## FLOW METERING

Venturi meter, orifice meter Pitot Tube Rotameter Turbine meters, Thermal meter

 $\propto_b v_b^2 - \propto_a v_a^2 = \frac{2(P_a - P_b)}{P}$  $\overline{V}_a = \left(\frac{D_b}{D_a}\right)^n \overline{V}_b$  $\Rightarrow V_b = \frac{1}{\sqrt{x_b - \left(\frac{A_b}{D_a}\right)^4 x_a}} \sqrt{\frac{2(P_a - P_b)}{g}}$ 

$$=\frac{C_V}{\sqrt{1-\beta^4}}\sqrt{\frac{2(P_a-P_b)}{P}}$$

Kirchic energy correction factor For an element of cross-sectional area ds, the mass flow rate = guds. where each man unit carries energy ut => Total energy trough ds per unt time dEx = (guds) " For entire Oross-Section => Kinetic energy per unit mass per unit man forcen to include in Bernoulli's egn. Ek = 25 uds in Bernoulli's egn. suds Vs

Flow Metering .... contd. For an orificemeter (measures flowrate) 10' refers to parameters at orifice  $U_0 = \frac{C_0}{\sqrt{1-\beta^4}} \sqrt{\frac{2(P_a-P_b)}{P}}$   $C_0 = 0.61$  for  $R_0 = \frac{D_0 U_0 P}{\mu} 730,000$ y Vena Contracta 1 Significant energy loss at orifice " Availability of straight pipe neguired at upstream and downstream. Pitot tube (measures local velocity) Static tube measures to (static premue)

Stocamline AB terminates at B (the stagnation point); 46 gets converted to  $\frac{P_s - P_o}{P}$  =  $\frac{1}{\sqrt{2(P_s - P_o)}}$ Venturimeter Problem , Colculate oil flowrate = (150 mm 0.01767 m²  $(\approx 0.1489 \text{ m}^3/\text{s})$ , Plot the change in pressure, as fluid travels through venturimete 300mm > A = 0.07 m<sup>2</sup> " Calculate  $f_1 - f_2$  ( $\approx 33.8 \text{ kfa}$ ) 1 1 1 oil of sp. Gr. = 0.9

## **EXAMPLE PROBLEM 6.2**

GIVEN: A pitot tube inserted in a flow as shown. The flowing fluid is air and the manometer liquid is mercury.

FIND: The flow speed.

## SOLUTION:

Basic equation: 
$$\frac{p}{\rho} + \frac{V^2}{2} + gz = \text{constant}$$

Assumptions: (1) Steady flow

(2) Incompressible flow

(3) Flow along a streamline

(4) Frictionless deceleration along stagnation streamline

Writing Bernoulli's equation along the stagnation streamline (with  $\Delta z = 0$ ) yields

$$\frac{p_0}{\rho} = \frac{p}{\rho} + \frac{V^2}{2}$$

 $p_0$  is the stagnation pressure at the tube opening where the speed has been reduced, without friction, to zero. Solving for V gives

$$V = \sqrt{\frac{2(p_0 - p)}{\rho_{\rm air}}}$$

From the diagram,

$$p_0 - p = \rho_{\rm Hg}gh = \rho_{\rm H_2O}gh(\rm SG_{\rm Hg})$$

and

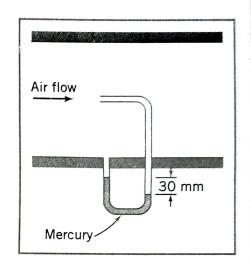
$$V = \sqrt{\frac{2\rho_{\text{H}_2\text{O}}gh(\text{SG}_{\text{Hg}})}{\rho_{\text{air}}}}$$

$$= \sqrt{\frac{2}{1000} \frac{\text{kg}}{\text{m}^3} \times \frac{9.81 \text{ m}}{\text{s}^2} \times \frac{30 \text{ mm}}{1000 \text{ mm}} \times \frac{13.6}{1.23 \text{ kg}}} \times \frac{\text{m}^3}{1.23 \text{ kg}}}$$

$$V = 80.8 \text{ m/s}$$

At T = 20°C, the speed of sound in air is 343 m/s. Hence, M = 0.236 and the assumption of incompressible flow is valid.

This problem illustrates the use of a pitot tube to determine the flow speed at a point.



Definition of DRAG gheory of Rotameter (i) the weight of the float = (rot. of float) (density) of

(ii) the buoyancy force = (rot. of float) (fluid density) of

(iii) the buoyancy force on the float = AfCD of 12

The DEDIT (ii) = (iii)

Since (i) and (ii) do not depend on flow rate or relocity, the

draw force for an analysis to of these forces is constant. Balance of three forces drag force for equilibration of three forces is constant.
i.e., u must remain constant, even when the flowrate changes. Flow rate =  $u \frac{\pi}{4} (D_t^2 - D_f^2) = u \frac{\pi}{4} \left[ 2D_f ah + a^2 h^2 \right] \approx u \frac{\pi}{2} D_f ah$ where Df is the diameter of the float. and D is the inner diameter of linearly tapered tube = Df + ah PRotameter has linear relationship between the flowrate and reading. In case of venturimeter/orificemeter, flow rate & Treading. Straight pipe section at inlet and ontlet is not required.