Introduction To Robotics

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September 4, 2024

Contents

Part I

Robotics

Textbook

Chapter 1

Unit 1

1.1 Introduction

This course is mainly going to focus on **Manipulators**. These machines are used to manipulate positions and the state of the objects in an environment. We're going to break down their movements into Dynamics Analysis akin to the work done in Computational Mechanics.

1.2 Syllabus

- Overview Of Robotics
- Kinematics Of Simple Robotic Systems
- Dynamics And Control Of Simple Robotic Systems

1.3 Glossary

1. Actuator - Does work upon receiving voltage
2. Encoder - Sensor that measures raw angle data.

Software for robotics - **v-rep**, MATLAB This software involves making a CAD model, and apply a mathematical model. Unity can also be used in making such models.

1.4 Degree Of Freedom

The degree of freedom of a mechanical system is defined as the no. of independent paramets need to completely define its position in space at a given time..

The degree of freedom is defined with respect to a reference frame. If the object is free to rotate and move, it means it has 6 degrees of freedom. Localization - Finding the position and orientation of an object in 3-dimensional space.

We call a system 'fully actuated' when there are as many actuators as there are degrees of freedom.

$$\text{No. of controlling inputs} < \text{No. of degrees of freedom}$$

Underactuated systems contain lesser actuators than the number of degrees of freedom

$$\text{No. of controlling inputs} = \text{No. of degrees of freedom}$$

Redundant systems contain more actuators than the number of degrees of freedom

$$\text{No. of controlling inputs} > \text{No. of degrees of freedom}$$

1.5 Kinematic Pair

Linkages are the basic elements of all mechanisms and robots. Links are rigid body member with nodes, and joints are connection between links at nodes. Allows relative motion between links.

1.6 Robotic Manipulator

- Why study kinematics and dynamics of robotic manipulator
  - To manipulate an object in space
  - Understand the workspace and limitations of a robotic manipulator
  - Understand and estimate contact force between end-effector and object being manipulated.

1.7 Pose of a rigid body

A rigid body is completely defined in space by its position and orientation with respect to a reference.

We use the terminology 'Inertial reference frame' to mean an observer where Newton's laws of physics apply. We use the terminology 'Inertial reference frame' to mean an observer where Newton's laws of physics apply and the frame itself does not accelerate. Generally the base of the robotic manipulator is treated as the inertial reference frame

We use unit vectors $\hat{x}, \hat{y}, \hat{z}$ to describe the basis vectors. For the orientation of the rigid body, since they lie in 3d space, we must define new basis vectors to define the orientation, $\hat{x'}, \hat{y'}, \hat{z'}$

$$\hat{x'} = x'_x\hat{x} + x'_y\hat{y} + x'_z\hat{z}$$

$$\hat{y'} = y'_x\hat{x} + y'_y\hat{y} + y'_z\hat{z}$$

$$\hat{z'} = z'_x\hat{x} + z'_y\hat{y} + z'_z\hat{z}$$

1. When the frame is translationally different from the original frame.

$$^{A}\vec{P} = {}^{B}\vec{P} + {}^{A}\vec{P}_{Borg}$$

   Where $^{A}\vec{P}$ is the position vector of P with respect to A, $^{B}\vec{P}$ is the position vector of P with respect to B, and $^{A}\vec{P}_{Borg}$ is the vector of A to B.

2. When the frame is oriented differently from the original frame. Generating a rotation matrix $^{B}_{A}R$ to rotate vectors from a frame B to A. Where A and B are reference frames, with B being oriented differently than A.

$$\begin{bmatrix} \hat{X}_b \cdot \hat{X}_a & \hat{Y}_b \cdot \hat{X}_a & \hat{Z}_b \cdot \hat{X}_a \\ \hat{X}_b \cdot \hat{Y}_a & \hat{Y}_b \cdot \hat{Y}_a & \hat{Z}_b \cdot \hat{Y}_a \\ \hat{X}_b \cdot \hat{Z}_a & \hat{Y}_b \cdot \hat{Z}_a & \hat{Z}_b \cdot \hat{Z}_a \end{bmatrix}$$

   We can simply the matrix into 3 column vectors, with the notation $^{A}X_B$ which means B with respect to A

$$\begin{bmatrix} ^{A}\hat{X}_B & ^{A}\hat{Y}_b & ^{A}\hat{Z}_B \end{bmatrix}$$

3. When the frame is both translationally and oriented different from the original frame

$$^{A}\vec{P} =^{A}_{B} R^{B}\vec{P} +^{A} \vec{P}_{Borg}$$

To simplify the equations, we write.

$$^{A}\vec{P} =^{A}_{B} T^{B}P$$

Where T becomes

$$^{A}_{B}T = \begin{bmatrix} ^{A}_{B}R_{3\times 3} & ^{A}P_{Borg} \\ 0_{1\times 3} & 1_{1\times 1} \end{bmatrix}$$

This T is the homogeneous transformation matrix.

The Rotation Matrix belongs to a category of matrices called $SO(3)$(Special Orthogonal Matrices)

1.8 Denavit Hartenberg Parameters

These parameters are used to assign the same co-ordinate frames while dealing with robotic manipulators to ensure that the entire scientific community are working under the same conventions.

- Number the link sequentially from 0 to n. Giving us $n+1$ links.
- Number the joints sequentially from 1 to n, Giving us n joints.
- Number of co-ordinate frames: $n+1$
- The Z_i axis is aligned with the $(i+1)^th$ joint axis.
- X_i is defined along the common normal between the Z_i and Z_{i-1} axis.(Common normal is the line which is perpendicular to both of these axes.)
- Y_i is obtained via cross product between Z_i and X_i axis.
- The origin is placed at this point of intersection of x_i, y_i and z_i
- We define H_i(which is the point of intersection of the common normal of the next axis with the current axis.), and 4 new terms:
  - a_i - Offset distance between two adjacent joint axes(The distance between O_i and H_{i-1})
  - d_i - Distance between H_{i-1} and O_{i-1}
  - α_i Angle between Z_i and Z_{i-1} when viewed from X_i, this is also known as the twist angle.
  - θ_i Angle between X_i and X_{i-1} when viewed from Z_i,

For a 3R Planar serial chain manipulator:

	a_i	d_i	α_i	θ_i
Joint i = 1	L_1	0	0	θ_1
Joint i = 2	L_2	0	0	θ_2
Joint i = 3	L_3	0	0	θ_3

1.9 Rotation Matrix

We have three reference frames, with a common origin. With the notation we have setup we can say, $\{0\}, \{1\}, \{2\}$ can be defined for a point P

$$
\begin{aligned}
{}^0P &=^0_1 R^1P \\
{}^0P &=^0_2 R^2P \\
{}^1P &=^1_2 R^2P \\
{}^0_2R &=^0_1 R^1_2R
\end{aligned}
$$

1.10 Derivation Using DH Parameters

These 4 parameters can be expressed by,

$$
{}^{i-1}A_i = T(z, d)T(z, \Theta), T(x, \alpha), T(x, a)
$$

1.11 Skew Symmetric Matrix

A matrix such that $A = -A^T$

So this means that,

$$
S + S^T = 0
$$

$$
\vec{a} = a_x\hat{i} + \vec{a_y}\hat{j}\vec{a_z}\hat{k}
$$

We define a matrix function,

$$
S(\vec{a}) = \begin{bmatrix} 0 & -a_z & a_y \\ a_z & 0 & -a_x \\ -a_y & a_x 0 & \end{bmatrix}
$$

So we can say for the basis vectors

$$
S(\hat{i}) = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & -1 \\ 0 & 1 & 0 \end{bmatrix}
$$

$$
S(\hat{j}) = \begin{bmatrix} 0 & 0 & 1 & \\ 0 & 0 & 0 & \\ -1 & 0 & 0dt & i0 \end{bmatrix}
$$

$$
S(\hat{k}) = \begin{bmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}
$$

Multiplying the matrix function's output with a vector is the same as doing a cross product with those two vectors.

$$S(\vec{a})P = \vec{a} \times \vec{p}$$

This matrix operation also has linearity in operations.

$$S(\alpha\vec{a} + \beta\vec{b})P = \alpha S(\vec{a}) + \beta S(\vec{b})$$

When multiplied with a rotation matrix.

$${}^{a}_{b}RS(\vec{a}){}^{a}_{b}R^{T} = S({}^{a}_{b}R\vec{a})$$

We know that,

$$\begin{aligned} RR^T &= I \\ R(\theta)R^t(\theta) &= I \\ \text{Taking the derivative} \\ \frac{dR(\theta)}{d\theta}R^T(\theta) + R(\theta)\frac{dR^T(\theta)}{d\theta} &= 0 \\ \frac{dR(\theta)}{d\theta}R^T(\theta) + R(\theta)\left(\frac{dR^T(\theta)}{d\theta}\right)^T &= 0 \end{aligned}$$

What this means is that the term $\frac{dR(\theta)}{d\theta}R^T(\theta)$ is a skew-symmetric matrix.
This means that the the term can be written as S,

$$S = \frac{dR(\theta)}{d\theta}R^T(\theta)$$

In other words, S becomes an operator on R to give us the derivative.

$$S(\hat{k})R(\theta) = \frac{dR(\theta)}{d\theta}$$

Taking both sides with respect to time,

$$\frac{dR(\theta)}{d\theta}\frac{d\theta}{dt} = \dot{\theta}S(\hat{k})R(\theta)$$

In other words,

$$\dot{R} = S(\dot{\theta}\hat{k})R(\theta)$$

So we have,

$$\dot{R} = S(\vec{\omega})R(\theta)$$

$$S(\vec{\omega}) = \begin{bmatrix} 0 & -\omega_z & \omega_y \\ \omega_z & 0 & -\omega_x \\ \omega_y & \omega_x & 0 \end{bmatrix}$$

$$\Omega = \begin{bmatrix} 0 & -\omega_z & \omega_y \\ \omega_z & 0 & -\omega_x \\ \omega_y & \omega_x & 0 \end{bmatrix}$$

$$
\begin{aligned}
{}^0P &=^0_1 R^1P \\
{}^0P &= R^1P \\
{}^0\dot{P} &= \dot{R}^1P + R^1\dot{P} \\
{}^0\dot{P} &= S(\vec{\omega})R^1P \\
{}^0\dot{P} &= \omega \times R^1\vec{p} \\
{}^0\dot{P} &= \omega \times R^1\vec{p} \\
\vec{v} &= \vec{\omega} \times \vec{r}
\end{aligned}
$$

Chapter 2

Unit 2 - Kinematics Of Robotic Manipulators

2.1 Forward And Inverse Kinematics

Forward kinematics is the use of the joint space to get to the task space. Inverse Kinematics is the use of the task space to get to the joint space.

Workspace - The space of all points that the end effector can reach.

2.2 Inverse Kinematics Of 2R Planar Structures

We solve for q_2 and eliminate q_1

2L$_1 L_2$

We have two cases,
Case 1: $-1 < \kappa < 1$ We have two distinct and real solutions of q_2
Case 2: $|\kappa| = 1$ We have one solution
Case 3: $|\kappa| < 1$ No solution exists

2.3 Forward Kinematics And Inverse Kinematics Of 3R Planar Structures

$$X_e = L_1 \cos q_1 + L_2 \cos(q_1 + q_2) + L_3 cos(q_1 + q_2 + q_3)$$

For a 3R Planar structure, the way to find the forward kinematics is straightforward.

What we get for the inverse kinematics is with 3 knowns, ${}^0X_e, {}^0Y_e, \phi$ where ($\phi = q_1 + q_2 + q_3$) we reduce the problem down to ${}^0X_2, {}^0Y_2$ by finding,

$$ {}^0X_e - L_3 \cos\phi = L_1 \cos q_1 + L_2 \cos q_{12}$$
$$ {}^0Y_e - L_3 \sin\phi = L_1 \sin q_1 + L_2 \sin q_{12}$$

Now we know that those terms are nothing but

$$
\begin{aligned}
{}^0X_2 &= L_1 \cos q_1 + L_2 \cos q_{12} \\
{}^0Y_2 &= L_1 \sin q_1 + L_2 \sin q_{12}
\end{aligned}
$$

Which we can solve the same as the 2R Planar Structure

2.4 Jacobian Forward Kinematics

Given $\dot{q_1}, \dot{q_2}$, how do we get ${}^0X_e, {}^0Y_e$? and similarly how do we get the angular velocities of a machine from the end effector's velocity.

We know that for 2R Planar SCMs,

$$
\begin{aligned}
{}^0X_e &= L_1cq_1 + L_2c(q_1+q_2) \\
{}^0Y_e &= L_1sq_1 + L_2s(q_1+q_2) \\
{}^0\dot{X}_e &= -\dot{q_1}L_1sq_1 - L_2s(q_1+q_2) \times (\dot{q_1}+\dot{q_2}) \\
{}^0\dot{Y}_e &= +\dot{q_1}L_1cq_1 + L_2c(q_1+q_2) \times (\dot{q_1}+\dot{q_2})
\end{aligned}
$$

We have,

$$\dot{X}_{2\times1} = J_{2\times2} \times \dot{q}_{2\times1}$$

We now have this for a specific case, when we generalize,

$$\dot{X} = \begin{bmatrix} {}^0_nv \\ \\ {}^0_n\omega \end{bmatrix} = J\dot{q}$$

So now we can write the term

$${}^0_n\omega = \sum_{i=1}^{n} \dot{\theta}_i z$$

2.5 Lab Questions

1. Consider the 3R Planar SCM with $L_1 = 2m$, $L_2 = 3m, L_3 = 4m$

Forward Kinematics, Find the co-ordinates of the end-effector in the base frame:

1. For $q = [q_1q_2q_3]^T = [30\deg 45\deg 60\deg]^T$
2. For $q = [q_1q_2q_3]^T = [270\deg 75\deg 10\deg]^T$

Inverse kinematics, Find the joint space variables,

1. For $\phi = q_1+q_2+q_3 = 0$ and $[{}^0X_e, {}^0Y_e] = [2,4]$
2. For $\phi = q_1+q_2+q_3 = 45$ and $[{}^0X_e, {}^0Y_e] = [5,5]$

1.

Part II

Practice Sheets

Practice Sheet 1 The notations used in our lectures are similar with this book.

- For Rotation Matrices, Pose of a rigid body, Euler Angles, Homogeneous Transformation —> read Chapter 2
- For DH Parameters and Coordinate Convention —> read Chapter 3, Sections 3.1 to 3.4