

# EN2110 - Electronics III

## Lecture 5 - Semiconductor Devices

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# Power Semiconductor Devices

# Challenges

- Challenges in power semiconductor device design are,
  - ① Obtaining a high breakdown voltage
  - ② Low forward voltage drop
  - ③ Low on-resistance
- Challenge is longer switching times of high-voltage, low-on-resistance devices
- The breakdown voltage of a reverse-biased p-n junction is a function of doping level
  - ① High breakdown voltage is obtained by low doping concentration and lengthy drift region
  - ② Hence, higher on-resistance
- In majority carrier devices (MOSFET and Schottky diode) - first-order relationship between ON-resistance and rated voltage
- In minority carrier devices (p-n diode, BJT, IGBT, and thyristor family) - conductivity modulation

# Conductivity Modulation

- When a minority-carrier device is at ON-state
  - ① Minority carriers are injected into the lightly doped drift region by the forward-biased p-n junction
  - ② High minority carrier concentration effectively reduces apparent resistivity of the region
- Minority-carrier devices exhibit lower ON-resistances than comparable majority-carrier devices
- But carrier injection gives rise reduced switching speed
  - ① Conducting state of semiconductor device is controlled by the presence or absence of key charge quantities within the device
  - ② Turn-ON and turn-OFF switching times are equal to the times required to insert or remove this controlling charge
  - ③ Minority-carrier devices exhibit significantly longer switching times
- Majority-carrier devices - low voltage + high switching frequency applications
- Minority-carrier devices - high voltage + low switching frequency applications

# Power Diode - Introduction

- Power diode consists of three layers instead of two layers in low power diodes
  - ➊ Heavily doped  $n$ -type substrate - Cathode
  - ➋ Lightly doped  $n^-$  epitaxial layer - Drift region (cannot be found in low power diodes)
  - ➌ Heavily doped  $p$ -type layer - Anode
- Drift region thickness - depends on breakdown voltage
- Cross-sectional area - depends on the total device current

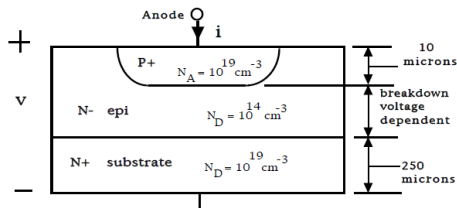
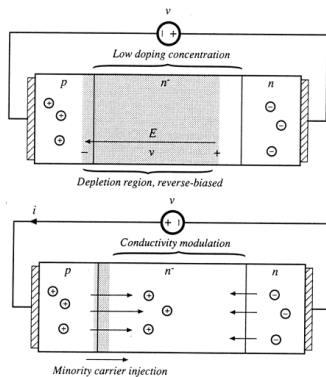


Figure: Cross section of a power diode

# Power Diode - Basic Operation



**Figure:** Power diode under reverse and forward biased states

- Applied voltage appears across the depletion region inside the  $n^-$  region under reverse-biased conditions
- Holes are injected across the forward-biased junction, and become minority carriers in the  $n^-$  region
- Effectively reduce the apparent resistivity of the  $n^-$  region via conductivity modulation
- Forward current  $i(t)$  is comprised of,
  - 1 Holes that diffuse across the  $p - n$  region and then recombine with electrons from the  $n$  region

# Power Diode Symbol, Characteristics and Packages

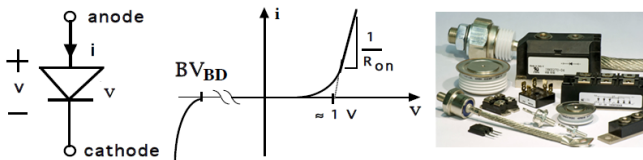


Figure: Power diode symbol, characteristics and packages

- Current grows linearly rather than exponentially
- Large current create ohmic drop that mask diode exponential characteristics
- This voltage drop across lightly doped drift region
- There is small leakage current until reverse biased voltage reach breakdown voltage ( $BV_{BD}$ )
- After  $BV_{BD}$ , current increase dramatically and it is limited by external circuit
- Excessive power dissipation may quickly destroy diode

# Power Diode - Switching Characteristics

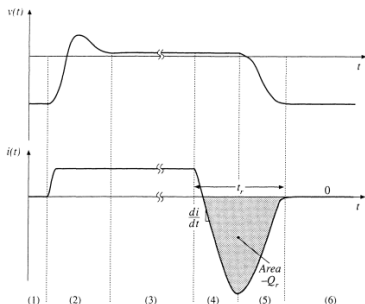


Figure: Voltage and current waveforms of a power diode

- During transients, significant deviations from the exponential characteristic are observed
- These deviations are associated with changes in the stored minority charge
- *Interval – 1*
  - ❶ Zero current and negative voltage (Maximum will be diode PIV)



# Switching Characteristics

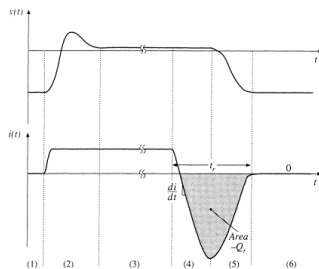


Figure: Voltage and current waveforms of a power diode

## Interval – 2

- ➊ Increasing current charges the effective capacitance of the reverse-biased diode
- ➋ Supplying charge to the depletion region and increasing the voltage  $v(t)$
- ➌ The voltage becomes positive, and the diode junction becomes forward-biased
- ➍ Voltage may rise to a peak value of several volts reflecting the somewhat large resistance of the lightly doped  $n^-$  region

# Switching Characteristics - Turn-OFF transient

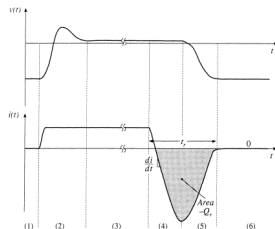


Figure: Voltage and current waveforms of a power diode

## Interval – 2

- ① Forward-biased  $pn^-$  junction continues to inject minority charge into the  $n^-$  region
- ② Conductivity modulation of the  $n^-$  region causes its effective resistance to decrease, and hence the forward voltage drop  $v(t)$  also decreases

- Diode become equilibrium - minority carrier injection rate and recombination rate are equal

## Interval – 3

- ① Diode operates in the ON state and forward voltage drop is given by the diode static  $I - V$  characteristics

# Switching Characteristics

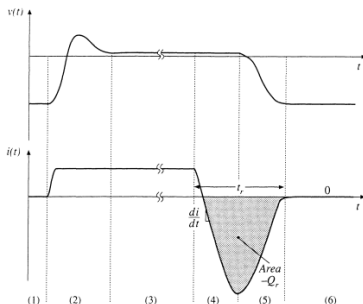


Figure: Voltage and current waveforms of a power diode

- Interval – 4

- ➊ Diode remains forward-biased while minority charge is present in the vicinity of the diode  $pn^-$  junction
- ➋ Stored minority charge is reduced by negative terminal current and by recombination
- ➌ At the end, stored minority charge has been removed and diode junction becomes reverse-biased

# Switching Characteristics

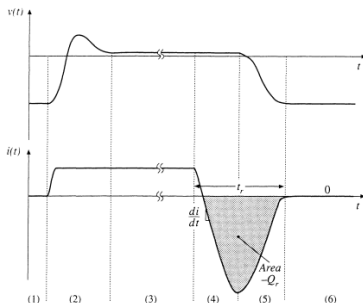


Figure: Voltage and current waveforms of a power diode

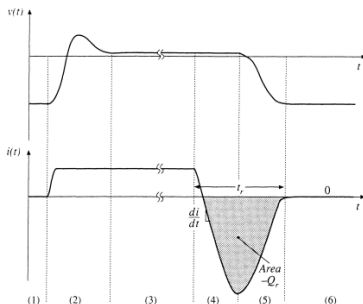
- Interval – 5

- ① Depletion region effective capacitance is then charged
- ② At the end of this period diode is able to block the entire applied reverse voltage

- Interval – 6

- ① Diode operates in the off state

# Switching Characteristics - Reverse Recovery



**Figure:** Voltage and current waveforms of a power diode

- Charge  $Q_r$  is called the recovered charge
- Portion of  $Q_r$  occurring during *interval* – 4 is actively removed minority charge
- Portion of  $Q_r$  occurring during *interval* – 5 is charge supplied to the depletion region
- Length of intervals 4 and 5 is called the *reverse recovery time* ( $t_{rr}$ )

# Diode Types - Based on $t_{rr}$

- Standard recovery
  - ① Reverse recovery time usually not specified
  - ② Use in  $50Hz$  and  $60Hz$  applications
- Fast recovery and ultra fast recovery
  - ① Reverse recovery time  $t_{rr}$  and recovered charge  $Q_r$  are specified by manufacturers
  - ② Fast recovery -  $nS$  to  $\mu S$
  - ③ Ultra fast recovery - Few  $nS$

# Power Diode - Parallel Operation

- Temperature coefficient of on-resistance and forward voltage drop of power semiconductor device play key role
- Diodes cannot be easily connected in parallel, because of their negative temperature coefficients
- Imbalance in device characteristics may cause one diode to conduct more current than the others
- Then that diode becomes hotter, which causes it to conduct even more of the total current
- Current does not divide evenly between the paralleled devices
- Current rating of one of the devices may be exceeded

# MOSFET



# Power Semiconductor Devices - MOSFET

- The power MOSFET is comprised of many small parallel-connected enhancement-mode MOSFET cells
- A cross-section of one cell is illustrated in figure

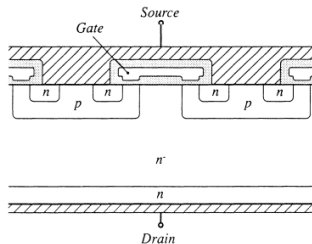


Figure: Cross section of power MOSFET

- Current flows vertically through the silicon wafer:
- The metallized drain connection is made on the bottom of the chip
- The metallized source connection and polysilicon gate are on the top surface

# MOSFET - OFF state Operation

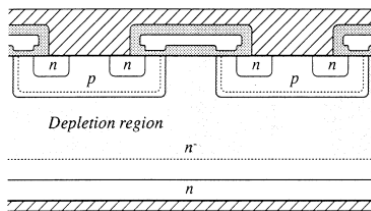


Figure: MOSFET operation when  $V_{DS} \geq 0$

- Both the  $pn$  and  $pn^-$  junctions are reverse-biased
- The applied drain-to-source voltage then appears across the depletion region of the  $pn^-$  junction
- The  $n^-$  region is lightly doped, such that the desired breakdown voltage rating is attained
- As the breakdown voltage is increased, the on-resistance becomes dominated by the resistance of the  $n^-$  region
- ON-resistance increases rapidly as there are no minority carriers to cause conductivity modulation

# MOSFET - ON state Operation

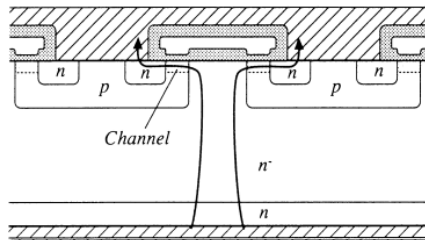


Figure: MOSFET operation when at ON state

- Sufficiently large positive gate-to-source voltage need to be applied
- A channel then forms at the surface of the  $p$  region, underneath the gate
- The drain current flows through the  $n^-$  region, channel,  $n$  region, and out through the source contact
- The on-resistance of the device is the sum of the resistances of the  $n$  region, the channel, the source and drain contacts

# MOSFET - Body Diode

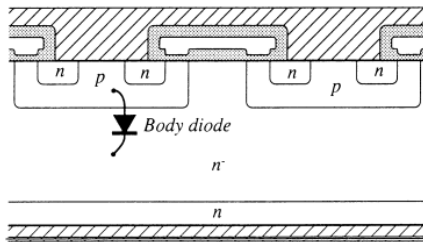


Figure: Formation of body diode

- The  $pn^-$  forms an effective diode in parallel with the MOSFET channel
- The body diode can become forward-biased when the drain-to-source voltage  $v_{DS}(t)$  is negative
- MOSFETs are not optimized with respect to the speed of their body diodes although they are capable to conduct total MOSFET current
- The large peak currents that flow during the reverse recovery transition of the body diode can cause device failure

# MOSFET - Static Characteristics

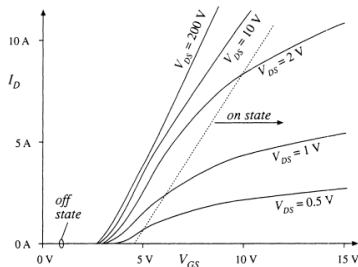


Figure: Static output characteristics of MOSFET

- The device operates in the OFF state when the gate-to-source voltage is less than the threshold voltage  $V_{th}$  (around 3V)
- When the gate-to-source voltage greater than 6 or 7 V, the device operates in the ON state
- The gate is driven to 12 or 15 V to ensure minimization of the forward voltage drop
- In the on state,  $V_{DS}$  roughly proportional to the  $I_D$

# MOSFET - Capacitances

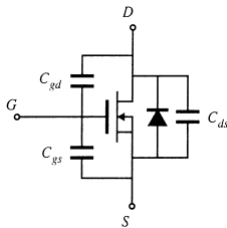


Figure: Equivalent MOSFET with body diode and capacitances

- The major capacitances of the MOSFET are illustrated
- Switching times of the MOSFET are determined by the times required for the gate driver to charge and discharge these capacitances

- The rate at which the drain current changes is dependent on the rate at which the gate-to-source capacitance is charged by the gate drive circuit
- The rate at which the drain voltage changes is a function of the rate at which the gate-to-drain capacitance is charged
- The drain-to-source capacitance leads directly to switching loss in PWM converters
- energy stored in this capacitance is lost during the transistor turn-on transition

# MOSFET - Characteristics of Capacitances

- The gate-to-source capacitance is essentially linear
- The drain-to-source and gate-to-drain capacitances are strongly nonlinear
- The incremental drain-to-source capacitance can be written as

$$C_{DS}(V_{DS}) = \frac{C_o}{\sqrt{1 + \frac{V_{DS}}{V_o}}}$$

- Where  $C_o$  and  $V_o$  are constants that depend on the construction of the device
- These capacitances can easily vary by several orders of magnitude as  $V_{DS}$  varies over its normal operating range
- For  $V_{DS} \gg V_o$

$$C_{DS}(V_{DS}) \approx C_o \sqrt{\frac{V_o}{V_{DS}}} = \frac{C'_o}{\sqrt{v_{DS}}}$$

# MOSFET - Selection

- The gate charge ( $Q_g$ )
  - ① The gate charge ( $Q_g$ ) is the charge that the gate drive circuit must supply to the MOSFET to raise the gate voltage from zero to some specified value
  - ② At a specified value of off state drain-to-source voltage - typically 80% of the rated  $V_{DS}$
  - ③ The total gate charge is the sum of the charges on the gate-to-drain and the gate-to-source capacitances
  - ④ The total gate charge is a measure of switching speed of the MOSFET
- ON-resistance
  - ① Conduction loss are the limiting factors
  - ② MOSFETs may be operated at average currents somewhat less than the rated value
- MOSFETs are usually the device of choice at voltages less than or equal to approximately 400 to 500 V
- Used for high switching speed applications
- But with high ON-state losses compared to minority carrier devices



# Bipolar Junction Transistor (BJT)

# BJT - Internal Structure

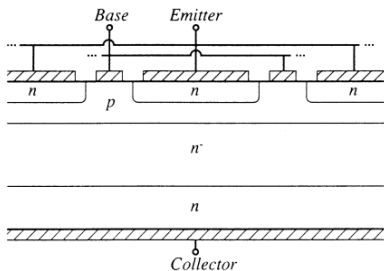


Figure: Cross section of NPN power BJT

- Current flows vertically through the silicon wafer
- A lightly doped  $n^-$  region - to obtain the desired voltage breakdown rating
- OFF-state operation
  - 1 Both  $pn$  BE junction and the  $pn^-$  BC junctions are reverse-biased
  - 2 The applied collector-emitter voltage then appears essentially across the depletion region of the  $pn^-$  junction

# BJT - Operation

- ON-state operation
  - ① Both junctions are forward-biased
  - ② substantial minority charge is then present in the  $p$  and  $n^-$  regions
  - ③ This minority charge causes the  $n^-$  region to exhibit a low on-resistance via the conductivity modulation effect
- Active region
  - ①  $pn$  BE junction is forward-biased and the  $pn^-$  BC junction is reverse-biased
  - ② The  $I_C$  is proportional to the base region minority charge, which in turn is proportional (in equilibrium) to the  $I_B$
- Quasi-saturation
  - ① Quasi-saturation occurs when the  $I_B$  is insufficient to fully saturate the device
  - ② The minority charge present in the  $n^-$  region is insufficient to fully reduce the on-resistance

# BJT - Switching Waveforms

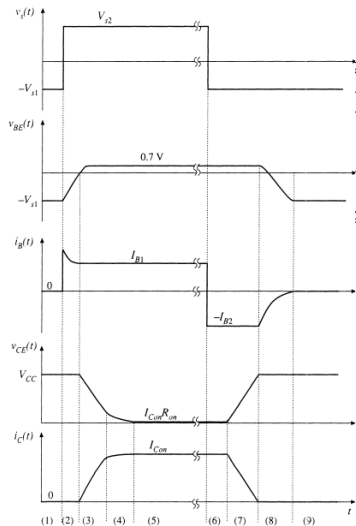


Figure: Switching waveforms

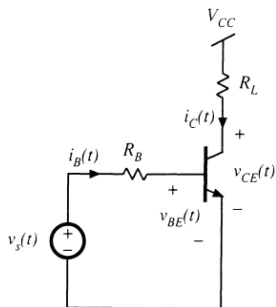
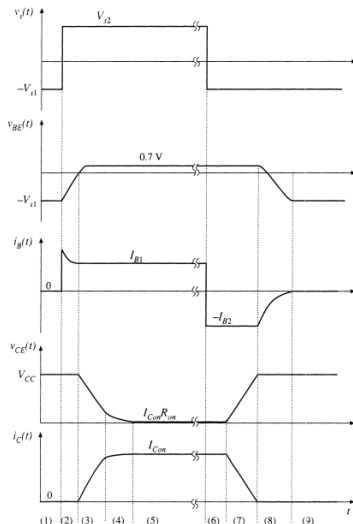


Figure: Power BJT in circuit

- Turn-ON and OFF waveforms of power BJT are shown in figure

# BJT - Switching Waveforms



## Interval 1

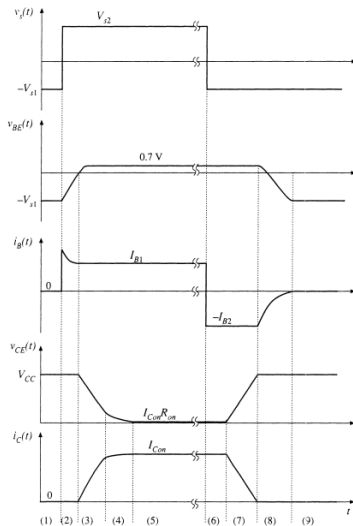
- ① The transistor operates in the off state
- ② The BE junction is reverse biased by the  $v_s(t) = -V_{s1}$

## Interval 2

- ① Turn-ON transition is initiated at the beginning of this interval
- ② Positive current is supplied by source  $v_s$
- ③ This current charges the capacitances of the depletion regions of the reverse biased BE and BC junctions
- ④ BE voltage exceeds zero sufficiently for the BE junction to become forward biased

Figure: Switching waveforms

# BJT - Switching Waveforms



## Interval 3

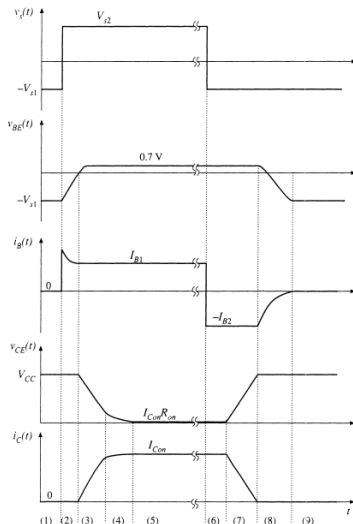
- ➊ Minority charge is injected across the base-emitter junction from the emitter into the base region
- ➋ Collector current is proportional to this minority base charge
- ➌ Decrease in collector voltage, reduce voltage across the reverse-biased BC depletion region (Miller) capacitance
- ➍ Turn-ON time can be reduced by reducing  $R_B$  or increasing  $v_s(t)$  due to increase of  $I_B$

## Interval 4

- ➊ BC  $pn^-$  junction becomes forward biased and minority carriers are then injected into the  $n^-$  region
- ➋ Apparent resistance of the  $n^-$  region decreases via conductivity modulation

Figure: Switching waveforms

# BJT - Switching Waveforms



## Interval 5

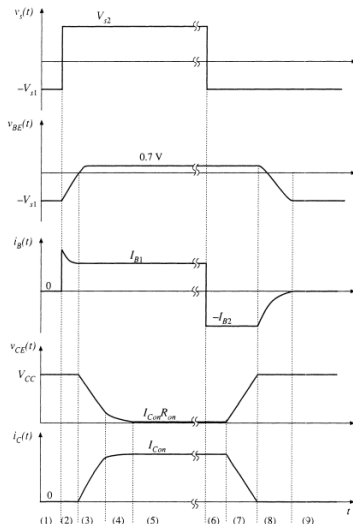
- ① Reaches on state equilibrium at the beginning of this interval

## Interval 6

- ① Turn-OFF process is initiated when the source voltage changes to  $v_s(t) = -V_{s1}$
- ② The BE junction remains forward biased as long as minority carriers are present in its vicinity
- ③  $I_C$  continues to be  $i_c(t) = I_{C,on}$  as long as the minority charge exceeds the amount necessary to support the active region conduction of  $I_{C,on}$
- ④ Negative base current actively removes the total stored minority charge
- ⑤ Recombination further reduces the stored minority charge
- ⑥ Length of this period is called as *storage time*

Figure: Switching waveforms

# BJT - Switching Waveforms



## Interval 7

- ① The collector current  $i_c(t)$  is now proportional to the stored minority charge
- ② The collector current decreases due to recombination and the negative base current
- ③  $I_B$  must charge the Miller capacitance and increase collector voltage

## Interval 8

- ① Reverse-biased base-emitter junction capacitance is discharged to voltage  $-V_{s1}$ ,

Figure: Switching waveforms



# Base Drive Current

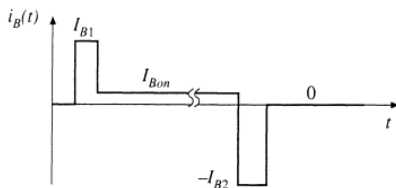


Figure: Base drive current

- It is possible to turn-OFF the transistor using  $I_{B2} = 0$
- This leads to very long storage and turn-off switching times (stored minority charge must be removed passively, via recombination)
- Initial  $I_{B1}$  is large in magnitude - charge is inserted quickly into the base, and the turn-ON switching times are short
- ON state current  $I_{Bon}$  is chosen, to yield a reasonably low CE forward voltage drop
- Turn-OFF switching times are minimized by large  $-I_{B2}$  that charge is removed quickly from the base

# Second Break Down

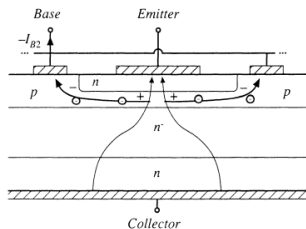


Figure: Second break down

- The lateral base current through the  $p$  region leads to a voltage drop in  $p$  material
- Turn-OFF instance
  - ① Base-emitter junction voltage to be greater in the center of the base region
  - ② Collector current to focus near the center of the base region
- Turn-ON instance
  - ① Collector current to crowd near the edges of the base region
- Hot spots are induced at the center or edge of the base region due to
  - ① CE voltage and  $I_C$  are simultaneously large during the switching transitions

# IGBT

# Introduction

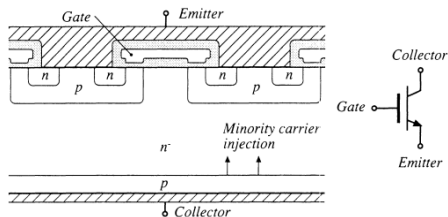


Figure: IGBT cross section

- Crosshatched regions are metallized contact and shaded regions are insulating silicon dioxide layers
- IGBT is a four-layer power semiconductor device having a MOS gate
- The function of the added  $p$  region is to inject minority charges into the  $n^-$  region while the device operates in the ON state
- The  $pn^-$  junction is forward-biased, and the minority charges injected into the  $n^-$  region cause conductivity modulation when IGBT conducts
- The forward voltage drops of these devices are typically 2 to 4V

# Equivalent Circuit

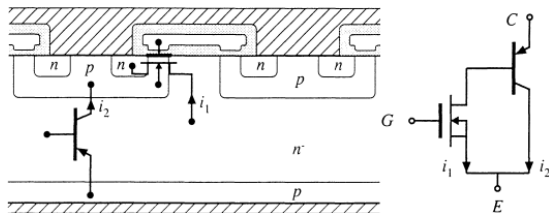


Figure: IGBT equivalent circuit

- The IGBT functions effectively as cascaded,
  - ① n-channel power MOSFET
  - ② PNP emitter-follower BJT
- Hence, there are two effective currents
- The price paid for the reduced voltage drop of the IGBT is its increased switching times

# Current Tailing

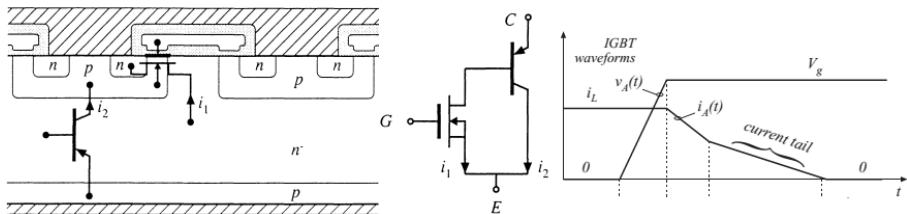


Figure: IGBT current tailing

- The effective MOSFET can be turned off quickly - by removing the gate charge
- This causes the channel current  $i_1$  to quickly become zero
- The PNP collector current  $i_2$  continues to flow as long as minority charge is present in the  $n^-$  region
- No way to actively remove the stored minority charge other than recombination
- The switching frequencies of PWM converters containing IGBTs are typically in the range 1 to 30kHz.

# IGBT - More Info

- $pn^-$  junction of the IGBT is not normally designed to block significant voltage
- Hence, IGBT has negligible reverse voltage-blocking capability
- IGBT ON resistance has positive temperature coefficient
- IGBTs can be easily connected in parallel, with a modest current derating
- Large modules are commercially available, containing multiple parallel-connected chips

# Silicon Controlled Rectifier (SCR)



# Introduction

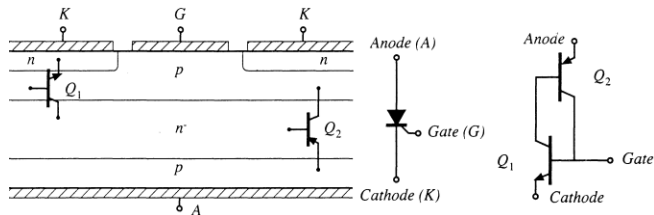


Figure: SCR cross section, symbol and equivalent circuit

- Silicon-controlled rectifier (SCR) is the oldest among conventional semiconductor power devices
- Devices having voltage ratings of 5000 to 7000 V and current ratings of several thousand amperes are available
- Four layer device
- Effective transistor  $Q_1$  is composed of the  $n$ ,  $p$ , and  $n^-$  regions, while effective transistor  $Q_2$  is composed of the  $p$ ,  $n^-$ , and  $p$  regions

# SCR Operation

- SCR can enter the on state when the applied  $v_{AK}$  is positive
- Positive gate current  $i_G$  causes  $Q_1$  to turn-ON
- This in turn supplies base current to  $Q_2$ , and causes it to turn-ON
- Effective connections of the base and collector regions of transistors  $Q_1$  and  $Q_2$  constitute a positive feedback loop
- Currents of the transistors will increase regeneratively
- Minority carriers are injected into all four regions, and the resulting conductivity modulation leads to very low forward voltage drop
- SCR cannot be turned off except by application of negative anode current or negative anode-to-cathode voltage
- During the turn-OFF transition, the rate at which forward anode to cathode voltage is reapplied must be limited, to avoid re triggering the SCR
- During turn-OFF time minority stored charge is
  - ① Actively removed via negative anode current
  - ② Recombination

# SCR Characteristics

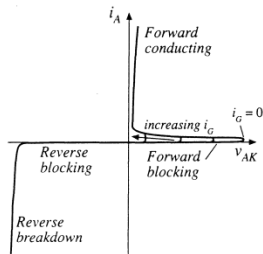


Figure: Characteristics curve

- The device is capable of blocking both positive and negative anode to cathode voltages
- One of the  $pn^-$  junctions is reverse-biased depending on applied voltage
- Depletion region extends into the lightly doped  $n^-$  region
- SCR is a voltage-bidirectional two quadrant switch
- The turn-ON transition is controlled actively via the gate current
- The turn-OFF transition is passive