

Arterial Vascular Impedance Calculation

AIM: To calculate Arterial Vascular Impedance, $Z[k] = \frac{P[k]}{Q[k]}$, where P is intra-arterial pressure (in mmHg) and Q is blood volume-flow (in ml/s).

Currently, the data (1,2,3) can be collected simultaneously using CMCdaq without any time- synchronization issue.

STEP1: The following are the data collected simultaneously:

1. Intra-arterial pressure ($p[n]$) at 4 KHz.

2. Video recorded at 30fps.

3. Audio recorded at 4KHz



From Ultrasound Machine

STEP2: Conversion to frequency domain:

2.1. $p[n] \rightarrow$ **DFT** $\rightarrow P[k]$, Sampling rate= 4000 samples/s.

2.2. Calculation of volume-flow: $q[n]$

2.2.1. Frame-wise area calculation: $a[n]$, $n = \text{frame no.}$

2.2.2. For one frame duration, no: of audio samples = $4000/30 = 133$ samples/frame: $x[n]$, $N=133$

2.2.3. $x[n] \rightarrow$ **DFT** $\rightarrow X[k] \rightarrow$ **Averaging** = average doppler shifted freq (f_D) \rightarrow conversion to average velocity, $v[n]$,

using, $f_D = \frac{2 \cdot f \cdot v \cos \theta}{c}$, f is the probe txn freq=11MHz, c is velocity of sound in blood=1580 m/s, $\theta = 60^\circ$.

2.2.4. Hence, calculation of volume flow, $q[n] = a[n] \cdot v[n]$

2.3. Conversion of $q[n]$ to frequency domain:

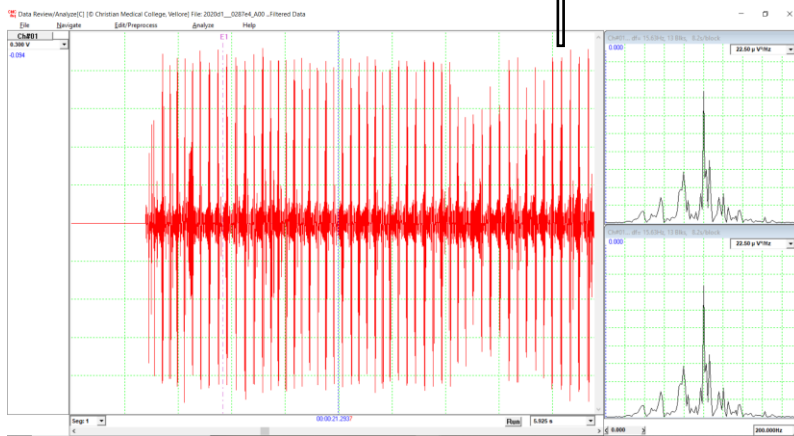
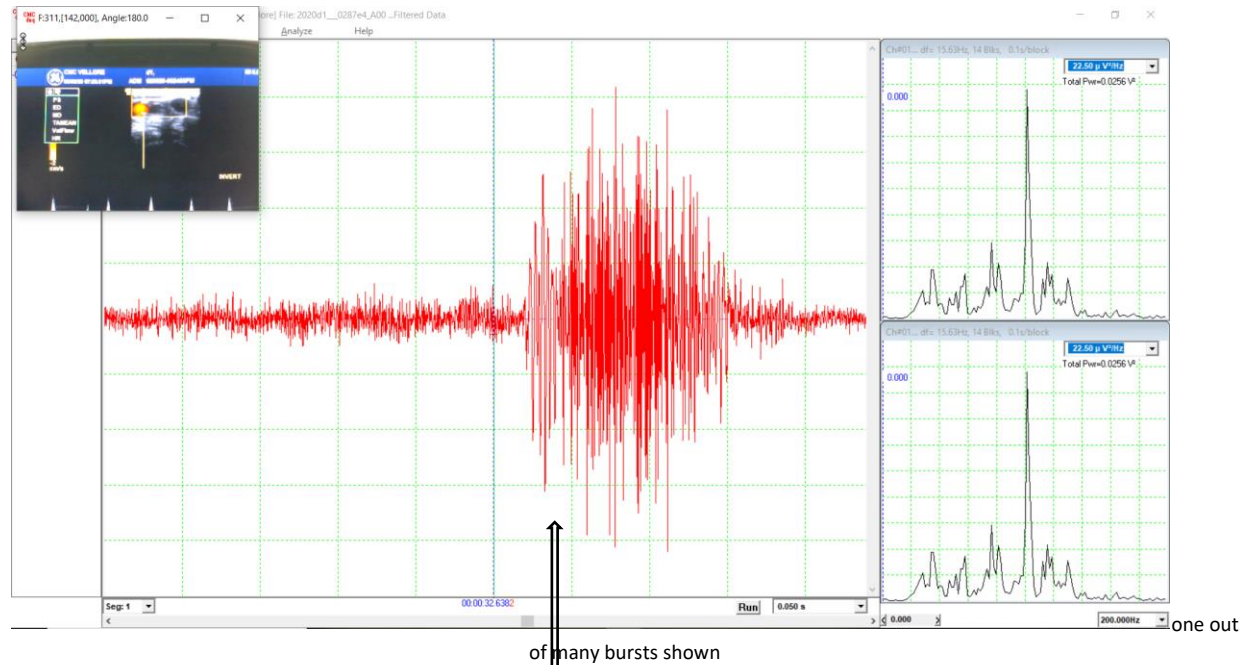
$q[n] \rightarrow$ **DFT** $\rightarrow Q[k] \rightarrow$ **Zero padding to 4000 samples** \rightarrow **IDFT** $\rightarrow q[n]$, $N=4000$

2.4. Arterial Vascular Impedance, $Z[k] = \frac{P[k]}{Q[k]}$

Summary of Calculations from Video (10fps) and audio (4KHz) collected simultaneously:

Data collection:

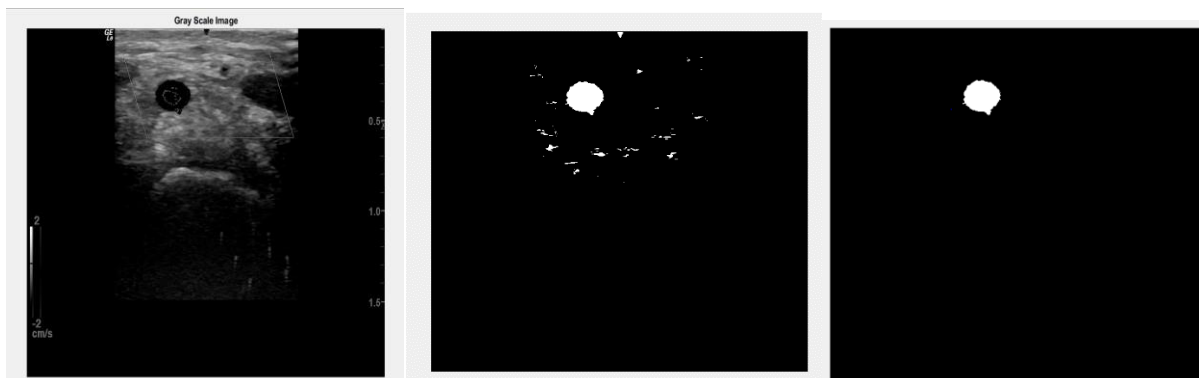
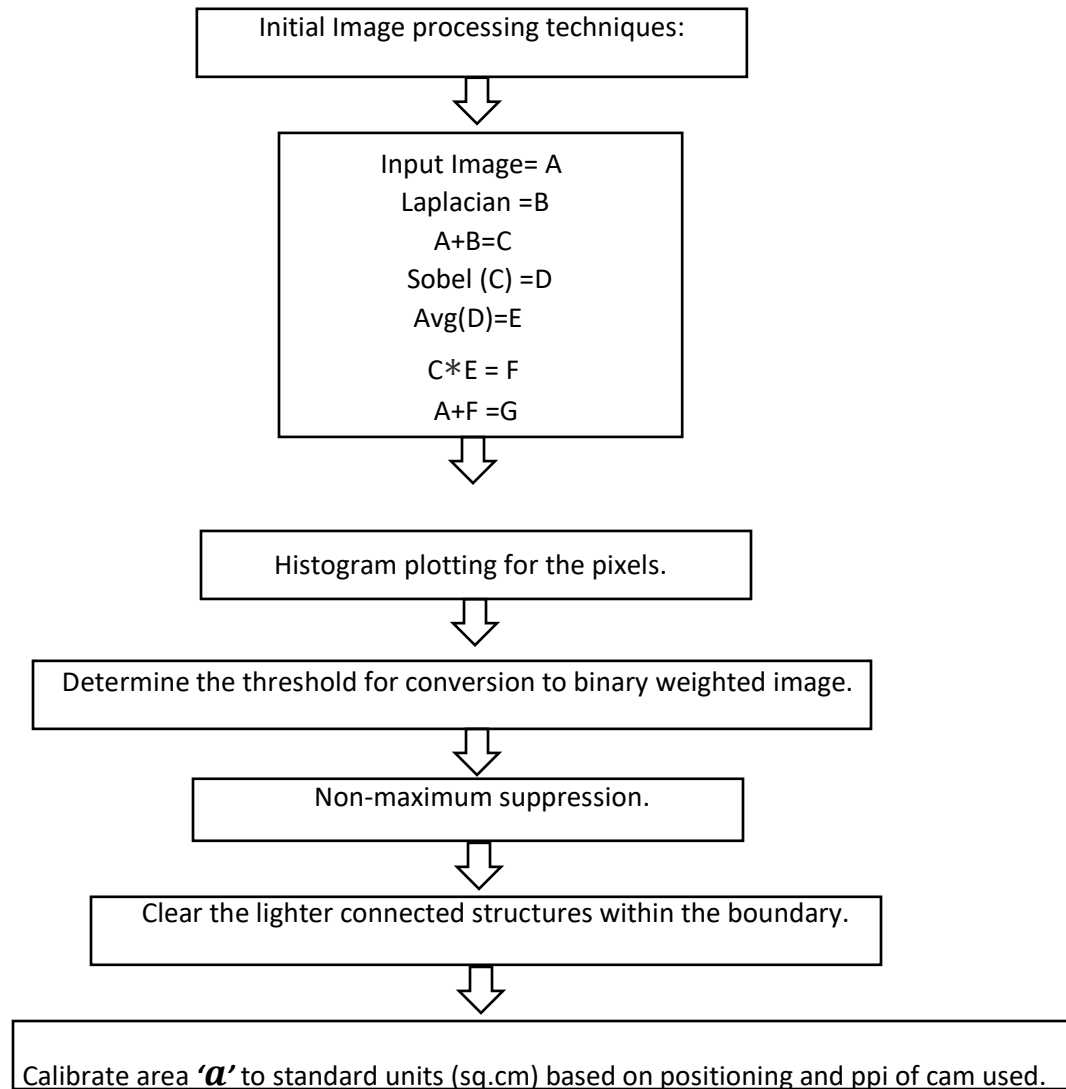
1. The doppler sound was recorded at 4KHz and video was recorded at 10fps , using CMCdaq, simultaneously.
Extraction: The doppler signal was low pass filtered at 31 Hz cut off. Also, 50Hz noise was filtered; the negative time (in the extracted text file) was corrected so that the video and doppler signal starts at 0 time instant.



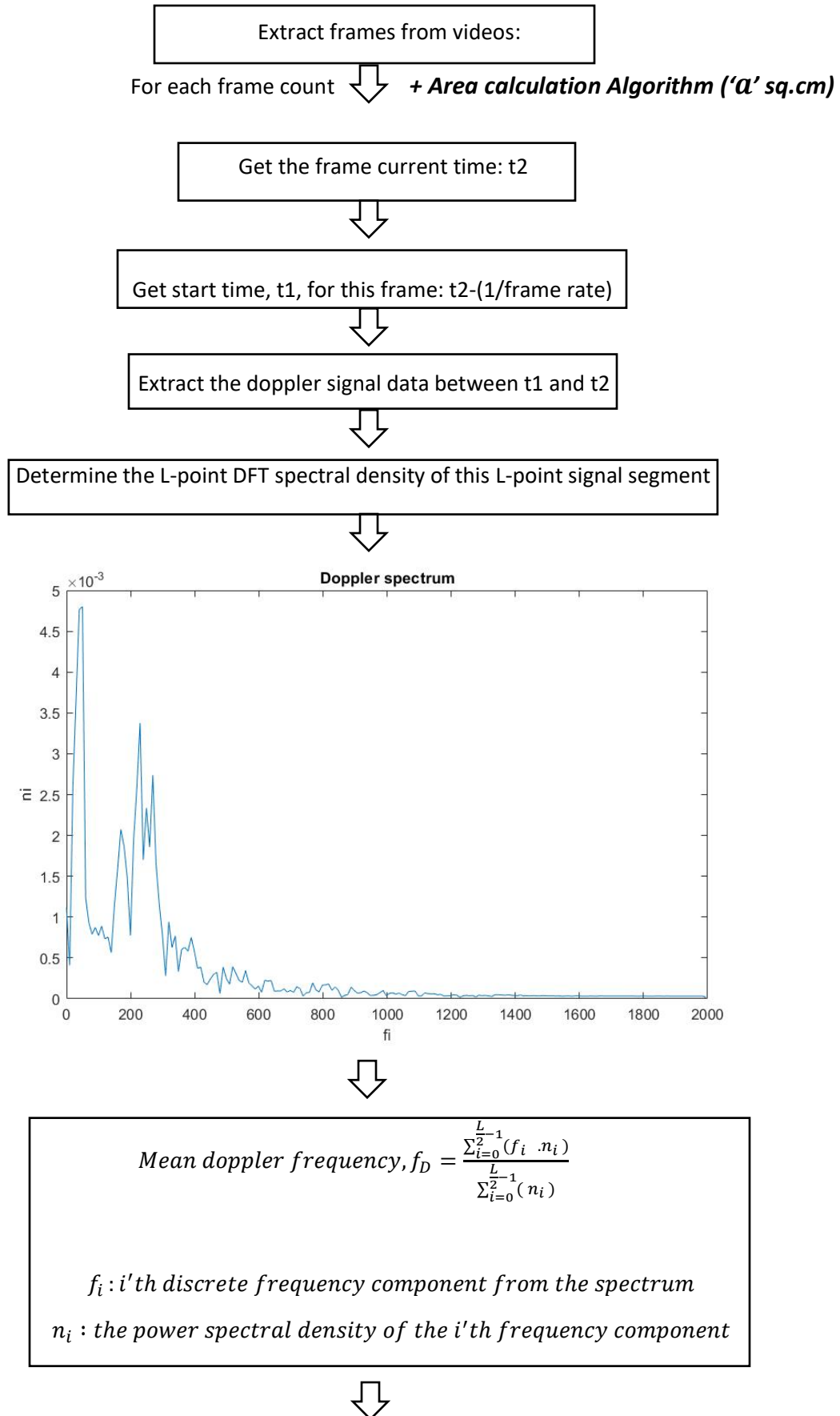
2. Intra-arterial pressure – to be collected simultaneously along with video and doppler on CMCdaq.
3. Volume Flow = (Mean flow velocity). (Area of cross-section)
4. Area of cross-section calculation:

4.1. Area calculation Algorithm:

Principle: Covert to binary weighted image and calculate the area based on the number of pixels within the boundary detected. This is converted to standard units based on PPI -value of ultrasound machine.



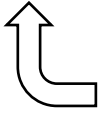
5. Mean flow velocity frame-wise:



$$\text{Mean doppler shifted frequency, } f_D = \frac{2 \cdot f \cdot v \cos \theta}{c}$$

$$\text{Hence, Mean velocity, } v = \frac{f_D \cdot c}{2 \cdot f \cdot \cos \theta}$$

Where, velocity of sound in blood, $c = 1580\text{m/s}$; θ = angle of insonation; f = transmitted frequency = 8MHz ; (convert to cm/s)

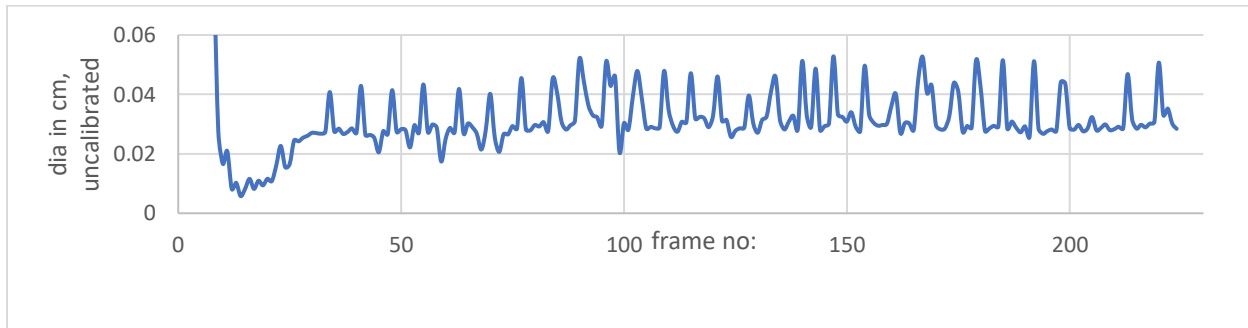


For this frame, calculate volume flow, $q = a \cdot v$; in cc/s

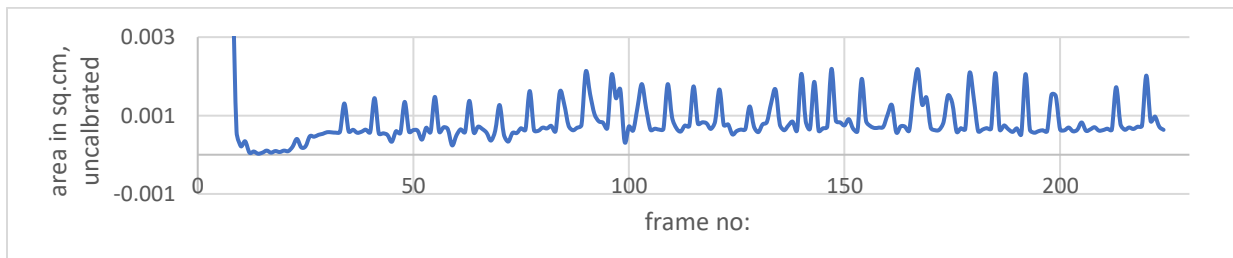
Repeat over all frames

Results:

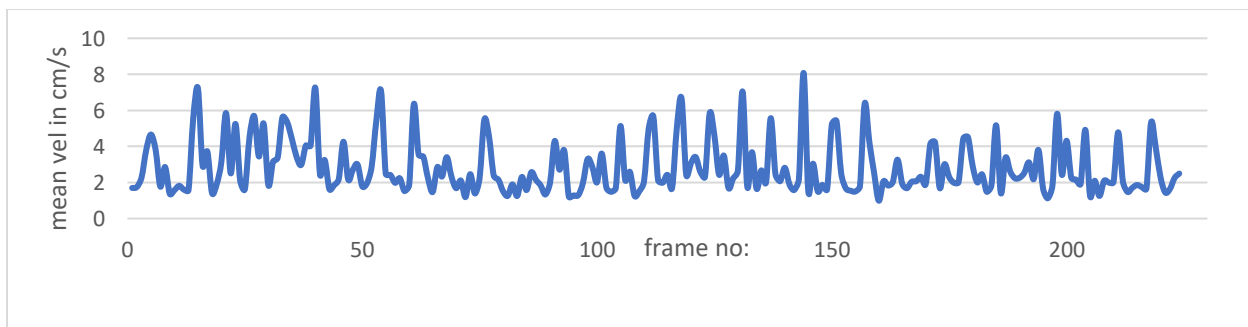
Diameter vs frame no. (NB: need to calibrate for correct dia measurement based on the webcam position which was not done for this data).



Area vs frame no:



Velocity vs frame no:

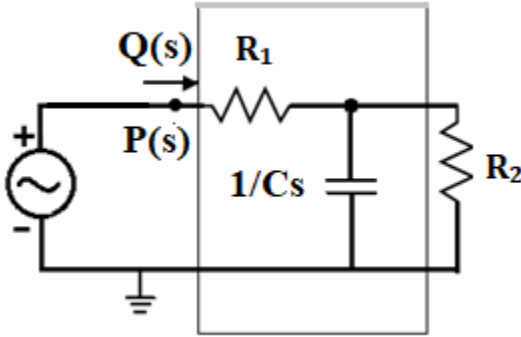


Hence, Volume flow will be: **area. Velocity**

6. As mentioned in page 1, 2.4, arterial vascular impedance can be calculated in frequency domain.

Physiological Interpretation:

The arterial lumped model can be simply modeled as a low pass filter as shown below, where, R_1 and C : compliant vessels; R_2 : (non-compliant vessels + veins + capillaries).



In Frequency domain, net arterial impedance = $Z(s) =$

$$\frac{P(s)}{Q(s)} = \frac{(R_1 \cdot R_2 \cdot Cs + R_2 + R_1)}{(R_2 \cdot Cs + 1)}$$

$$\frac{P(j\omega)}{Q(j\omega)} = \frac{(R_1 \cdot R_2 \cdot j\omega C + R_2 + R_1)}{(R_2 \cdot j\omega C + 1)} = Z(j\omega)$$

$$|Z(\omega)| = \frac{\sqrt{(R_1^2 + R_2^2 + 2 R_1 \cdot R_2 + R_1^2 \cdot R_2^2 \cdot \omega^2 \cdot C^2)}}{\sqrt{(1 + R_2^2 \cdot \omega^2 \cdot C^2)}}$$

$$\begin{aligned} \angle Z(\omega) &= \tan^{-1} \left(\frac{\omega \cdot C \cdot R_1 \cdot R_2}{R_2 + R_1} \right) - \tan^{-1}(\omega \cdot C \cdot R_2) \\ &= \angle(\text{Pressure}) - \angle(\text{Flow}) \end{aligned}$$

→ Arterial Vascular Impedance, $|Z(\omega)| \cdot \angle Z(\omega)$

From the **phase response** of Arterial Vascular Impedance, the nature of R and C of the model can be discussed.

For instance, a phase lag of 90° between voltage and current would imply a pure capacitive component, while an in-phase V and I denotes purely resistive circuit. Voltage and current electrical equivalence explains how pressure and flow would work in the lumped model for arterial tree. More the compliance factor, we would expect a phase difference between pressure and flow (leading, analogous to current) waveform. Lesser the compliance or more the resistant / stiffer the vessels are, minimum (or no) phase difference would be expected between pressure and flow. Area of cross-section is constant for a stiffer vessel. In a compliant system, the phase would be negative between 0° and 90° . In a resistant system, it would be zero. Hence, it is crucial to preserve the phase information of all these signals through synchronous data collection which can be achieved using CMCdaq. Lead II ECG data along with (doppler+video+pressure) channels would give additional information on cardiac cycle timing information for any validation.

From the **frequency spectrum**, solving for 3 equations from 3 impedance values, R_1 , R_2 and C_1 can be resolved.