

12) Boundary Condition are the pre assumptions that are made in order to derive any formula and Equations. These are the criteria which are considered to be followed by the system which is used to derive the formula as equation.

2) Stoke's theorem :-

$$\int \vec{A} \cdot d\vec{l} = \int (\vec{\nabla} \times \vec{A}) \cdot \vec{ds}$$

Consider any surface S which is divided into ~~less~~ many differential surfaces that are $ds_1, ds_2, ds_3, \dots, ds_n$.

And the surface is enclosed by the line L .

$$\text{So, } \oint \vec{A} \cdot d\vec{l} = \int_{ds_1} \vec{A} \cdot \vec{dl} + \int_{ds_2} \vec{A} \cdot \vec{dl} + \int_{ds_3} \vec{A} \cdot \vec{dl} \\ + \int_{ds_n} \vec{A} \cdot \vec{dl}$$

Now, from the definition of curl,

$$\vec{\nabla} \times \vec{A} = \int \frac{\vec{A}' dl}{ds}$$

$$(\vec{\nabla} \times \vec{A}) ds = \int \vec{A} \cdot \vec{dl}$$

$$\Rightarrow \int \vec{A} \cdot \vec{dl} = (\vec{\nabla} \times \vec{A}) ds + (\nabla \times A) ds_2 \\ + (\nabla \times A) ds_3 + \dots + (\vec{\nabla} \times \vec{A}) ds_n$$

$$\Rightarrow \int \vec{A} \cdot \vec{dl} = (\vec{\nabla} \times \vec{A})(ds_1 + ds_2 + ds_3 + \dots + ds_n)$$

$$\therefore \boxed{\int \vec{A} \cdot \vec{dl} = \int_S (\vec{\nabla} \times \vec{A}) \cdot \vec{ds}}$$

3) i) Electric flux & Electric flux density

Electric flux is the no. of electric field lines that is produced due to flow of electric current inside a curve.

Electric flux density is the no. of amount flux passing through a unit surface area i.e., The no. of electric field lines passing through the unit surface area,

ii) Displacement current is the current which flows in an open ckt. ie, where there is no close path for the charges to flow.

iii) The Laplacian operator is a differential operator given by the divergence of the gradient of a function in Euclidean space.

iv) Poisson's and Laplace Eqⁿ:

Poisson's Equation is the partial differential Equation which is used to decide the potential field caused by a given charge as man density distribution.

Laplace eqn is a second order diff. eq which is often written as $\nabla^2 f = 0$, ∇ is the gradient operator $f(x, y, z)$. Laplace eqn maps the scalar function to scalar function.

(1) Using Gauss's Law of Electrostatic

$$\nabla \cdot E = \frac{\rho}{\epsilon_0}$$

where, $E \rightarrow$ Electric field intensity

ρ = Total charge density

$\epsilon_0 \rightarrow$ Electric permiability of the material.

Then, $V = \frac{1}{2} \int \rho \phi dV$ (Energy & Potential)
 $= \frac{1}{2} \int \epsilon_0 (D \cdot E) \phi dV$

we have,

$$V = \frac{\epsilon_0}{2} \int \nabla \cdot (E \phi) dV - \frac{\epsilon_0}{2} \int (\nabla \phi) \cdot E dV.$$

Using divergence theorem and taking the area to be at infinity where $\phi(\infty) = 0$,

$$\therefore V = \frac{\epsilon_0}{2} \int \phi E \cdot dA - \frac{\epsilon_0}{2} \int (E) \cdot E dV.
= \frac{1}{2} \int \epsilon_0 E_c^2 dV.$$

So The energy density \Rightarrow
$$U_c = \frac{1}{2} \epsilon_0 |E|^2$$

5) Maxwell's Equation!

① Maxwell's 1st Eq,

According to Gauss theorem,

$$\oint_S \vec{E} \cdot d\vec{s} = \frac{q}{\epsilon_0} \quad (1)$$

Where, q is the total charge which can be written.

$$q = \iiint_V \rho dV \quad (2)$$

ρ is the volume charge density.

From eq (1),

$$\oint_S (\nabla \cdot \vec{E}) dV = \iiint_V \frac{\rho}{\epsilon_0} dV$$

$$\therefore \boxed{\nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0}}$$

In case of charge free surface,

$$\boxed{\nabla \cdot \vec{E} = 0}$$

But in vacuum, $\vec{D} = \epsilon_0 \vec{E}$ eq (3) becomes

$$\boxed{\nabla \cdot \vec{D} = \rho}$$

② Maxwell's 2nd Eq:

Since there is no undated magnetic poles exists.

Thus the no. of magnetic lines of force entering a surface in a magnetic field is equal to the no. of magnetic line leaving the surface.

So, mathematically,

$$\iint_S \vec{B} \cdot d\vec{s} = 0$$

$$\iiint_V (\vec{\nabla} \cdot \vec{B}) dV = 0$$

$$\vec{\nabla} \cdot \vec{B} = 0$$

③ Maxwell's 3rd Equation

According to faraday's Law of EMI whenever there is change in magnetic flux link with a closed Ckt., an emf is induced in its which is directly proportional to the negative rate of change of magnetic flux.

$$\therefore e = -\frac{d\phi}{dt}$$

$$\Rightarrow -\frac{d}{dt} \iint_S \vec{B} \cdot d\vec{s} = 0$$

But the electric flux produced due to change in magnetic flux, the emf induced in the closed CLCT will be equal to line integration of the electric field along with the closed CLCT

$$\epsilon = \int \vec{E} \cdot \vec{dl}$$

$$\phi_c = \int_C \vec{F} \cdot \vec{dl} = - \int_S \frac{\partial \vec{B}}{\partial t} \cdot \vec{ds}$$

$$\iint (\nabla \times \vec{E}) \cdot \vec{ds} = - \iint_S \frac{\partial \vec{B}}{\partial t} \cdot \vec{ds}$$

$$(\nabla \times \vec{E}) = - \frac{\partial \vec{B}}{\partial t}$$

④ Maxwell's 4th equation

According to Ampere's law curl of \vec{B} is

equal to

$$\nabla \times \vec{B} = \mu_0 (J + J_d)$$

$$d\vec{w} \cdot (\nabla \times \vec{B}) = \mu_0 d\vec{w} \cdot (J + J_d)$$

$$\Rightarrow d\vec{w} \cdot \vec{s} = - d\vec{w} \cdot \vec{J_d}$$

$$\text{div} \cdot \vec{J} = -\frac{d\phi}{dt}$$

from Maxwell first equation

$$\nabla \times \vec{E} = \frac{1}{\mu_0}$$

$$\vec{E} = \mu_0 (\vec{\nabla} \times \vec{B})$$

$$\text{div} \cdot \vec{J}_{ct} = \frac{d(\mu_0 (\vec{\nabla} \times \vec{B}))}{dt}$$

$$\boxed{\vec{J}_{ct} = \mu_0 \frac{d\vec{B}}{dt}}$$

Putting in eq
early

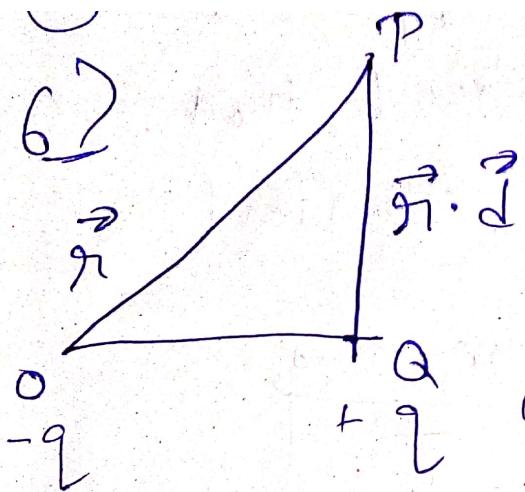
$$\vec{\nabla} \times \vec{B} = \mu_0 (\vec{J} + \mu_0 \frac{d\vec{B}}{dt})$$

in case of vacuum.

$$\vec{B} = \text{Magnetic field} \vec{B} = \mu_0 \vec{E}$$

$$\vec{\nabla} \times (\mu_0 \vec{B}) = \mu_0 (\vec{J} + \mu_0 \vec{E})$$

$$\boxed{\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}}$$



Two equal and opposite, point charges are separated by a distance, small compare of distance at which the

potential due to the charge configuration is demand are said to be contribute an electric dipole.

The potential is given by:

$$\Phi_{\text{dip}} = \frac{q}{4\pi\epsilon_0(\vec{r} \cdot \vec{r})} - \frac{q}{4\pi\epsilon_0(\vec{r})}$$

$$\frac{1}{(\vec{r} - \vec{d})} = \left[d^2 - 2\vec{r} \cdot \vec{d} + \vec{d}^2 \right]^{-\frac{1}{2}} [a^2 - 2ab + c]$$

$$= \frac{1}{2} \left[1 - \frac{2\vec{r} \cdot \vec{d}}{d^2} + \frac{\vec{d}^2}{r^2} \right]^{-\frac{1}{2}}$$

$$= \frac{1}{2} \left[\frac{1 - 2\vec{r} \cdot \vec{d}}{r^2} \right]^{-\frac{1}{2}}$$

$$\frac{1}{\vec{r} - \vec{d}} \approx \frac{1}{r} \left[1 + \frac{\vec{r} \cdot \vec{d}}{d^2} \right]$$

$$\phi_s = \frac{q}{4\pi\epsilon_0 r} = \frac{\vec{r} \cdot \vec{d}}{r^3}$$

For dipole, \vec{d} is approached towards D once q is allowed to approach towards infinity (∞) much that the term $q \cdot \vec{d}$ remain constant.

So, $\frac{q \cdot \vec{d}}{r}$ So, $q \cdot \vec{d}$ (3) becomes,

$$\boxed{\phi_s = \frac{\vec{p} \cdot \vec{r}}{4\pi\epsilon_0 r^2}}$$

Q) The Point charges are $-4nc$, $-5nc$, $-1nc$ at $(0, 0, 0)$, $(0, 0, 2)$, $(2, 0, 0)$ w.r.t. origin.

$$\begin{aligned} W_E &= W_1 + W_2 + W_3 \\ &= 0 + (-1) \times \phi_{21} + (-1) \times (\phi_{31} + \phi_{32}) \end{aligned}$$

$$= \frac{1}{u \pi E_0} (2u) = \frac{6}{\pi E_0}$$

$$\textcircled{8} \quad F = 2n^2 \hat{a}_n - 3n^2 \hat{a}_y - 6y^2 \hat{a}_z$$

from $(1, 0, 0)$ to $(0, 0, 0)$.

$$\int \vec{F} \cdot d\vec{l} = \int 2n^2 \hat{a}_n - \int 3n^2 \hat{a}_y - \int 6y^2 \hat{a}_z$$

$$\int_0^1 2n^2 \hat{a}_n \left[\frac{2n^3}{3} \right]_0^1 = \frac{2}{3}$$

① $(0, 0, 0)$ to $(0, 1, 0)$

$$\int F \cdot dl = \int 2n^2 \hat{a}_n - \int 3n^2 \hat{a}_y - \int 6y^2 \hat{a}_z$$

1. $n=0$

$$= \underline{\underline{0}}$$

② $(0, 1, 0)$ to $(1, 1, 1)$.

$$\int F \cdot dl = \int 2n^2 \hat{a}_n - \int 3n^2 \hat{a}_y - \int 6y^2 \hat{a}_z$$

$$= \left[\frac{2n^3}{3} \right]_0^1 - \left[\frac{6y^3}{3} \right]_0^1$$

$$= \frac{2}{3} - \frac{6}{3} = \underline{\underline{-4}}$$

③ $(1, 1, 1)$ to $(1, 0, 0)$.

$$\int F \cdot dl = \int 2n^2 \hat{a}_n - \int 3n^2 \hat{a}_y - \int 6y^2 \hat{a}_z$$

$$- \int 3n^2 \hat{a}_y - \int 6y^2 \hat{a}_z$$

$$\text{Now using } \frac{n_1 - n_2}{n_1 + n_2} = \frac{y - y_1}{y - y_2} = \frac{z - z_1}{z - z_2}$$

$$\begin{aligned} & n = y = z \\ \rightarrow & - \int_1^0 3yy - \int_1^0 6zz^2 \\ = & -3 \int_1^0 y^2 - \int_1^0 6z^3 \\ = & 1 + \frac{6}{4} = \frac{10}{4} \end{aligned}$$

$$10) E \cdot ds = \mu_m z \hat{a}_n - y^2 \hat{a}_y +$$

the cube bounded by $n=0, n=2$,
 $y=0, y=2, z=0, z=2$,

$$\begin{aligned} \oint E \cdot ds &= \iint y^2 dndz \\ &= - \int_0^2 \int_0^2 y^2 dndz. \text{ at } y=2 \\ &= - \int_0^2 [y^2]_0^2 dz = - \int_0^2 [4x2]^2 dz \\ &= - \int_0^2 16 dz \\ &= \underline{\underline{0 - 32}} \end{aligned}$$

$$\begin{aligned}
 \oint E ds_4 &= \iint_{\text{square}}^{22} yz \, dz \, dy \\
 &\approx 2 \int_0^2 \int_0^2 y \, dy \, dz \\
 &\approx 2 \int_0^2 \left[\frac{y^2}{2} \right]_0^2 \, dz \\
 &\approx 4 \int_0^2 dz = 4[2]_0^2 = \underline{\underline{8}}
 \end{aligned}$$

$$\begin{aligned}
 \oint E ds_3 &= -4n z \, dz = -8 \left[\frac{z^2}{2} \right]_0^2 \, dy \\
 &\quad \cancel{\underline{\underline{zds_2}}} = -8 \times 0 [4]_0^2 \, dy \\
 &= 0 \cancel{16} \times 2 = \underline{\underline{32}}
 \end{aligned}$$