psi & \text{albbim ant to sau} \\ \theta_2 & 0 & 0 & \text{albbim ant to sau} \\ \theta_3 & 0 & 0 & \text{albbim ant to sau} \\ 0 & 0 & 0 & 0 & \text{albbim ant to sau} \\ 0 & 0 & 0 & 0 & \text{albbim ant to sau} \\ 0 & 0 & 0 & 0 & \text{albbim ant to sau} \\ 0 & 0 & 0 & 0 & 0 & 0 & \text{albbim ant to sau} \\ 0 & 0 & 0 & 0 & 0 & 0 & \text{albbim ant to sau} \\ 0 & 0 & 0 & 0 & 0 & 0 & \text{albbim ant to sau} \\ 0 & 0 & 0 & 0 & 0 & 0 & \text{albbim ant to sau} \\ 0 & 0 & 0 & 0 & 0 & 0 & \text{albbim ant to sau} \\ 0 & 0 & 0 & 0 & 0 & 0 & \text{albbim ant to sau} \\ 0 & 0 & 0 & 0 & 0 & 0 & \text{albbim ant to sau} \\ 0 & 0 & 0 & 0 & 0 & 0 & \text{albbim ant to sau} \\ 0 & 0 & 0 & 0 & 0 & 0 & \text{albbim ant to sau} \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0$	0 05 02	Transformation Ratifices
vehicle motion; attitude dynamics	ro drs ( Yill Brity ) roules	celestial mechanics; spinning or rolling bodies	Application
ψ (heading/yaw), θ (attitude/pitch), φ (bank/roll)	h Euler angle tation), $\phi$ (spin)	φ (precession), θ (nutation), ψ (spin)	Sequence of Assigner
3-2-1 (AASA Standard Airplane)	ard Aerospace)	3-1-3 (Historically Significant)	

# Attitude Estimation (WAY oversimplified)

- Frequently systems (robots, aircraft, spacecraft) have an inertial measurement unit (IMU)  $\rightarrow \omega_1, \omega_2, \omega_3$
- · How can we estimate the attitude of a system from IMU (angular velocity) data?
  - We can't just integrate the angular velocities  $\omega_1,\omega_2,\omega_3$  to get the angles  $\phi,\theta,\psi$
  - · Why?
- Use [B] to estimate Euler angle rates from angular velocities:

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = [B]^{-1} \begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix}$$

· Then integrate Euler angle rates to get Euler angles:

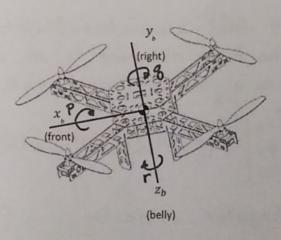
$$\begin{split} \phi &= \int \dot{\phi} dt \quad \text{or} \quad \phi_{k+1} = \phi_k + \dot{\phi}_k \Delta t \\ \theta &= \int \dot{\theta} dt \quad \text{or} \quad \theta_{k+1} = \theta_k + \dot{\theta}_k \Delta t \\ \psi &= \int \dot{\psi} dt \quad \text{or} \quad \psi_{k+1} = \psi_k + \dot{\psi}_k \Delta t \end{split}$$

• In practice, MUCH more sophisticated methods are used (sensor fusion, Kalman filters, etc.)

Body-fixed frame B at G

Angular velocity:

$$2\omega^3 = \begin{bmatrix} P \\ q \\ r \end{bmatrix}$$
 or  $\vec{\omega} = P \hat{\lambda}_B + Q \hat{j}_B + r \hat{k}_B$ 



Angular acceleration:

$$\vec{\lambda} = \left(\frac{d\vec{w}}{dt}\right)_{rel} + \vec{w} \times \vec{w} = \vec{p} \hat{i}_{8} + \vec{q} \hat{j}_{8} + \vec{r} \hat{k}_{8}$$

Moment acting on body:

$$\vec{M} = (\vec{F}_3 + \vec{F}_4 - \vec{F}_1 - \vec{F}_2) L \hat{\lambda}_B + (\vec{F}_1 + \vec{F}_3 - \vec{F}_2 - \vec{F}_4) L \hat{J}_B$$

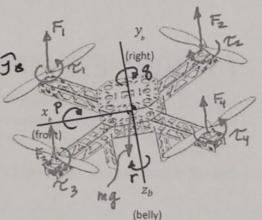
$$+ (\tau_2 + \tau_3 - \tau_1 - \tau_4) \hat{\lambda}_B$$

Assume planes of symmetry Euler's equations:

$$\dot{P} = \frac{I_{y} - I_{z}}{I_{x}} g_{\Gamma} + \frac{L}{I_{x}} (F_{3} + F_{4} - F_{1} - F_{2})$$

$$\dot{g} = \frac{T_{z} - I_{x}}{I_{y}} p_{\Gamma} + \frac{L}{I_{y}} (F_{1} + F_{3} - F_{2} - F_{4})$$

$$\dot{r} = \frac{T_{x} - I_{y}}{I_{z}} p_{g} + \frac{L}{I_{z}} (\tau_{2} + \tau_{3} - \tau_{1} - \tau_{4})$$



3 rotational EOMs

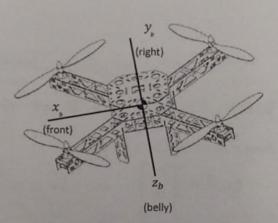
To find orientation ("attitude") of the body relative to an inertial frame, use a 3-2-1 Euler angle sequence

$$\begin{bmatrix} x_{B} \\ y_{B} \\ z_{B} \end{bmatrix} = \begin{bmatrix} R_{x}(\phi) \end{bmatrix} \begin{bmatrix} R_{y}(\Theta) \end{bmatrix} \begin{bmatrix} R_{z}(\psi) \end{bmatrix} \begin{bmatrix} x_{z} \\ y_{z} \\ z_{z} \end{bmatrix}$$

Angular velocity:

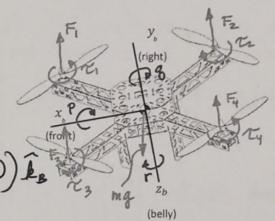
$$\begin{bmatrix} P \\ Q \\ r \end{bmatrix} = \begin{bmatrix} B \end{bmatrix} \begin{bmatrix} \dot{\psi} \\ \dot{\phi} \end{bmatrix} = \begin{bmatrix} -s\theta & 0 & 1 \\ c\theta s\phi & c\phi & 0 \\ c\theta c\phi & -s\phi & 0 \end{bmatrix} \begin{bmatrix} \dot{\psi} \\ \dot{\phi} \\ \dot{\phi} \end{bmatrix}$$

$$\begin{bmatrix} \dot{\phi} \\ \dot{\phi} \\ \dot{\phi} \end{bmatrix} = \begin{bmatrix} B \end{bmatrix}^{-1} \begin{bmatrix} P \\ g \\ r \end{bmatrix} \implies \begin{vmatrix} \dot{\phi} = \frac{1}{c\theta} (g s \phi + r c \phi) \\ \dot{\phi} = g c \phi - r s \phi \\ \dot{\phi} = \frac{1}{c\theta} (g s \phi + r s \theta c \phi) + p \end{bmatrix}$$



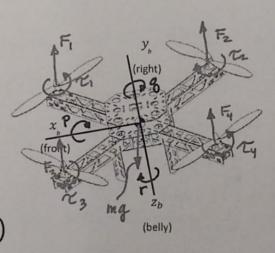
rotational 6 EO MS

$$F = -mgsin \Theta \Sigma_B + mgcos \Theta sin \Phi J_B + \left( mgcos \Theta cos \Phi - (F_1 + F_2 + F_3 + F_4) \right) \hat{I}_B$$



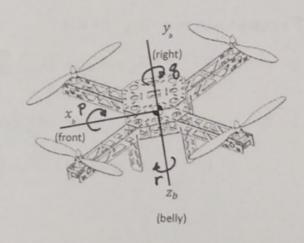
#### Acceleration:

$$\vec{\Delta}_{G} = \frac{d\vec{v}_{G}}{dt} = \left(\frac{d\vec{v}_{G}}{dt}\right)_{rel} + \vec{w} \times \vec{v}_{G}$$



$$\dot{u} = rv - gw - gsin\theta$$
 $\dot{v} = pw - ru + gcos\theta sin\theta$ 
 $\ddot{u} = gu - pv + gcos\theta cos\theta - (F_1 + F_2 + F_3 + F_4)/M$ 
 $= gu - pv + gcos\theta cos\theta - (F_1 + F_2 + F_3 + F_4)/M$ 

To find position of the body relative to an inertial frame:



(belly)

 $P_{n} = u c \phi c \psi + v (s \phi s \theta c \psi - c \phi s \psi) + w (c \phi s \theta c \psi + s \phi s \psi)$   $\dot{P}_{e} = u c \theta s \psi + v (s \phi s \theta s \psi + c \phi c \phi) + w (c \phi s \theta s \psi - s \phi c \psi)$   $-\dot{u} = -u s \theta + v s \phi c \theta + w c \phi c \theta$ 

$$\dot{P} = \frac{T_{N} - T_{Z}}{T_{X}} \theta \Gamma + \frac{L}{T_{X}} (F_{3} + F_{4} - F_{4} - F_{2})$$

$$\dot{\theta} = \frac{T_{Z} - T_{X}}{T_{Y}} P \Gamma + \frac{L}{T_{Y}} (F_{1} + F_{3} - F_{2} - F_{4})$$

$$\dot{\Gamma} = \frac{T_{X} - T_{Y}}{T_{Z}} P \theta + \frac{1}{T_{Z}} (T_{Z} + T_{3} - T_{4} - T_{4})$$

$$\dot{\Psi} = \frac{1}{C_{Q}} (\theta_{S} + \Gamma_{Q} +$$

and translation