

INDIAN INSTITUTE OF TECHNOLOGY

DATE

SHEET NO.

Expt No.	Name of Experiment	Page No.	Date of Experiment	Date of Submission	Remarks
04→	To chart the flow projectile for an orifice/nozzle with a Hook's gauge .		10/01/23	17/01/23	9.5/10
05→	Pipeline viscometer		17/01/23	24/01/23	9/10
06(a)→	Calibration of Venturi meter		24/01/23	31/01/2023	8.5/10
	(b) Calibration of rotameter				
07→	pitot tube		31/01/23	07/02/2023	9/10
08→	Flow through triangular Notch weirs		07/01/23	14/02/2023	9.5/10

DATE 10/01/23

Experiment → 04
Hooke's gauge

SHEET NO. 1

Objective : → To chart the flow projectile for an orifice/nozzle with Hooke's gauge and hence to calculate:

- (a) Coefficient of Velocity C_v
- (b) Coefficient of discharge C_d
- (c) Coefficient of Contraction C_c

Theory:

A jet of liquid flowing through an orifice/nozzle under pressure will assume a parabolic path for a free fall condition.

$$x = v_x t$$

$$y = \frac{1}{2} g t^2$$

Actual velocity of the jet using equation (1) & (2)

$$v = \sqrt{\frac{g h^2}{2y}}$$



Since the constant head is maintained in liquid tank, theoretical velocity can be given as:

$$V_{th} = \sqrt{2g\Delta H}$$

Hence $c_v = \frac{\text{Actual Velocity } V}{\text{Theoretical velocity } V_{th}} = \sqrt{\frac{g n^2 / 24}{2g\Delta H}}$

Since there is Contraction of the jet, coefficient of contraction,

(C) is the ratio between the jet areas at Vena Contracta and at the orifice.

$$c_d = \frac{\text{Actual discharge}}{\text{Theoretical discharge}} = \frac{c_v}{A_m}$$

Apparatus

Hook's gauge, stop watch, bucket, weighing balance.

Procedure

Maintain constant head of liquid with the help of bypass valve and measure the actual flow rate. Measure the actual flow rate. Measure the actual co-ordinates of various point of the jet and repeat the same for two liquid free heads.

Calculation procedure

$$\text{Actual velocity } (v) = \sqrt{\frac{g n^2}{2y}}$$

$$d = 1.0998 \text{ cm}$$

$$\text{for } Q = 14 \text{ L/min}$$

$$= 233.33 \text{ cm}^3/\text{s}$$

$$\text{head} = 4.9 \text{ cm}$$

$$\textcircled{1} \quad n = 5 \text{ cm} \quad g = 3 \text{ cm}$$

$$V = \sqrt{\frac{g n^2}{2y}} = 63.93 \text{ cm/s}$$

$$V_{th} = 92.91 \text{ cm/s}$$

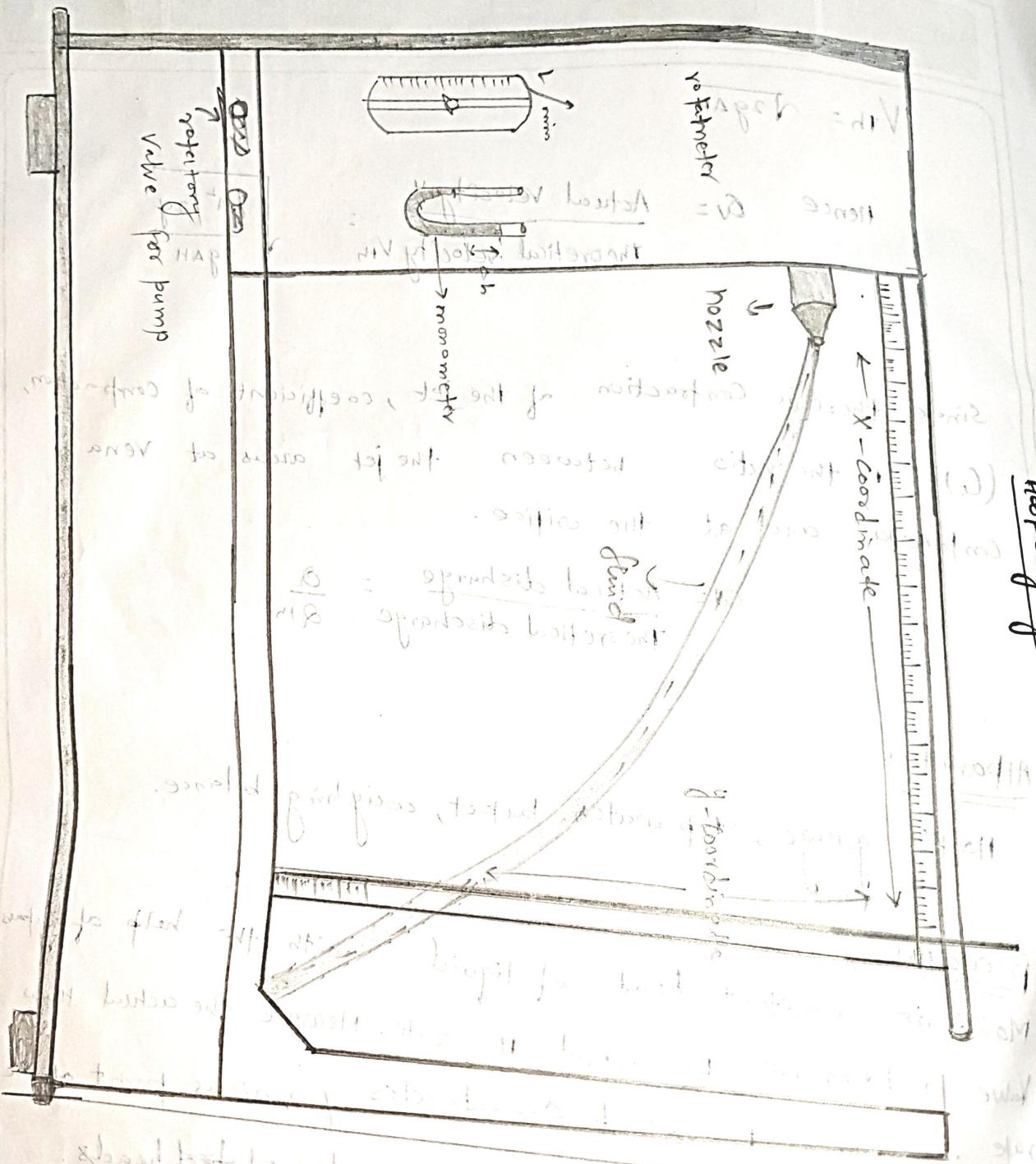
$$C_V = \frac{n}{\sqrt{4y \Delta n}} = 0.688$$

$$Q = \frac{\pi}{4} d^2 V = \frac{\pi}{4} \frac{242.93}{4} \text{ cm}^3/\text{s} = 60.73$$

$$Q_{th} = 233.33 \text{ cm}^3/\text{s}$$

$$C_d = \frac{Q}{Q_{th}} = 0.26027, \quad C_C = \frac{C_d}{C_V} = 0.377$$

Hooke's gauge:



ObservationTable No. 1

$$Q = 8 \text{ L/min}$$

, Head = 3.6 cm

RUN NO	X(cm)	y(cm)	C _v	C _d	C _e
1	5	3.5	0.704	0.421	0.59
2	10	5	1.417	0.705	0.602
3	15	7	1.494	0.894	0.598
4	20	10.5	1.626	0.9739	0.598
5	25	14	1.76	1.0545	0.598

$$Q = 10 \text{ L/min}$$

Head = 4 cm.

RUN NO.	X(cm)	y(cm)	C _v	C _d	C _e
1	5	4	0.628	0.318	0.504
2	10	4.5	1.178	0.625	0.531
3	15	5.5	1.599	0.849	0.530
4	20	7	1.889	1.004	0.531
5	25	9.5	2.027	1.023	0.504

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flow rate = 12 L/min

Head = 4.2 cm

run no.	x (cm)	y (cm)	C _v	C _d	C _c
1	5	3.5	0.652	0.28	0.43
2	10	4	1.22	0.526	0.43
3	15	4.8	1.64	0.7202	0.43
4	10	5.7	2.04	0.8812	0.43
5	15	7.3	2.25	0.97	0.43

flow rate = 14 L/min

Head = 4.4 cm

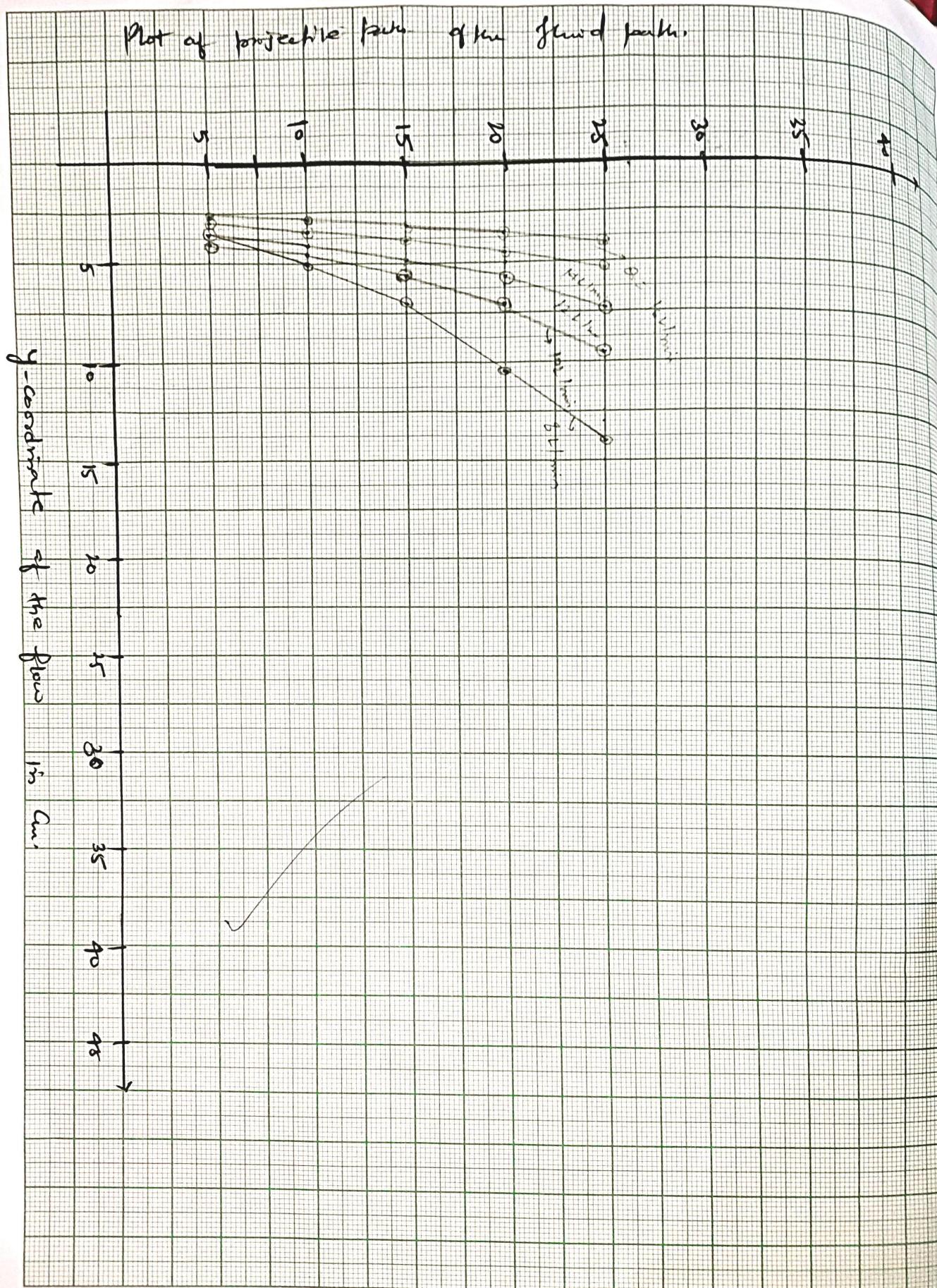
run no.	x (cm)	y (cm)	C _v	C _d	C _c
1	5	3	0.68	0.2607	0.377
2	10	3.5	1.27	0.4814	0.377
3	15	3.9	1.810	0.684	0.377
4	20	4.5	2.247	0.849	0.377
5	25	5.3	2.5884	0.978	0.377

flow rate = 16 L/min

Head = 4.7 cm

run no.	x (cm)	y (cm)	C _v	C _d	C _c
1.	5	2.7	0.701	0.240	0.342
2.	10	2.8	1.378	0.471	0.342
3.	15	3.1	1.964	0.6772	0.342
4.	20	3.5	2.465	0.843	0.342
5.	25	4.5	2.813	0.962	0.342

Plot of projectile paths of the glued paths.



• Discussion

Measurement of the Venaconstricta is useful in echo Cardiography, where it describes the smallest area of the blood flow jet as it exists at least value. This corresponds to effective orifice area calculator ~~at least~~ Valves using the continuity equation.

The effect is also observed in flow from a tank into pipe or sudden contraction in pipe diameter. streamline will converge just down stream of the diameter change, & a region of separated flow occurs from the diameter change and extends past the Vena Constricta. The formation of Vena Constricta can be seen in Venturi meter. The reason for this phenomena is that fluid streamline cannot abruptly change direction.

- Due to scale error, the Value of C_D goes over 1.
also ~~removes~~ in calculation

Precautions

- 1 → Take the reading of discharge accurately.
- 2 → Take value of h without any parallax error.
- 3 → Take reading from ~~top~~ hook gauge Carefully.
- 4 → Water flow should be steady and uniform.

⇒ Explain the plot = ?

Rat
17 Jan 2023

Pipeline Viscometer

→ Aim → To prepare the shear diagram for the fluid under study & to calculate its viscosity.

→ Theory → When a fluid flows through a pipe, it experiences drag because of stationary boundary wall of pipe. The fluid being viscous there sets in a velocity gradient. If Δp is the pressure drop due to drag over a length of pipe L. at diameter D, at the viscometer flow rate of fluid Q, then the shear stress at wall & average rate of shear are given by

$$\tau_w = \frac{\Delta p \cdot D}{4L}$$

$$\left(\frac{du}{dr}\right)_{avg} = \frac{32Q}{\pi D^3}$$

τ_w → Shear stress, kg/mm^2

Δp → Pressure drop

D → Diameter of pipe, m

Procedure

1) Open pipe valve wait for 1-2 seconds so that there is steady flow is maintained inside pipe.

2) Set a timer & collect water at other end & measure the pressure drop manometric system.

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- 3) Change Valve opening & take different readings.
- 4) Repeat the experiment for different pipe dimensions & notedown the required readings.

→ Observation & Calculation

Inside diameter:

$$\text{Pipe } \rightarrow 1 = 1.3 \text{ cm}$$

$$\text{Pipe } \rightarrow 2 = 6 \text{ mm}$$

$$\text{Pipe } \rightarrow 3 = 5 \text{ mm}$$

$$\text{Pipe } \rightarrow 4 = 3 \text{ mm}$$

Manometric fluid $\Rightarrow CCl_4$ $\rho_{CCl_4} = 1.6 \text{ g/cm}^3$

Manometric fluid $\Rightarrow CH_4$

Manometric fluid $\Rightarrow CCl_4$

Manometric fluid \Rightarrow Mercury

Thickness = 1.5 cm

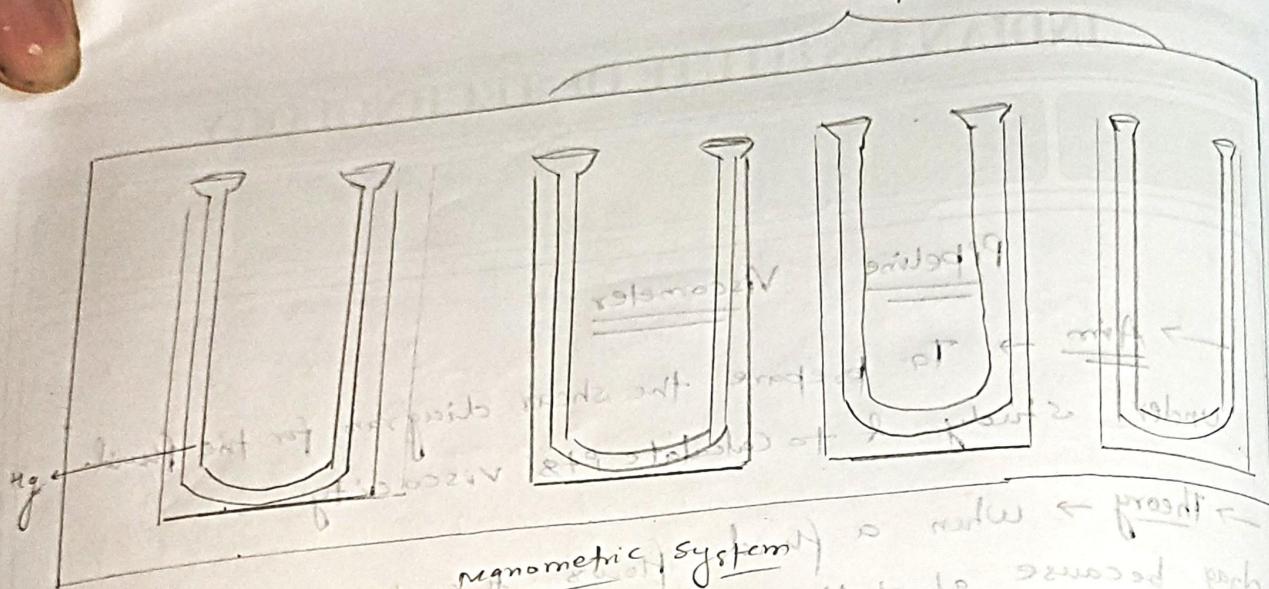
length of pipes, $L = 186 \text{ cm}$.

→ Pipe 1

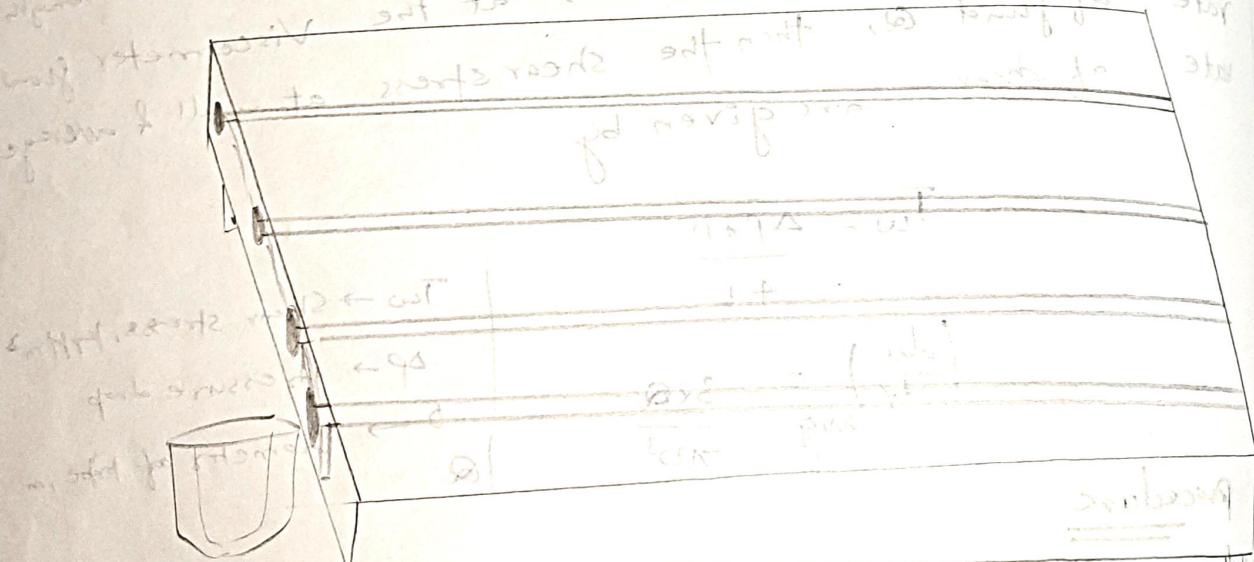
$$d = 1.3 \text{ cm}$$

SLNO	Mass of fluid collected (kg)	time (s)	Volumetric flowrate (m^3/s)	Manometer height		Δh	ΔP
				left	right		
1	400×10^{-3}	10	4×10^{-5}	5.7	11.7	6	36
2	362×10^{-3}	10	3.62×10^{-5}	6.7	10.8	4.1	24.6
3	305×10^{-3}	10	3.05×10^{-5}	7.4	10.3	2.9	17.4
4	228×10^{-3}	10	2.25×10^{-5}	7.9	9.6	1.7	10.2

CCl₄



chromatographic system is never → product
is not yet known pronounced probability for some parts of
the mixture to spread more than others
leading to different parts of the mixture to be measured in different
parts of the system refer to → effect of
with retention set to 0 → effect of → effect of
position + 1 → next reads off set → effect of → effect of
of mixing.



Bucket is not empty or massless so it finds itself 160 g
and abides by the law of the balance for weight
and pressure tends to replace the weight of the
material in its place.

111110013

Satish Khan

500

50
30
20

10

→

(τ_{22} / m^3)
 $\times 10^{-3}$

50
40
30
20
10

10
20
30
40
50

10
20
30
40
50

10
20
30
40
50

100
200
300
400
500

1000
10000
100000
1000000

dy/dt (sec)
LOG LOG 2CV x 3 CYCLES

LOG LOG 2CV x 3 CYCLES

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Pipe 2 $d = 6 \text{ mm}$

SL.NO	Mass of fluid collected (kg)	time (s)	Volumetric flow rate (m^3/s)	Manometer height left	Manometer height right	difference Δh (cm)	ΔP
1	80×10^{-3}	1 min	1.33×10^{-6}	6.8	4	2.8	16.8
2	150×10^{-3}	1 min	2.5×10^{-6}	8.1	2.5	5.6	33.6
3	34×10^{-3}	1 min	0.567×10^{-6}	6.1	4.7	1.4	8.4
4	125×10^{-3}	1 min	2.08×10^{-6}	7.8	3	4.8	28.8

Pipe 3 $d = 5 \text{ mm}$

SL.NO	Mass of fluid collected (kg)	time (s)	Volumetric flow rate (m^3/s)	Manometric height left	Manometric height right	difference Δh	ΔP
1	135×10^{-3}	1 min	2.25×10^{-6}	8.7	9	0.3	1.8
2	70×10^{-3}	1 min	1.67×10^{-6}	7.7	2.9	4.8	28.8
3	45×10^{-3}	1 min	0.75×10^{-6}	5.8	4.1	1.7	10.2
4	13×10^{-3}	1 min	0.21×10^{-6}	5.4	4.7	0.7	4.2

Pipe 4 $d = 3 \text{ mm}$

SL.NO	Mass of fluid collected	time (s)	Volumetric flow rate (m^3/s)	Manometric height left	Manometric height right	difference Δh	ΔP
1	30×10^{-3}	10 s	0.8×10^{-5}	12.7	5.1	7.6 cm	108.8
2	32×10^{-3}	10 s	0.32×10^{-5}	12.7	6.1	6.6 cm	83.8
3	28×10^{-3}	10 s	0.28×10^{-5}	11.4	7.4	4 cm	50.4
4	12.8×10^{-3}	10 s	0.125×10^{-5}	10.3	8.64	1.8	22.8

Result :-Pipe → 1

<u>SL. No</u>	$Q = \text{Volumetric flow rate} (\text{m}^3/\text{s})$	$\tau_w = \text{Shear stress} (\text{kg}/\text{fm}^2)$	$\frac{dy}{dx}$
1	4×10^{-5}	62.9×10^{-3}	185.451
2	3.62×10^{-5}	42.93×10^{-3}	167.833
3	3.05×10^{-5}	30.40×10^{-3}	141.466
4	2.25×10^{-5}	17.82×10^{-3}	104.31

Pipe → 2

<u>SL. NO</u>	$Q = \text{Volumetric flow rate} (\text{m}^3/\text{s})$	$\tau_w = \text{shear stress} (\text{kg}/\text{fm}^2)$	$\frac{dy}{dx}$ (unit)?
1	1.33×10^{-6}	13.54×10^{-3}	62.71
2	2.15×10^{-6}	27.09×10^{-3}	117.89255
3	5.66×10^{-7}	6.77×10^{-3}	23.9688
4	2.08×10^{-6}	22.22×10^{-3}	98.088

$\mu_2 = 0.244 \times 10^{-3}$

Pipe - 3

$$D = 5 \text{ mm}$$

SL. NO	$Q (m^3/s)$	T_w	du/dy
1	2.25×10^{-6}	1.20×10^{-3}	183.34
2	1.67×10^{-6}	19.35×10^{-3}	136.083
3	0.75×10^{-6}	6.85×10^{-3}	61.11
4	0.21×10^{-6}	2.82×10^{-3}	17.11

Pipe - 4

$$A_3 = 0.38 \times 10^{-3}$$

$$d = 3 \text{ mm}$$

SL. NO	$Q (m^3/s)$	$T_w (kg/m^2)$	du/dy
1	0.3×10^{-5}	936.93×10^{-3}	1131.75
2	0.32×10^{-5}	33.709×10^{-3}	1207.2197
3	0.28×10^{-5}	263.22×10^{-3}	1056.371
4	0.125×10^{-5}	91.45×10^{-3}	471.5702

$$A_4 = 5.3 \times 10^{-3}$$

$$\mu = \frac{(u_1 + u_2 + u_3 + u_4)}{4} = \frac{0.9025 \times 10^{-3}}{4} \text{ Pa-s}$$

$$= 1.77 \times 10^{-3}$$

→ Precaution →

- (1) for the experiment to work, flow should be laminar. Re < 2100
- (2) we need to graduate the flow of water very carefully

→ Discussion :-

- (1) The results are presented here as well shear stress against the apparent shear rate. It is seen that flow curve depends on both the tube length & diameter reduction in measured viscosity with a decrease in the tube diameter is manifestation of the wall effect.
- (2) Wall effect can be corrected if experimental data are taken with at least three tube diameters.
- (3) To obtain the true shear-stress rate curve from viscometry allowances must be made for the influence of wall effects & end effect in the observed results.
- (4) Take sufficiently large to ratio for pipes so that entrance effect can be neglected.



Calibration of a Venturiometer

Aim → 1 → To prepare a venturiometer calibration chart for the Venturiometer ($Q \propto \Delta h$).

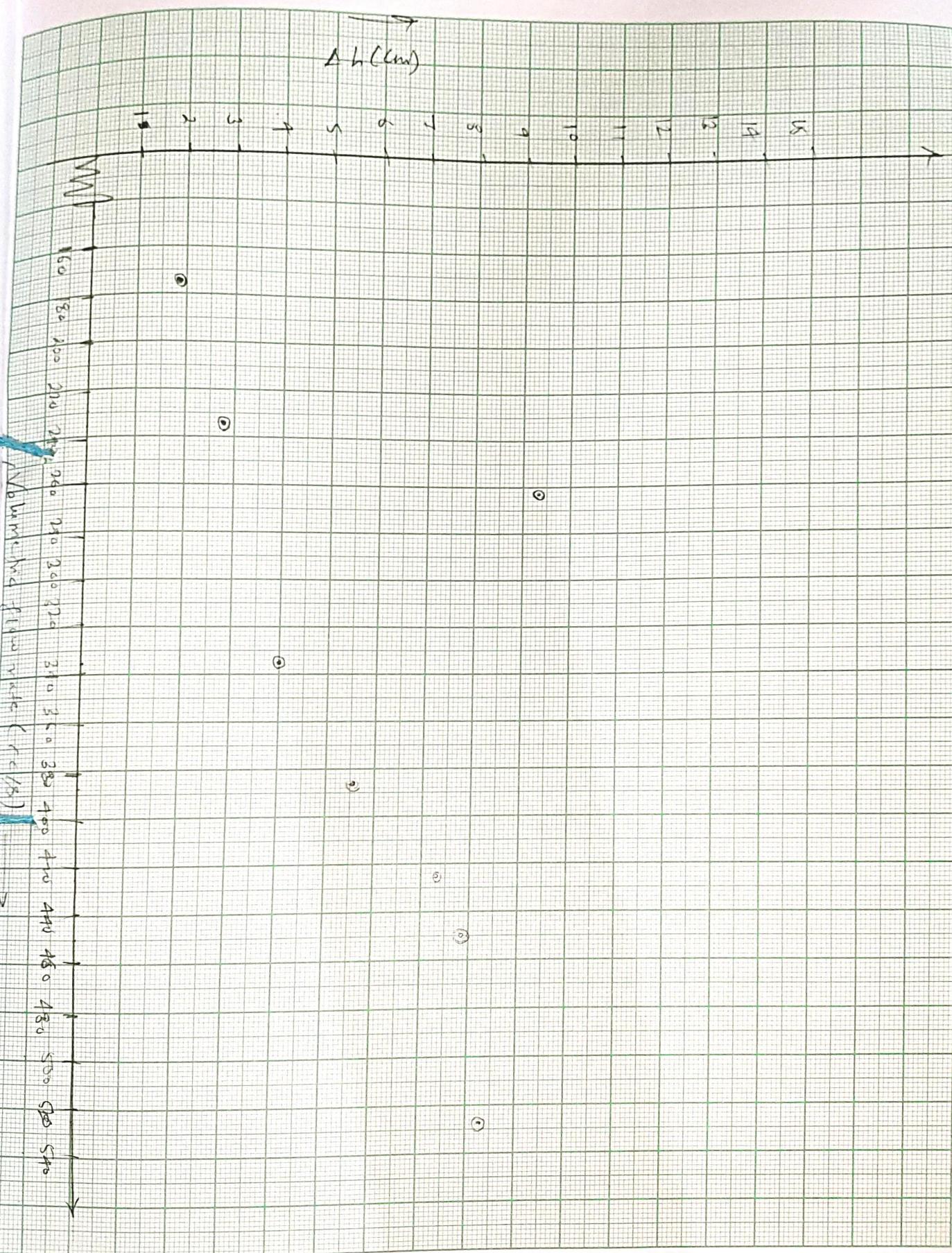
2 → To make a plot showing variation of coefficient of discharge of the Venturiometer & Reynolds number (C_v vs N_{Re}) based on Venturi-throat.

→ Theory :- A Venturiometer consists of a converging & diverging section connected to the main pipeline. As the velocity increases gradually in the upstream convergent section, the pressure of the fluid keeps decreasing. The velocity then gradually decreases in the divergent section & the original pressure is largely recovered.

Venturiometer works on the principle of Bernoulli's principle.

$$Q = C_v \times a \sqrt{\frac{2g(P_1 - P_2)}{d(1 - \beta^4)}}$$

$$C_v = \frac{Q}{a} \times \sqrt{\frac{(1 - \beta^4)d}{2g(P_1 - P_2)}} = \frac{Qk}{\sqrt{\Delta p}}$$



Where

$K = \text{Constant}$

$a = \text{area of throat (cm}^2\text{)}$

$$\rightarrow \beta = \frac{\text{diameter of throat}}{\text{diameter of pipe}}$$

$\rightarrow C_v = \text{Coff of discharge}$

$\rightarrow P = \text{pressure g/cm}^2$

$\rightarrow h = \text{manometer liquid head difference (cm)}$

$\rightarrow Q = \text{Volumetric flow rate of fluid (cc/s)}$

$\rightarrow d_{\text{fluid}} = \text{density of } \xrightarrow{\text{flowing}} \text{fluid & manometric fluid (g/cc)}$

$\rightarrow w = \text{mass flow rate of the liquid.}$

\rightarrow Apparatus required :-

1 \rightarrow Venturimeter

2 \rightarrow Stopwatch

3 \rightarrow Bucket

4 \rightarrow Weighing Balance

5 \rightarrow Manometer

\rightarrow procedure:- Measure the flowrate & write down the manometer readings.

\rightarrow observation & results:-

Pipe size = 2 inch

Diameter of the throat = 1 inch = 2.54 cm

Area of throat = 5.06 cm^2

Mass of empty bucket = 2750 g

Paynt d₅ nu -

W W W W W
30 100 120 140 160 180 200 220 240 260 280

0.3
0.4

0.4
0.5

0.5
0.6

0.6
0.7

0.7
0.8

0.8
0.9

0.9
1.0

1.0
1.1

1.1
1.2

1.2
1.3

1.3
1.4

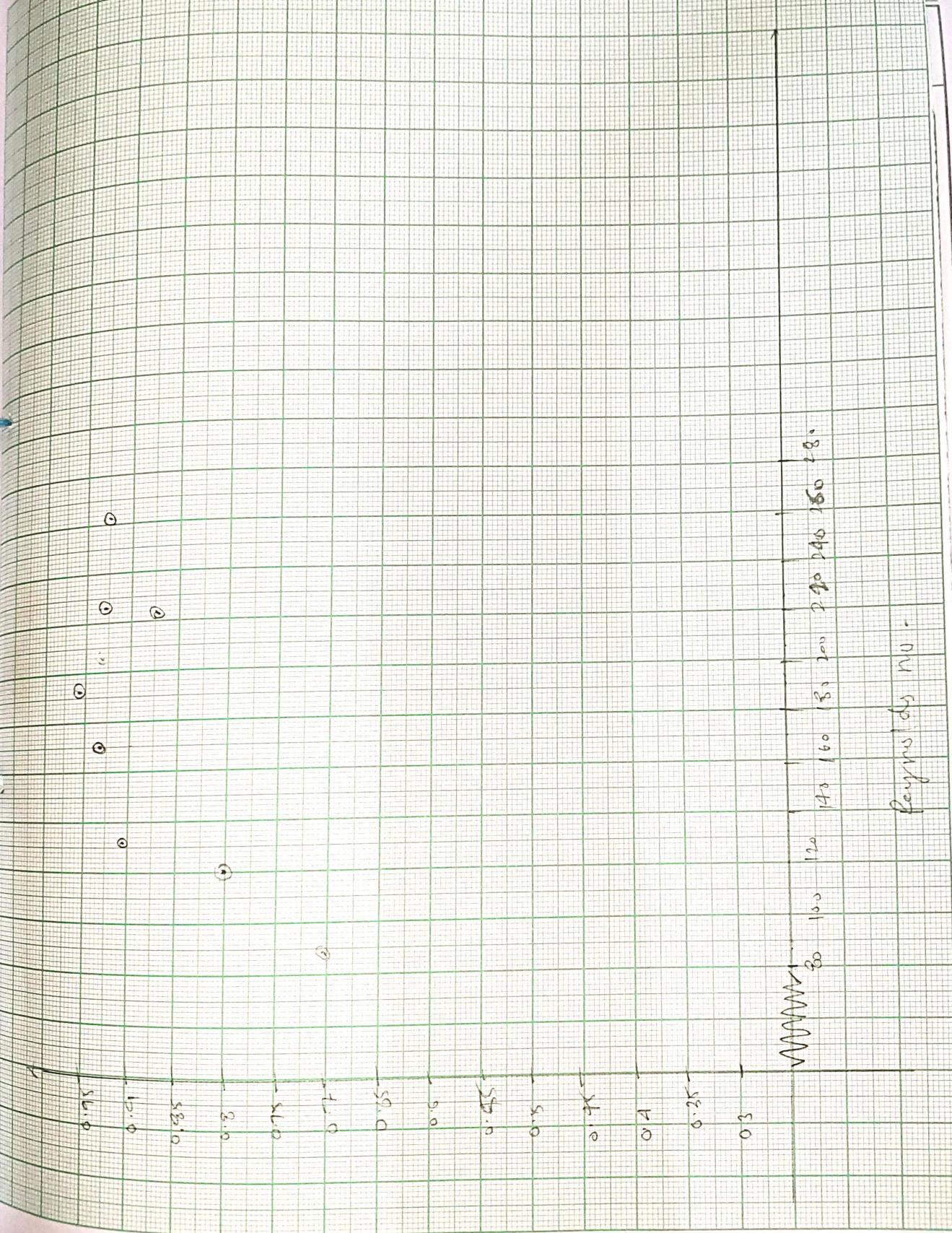
1.4
1.5

1.5
1.6

1.6
1.7

1.7
1.8

1.8
1.9



RUN NO	Amount of liquid (kg)	Time(s)	Manometer readings			q (cc/s)	NRe	Cv
			LHS	RHS	Δh			
1	1750	10	18.5	16.4	1.9	175	87.72	0.707
2	2375	10	18.8	16.1	2.7	237.5	119.05	0.804
3	3375	10	19.1	15.4	4	337.5	169.18	0.934
4	3875	10	20.1	14.6	5.5	387.5	194.244	0.958
5	2625	10	22.2	12.9	9.3	262.5	131.584	0.920
6	2250	5	21.4	13.5	7.9	450	225.57	0.935
7	2125	5	20.7	14.3	6.4	425	213.04	0.891
8	2625	5	21.6	13.3	8.3	525	263.169	0.932
9	2750	5	22.8	12	10.8	550	275.20	
10	3250	5	23.9	11.3	12.6	650	235.81	

Calculation :-

$$q = \frac{V}{t} = \frac{m/d}{t}$$

$$\beta = \frac{d_{throat}}{d_{pipe}} = \frac{1}{2}$$

$$q = C_v \times A \sqrt{\frac{2g(\rho_1 - \rho_2)}{d(1 - \beta^4)}}$$

$$\Delta P = \rho_1 - \rho_2 = \Delta h (d_m - d) g$$

$$d_m (density) = 1.6 g/cc$$

$$d = 1 g/cc$$

$$d_{throat} = 1 \text{ inch}$$

~~area of throat = 5.087 cm²~~

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$$d_{throat} = 1 \text{ inch}$$

$$d_{pipe} = 2 \text{ inch}$$

Area of throat = $\frac{\pi}{4} (2.54)^2 = 5.067 \text{ cm}^2$

$$C_v = \frac{q}{a} \sqrt{\frac{(1 - \beta^2)d}{2g(p_1 - p_2)}} = q K / \sqrt{\Delta P}$$

~~$\rho_1 - \rho_2 = \Delta h (dm - d) \times g$~~

$$\rho_1 - \rho_2 = 1.9 \times (0.6) \times 9.8$$

$$C_v = \frac{175}{5.067} \sqrt{\frac{(1 - \frac{1}{16}) \times 1}{2 \times 9.81 \times 1.9 \times 0.6}} = 34.537 \times 1 = 0.707$$

$$f_e = \frac{f v d}{\mu} = \frac{f q}{a \times \mu} \frac{d}{\mu} = \frac{\frac{f^2 d}{4} \frac{d}{\mu}}{\pi d^2 \mu} \quad \text{①} = \frac{q \times 4}{\pi d \mu}$$

$$= \frac{175 \times 4}{3.14 \times 2.54} = 87.72$$

Discussion:

- A Venturiometer is a device used to measure the flow rate of fluid in pipe. In a ~~at~~ calibration experiment, the Venturiometer is first installed in the pipe, and the fluid flow rate is measured using a calibrated flow meter.
- Calibration process should be repeated regularly to ensure that the Venturiometer remains accurate over time. Additionally, the calibration should be done with the same fluid and at similar temperature and pressure as in the operating condition.
- The experiment calibration ensures the accuracy of the flow measurement. The process involves measuring and fluid flow rate using a calibrated flow meter and comparing it to the reading obtained from the Venturiometer at various flow rates.



P. Anup Singh
31/01/23

Calibration of Rotameter

- 1 → Objective (i) To know the different part of Rotameter
(ii) To calibrate the rotameter by plotting Rotameter reading vs actual flow rate of liquid.
(iii) To plot rotameter vs percentage error.

→ Theory :-

Rotameter is a Variable area meter in which pressure drop is nearly constant. The annular area between the float & tapered tube changes with flow rate of liquid for a given flow rate the flow attains an equilibrium position which the weight of float is balanced by buoyant & dry force.

$$f_{Dg} = g(m_{float} - m_{float}(\rho_{liq}/\rho_{float})) = m_{float}g(1-\rho_{liq}/\rho_{float})$$

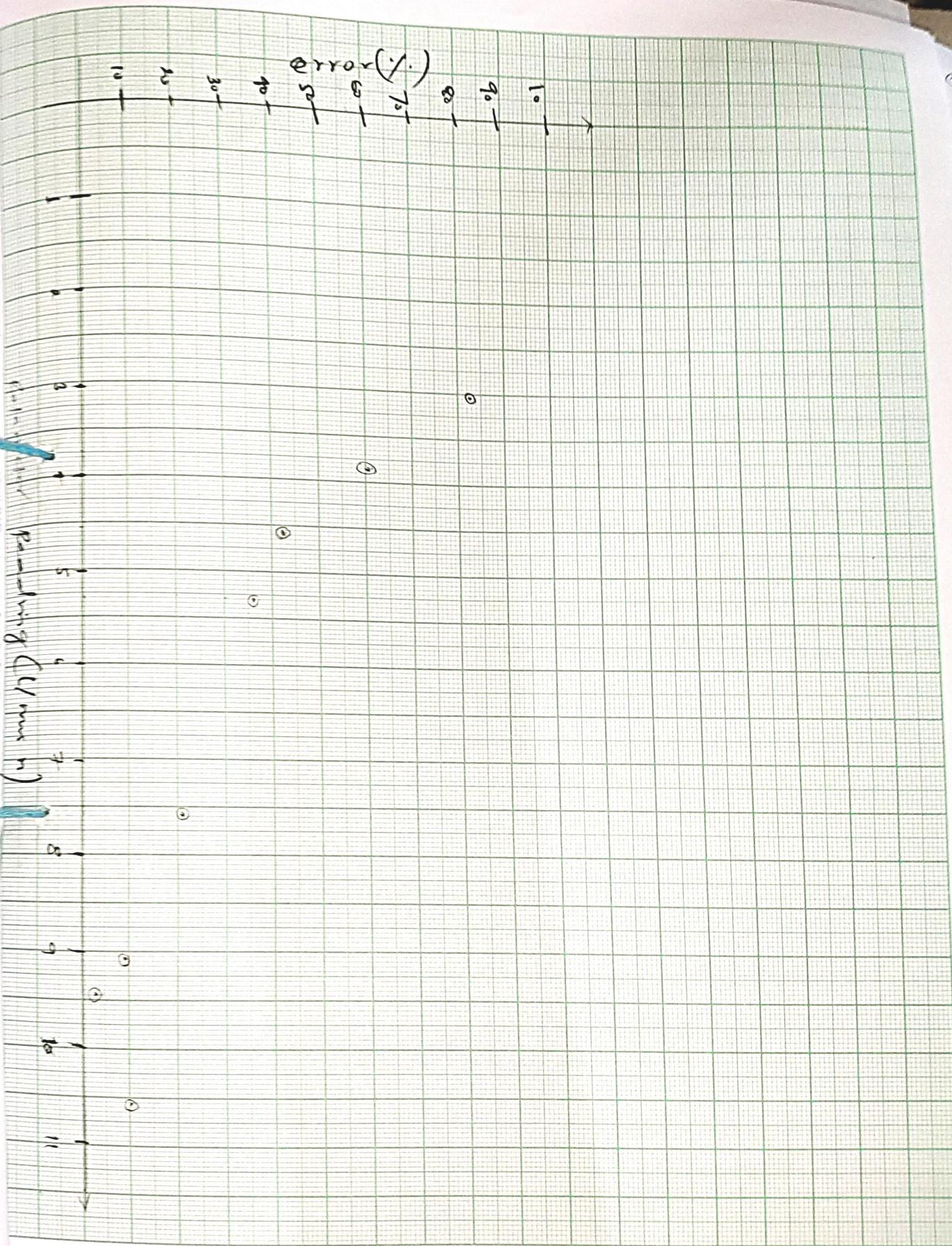
where,

f_D = drag force

m_{float} = mass of the float

ρ_{liq} = density of liquid

ρ_{float} = density of float



→ procedure:-

1 → Measure the flow rate of ~~the~~ liquid & note the rotameter reading.

2 → Vary flow rate to cover entire range of rotameter.

→ observation & results:-

Density of the liquid =

Mass of empty bucket = ~~200~~

RUN. NO	Weight of liquid (kg)	Time (s)	flow rate (L/min)	Rotameter reading (cm)	V. due per min
1	250	30	0.5	0.8 = 3.02	82.62%
2	750	30	1.5	1 = 3.782	60.36%
3	875	20	2.625	1.2 = 4.342	42.2%
4	1125	20	3.375	1.4 = 5.299 7.54	36.3%
5	1000	10	6	2 = 9.08	20.7%
6	1375	10	8.25	2.4 = 9.084	9.25%
7	1375	10		2.5	
8	1625	10	9.75	2.8 = 9.46	2.9%
9	2000	10	12	3 = 10.599	11.16%
10	1625	20		3.8	

Calculation :- Run 1

$$\bar{Q} = \frac{0.25}{30} = 0.5 \text{ L/min}$$

$$1 \text{ gallon} = 3.785 \text{ L}$$

Scale

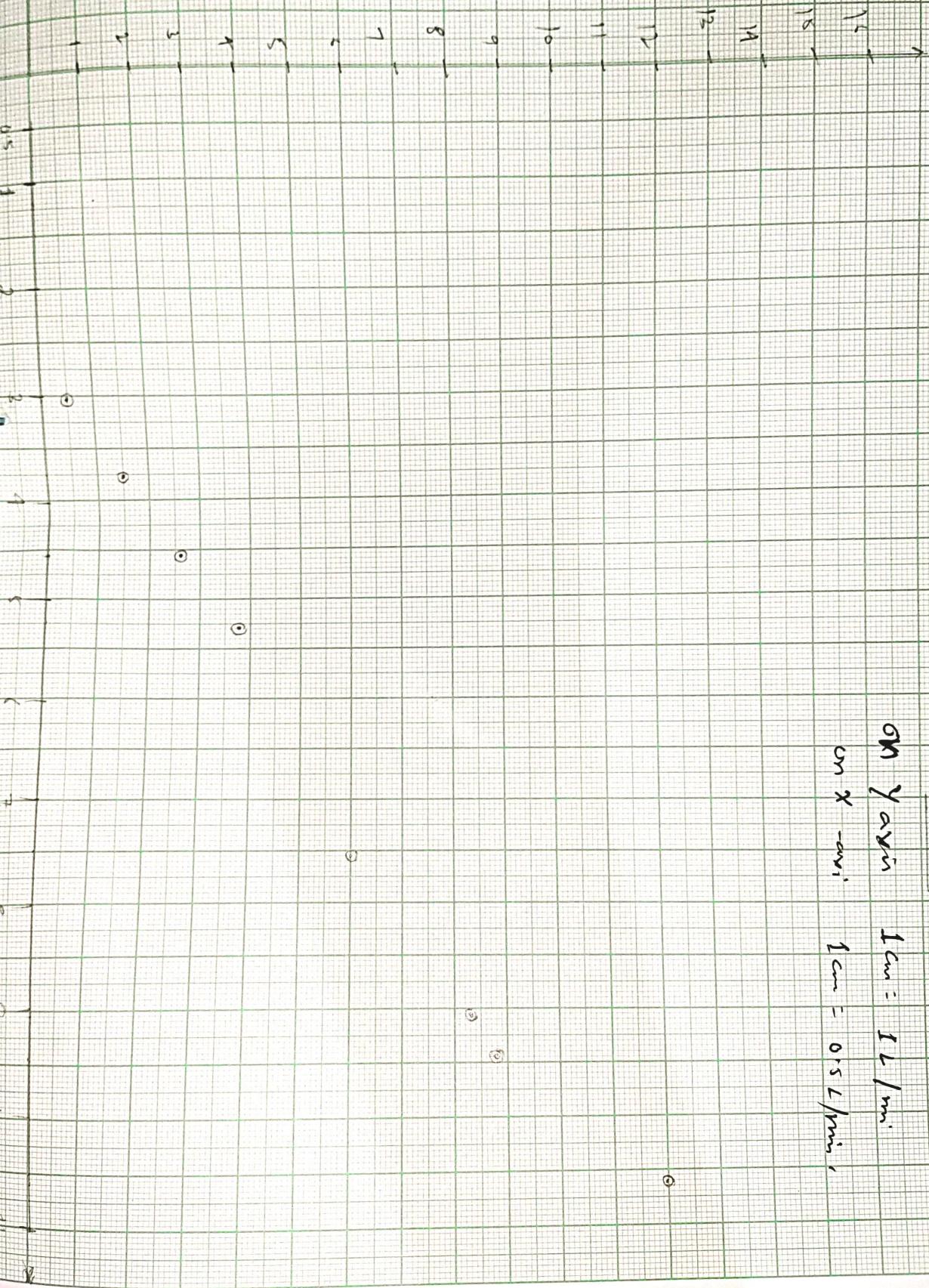
on Y-axis

1 cm = 1 L/min

on X-axis
1 cm = 0.5 L/min

flow rate (L/min)

Flow meter reading (L/min)



Q = 0.8 gallon = 3.02 L, Rotameter reading = 3.02 l/min

$$\text{percentage deviation} = \frac{3.02 - 0.5}{3.02} \times 100 \\ = 82.62\%.$$

Discussion 8 :-

→ A rotameter has 3 basic components

(i) A tapering tube

(ii) A float inside the tapering tube

(iii) Measurement marking on the tapering tube.

→ Water or any other liquid is inlet at bottom of the rotameter which then flows through the tube and outlet from the top which is collected in a bucket and measured.

→ Rotameter has less friction, low cost and easy to install and use. Hence, has a great industrial importance.

→ It is designed in accordance with the basic eqn for Volumetric flow rate.

$$Q = KA\sqrt{gh}$$

→ There are certain factors that affect the measurement of a flow rate → fluid temperature, pressure, specific gravity.

Precautions :-

→ Converts the unit before Calculations.

→ wait for the float to settle before taking the reading.

~~P. G. S. J. S. 31/01/23~~

Pitot tube

→ Aim → Calibration of pitot tube & measurement of fluid velocity.

→ Theory → A pitot tube is a simple device meant for measuring the velocity of a fluid at any point. In its simple form, the pitot tube consists of a tube whose lower end is bent at right angles. The device is placed in a moving fluid with lower opening directed in the upstream direction. The liquid level in the pitot tube will depend on the velocity of stream. The point will depend on the velocity of stream. The pitot tube is meant for measuring the velocity at any point in a stream of liquid flowing in a pipeline. Consider the two points A & B. The point B is just at the inlet to the pitot tube while the point A is at the same level as that of B but at some distance from B & outside the pitot tube.

Let u be the velocity of A,
pressure head at A, $\frac{P_A}{\rho g} = H_1$

at B, there is no velocity & the pressure head at B.

$$= \frac{P_B}{\rho g} = H_2 + \Delta h$$

✓

Sr. No.	Flow rate (lpm)	Position, y(cm)	Manometric reading h(left) h(right)	Δh	Velocity (cm/s)	Vavg	$v\Delta h$
1	20	2.2	26.3				
		3	26	28.8	2.5	88.59120865	0 0
		3.5	25.8	29.4	3.4	103.3142152	
		4.5	26.6	29.5	3.7	107.7758569	
		2.2	25.5	28.6	2	79.2383859	29.2372 1.702938637
2	25	3	25	29.8	4.3	116.1862809	
		3.5	25.5	30.5	5.5	131.4019975	
		4.5	26.8	30	4.5	118.8575788	
		2.2	25	28.5	1.7	73.05418215	36.5465 2
		3	24.5	30.5	5.5	131.4019975	
3	30	3.5	25.3	31	6.5	142.8490317	
		4.5	26	30.3	5	125.2868888	
		2.2	25	29.3	3.3	101.7835496	43.8558 2.252776065
		3	22	30.5	5.5	131.4019975	
		3.5	23.5	33.5	11.5	190.0069745	
4	35	4.5	26	32	8.5	163.3541173	
		2.2	25	29.5	3.5	104.8225317	51.1651 2.692582404

Where, Δh = difference in the two legs of the manometer
 The point B where the velocity has reached zero
 is called stagnation pressure.

Applying Bernoulli's theorem to the point A & B

$$\frac{1}{2} \rho_w V^2 + \rho g H = 0 + \rho g (H + \Delta h)$$

$$\frac{1}{2} \rho_w V^2 = \rho g \Delta h$$

$$V = \sqrt{\frac{2 \rho g \Delta h}{\rho_w}}$$

To take into account of losses in the actual cases
 the Velocity is given by.

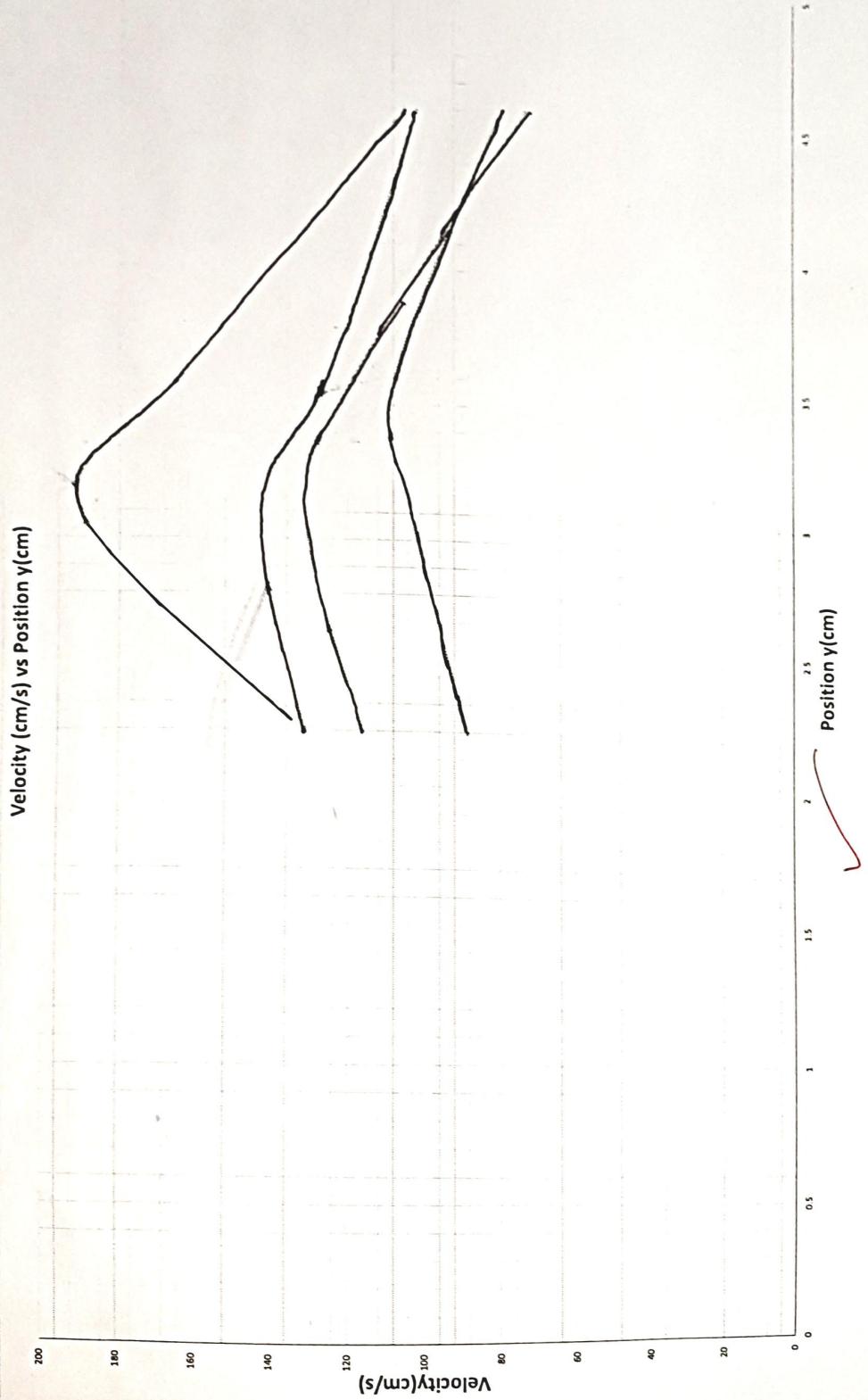
$$V = C_v \sqrt{\frac{2 \rho g \Delta h}{\rho_w}}$$

where, C_v = pitot tube coefficient.

The pitot tube is used to measure the velocity of a liquid
 in a pipe then we must adopt some method to know
 the static pressure head H , for instance, we may use a
 pitot tube & a vertical piezometer tube & measure the
 difference of the liquid level in the two tubes.

In another arrangement the pitot tube & vertical tube
 connected to the pipe may be connected to the U-tube
 containing a heavy liquid in the U-tube is y .

Then, $h = (\rho - \rho_w) y$



where,

$$\frac{s = \text{specific gravity of the heavy liquid in U-tube}}{\text{specific gravity of the liquid flowing in the pipe}}$$

→ procedure :—

- 1 → filled the water in the circulating tank through a water inlet to $\frac{3}{4}$ level.
- 2 → Connected manometer & released air through stopcocks.
- 3 → Start the water pump.
- 4 → Adjust flowrate through Valve (v_1) & closed valve (V_2) a little to set a water flow rate in pitot tube.
- 5 → Took the flow flow rate reading in rotameter & pressure drop in manometer.
- 6 → Repeat the step 3 & 4 for Various flow rates & record the reading in tube below be drawn the liquid in pitot tube of water.
- 7 → Above procedure may also be repeated for different depth of pitot tube.



$V_{avg} \text{ vs } \Delta h$

$$y = 2.6346x + 1.3332$$

• 11.10122048

• 11.10122048

• 11.10122048

• 20.23220142

$V_{avg} \text{ (cm/s)}$

$\Delta h \text{ (cm)}$

Sample Calculations:

$$d = 3.8 \text{ cm}$$

$$\text{area} = \frac{\pi}{4} d^2 = 11.4 \text{ cm}^2$$

$$V_{avg} = \frac{\text{Flow rate}}{\text{Area}}$$

$$V = \sqrt{\frac{2 S c f g (h_2 - h_1)}{\rho_{water}}}$$

$$\frac{f_{CC14}}{\rho_{water}} = 1.6 \quad \text{and} \quad g = 981 \text{ cm}^2/\text{s}$$

when flow rate = 20 LPM and $AH = 2.5$

$$V = \sqrt{\frac{2 \times 1.6 \times 981 \times 2.5}{1}} = 88.58 \text{ cm/s}$$

$$V_{avg} = \frac{\frac{20 \times 10^{-3}}{60}}{11.4 \times 10^{-4}} = 0.292 \text{ m/s}$$

Plotted a graph V_{avg} and T_{dh} and determined the time ~~of~~ and coefficient of Velocity of pitot tube.

$$C_V = \frac{\text{slope}}{\sqrt{2g}} = \frac{2.634 \text{ s}}{\sqrt{2 \times 981 \times 1.6}} = 0.047$$



→ Discussion:

The errors in the values are because:

- (i) The fluid flow is viscous, which is not taken into consideration in our computations.
- (ii) Instrument like pitot tube could get blocked because it is not in use for long time which gives error in readings.
- (iii) Capillary rise due to surface tension in manometer tube gives error in readings.
- (iv) frictional losses are also not taken into account.
- (v) The flow was ~~laminar~~ - which was expected to be laminar may be due to operating at low flow rate.

→ Precautions:-

- (i) Don't fill the tank above full level.
- (ii) Drain the water after using the instrument to avoid caking of algae.
- (iii) Maintain laminar flow.
- (iv) Use only mild detergents to clean the instruments, never use any organic solvent or strong acid or alkalies.
- (v) Ground the instruments properly to avoid electric shock.

Ran
X.01.23

flow through triangular notch ~~weirs~~ weirs

→ objective:-

- To make a Calibration plot (I_{vsh})
- To plot C_d Vs q

→ Theory

Weirs are the area meters to measure flow rate of liquid in open channels. for a sharp crested wire, the following equation gives the fluid flow rate.

$$q_{ac} = \frac{8}{15} C_d \sqrt{2g} (\tan \theta_2) h^{5/2}$$

Where,

C_d = coefficient of discharge

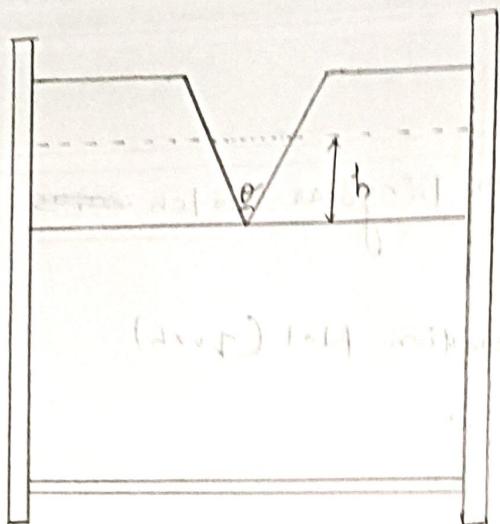
h = height of the liquid level above the wire crest (m)

q_{ac} = actual Volumetric flow rate of liquid (cc/s)

θ = angle of notch in degree

francis equation:

$$I_m = 25.6 (\tan \theta_2)^{0.996} h^{2.47}$$



V-notch or

triangular notch

(down) fall with constant bottom (d)

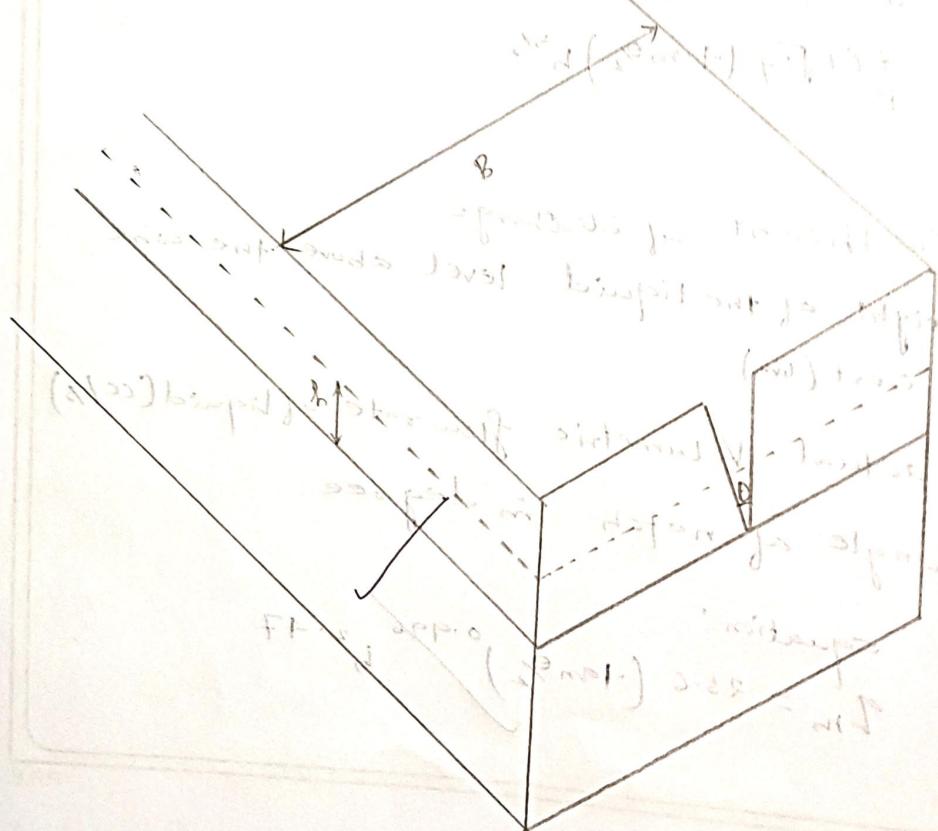
bottom (d)

bottom

~~water level decreases after entering the notch area~~

~~Water level increases after leaving the notch area~~

~~Bottom profile remains constant throughout the channel length~~



bottom

Apparatus required:-

open channel with V-notch, stopwatch, bucket, weighing balance.

Procedure :-

- 1 → find out angle by measuring height & breath of the notch.
- 2 → Adjusted the pointer for zero flow rate & note down the readings.
- 3 → Adjust the level of the liquid & measure h & found the actual discharge rate.
- 4 → repeat it a few times.

Observation :-

Height of V-notch = 15.132 cm ,

Breath of V-notch = 15.494 cm .

∴ Angle of notch in degrees = 59.22° .

Also weight of bucket = 1.8 kg .

Run No.	Water Collected (Kg)	Time (s)	h (cm)	q (cc/s)	Cd	qth (cc/s)	% Variation
1	0.5	30	19.1	16.66666667	0.8752386674	18.97041787	0.1214391383
2	2	30	18.4	66.66666667	1.109827828	59.02290949	-0.1295049201
3	3	20	17.7	150	1.139957764	128.0806105	-0.1711374531
4	3.5	10	16.4	350	0.9652446394	348.6814143	-0.003781634479
5	4.5	10	16.1	450	1.031145995	418.7212163	-0.07470073754
6	5	10	15.7	500	0.9126542841	524.2169555	0.04619643684
7	6	10	15.3	600	0.889113309	644.1027157	0.06847155688
8	7.5	10	15	750	0.9607324527	743.8076102	-0.008325257396
9	4	5	14.7	800	0.8929986269	852.1649084	0.06121456998
10	4.5	5	14.5	900	0.9202448532	929.3223109	0.03155235866

Sample Calculation

$$\text{Dead height} = 20.3 \text{ cm}$$

$$\text{water collected} = 3.5 \text{ kg}$$

$$\text{time} = 108$$

$$h = 16.4$$

$$\Delta h = 3.9$$

$$q = V/t = \frac{m/s}{t} = \frac{350}{108} = 3.26 \text{ cc/s}$$

$$\text{Notch angle } (\theta) = 54.22^\circ$$

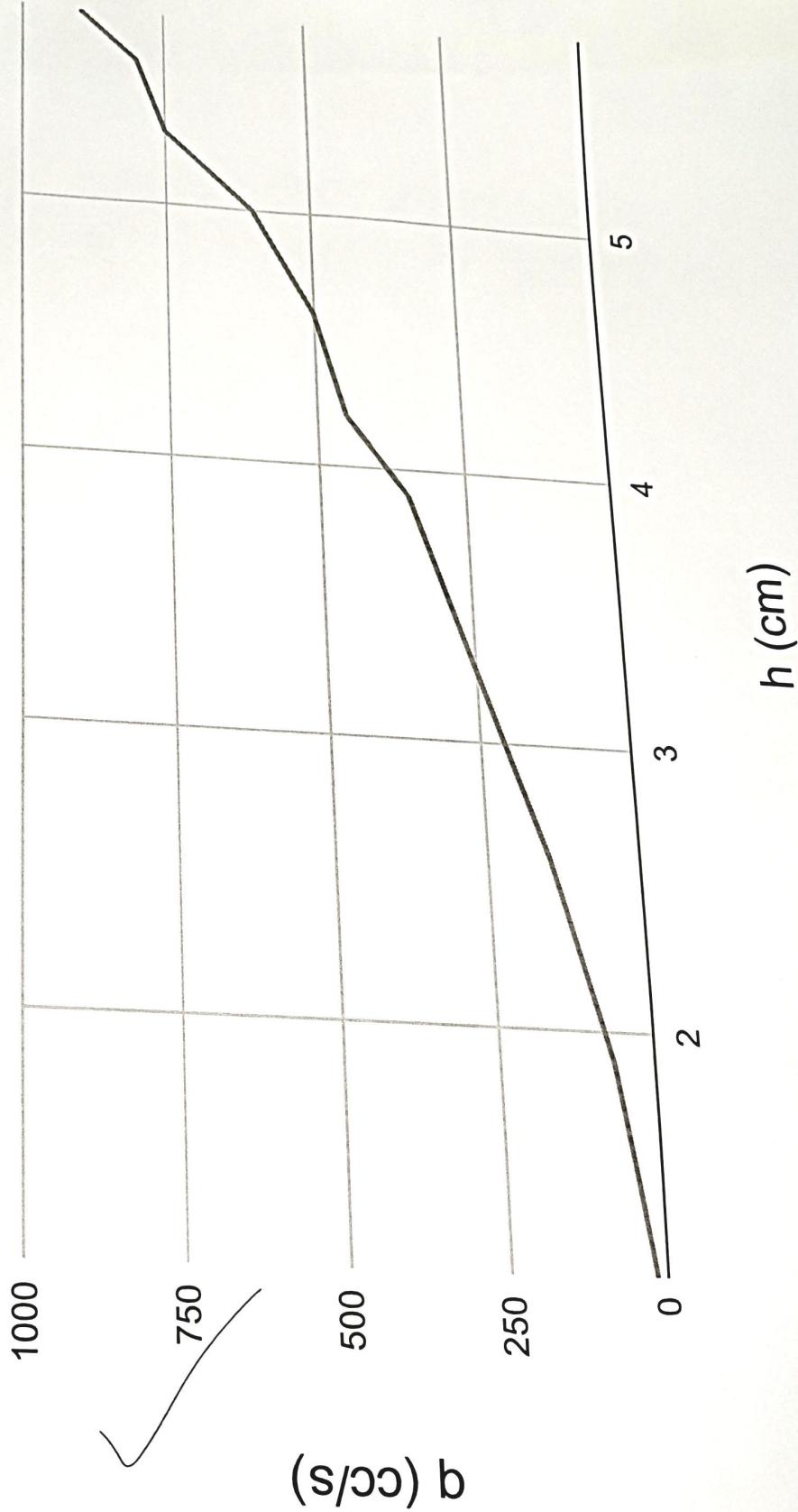
$$\begin{aligned} q^{\text{th}} &= 23.6 \left(\tan \theta_2 \right)^{0.996} h^{2.47} \\ &= 23.6 (0.512)^{0.996} (3.9)^{2.47} \cancel{3.26 \text{ cc/s}} \\ &= 348.68 \text{ cc/s} \end{aligned}$$

$$q_{\text{act}} = \frac{g}{15} \times C_d \times \sqrt{2g} \tan(\theta_2) h^{5/2}$$

$$350 = \frac{g}{15} \times C_d \times \sqrt{2 \times 9.81} \tan(\theta_2) (3.9)^{5/2}$$

$$C_d = 0.96$$

q vs h



Cd vs q

1.25

1.00

0.75

0.50

0.25

Cd

800
600
400
200
0.00

q (cc/s)





Discussion

- (i) Some water gets collected on the triangular notch which might give the wrong flow rate of water.
- (ii) During the first 3 trials the η variation becomes low & steady, then suddenly increases for last run so we can say that at some optimum flow rate, η . Variation is low beyond this flow rate is random.
- (iii) There is a bend in the scale that measures the height of water which gives an error.
- (iv) Random error of stopwatch is also counted.

Precautions :-

- (i) Don't start the pump if supply is less than 300V.
- (ii) Don't forget to give electric earth & neutral wire connection correctly, frequently test one in three months grease Visual

9.5
10
Chiranjeevi
14/12/2023