

# INDIAN INSTITUTE OF TECHNOLOGY KHARAGPUR

## End-Spring Semester Examination 2022-23

Date of Examination: 25-04-2023 Session: (FN/AN) AN. Duration: 3 hrs.

Full Marks: 50

Subject No.: CH21204

Subject: Heat Transfer

Department/Center/School: Chemical Engineering

Specific charts, graph paper, log book etc., required: NIL

Special Instructions (if any):

• All questions are compulsory.

Assume any missing data, if necessary, with proper justification.

• Answer each part in one place.

• Mention the part number you are answering.

• No queries will be entertained during the examination.

#### PART - I

1. For fully developed laminar flow in a circular tube subjected to constant surface heat flux, derive the expression for fluid temperature profile in the tube and the Nusselt number.

(6+4=10)

- 2. Water, flowing at a rate of 0.5 kg/s through a 10 m long pipe with an inside diameter of 2 cm, is being heated with uniform wall heat flux at a rate of  $5 \times 10^4$  W/m². Assuming fully developed flow, calculate:
  - a. the pressure drop per unit pipe length in kPa/m
  - b. the heat transfer coefficient based on the Colburn analogy in W/m<sup>2</sup>K
  - c. the heat transfer coefficient based on the Dittus-Boelter correlation in W/m<sup>2</sup>K
  - d. the difference between the wall temperature and the local mean water temperature
  - e. the temperature enhancement experienced by the mean water temperature in the longitudinal direction from the inlet to the outlet

Data given: Water properties at 20°C

k = 0.59 W/(m.K), Pr = 7.07,  $c_p = 4.2 \text{ kJ/(kg.K)}$ ,  $\rho = 0.998 \text{ g/cm}^3$ , v = 1 cSt

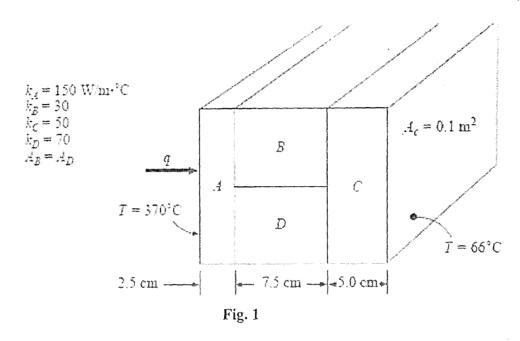
(2+2+2+2+2=10)

3. Draw the boiling curve and identify the burnout point on the curve. Explain how burnout is caused. Why is the burnout point avoided in the design of boilers?

### PART - II

1. It is required to calculate the heat flux through the composite wall shown in Fig. 1. Discuss if the assumption of one-dimensional heat flow is justified for the calculation.

(2)



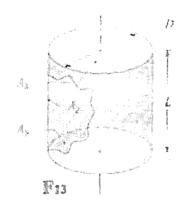
- 2. Consider a shielding wall of thickness L for a nuclear reactor. The wall receives gamma ray flux such that heat is generated within the wall according to the relation  $\dot{q} = \dot{q}_0 e^{-ar}$  where  $\dot{q}_0$  is the heat generation at the inner face of wall exposed to the gamma -ray flux and a is a constant. The constant heat generation maintains the inner surface at a constant temperature Ti while the outer surface is adiabatic
  - (i) Represent the problem with a proper sketch containing all details and nomenclatures. (2)
  - (ii) Starting from the generalized heat conduction equation for constant thermal conductivity in rectangular coordinates

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} + \frac{\dot{q}}{k} = \frac{1}{\alpha} \frac{\partial T}{\partial t}$$

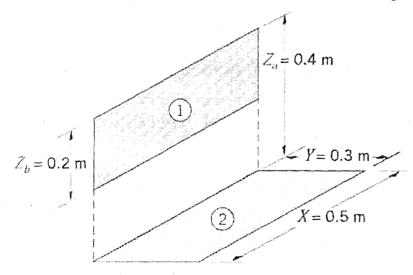
- (a) derive an expression (using the specified nomenclatures in (i)) to obtain the temperature profile in the wall
- (b) Mathematically state the boundary conditions for obtaining the temperature profile. (The complete solution of the profile is not required). (3)
- 3. It is required to cool a 3.0 cm (side) steel cube (specific heat capacity = 460 J/kg ( $^{0}$ C), thermal conductivity= 40 W/m  $^{0}$ C, density = 7800kg/m<sup>3</sup>) from a temperature of 450 $^{0}$ C to 150  $^{0}$ C. The cooling can be either by (i) exposing the cube to air at room temperature of 40 $^{0}$ C (h= 7 W/m<sup>2</sup>  $^{0}$ C) or (ii) submerging into boiling water where h= 10000 W/m<sup>2</sup>  $^{0}$ C.

- (i) With proper justification, state under which condition we can use lumped capacity method for estimating the rate of cooling

  (4)
- (ii) Sketch the transient temperature profile for the two cases
- (2) ed capacity method
- (iii) Calculate the time required for cooling under the condition where lumped capacity method is applicable. (4)
- 4. Iron plate appears grey when cold and bright yellow when hot. Why? (2)
- 5. Calculate the view factors specified in each problem for the following geometries. The graphs below may be referred for calculations. (3+3)
  - (a)  $F_{13}$  for right circular cylinder of diameter D and length L where L=1.5D

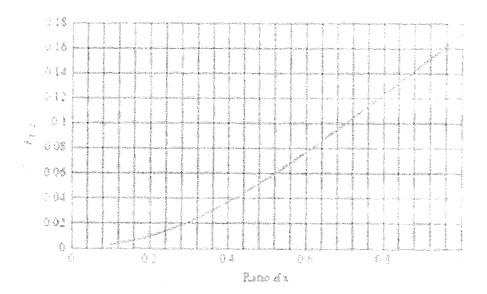


(c)  $F_{12}$  for surfaces 1 and 2 which are perpendicular but do not share a common edge



### Radiation Shape Factor for radiation between

### (a) parallel equal coaxial disks



## (b) perpendicular rectangles with a common base

