

THE CONJUGATE UNSCENTED TRANSFORM

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TO EVALUATE THE INTEGRAL

$$E[f(x)] = \int f(x)N(x, \mu | P)dx$$

An Experimental Investigation

MOTIVATION

- We would like to compute Multi-Dimensional Expectation Integrals.
- Analytical expressions for these multi-dimension integrals exist only for linear systems and only for few moments
- the well celebrated Kalman filter provides the analytical expressions for mean and covariance of linear system subject to Gaussian white noise and Gaussian initial condition errors
- one often do not have direct analytical solution for these integrals and have to approximate integral values by making use of computational methods.
- Monte Carlo (MC) methods, Gaussian Quadrature Rule, Unscented Transformation (UT) and Cubature methods.

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MOTIVATION

- These methods basically differ from each other in the generation of these specific points
- MC methods involves random samples from the specified pdf while Gaussian quadrature scheme involves deterministic points
- Both deterministic Gaussian quadrature and MC methods are very popular but both methods require extensive computational resources and effort
- For one-dimensional integrals, one needs m quadrature points according to the Gaussian quadrature scheme to reproduce the expectation integrals involving $2m - 1$ degree polynomial functions.
- for a generic N -dimensional system, one needs to take the tensor product of 1–dimensional m quadrature points and hence one would require a total of m^N quadrature points (also known as cubature points)

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- Even for a moderate dimension system involving 6 random variables, the number of points required to evaluate the expectation integral with only 5 points along each direction is $5^6 = 15,625$
- But fortunately the Gaussian quadrature rule is *not minimal* for $N \geq 2$ and there exists cubature rules with reduced number of points
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MOTIVATION - NONLINEAR FILTERING: FROM THE BASICS

Consider a discrete dynamic system with noise

$$x_{k+1} = f(x_k, k) + v_k$$

The PDF of this dynamic system propagates according to the **Chapman Kolmogorov Equation.**

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- $P(x_k)$ in the CKE need not be gaussian at all times even though the initial condition was gaussian.
- It would be gaussian at all time only when system is linear and the noise is also gaussian. In this case it is very easy to solve this equation analytically.
- Incase the the system in nonlinear and noise is gaussian, the CKE would be

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EXTENDED KALMAN FILTER

- $P(x_k)$ is not always gaussian and there is no analytical solution to this equation.
- Hence the EKF emerged that can provide an **analytical solution** to this CKE by considering the following **two approximations**
- $P(x_k)$ is replaced by an equivalent gaussian PDF that has the same first two moments as the original PDF $P(x_k)$.
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- The EKF works well for systems in which the linearized dynamics is a good approximation to the nonlinear system-
Higher order terms in Taylor series are negligible.
- If the nonlinearity is too strong the EKF would diverge.
- Above that during the linearization process the computation of the jacobian is **computationally expensive**.
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Propagation of mean

$$\mu_{k+1} = f(\mu_k)$$

Propagation of Covariance

$$P_{k+1} = AP_kA^T + Q_k$$

Where A is the jacobian of the system.

$$A = \frac{\partial f}{\partial x}|_{\mu_k}$$

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LINEAR REGRESSION KALMAN FILTER

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- Firstly sample points are chosen about the current mean at time k such that the mean of the samples and covariance of the samples match the current mean and current covariance.

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- Firstly sample points are chosen about the current mean at time k such that the mean of the samples and covariance of the samples **match** the current mean and current covariance.

- Each point is propagated using the **nonlinear dynamics** of the system to time step $k + 1$.
- Now between the current sample points at time k and the corresponding propagated points at time $k + 1$ a **linear model is fit** which gives rise to the linearized dynamics of the system at time k .
- Now this linearized dynamics is used to compute the mean and covariance at time step $k + 1$.

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The sample points at time k are chosen such that

$$\mu_k = \frac{1}{n} \sum_{i=1}^N X^i$$
$$P_k = \frac{1}{n} \sum_{i=1}^N (X^i - \mu_k)(X^i - \mu_k)^T$$

And now each sample point is individually propagated using nonlinear dynamics

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Now trying to fit a linear model between the points (Y^i, X^i)

$$Y = AX + B$$

This is standard linear fit procedure by minimizing the least square error

$$\begin{aligned}e_i &= Y^i - AX^i - B \\E &= (e_i)^T (e_i)\end{aligned}$$

The mean and covariance at time $k+1$ can be found from the Kalman filter propagation equations

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THE UNSCENTED KALMAN FILTER-UKF

- The UKF works in the same ways as the LRKF but the samples are chosen in a **determined** way such that they always match the mean and covariance or higher moments at the current step.
- The points are propagated using the **nonlinear dynamics**. The mean and covariance at time step $k + 1$ are calculated from these propagated points.
- The **first approximation** the UKF does to the CKE is that it replaces the current state PDF with a gaussian PDF with same first two moments.

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One could look at the UKF in the following perspective, starting from CKE

$$P(x_{k+1}) = \int N(x_{k+1}|x_k)P(x_k)dx_k$$

Replacing the state PDF with gaussian pdf with equivalent mean μ_k and covariance P_k .

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Calculating the mean of $P(x_{k+1})$ by integrating on both side wrt x_{k+1} .

$$\begin{aligned}\mu_{k+1} &= \int \int N(x_{k+1} - f(x_k)|Q_k)dx_{k+1}N(x_k)dx_k \\ &= \int f(x_k)N(x_k)dx_k\end{aligned}$$

The covariance can be calculated from the second raw moment

$$\begin{aligned} E[x_{k+1}x_{k+1}^T] &= \int \int x_{k+1}x_{k+1}^T N(x_{k+1} - f(x_k) | Q_k) dx_{k+1} N(x_k) dx_k \\ &= \int (f(x_k)f(x_k)^T + Q_k) N(x_k) dx_k \end{aligned}$$

By parallel axis theorem for moments the covariance is calculated as

$$P_k = E[x_{k+1}x_{k+1}^T] - \mu_{k+1}\mu_{k+1}^T$$

- Thus by evaluating two integrals we get the mean and covariance.
- The second raw moment and the mean need to be evaluated accurate enough or else the parallel axis theorem for moments might render the **covariance to be positive semi definite**.

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THE CONJUGATE UNSCENTED TRANSFORM- CUT

We try to propose a **new method of Gaussian Cubature** to evaluate the integrals and hence may be a potential application as a **new filter**. Later we show that the UKF and CKF are inline with the present construction. Basic Philosophy of CUT:

- The basic philosophy in this analysis is "**To evaluate the integral involving gaussian weight function with as few points as possible**".
- Any Gaussian Quadrature rule has to capture the moments of the continuous PDF
- For example consider the Gauss-Hermite quadrature, as we increase the number of quadrature points more moments are captured and hence higher degree polynomials can be integrated.

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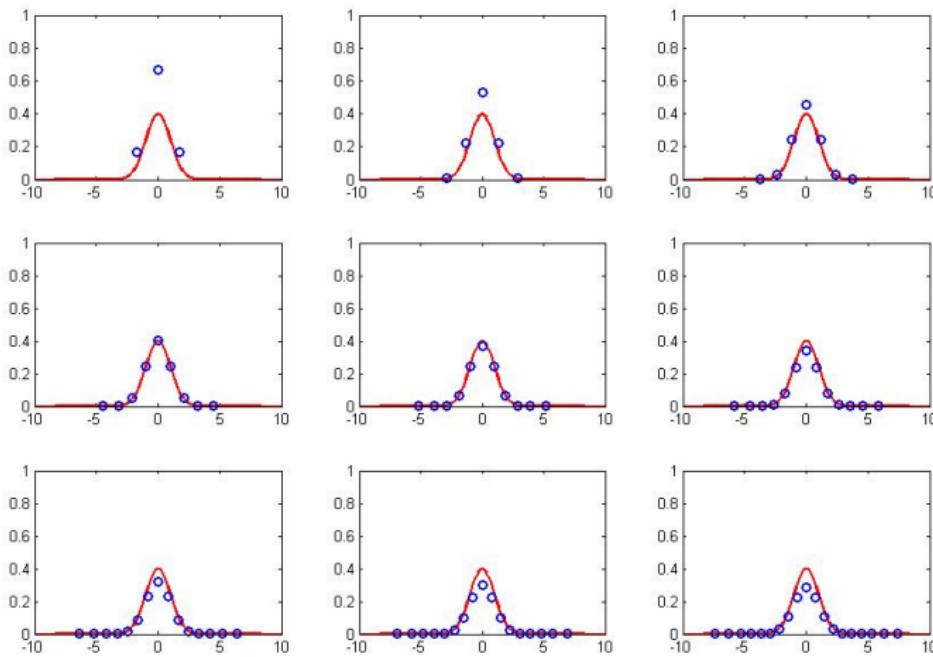


FIGURE: Guass hermite quadrature for 1D

- In general for a N-Dimensional system, to integrate a polynomial of degree $2m + 1$ we need a total of $(m + 1)^N$ quadrature points.
- This is a **very big number** for higher dimensional system and **this is the basis of our motivation to develop a method with reduced number of points.**
- Ideally one would like to capture all the **infinite** moments of the PDF.
- In practice this is difficult to achieve or might be computationally expensive. Thus often only the lower order moments are captured. This highly limits the type of functions that can be integrated with good numerical accuracy.

GAUSS HERMITE PRODUCT RULE

The 1D Gauss Hermite rule can be extended to any dimension for an i.i.d set of random variable $(x_1, x_2, \dots x_N)^T$.

$$E[f(x_1, x_2, \dots x_N)]$$

$$\begin{aligned} &= \int \int \dots \int f(x_1, x_2, \dots x_N) N(x_1, x_2, \dots x_N, 0|I) dx_1 dx_2 \dots dx_N \\ &= \int \int \dots [\int f(x_1, x_2, \dots x_N) N(x_1, 0|1) dx_1] N(x_2, 0|1) dx_2 N(x_3, 0|1) \\ &\quad \dots N(x_N, 0|1) dx_N \end{aligned}$$

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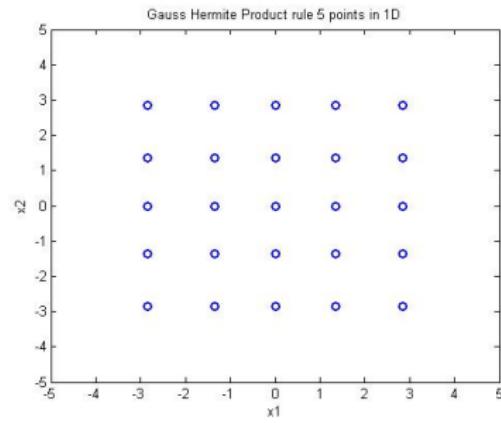
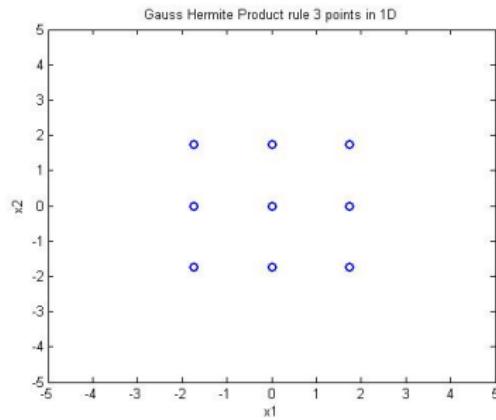


FIGURE: Guass hermite product rule for 2D

TRANSFORMATION OF A NORMAL PDF WITH ARBITRARY MEAN AND COVARIANCE INTO A NORMAL PDF WITH ZERO MEAN AND IDENTITY COVARIANCE

- Any jointly distributed Normal PDF can be transformed into a Gaussian PDF of zero mean and identity covariance of same dimension.
- This way one could find the cubature points in the i.i.d space and then transform each point into the original jointly distributed space.

$$\begin{aligned}(x - \mu)^T P^{-1} (x - \mu) &= (x - \mu)^T U^T \Sigma U (x - \mu) \\ &= (x - \mu)^T U^T \sqrt{\Sigma} \sqrt{\Sigma} U (x - \mu)\end{aligned}$$

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$$\begin{aligned}y &= \sqrt{\Sigma} U (x - \mu) \\ (x - \mu)^T P^{-1} (x - \mu) &= y^T y\end{aligned}$$

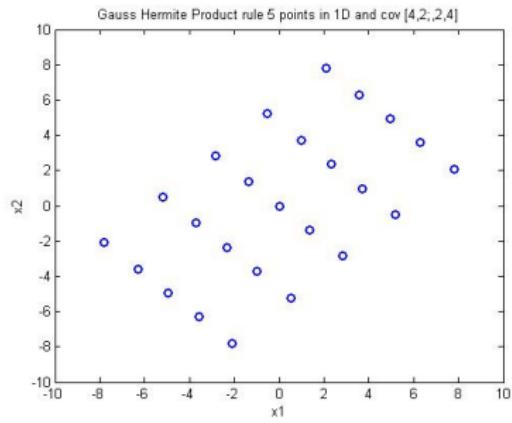
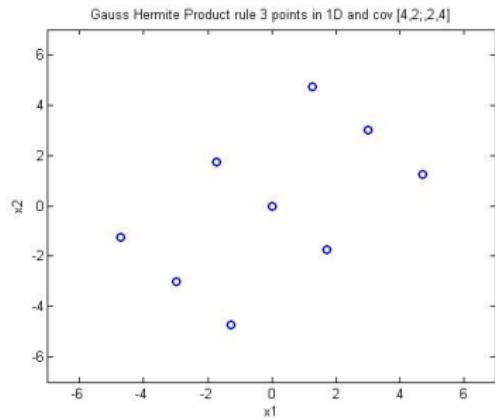


FIGURE: Guass hermite product rule for 2D for Cov [4,2;2,4]

Expectation Integral

- Let us consider the problem of computing expected value of a function $f(x)$ with respect to a Gaussian density function.
- In addition consider the mean and covariance of the Gaussian function to be zero and unity, respectively.

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$$E[f(x)] = \int f(x)N(x, 0|1)dx \quad (2)$$

Taking the Taylor series expansion of $f(x)$ about the mean

$$\begin{aligned} E[f(x)] &= f(0) + \nabla f(0)E[x] + \frac{1}{2!}\nabla^2 f(0)E[x^2] \\ &\quad + \frac{1}{3!}\nabla^3 f(0)E[x^3] + \frac{1}{4!}\nabla^4 f(0)E[x^4]\dots \end{aligned} \quad (3)$$

- Notice that the problem of evaluating the expected value of nonlinear function $f(x)$ has reduced to computing higher order moments of x .
- Thus by increasing the number of terms in the Taylor series expansion, one can obtain more accurate value of the expectation integral.



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- Now consider the discrete approximation of the expectation integral as a weighted average of $f(x)$ evaluated at each quadrature/sigma point set
- Let the sigma point set be (x_1, x_2, \dots, x_n) with corresponding weights (w_1, w_2, \dots, w_n) :

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- Notice that these constraint equations conveys that the sigma points x_i should satisfy the infinite moment equations in the domain of the pdf.
- Thus, if $f(x)$ is a polynomial function of degree d then sigma points should be chosen to reproduce first d moments of the pdf exactly to guarantee the exact evaluation of the expectation integral.
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To evaluate the cubature points and weights of any PDF, the following procedure is followed

- Evaluate the**moments** of the continuous PDF
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MOMENT CONSTRAINT EQUATIONS

The equivalent discrete moments are written in terms of the assumed variables- **positions and weights**

TABLE: Equivalent Moments for 2D till order 4

Continuous	Discrete	Continuous	Discrete
$E[x]$	$\sum_{i=1}^n w_i x_i$	$E[y]$	$\sum_{i=1}^n w_i y_i$
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Table 1 gives the moment constraint equations that have to be solved for the **weights w_i and points x_i** .

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- Particularly the Higher order raw moments just need the covariance matrix.

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for example the **fourth moment** is

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And the **sixth moment** is

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$$\begin{aligned} &= E[x_1x_2]E[x_3x_4]E[x_5x_6] + E[x_1x_2]E[x_3x_5]E[x_4x_6] \\ &\quad + E[x_1x_2]E[x_3x_6]E[x_4x_5] + E[x_1x_3]E[x_2x_4]E[x_5x_6] \\ &\quad + E[x_1x_3]E[x_2x_5]E[x_4x_6] + E[x_1x_3]E[x_2x_6]E[x_4x_5] \\ &\quad + E[x_1x_4]E[x_2x_3]E[x_5x_6] + E[x_1x_4]E[x_2x_5]E[x_3x_6] \\ &\quad + E[x_1x_4]E[x_2x_6]E[x_3x_5] + E[x_1x_5]E[x_2x_3]E[x_4x_6] \\ &\quad + E[x_1x_5]E[x_2x_4]E[x_3x_6] + E[x_1x_5]E[x_2x_6]E[x_3x_4] \\ &\quad + E[x_1x_6]E[x_2x_3]E[x_4x_5] + E[x_1x_6]E[x_2x_4]E[x_3x_5] \\ &\quad + E[x_1x_6]E[x_2x_5]E[x_3x_4] \end{aligned}$$

NORMAL DISTRIBUTION

As the Normal PDF is symmetric, we would like to **exploit this symmetry** in finding the cubature points. The points we like to seek have the following properties

- **Fully symmetric** :- thus satisfying all odd order moments at no further cost
- Weights sum up to 1
- All weights are to be **positive**
- As the points are symmetric, each point has an equivalent point located on the other side of the mean at the same distance.
- These two points together lie on a line passing through the mean. We later name this line as a particular '**axis**'.
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TERMINOLOGY

To proceed with the method we describe, the following **terminology or definitions** that might be handy

GENERATOR SET

- This definition has been used quite a lot in literature to describe a set containing all permutations, including sign permutations of the elements in a set $\{u_1, u_2, u_3, \dots, u_r, 0, 0, 0, \dots, 0\}$, where u_1, u_2, \dots are real numbers.
- for example the generator set $(1, 1, 0)$ is equivalent to $(1, 1, 0)$, $(1, 0, 1)$, $(0, 1, 1)$, $(-1, 1, 0)$, $(1, -1, 0)$, $(-1, 0, 1)$, $(1, 0, -1)$, $(0, -1, 1)$, $(0, 1, -1)$, $(0, -1, -1)$, $(-1, -1, 0)$, $(-1, 0, -1)$

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THE VARIABLES USED

- Once the appropriate axis are chosen, the points are constrained to be on these axis such that a symmetric set of points that have the same weight are at equal distance from the origin.
- The distance variables are $r_1, r_2\dots$ measured from the origin to the appropriate set of points.
- The points at distance r_1 have weight w_1 and so on.

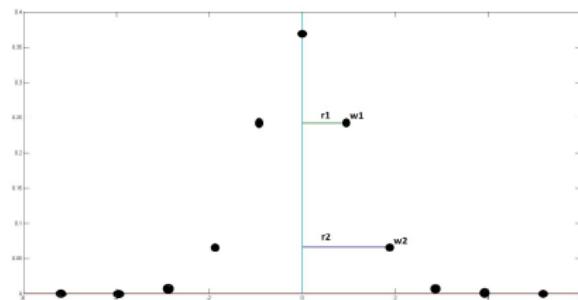


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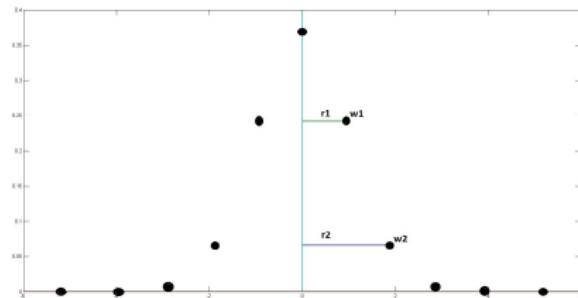


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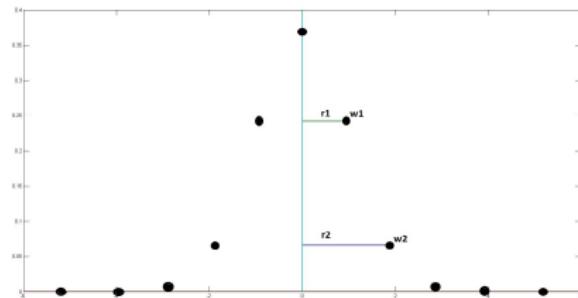


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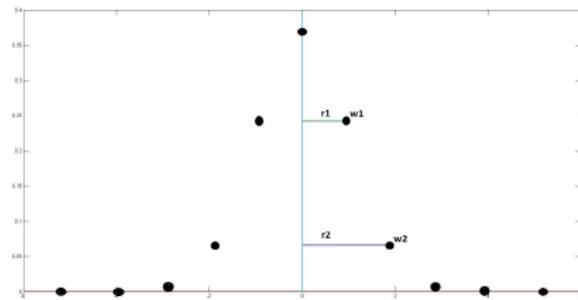


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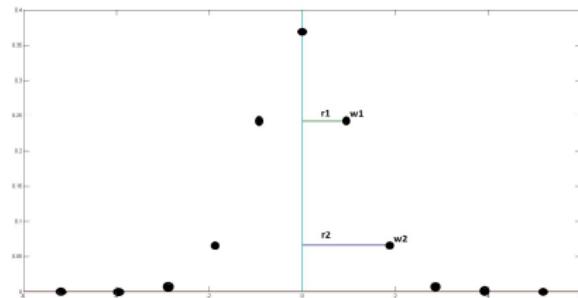


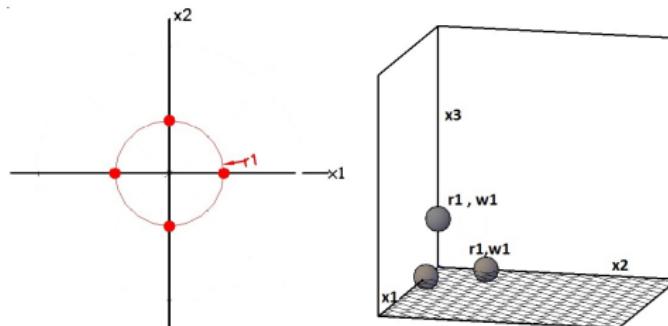
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PRINCIPAL AXIS

The orthogonal axis in cartesian space intersecting at the origin. These are the axis corresponding to each column of the identity covariance matrix. Thus there are N principal axis or $2N$ distinct points on the principal axis for N -Dimensional system. We list the points on principal axis as

$$\sigma_i \in \{\pm\sqrt{P_j} | \{j\} \in \{1, 2, \dots, N\}\} \quad (9)$$

$$i = 1, 2, 3, \dots, 2N. \quad (10)$$



CUBATURE POINTS CONSTRAINED TO THE PRINCIPAL AXIS TO SATISFY THE 2nd ORDER MOMENTS

For an i.i.d random variables (X_1, X_2, \dots, X_N) the N-Dimensional normal PDF has Identity covariance and zero mean. The **first four moments** of this continuous PDF are

$$E[X_i^2] = 1$$

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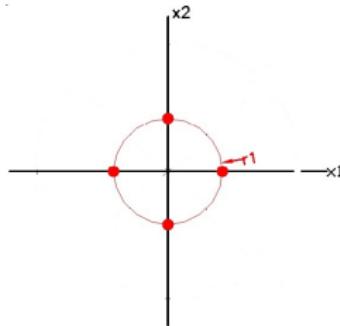


FIGURE: distances and weights

For example consider the 2D system. The points on these axis when enumerated as a list is $(r_1, 0)$, $(0, r_1)$, $(-r_1, 0)$, $(0, -r_1)$. The equivalent discrete moments are

$$2r_1^2 w_1 = 1$$

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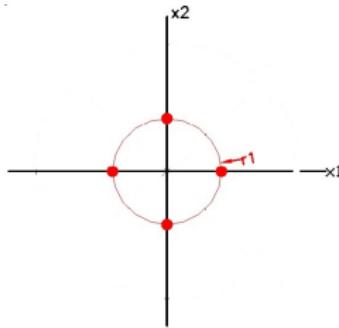


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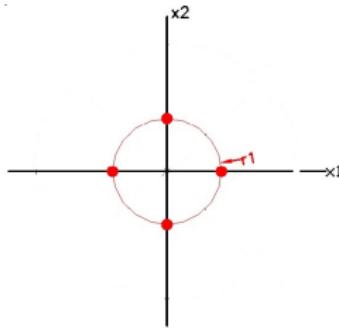


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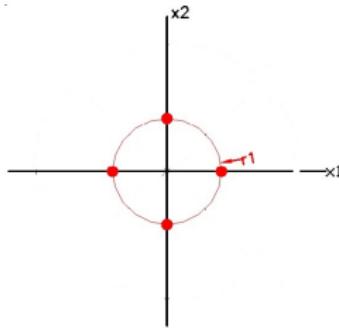


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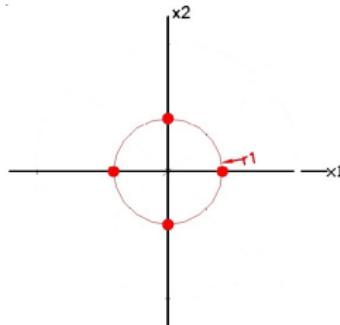


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This set of equations are in fact the same for any dimension. The central weight is calculated as

$$w_0 = 1 - 2Nw_1 \quad (11)$$

One of the 4^{th} order cross moment **cannot be satisfied** by selecting such points on the principal axis.

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- The $2N + 1$ sigma points for the unscented Transform are chosen such that 1 point is the origin and $2N$ points of equal weight are constrained to lie on the principal axis.
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As there is no point at the mean, the central weight can be taken 0.

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- Infact the UT can **capture one of the 4th order moment exactly** but the CKF has an error in all the fourth order moments.
- This is also illustrated by examples later on in the results section.

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$$|3 - (N + \kappa)| \quad (13)$$

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$$|2N^2 \frac{1}{2N} - 3| \equiv |N - 3| \quad (14)$$

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M^{th} -CONJUGATE AXIS

For a N-Dimensional system where $M \leq N$, the axis that are constructed from all the combinations of the set of principle axis taken M at a time. For example, the N^{th} -Conjugate set of axis for N-Dimensional system have 2^N distinct points or 2^{N-1} axis and the 2^{nd} -Conjugate set of axis for N-Dimensional system has $2N(N - 1)$ distinct points or $N(N - 1)$ axis. We label the set of M^{th} conjugate axis as c_i^M , where the points are listed as c_i^M

$$c_i^M \in \{\pm \sigma_{n_1} \pm \sigma_{n_2} \pm \dots \pm \sigma_{n_M} \mid \{n_1, n_2, \dots, n_M\} \subset \{1, 2, \dots, N\}\}$$

$$i = 1, 2, \dots, 2^M \binom{N}{M}$$

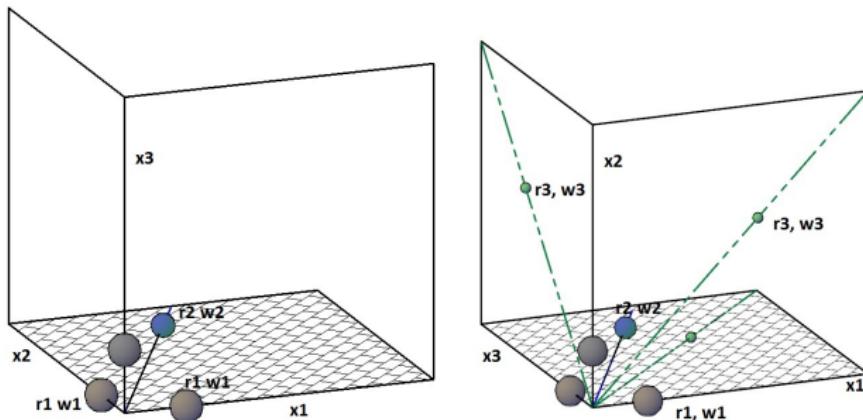
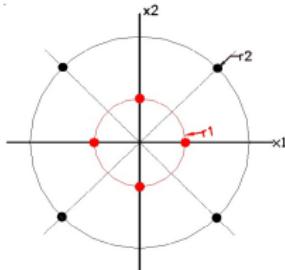


FIGURE: distances and weights

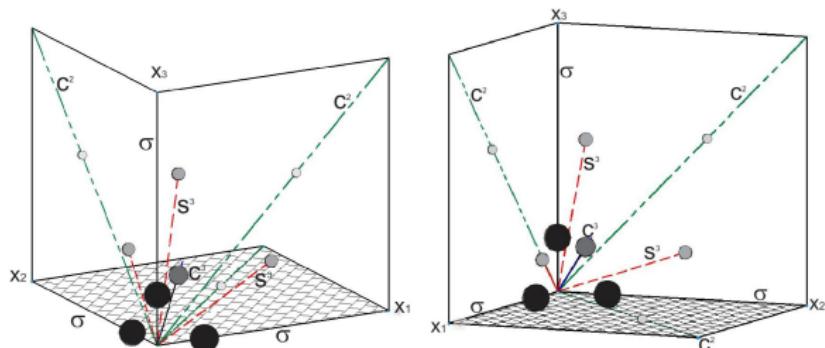
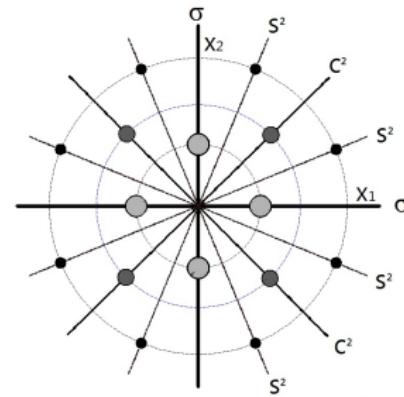


FIGURE: Symmetric set of points and axis 2D and 3D space

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- But this method suffers the same problem of having a **negative weight above dimension 4.**
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THE CONJUGATE UNSCENTED TRANSFORM METHOD TO CAPTURE ALL THE 4TH MOMENT

- The first set of points are chosen on the principal axis at a distance of r_1 and weight w_1 each.
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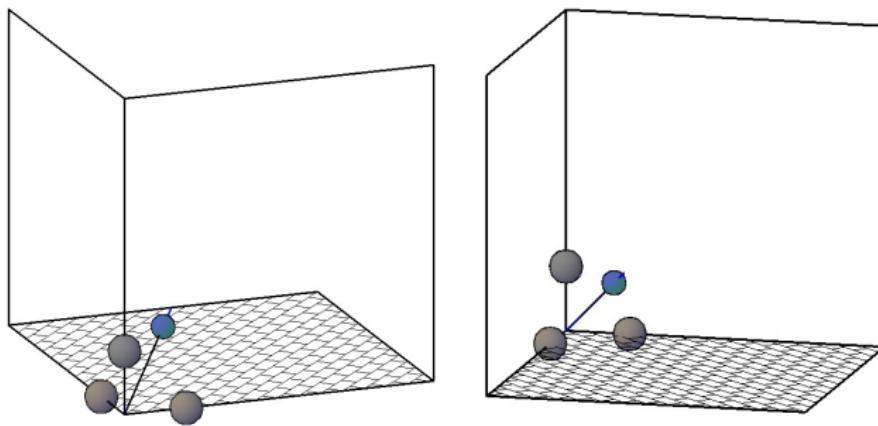
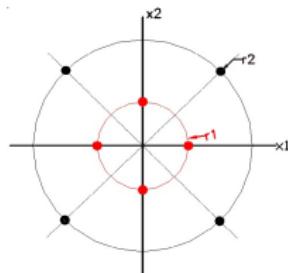
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These set of equations can be **solved analytically** in the following 2 schemes because there is no constraint on w_0 except that it should be positive

Solution 1

The w_0 is solved for by minimizing the square of error in sixth moment

$$\text{Min} \quad (2r_1^6 w_1 + 2^N r_2^6 w_2 - 15)^2$$

This is applied for dimensions 1 and 2

TABLE: Optimization Solution for $N = 1$ and $N = 2$

Variable	$N = 1$	$N = 2$
r_1	1.4861736616297834	2.6060099476935847
r_2	3.2530871022700643	1.190556300661233
w_0	0.5811010092660772	0.41553535186548973
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Solution 2 For dimension greater than 2, the central weight is eliminated thus **reducing 1 point**. For $N > 2$

$$w_0 = 0$$

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SIGMA POINTS FOR CUT4

TABLE: Sigma Points for CUT4

	Position	Weights
$1 \leq i \leq 2N$	$X_i = r_1 \sigma_i$	$W_i = w_1$
$1 \leq i \leq 2^N$	$X_{i+2N} = r_2 c_i^N$	$W_{i+2N} = w_2$
Central weight	$X_0 = \mathbf{0}$	$W_0 = w_0$
$n = 2N + 2^N (+1)$		

IN SUMMARY

- Solve the distance and weight variables
- Generate the principle axis and Conjugate axis
- Generate the sigma points
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NUMERICAL RESULTS FOR CUT4

Results of integration compared to Gauss Hermite integration for 3D system

The total number of cubature points involved in this method to capture all the moments till 4th order is $2N + 2^N$

$$P = \begin{bmatrix} 4 & 2 & 1 \\ 2 & 9 & 1 \\ 1 & 1 & 16 \end{bmatrix}$$

$$\begin{aligned} F = & x_1^4 + x_2^4 + x_3^4 + x_1^3x_2 + x_1^2x_2^2 + \\ & + x_3^2x_2^2 + x_1^2x_3^2 + x_1^3x_3 + x_2^3x_3 + x_3^3x_2 \end{aligned}$$

NUMERICAL RESULTS FOR CUT4

No. of pts	$2^3 = 8$	$3^3 = 27$	$4^3 = 64$	Analytical
GH	1056.95571	1797.99999	1798.00	1798.00
% error wrt Truth	41.2149211	4.299e-013	3.0350e-013	0

	No. of pts	Integration result	% error
CUT4	15	1797.99999	6.3552080e-010

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Results of integration compared to Gauss Hermite integration for 8D system

The total number of cubature points involved in this method to capture all the moments till 4th order is $2N + 2^N$

$$P = 10I_{8x8}$$

$$F = x_1^4 + x_8^2 * x_2^2 + x_3^2 + x_4^2 * x_5^2$$

No. of pts	$2^8 = 8$	$3^8 = 6561$	$4^8 = 65536$	Analytical
GH	256	614	614	614
% error	32.573	5.18441605e-013	6.591614e-012	0

	No. of pts	Integration result	% error
CUT4	273	614	1.0368832104e-012

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% error	32.573	5.18441605e-013	6.591614e-012	0

	No. of pts	Integration result	% error
CUT4	273	614	1.0368832104e-012

NUMERICAL RESULTS FOR CUT4

$$P_1 = \begin{bmatrix} 114.2595 & 90.1397 & 8.9751 \\ 90.1397 & 92.2504 & 29.1237 \\ 8.9751 & 29.1237 & 84.0908 \end{bmatrix} \quad (15)$$

$$P_2 = 100I_{(10 \times 10)} \quad (16)$$

$$f(X) = (\sqrt{1 + X^T X})^4 \quad (17)$$

TABLE: CUT4

method	n_1	μ_1 % error	n_2	μ_2 % error
GH2	8	52.36	1024	16.39
GH3	27	$4.89e - 014$	59049	$7.23e - 012$
CUT4	14	0	1044	$6.72e - 012$

6TH ORDER CONJUGATE UNSCENTED TRANSFORM - CUT6

Cubature points that are 6^{th} moment equivalent

- We **attempt** to capture all the 6^{th} order moments till 6D
- In addition to the axis chosen for the fourth moment one additional set of axis is considered
- 1 point on the mean, first set of points on the principal axis at distance r_1 and each weight w_1 .
- Second set on the Nth-Conjugate axis with distance r_2 and weight w_2 .
- Third set of axis are chosen on the 2nd conjugate axis with points at distance r_3 and weight w_3

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6TH ORDER CONJUGATE UNSCENTED TRANSFORM - CUT6

Cubature points that are 6^{th} moment equivalent

- We **attempt** to capture all the 6^{th} order moments till 6D
- In addition to the axis chosen for the fourth moment one additional set of axis is considered
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SIGMA POINTS OF CUT6

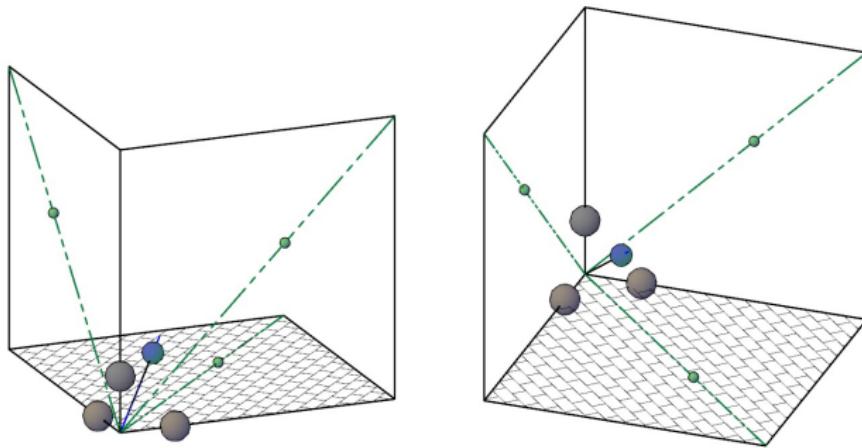
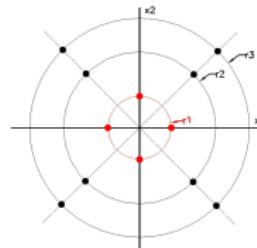


FIGURE: distances and weights



University at Buffalo

The State University of New York

MOMENTS TILL 6TH ORDER

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$$E[X_i X_j] = 0$$

$$E[X_i^4] = 3$$

$$E[X_i^3 X_j] = 0$$

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CUT6 - SOLUTION TO THE SYSTEM

Procedure followed

- These nonlinear equations are in a way linear with respect to the weights
- The last 3 equations can be solved for w_1 , w_2 and w_3 symbolically in terms of the other variables r_1 , r_2 and r_3
- Substituting these into the first 3 equations the overall order of the system is reduced.

$$w_1 = \frac{8 - N}{r_1^6}$$

$$w_2 = \frac{1}{2^N r_2^6}$$

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IN SUMMARY CUT6, ($N \leq 6$)

TABLE: Sigma Points for CUT6, ($N \leq 6$)

	Position	Weights
$1 \leq i \leq 2N$	$X_i = r_1 \sigma_i$	$W_i = w_1$
$1 \leq i \leq 2^N$	$X_{i+2N} = r_2 c_i^N$	$W_{i+2N} = w_2$
$1 \leq i \leq 2N(N-1)$	$X_{i+2N+2^N} = r_3 c_i^2$	$W_{i+2N+2^N} = w_3$
Central weight	$X_0 = \mathbf{0}$	$W_0 = w_0$
$n = 2N^2 + 2^N + 1$		

IN SUMMARY FOR ($N \leq 6$)

- Solve the distance and weight variables
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SIGMA POINTS FOR CUT6, ($7 \leq N \leq 9$)

- The previous method of CUT6 is valid only till dimension 6.
- After dimension 6 we have negative weights.
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The set of 6^{th} order moment constraint equations in terms of these new sigma points are given as:

$$2r_1^2w_1 + 2^N r_2^2w_2 + 4(N-1)(N-2)r_3^2w_3 = 1$$

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$$1 - 2Nw_1 - 2^N w_2 - (4n(n-1)(n-2)/3)w_3 = w_0$$

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SIGMA POINTS FOR CUT6, ($7 \leq N \leq 9$)

In Summary

TABLE: Sigma Points for CUT6, ($7 \leq N \leq 9$)

	Position	Weights
$1 \leq i \leq 2N$	$X_i = r_1 \sigma_i$	$W_i = w_1$
$1 \leq i \leq 2^N$	$X_{i+2N} = r_2 c_i^N$	$W_{i+2N} = w_2$
$1 \leq i \leq 4n(n-1)(n-2)/3$	$X_{i+2N+2^N} = r_3 c_i^3$	$W_{i+2N+2^N} = w_3$
Central weight	$X_0 = \mathbf{0}$	$W_0 = w_0$

$n = 2N + 2^N + 4n(n-1)(n-2)/3 + 1$

NUMERICAL RESULTS OF CUT6

Results of integration compared to Gauss Hermite integration for 4D system

The total number of cubature points involved in this method to capture all the moments till 6th order is $2N^2 + 2^N + 1$

$$P = \begin{bmatrix} 4 & 1 & 2 & 1 \\ 1 & 9 & 2 & 3 \\ 2 & 2 & 16 & 4 \\ 1 & 3 & 4 & 25 \end{bmatrix}$$

$$\begin{aligned} F = & x_1^6 + x_2^6 + x_3^6 + x_4^6 + x_1^4 + x_2^4 + x_3^4 + x_4^4 + x_1^2 x_2^2 x_3^2 + \\ & + x_1^3 x_3 + x_1^2 x_2^4 + x_3^4 x_2^2 + x_1^2 x_3^4 + x_1^3 x_3 + x_2^3 x_3 + x_3^3 x_2 \end{aligned}$$

NUMERICAL RESULTS OF CUT6

No. of pts	$2^4 = 16$	$3^4 = 81$	$4^4 = 256$	$5^4 = 64$	Analytical
GH	84462.6354	293311.8446	375417.9999	375417.9999	375417.9999
% error	77.5017	21.8705	9.0702e-012	8.9152e-012	0

	No. of pts	Integration result	% error
CUT6	49	3.7541800e+005	8.062475e-013

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$$P = 10I_{6x6} \quad (18)$$

$$F = x_1^6 + x_1^2x_2^2x_3^2 + x_1^4x_6^2 + x_5^4 + x_3^2x_4^2$$

NUMERICAL RESULTS OF CUT6

No. of pts	$2^6 = 64$	$3^6 = 729$	$4^6 = 4096$	$5^6 = 15625$	A
GH	6.035000e+003	1.943500e+004	2.543500e+004	2.543500e+004	2.5
% error	76.2728	23.589	1.5633e-011	1.58906e-011	0

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CUT6	137	2.543500e+004	3.4583111e-008

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NUMERICAL RESULTS OF CUT6

$$P_3 = 100I_{(4 \times 4)}$$

$$P_4 = 100I_{(9 \times 9)}$$

TABLE: CUT6

method	n_3	μ_3 % error	n_4	μ_4 % error
GH3	81	12.45	19683	4.18
GH4	256	$2.31e - 013$	262144	$1.37e - 009$
CUT6	49	$6.49e - 013$	1203	$6.26e - 009$

CUBATURE POINTS TO CAPTURE ALL THE 8TH ORDER MOMENTS

- All the axis used before were not able to capture all the 8th order moments
- Only points that lie in the full N-D space enter the 8th order moments.
- I was only able to capture the moments till 6th dimension.
- Due to the complex nature of the equation I was not able to find a trend in the set of equations to generalize it.
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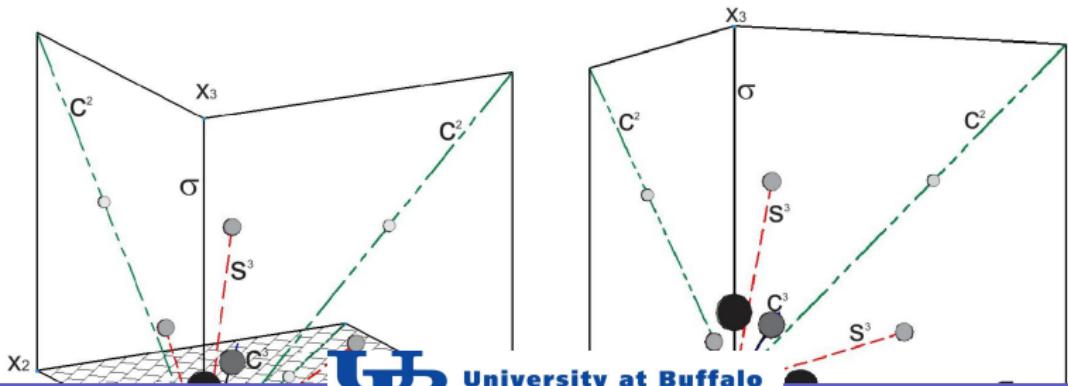
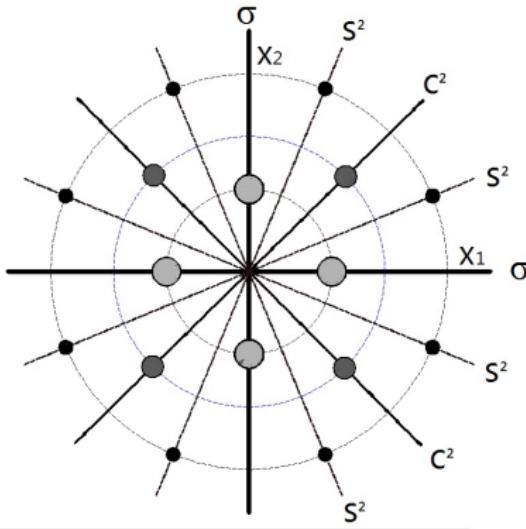
Nth-SCALED CONJUGATE AXIS

For a N-Dimensional system ,the axis that are constructed from all the combinations of the set of principle axis such that in every combination exactly one principle axis is scaled by a scaling parameter 'h' .The *Nth*-Scaled Conjugate set of axis for N-Dimensional system has $N2^N$ distinct points or $N2^{N-1}$ axis. We label the set of *Nth*-Scaled conjugate axis as $s^N(h)$, where the points are listed as $s_i^N(h)$

$$s_i^N(h) \in \{(\pm h\sigma_{n_1} \pm \sigma_{n_2} \pm \dots \pm \sigma_{n_N}) | (n_1, n_2, \dots, n_N) \in (1, 2, \dots, N)\} \quad (19)$$

$$\& n_1 \neq n_2 \neq \dots \neq n_N \} \quad (20)$$

$$i = 1, 2, 3, \dots, N2^N \quad (21)$$



- 1 point on the mean
 - A set of points on the principal axis
 - A set of points on the Nth-conjugate axis
 - A set of points on the 2nd-conjugate axis
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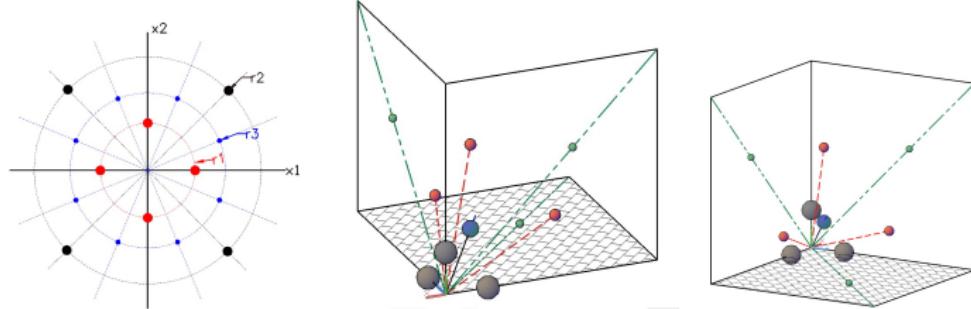


FIGURE: distances and weights

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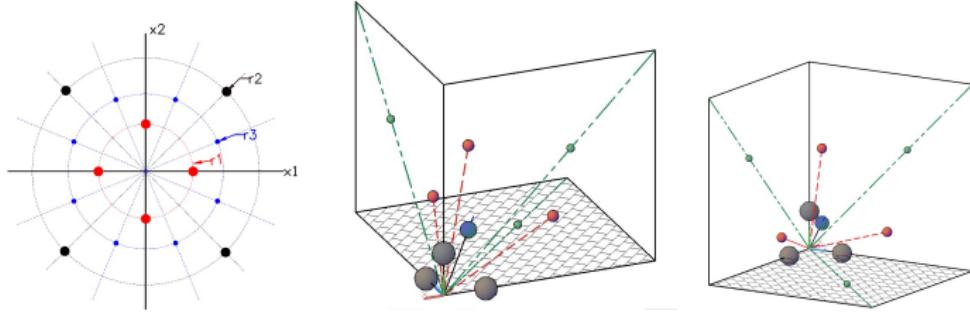


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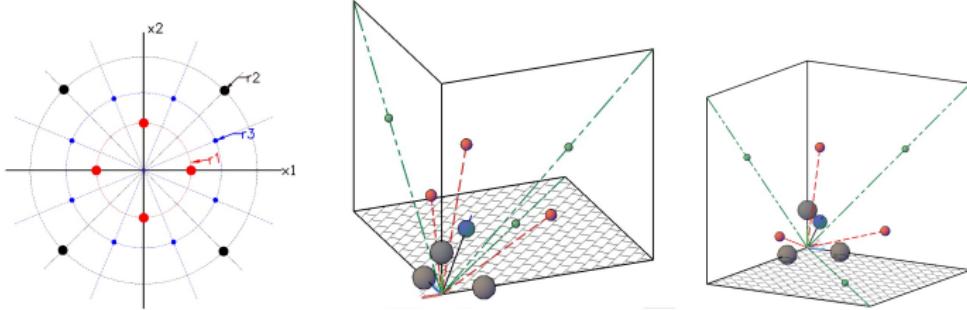


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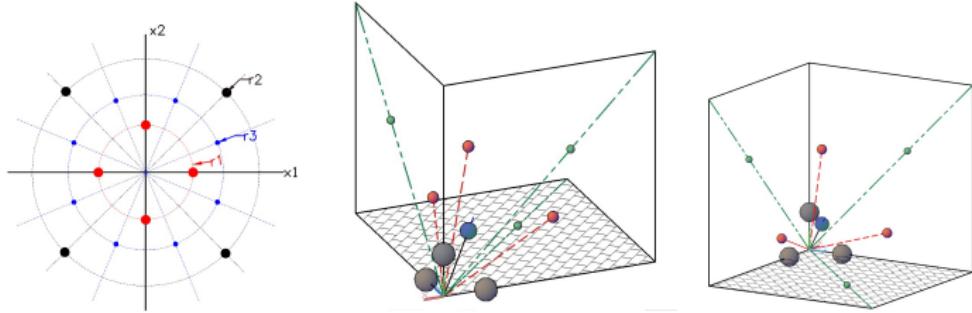


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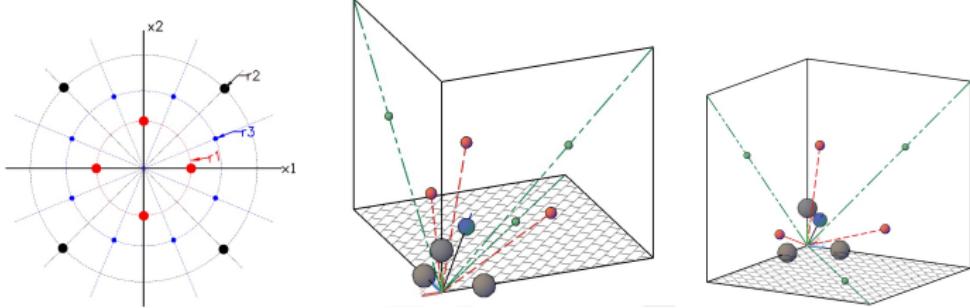


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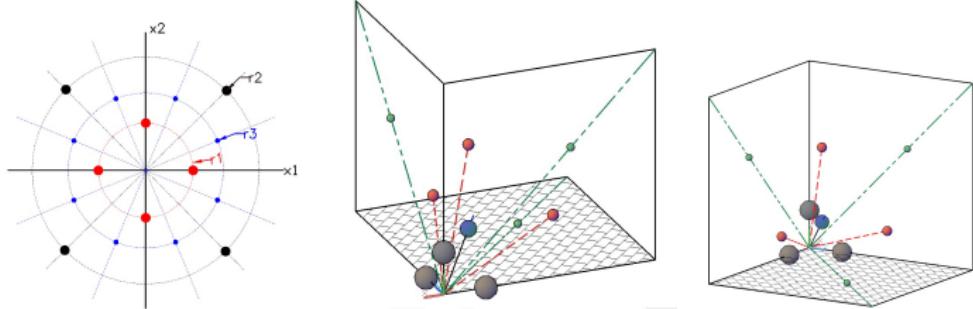


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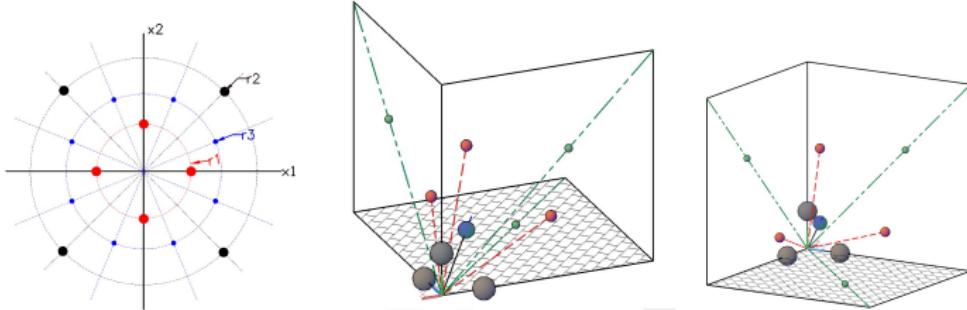


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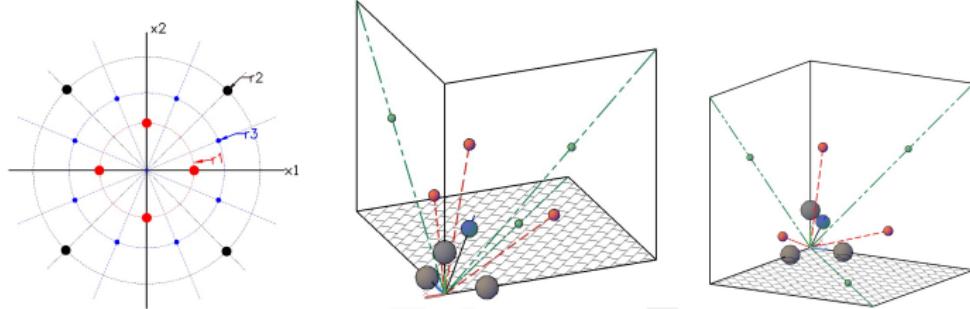


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MOMENT CONSTRAINT EQUATIONS TILL 8TH MOMENT

Only the even moments are shown that are to be satisfied. There are
11 non-zero moments for any dimension in all

$$E[X_i^2] = 1$$

$$E[X_i^4] = 3$$

$$E[X_i^2 X_j^2] = 1$$

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$$E[X_i^8] = 105$$

$$E[X_i^6 X_j^2] = 15$$

$$E[X_i^4 X_j^4] = 9$$

$$E[X_i^4 X_j^2 X_k^2] = 3$$

$$E[X_i^2 X_j^2 X_k^2 X_l^2] = 1$$

MOMENT CONSTRAINT EQUATIONS TILL 8TH MOMENT FOR 4D SYSTEM

$$2r_1^2w_1 + 16r_2^2w_2 + 12r_3^2w_3 + 16r_4^2w_4 + 24r_5^2w_5 + 48r_6^2w_6 + 16h^2r_6^2w_6 = 1$$

$$2r_1^4w_1 + 16r_2^4w_2 + 12r_3^4w_3 + 16r_4^4w_4 + 24r_5^4w_5 + 48r_6^4w_6 + 16h^4r_6^4w_6 = 3$$

$$16r_2^4w_2 + 4r_3^4w_3 + 16r_4^4w_4 + 16r_5^4w_5 + 32r_6^4w_6 + 32h^2r_6^4w_6 = 1$$

$$2r_1^6w_1 + 16r_2^6w_2 + 12r_3^6w_3 + 16r_4^6w_4 + 24r_5^6w_5 + 48r_6^6w_6 + 16h^6r_6^6w_6 = 15$$

$$16r_2^6w_2 + 4r_3^6w_3 + 16r_4^6w_4 + 16r_5^6w_5 + 32r_6^6w_6 + 16h^2r_6^6w_6 + 16h^4r_6^6w_6 = 3$$

$$16r_2^6w_2 + 16r_4^6w_4 + 8r_5^6w_5 + 16r_6^6w_6 + 48h^2r_6^6w_6 = 1$$

$$2r_1^8w_1 + 16r_2^8w_2 + 12r_3^8w_3 + 16r_4^8w_4 + 24r_5^8w_5 + 48r_6^8w_6 + 16h^8r_6^8w_6 = 105$$

$$16r_2^8w_2 + 4r_3^8w_3 + 16r_4^8w_4 + 16r_5^8w_5 + 32r_6^8w_6 + 16h^2r_6^8w_6 + 16h^6r_6^8w_6 = 15$$

$$16r_2^8w_2 + 4r_3^8w_3 + 16r_4^8w_4 + 16r_5^8w_5 + 32r_6^8w_6 + 32h^4r_6^8w_6 = 9$$

$$16r_2^8w_2 + 16r_4^8w_4 + 8r_5^8w_5 + 16r_6^8w_6 + 32h^2r_6^8w_6 + 16h^4r_6^8w_6 = 3$$

$$16r_2^8w_2 + 16r_4^8w_4 + 64h^2r_6^8w_6 = 1$$



University at Buffalo

The State University of New York

MOMENT CONSTRAINT EQUATIONS TILL 8TH MOMENT FOR 5D SYSTEM

$$2r_1^2w_1 + 32r_2^2w_2 + 16r_3^2w_3 + 32r_4^2w_4 + 48r_5^2w_5 + 128r_6^2w_6 + 32h^2r_6^2w_6 = 1$$

$$2r_1^4w_1 + 32r_2^4w_2 + 16r_3^4w_3 + 32r_4^4w_4 + 48r_5^4w_5 + 128r_6^4w_6 + 32h^4r_6^4w_6 = 3$$

$$32r_2^4w_2 + 4r_3^4w_3 + 32r_4^4w_4 + 24r_5^4w_5 + 96r_6^4w_6 + 64h^2r_6^4w_6 = 1$$

$$2r_1^6w_1 + 32r_2^6w_2 + 16r_3^6w_3 + 32r_4^6w_4 + 48r_5^6w_5 + 128r_6^6w_6 + 32h^6r_6^6w_6 = 15$$

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$$32r_2^6w_2 + 32r_4^6w_4 + 8r_5^6w_5 + 64r_6^6w_6 + 96h^2r_6^6w_6 = 1$$

$$2r_1^8w_1 + 32r_2^8w_2 + 16r_3^8w_3 + 32r_4^8w_4 + 48r_5^8w_5 + 128r_6^8w_6 + 32h^8r_6^8w_6 = 105$$

$$32r_2^8w_2 + 4r_3^8w_3 + 32r_4^8w_4 + 24r_5^8w_5 + 96r_6^8w_6 + 32h^2r_6^8w_6 + 32h^6r_6^8w_6 = 15$$

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$$32r_2^8w_2 + 32r_4^8w_4 + 32r_6^8w_6 + 128h^2r_6^8w_6 = 1$$

SOLUTION FOR 5D SYSTEM

$$h = 3$$

$$r_5 = 2$$

$$r_1 = 2.3143708172807447$$

$$r_2 = 0.8390942773980102$$

$$r_3 = 1.8307521253266494$$

$$r_4 = 1.3970397430644959$$

$$r_6 = 1.1134786327367021$$

$$w_1 = 0.010529034221546607$$

$$w_2 = 0.015144019639537572$$

$$w_3 = 0.0052828996967816825$$

$$w_4 = 0.0010671298950159158$$

$$w_5 = 0.000651041666666666$$

$$w_6 = 0.00013776017592074394 \quad (22)$$

SOLUTIONS OF CUT8 FOR $2 \leq N \leq 6$,

TABLE: Cut8 : for $2 \leq N \leq 6$,

Variable	2D	3D	4D	5D
r_1	2.068136061121187	2.255137265545780	2.201709071472343	2.314370817280745
r_2	0.8491938499087475	0.7174531274600530	0.7941993714175681	0.8390942773980102
r_3	1.138654980847415	1.843019437068797	1.872574360506295	1.830752125326649
r_4	1.861619935018895	1.558481032725744	1.329116430064565	1.397039743064496
r_5	—	—	2	2
r_6	—	1.305561500466050	1.125865581272049	1.113478632736702
w_1	0.04382264267013926	0.024631993437193266	0.01811008737283111	0.010529034221546607
w_2	0.1405096621714662	0.08151009408908164	0.032063273384586845	0.015144019639537572
w_3	0.0009215768861610588	0.009767235524166815	0.006614353755080834	0.0052828996967816825
w_4	0.01240953967762697	0.00577248937435553	0.003489906522946932	0.0010671298950159158
w_5	—	—	0.0006510416666666666	0.0006510416666666666
w_6	—	0.000279472936899139	0.00025218336987488566	0.00013776017592074394
h	3	2.74	3	3

NUMERICAL RESULTS FOR CUT8

Results of integration compared to Gauss Hermite integration for 5D system

For a N-D system the total number of points required to capture the 8th moment by this scheme are

$$1 + 2N^2 + \frac{4N(N-1)(N-2)}{3} + (N+2)2^N.$$

The covariance of the gaussian Kernel

$$P = 1000I_{5 \times 5} \quad (23)$$

$$X = [x_1, x_2, x_3, x_4, x_5] \quad (24)$$

$$\begin{aligned} F(X) = & x_1^8 + x_2^8 + x_3^6 + x_4^6 + x_1^4 x_5^4 + x_2^4 x_3^4 + x_4^2 + x_1^2 x_2^2 x_3^2 x_4^2 + \\ & + x_1^3 x_3 + x_1^4 x_2^2 x_5^2 + x_3^4 x_2^2 + x_1^2 x_3^4 + x_1^3 x_3 + x_2^3 x_3 + x_3^3 x_2 \end{aligned} \quad (25)$$

Evaluating the integral

$$f = \int F(X)N(X, 0|P)dX \quad (26)$$

NUMERICAL RESULTS FOR CUT8

No. of pts	$2^5 = 32$	$3^5 = 243$	$4^5 = 1024$	$5^5 = 3125$	1
GH	6.0962801e+012	7.6616634e+013	1.84964e+014	2.329646e+014	2
% error	97.38317	67.11233	20.6039857	5.184531e-011	0

	No. of pts	Integration result	% error wrt Truth
CUT8	355	2.3296463e+014	5.1509964e-011

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CUT8	355	2.3296463e+014	5.1509964e-011

NUMERICAL RESULTS FOR CUT8

$$P_5 = 100I_{(5 \times 5)}$$

$$P_6 = 100I_{(6 \times 6)}$$

TABLE: CUT8

method	n_5	μ_5 % error	n_6	μ_6 % error
GH4	1024	3.45	4096	2.49
GH5	3125	$4.73e - 012$	15625	$9.29e - 012$
CUT8	355	$7.52e - 012$	745	$6.63e - 012$

RESULTS FOR NON- POLYNOMIAL NONLINEARITY

Polar to Cartesian coordinates transformation

- A radar has error in its radial and angular measurements
- We would like to see how this error is transformed into cartesian coordinates
- We would like to compute the expected value in the cartesian coordinates

In effect we are trying to evaluate the integral

$$\begin{aligned} E[(x,y)^T] &= E[(rcos(\theta),rsin(\theta))^T] \\ &= \int \int (rcos(\theta),rsin(\theta))^T N((r,\theta), (\mu_r, \mu_\theta | P)) dr d\theta \end{aligned}$$

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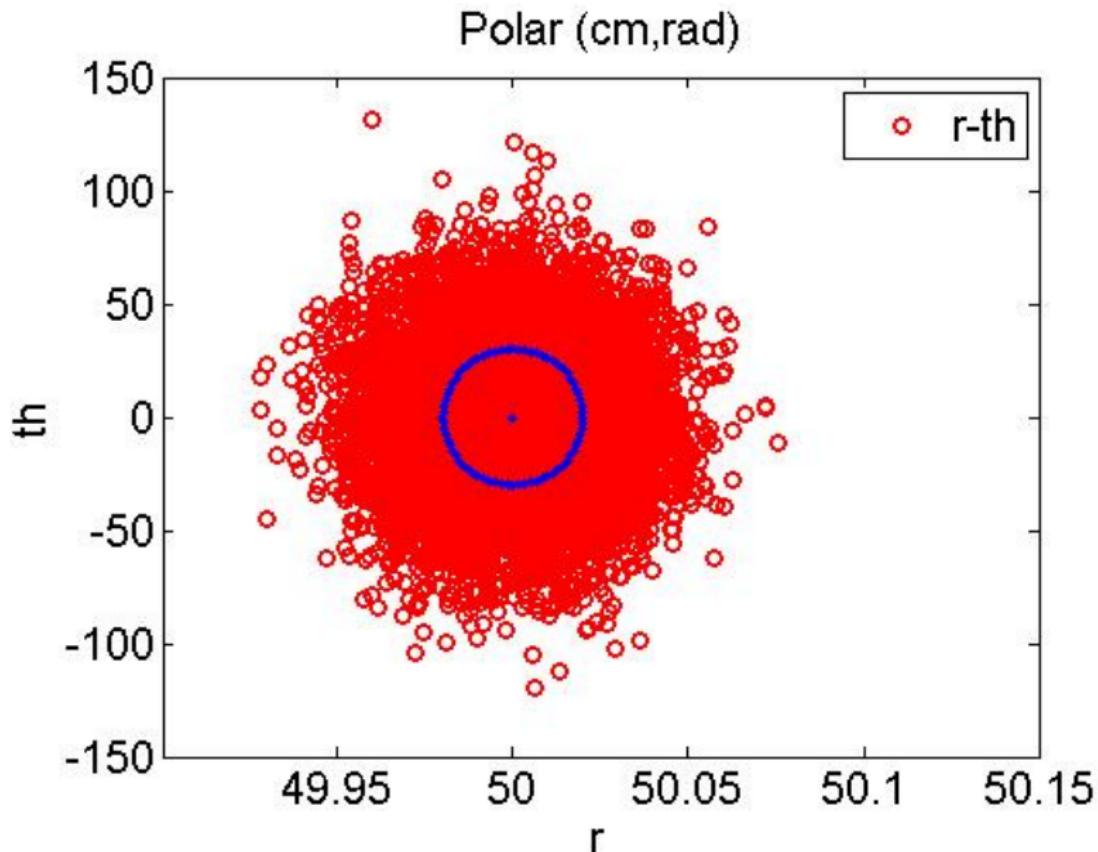


FIGURE: 2D and 3D visualization of 5th order moments

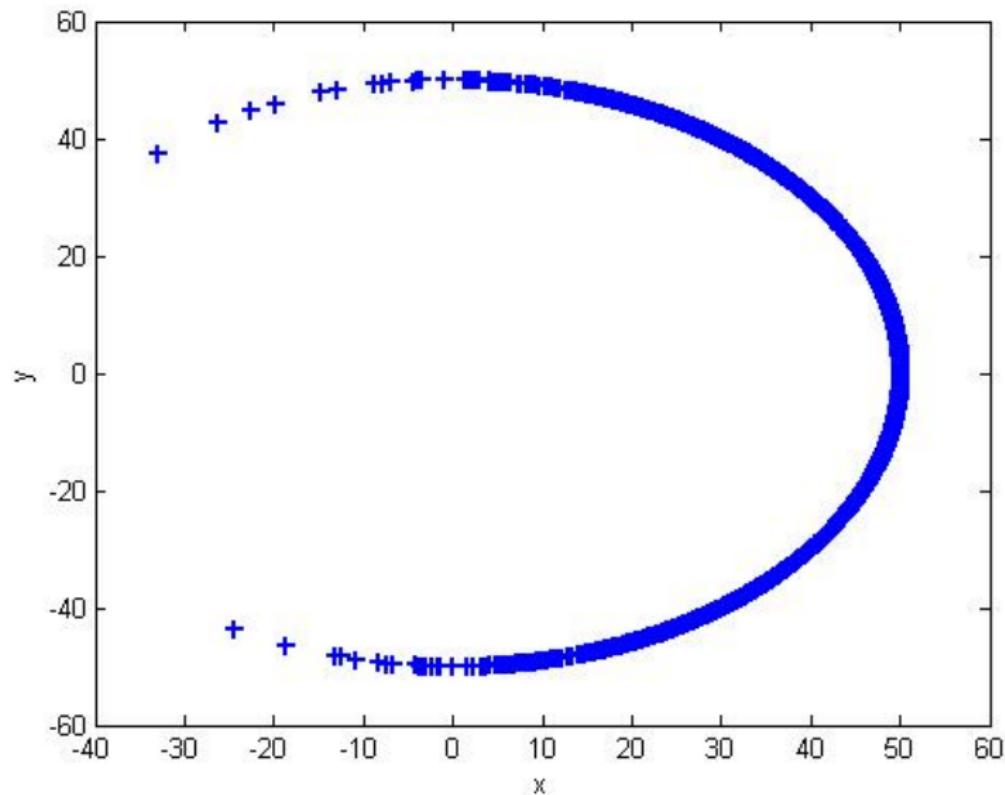


FIGURE: 2D and 3D Gegenbauer polynomials 5th order moments

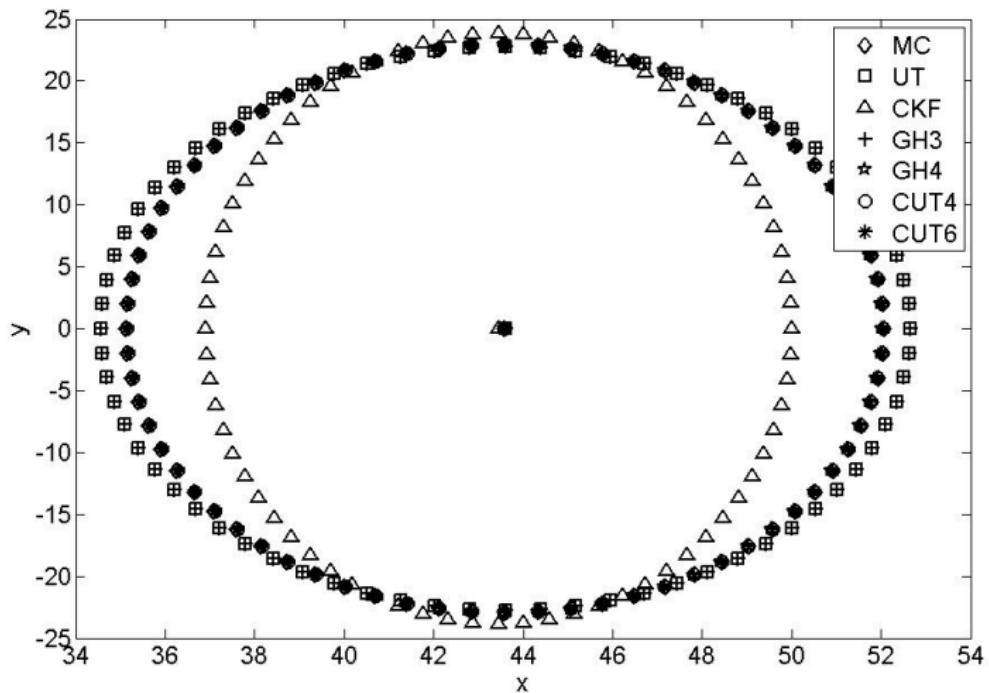


FIGURE: 2D and 3D Cubature points to satisfy 6th order moments

EXPECTED VALUE OF NORMAL PDF

Normal Distribution The integral being evaluated is

$$E[N(x, \mu | P)] = \int N(x, \mu | P)N(x, \mu | P)dx$$

The parameters used are

$$\mu = 0$$

$$P = I$$

TRUE VALUE OF INTEGRAL

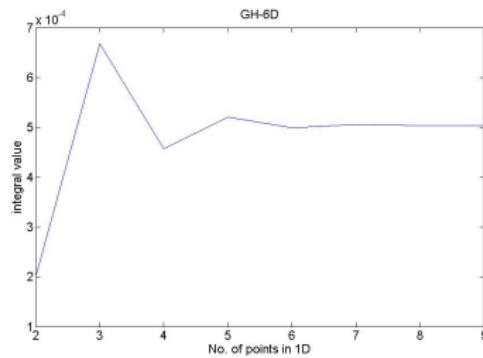
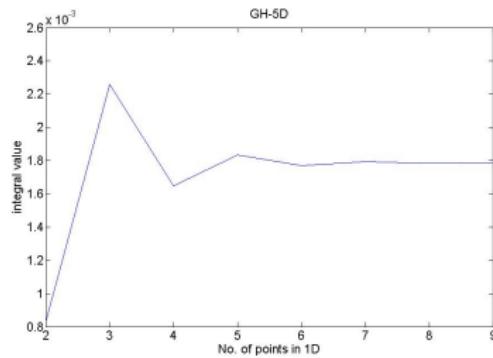
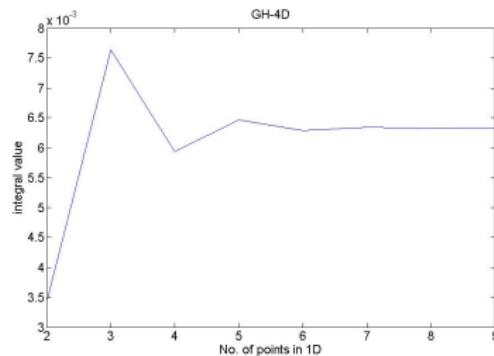
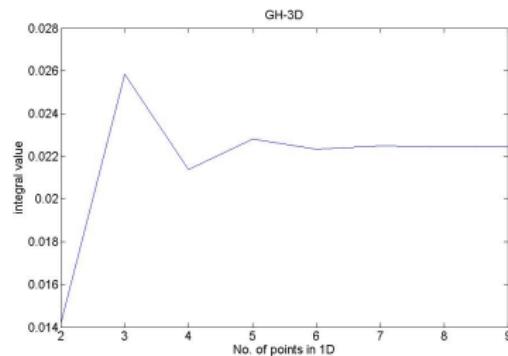


TABLE: Results of the integration interms of % rel. error

Dimension	CKF	UT	CUT4	CUT6	CUT8
3	36.902	36.902	27.042	13.273	1.5688
4	45.880	45.880	46.571	23.276	2.0279
5	53.581	53.581	73.768	28.056	6.8219
6	60.186	60.186	110.90	13.393	15.793

TABLE: Number of points in each method

Dim	GH-5	GH-6	GH-7	CKF	UT	CUT4	CUT6	CUT8
3	125	216	343	6	7	15	27	59
4	625	1296	2401	8	9	25	49	161
5	3125	7776	16807	10	11	43	83	355
6	15625	46656	117649	12	13	77	137	745

EXPECTED VALUE OF EXPONENTIAL FUNCTION

Normal Distribution The integral being evaluated is

$$E[N(x, \mu | P)] = \int \exp\left(-\sum_{i=1}^N x_i\right) N(x, \mu | P) dx$$

The parameters used are

$$\mu = 0$$

$$P = I$$

TRUE VALUE OF INTEGRAL

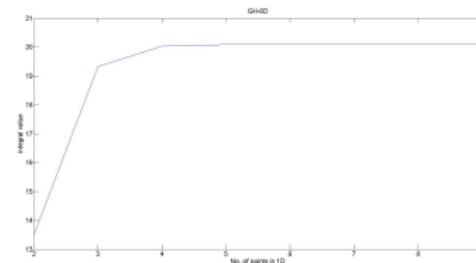
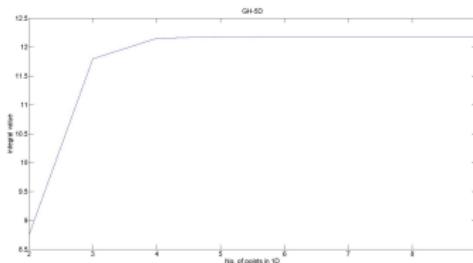
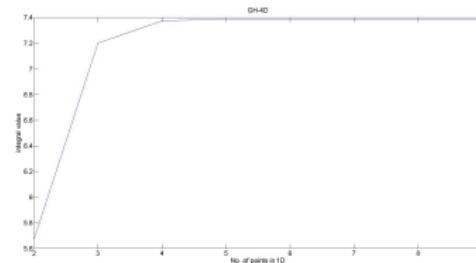
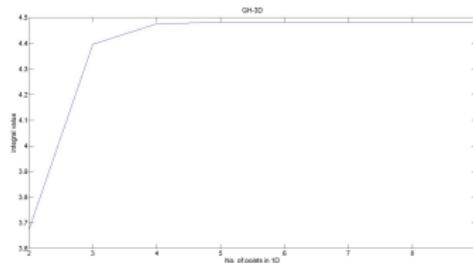


TABLE: Results of the integration interms of % rel. error

Dimension	CKF	UT	CUT4	CUT6	CUT8
3	34.9670	34.9670	5.6510	1.5589	0.0813
4	49.0842	49.0842	7.7049	2.0998	0.6467
5	61.1601	61.1601	9.7754	7.0631	1.4656
6	70.9523	70.9523	12.0018	11.6941	1.2176

TABLE: Number of points in each method

Dim	GH-4	GH-5	GH-6	CKF	UT	CUT4	CUT6	CUT8
3	64	125	216	6	7	15	27	59
4	256	625	1296	8	9	25	49	161
5	1024	3125	7776	10	11	43	83	355
6	4096	15625	46656	12	13	77	137	745

NON -POLYNOMIAL FUNCTION: 4

$$f(\mathbf{X}) = (\sqrt{1 + \mathbf{X}^T \mathbf{X}})^\alpha, \mathbf{X} \in \mathbb{R}^N$$

- This benchmark problem was introduced by CKF.
- It has been discussed that computing the expectation of $f(\mathbf{X})$ for negative values for α is a challenging task.
- Negative values lead to a delta-sequence functions, which is a very notorious function when using quadrature rules.
- For simulation purposes, $\alpha = -3$ and the covariance of the zero mean Gaussian pdf is assumed to be 0.1 times the identity matrix. T
- The covariance is intentionally scaled down by 0.1 to make the integral value converge with reasonable number of points.

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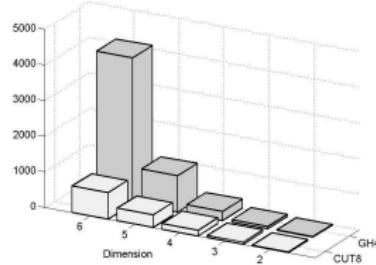
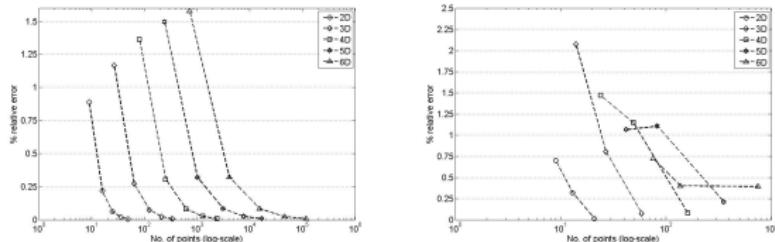
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Therefore to achieve 0.5% accuracy, we need atleast GH4 for Gauss Hemrite quadrature rule and atleast CUT8. There is a significant difference in the number of points to achieve this order of accuracy.

OBJECTIVE 2

TO EVALUATE THE UNIFORM EXPECTATION INTEGRAL

$$E[f(x)] = \int_{-1}^1 f(x)dx$$

The domain of integration is a N-Dimensional Hypercube with each side of length 2 units.

OBSERVATIONS

- The uniform Distribution is also a centrally symmetric function
- The same axis of symmetry can be used
- But there is an additional constraint involved: *All the cubature points must lie within the domain of the pdf i.e. within a hypercube*
- Because of this additional constraint, the procedure is even more difficult

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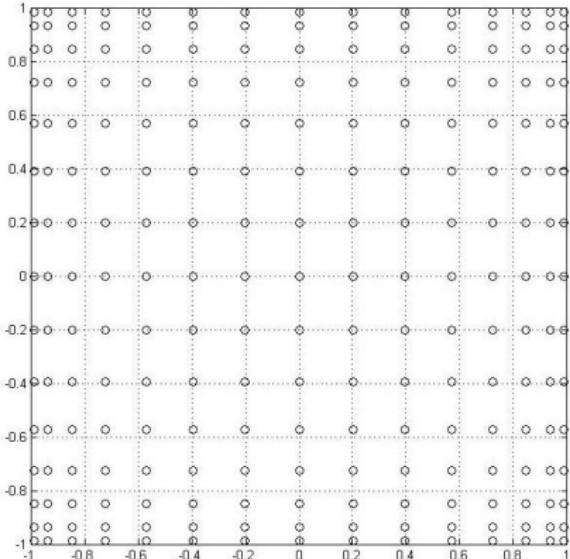
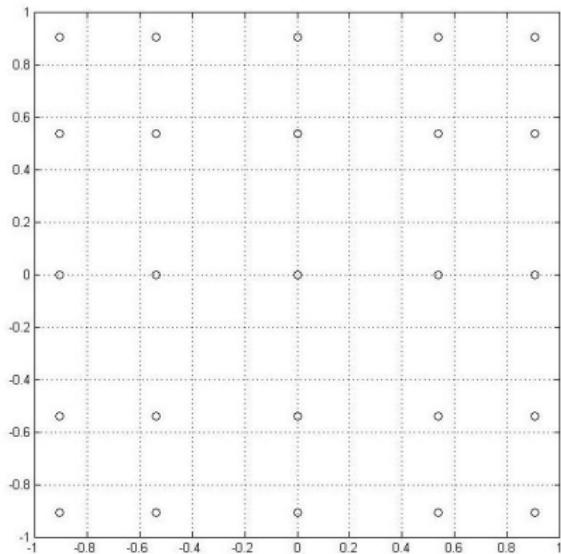
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GAUSS LEGENDRE PRODUCT RULE



We are looking for cubature points of uniform pdf with the following properties

- The sigma points have to satisfy the **moments of the uniform pdf.**
- All the weights to be **positive**.
- All the weights **sum upto 1**.
- All sigma points lie **within the hypercube**.
- All weights and sigma points have to be **real**.

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MOMENTS OF UNIFORM PDF

For a 1-D uniform pdf between -1 and 1, the moments are given by

$$\mu_n = E[x^n] = \frac{(2)^n + (-2)^n}{2^{(n+1)}(n+1)} \quad (27)$$

All odd moments are zero

For N-Dimensional moments, we can consider an i.i.d. space such that

$$E[x_1^{n_1}x_2^{n_2} \cdots x_m^{n_m}] = \mu_{n_1}\mu_{n_2} \cdots \mu_{n_m} \quad (28)$$

SIGMA POINTS TO CAPTURE 4TH ORDER MOMENTS OF UNIFORM DISTRIBUTION

For dimension $2 \leq N \leq 5$

- Choose principal axis and Nth-Conjugate axis
- Works only till 5-D after which some points go outside the cube
- This is also documented by Stroud in his paper. His work is mostly on symmetrical spherical regions.

Example integrating a 4th degree polynomial in 5D

	No. of pts	Integration result
CUT4-Uniform	42	7.5556
GL3	243	7.5556

SIGMA POINTS TO CAPTURE 6TH ORDER MOMENTS OF UNIFORM DISTRIBUTION

For dimension $N = 4$

- Choose principal axis ,2nd Conjugate Axis and Nth-Conjugate axis

Example integrating a 6th degree polynomial in 4D

	No. of pts	Integration result
CUT6-Uniform	57	15.2603
GL4	256	15.2603

UNDERSTANDING THE STRUCTURE OF GAUSS LEGENDRE PRODUCT RULE

For a 4D system the GL5 has the structure

TABLE: GL5 Structure

1	1	1	1
0.5942	1	1	1
0	1	1	1
0.5942	0.5942	1	1
0	0	1	1
0.5942	0.5942	0.5942	1
0	0.5942	0.5942	1
0	0	0.5942	1
0	0	0	1
0	0	0	0

TABLE: The generator set

1	1	1	1	r_1
h	1	1	1	r_2
0	1	1	1	r_3
p	q	1	1	r_4
0	0	1	1	r_5
r	s	t	1	r_6
0	k	m	1	r_7
0	0	a	1	r_8
0	0	0	1	r_9
0	0	0	0	r_{10}

COST FUNCTION

COST FUNCTION

How do we frame a cost function such that we have minimum points as possible while satisfying the moment equations.

MOMENT CONSTRAINTS

- The constraints have polynomial type nonlinearity
- The degree of the polynomials can be reduced by some substitutions
- Gradient based methods of optimization might fail.
- Polynomial solver might help (*Currently working on it*)
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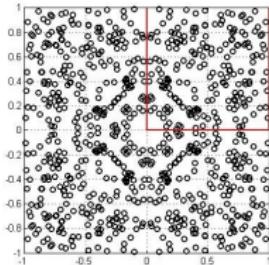
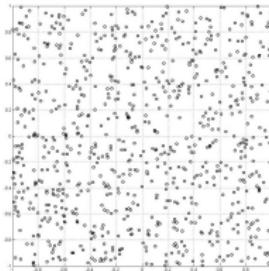
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RANDOM IDEA 1: A FULLY SYMMETRIC SAMPLE

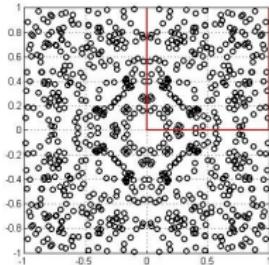
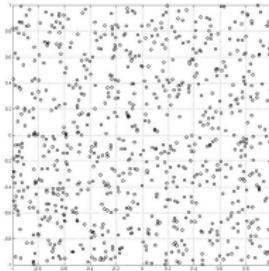
- Consider a 2 Dimensional square (-1,-1) to (1,1)
- Take a sample from the red square (0,0) to (1,1)
- make this sample fully symmetric



Moment	conv-rand-samp	Full-sym-rand-samp	True
$E[x_1^2]$	0.3407	0.3207	0.3333
$E[x_1x_2]$	0.0120	0	0
$E[x_2^2]$	0.3328	0.3207	0.3333
$E[x_1^4]$	0.2073	0.1830	0.2
$E[x_1^3x_2]$	0.0052	0	0
$E[x_1^2x_2^2]$	0.1139	0.1082	0.1111
$E[x_1x_2^3]$	0.0026	0	0
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Tot. samp	800	800	-

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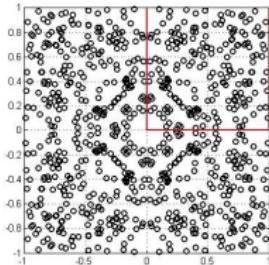
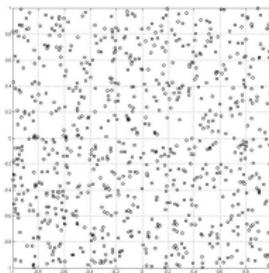
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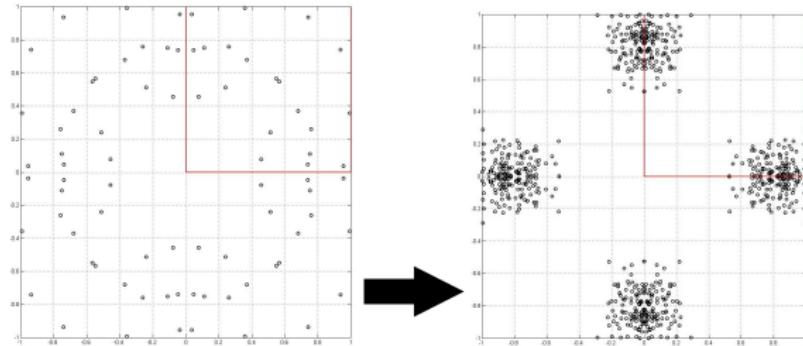
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A RANDOM IDEA 2:

Can we have an iterative process such that we can sample and then resample again with respect to the constraints.... **the samples might converge to the quadrature points**. Can we build such an Algorithm to *ESTIMATE the cubature points*



The samples in the second figure have the same 2nd moment as that of uniform pdf. I have created the samples from gaussian pdf centered about the exact cubature point.



University at Buffalo

The State University of New York

DISCUSSION

- Is there a better way to solve the fully nonlinear system of moment equations.
- How to find the minimal number of cubature points -or- to be optimistic how to prove that the cubature points by this method is minimal.
- Is it really advantageous to develop higher order methods from a filtering point of view. If the first approximation is dominantly wrong does it help in using higher order cubature points

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DISCUSSION

- How to identify the non-polynomial type of functions that can be integrated by these methods accurately, How do we develop Error estimates. For example for 1D Gauss Hermite quadrature the error estimate is $E = \frac{n! \sqrt{\pi}}{2^n (2n)!} f^{2n}(\xi)$
- How do we generalize this method or how do we find a mathematically rigorous theory/algorithm to generate cubature points for any moment and any dimension.
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