



Departament de Projectes

d'Enginyeria

UNIVERSITAT POLITÈCNICA DE CATALUNYA

Secció de Terrassa

Degree: Aerospace Engineering

Course: Engineering Projects

Title and acronym of the project:

Cubesat Constellation

Astrea

Contents: Report Attachments

Group: G4 EA-T2016

Delivery date: 22-12-2016

Students:

Cebrián Galán, Joan	Fontanes Molina, Pol
Foreman Campins, Lluís	Fraixedas Lucea, Roger
Fuentes Muñoz, Óscar	González García, Sílvia
Herrán Albelda, Fernando	Kaloyanov Naydenov, Boyan
Martínez Viol, Víctor	Morata Carranza, David
Pla Olea, Laura	Pons Daza, Marina
Puig Ruiz, Josep	Serra Moncunill, Josep Maria
Tarroc Gil, Sergi	Tió Malo, Xavier
Urbano González, Eva María	

Customer: Pérez Llera, Luís Manuel

Contents

List of Tables	ii
List of Figures	iii
I ANNEX I: Orbit Design	1
1 Orbit Geometry	2
1.1 Keplerian Geometry	3
1.2 Dynamic equations	5
2 Orbital Coverage	7
2.1 Satellite Footprint	7
2.1.1 Introduction	7
2.1.2 Footprint Computation	8
2.2 Elevation Angle	9
2.2.1 Elevation angle cone	10
2.2.2 Atmospheric restrictive conditions	10
2.2.3 Elevation angle of other current constellations	13
2.3 Minimum Plane Inclination	14
2.4 Satellite to Satellite Visibility	15
2.5 Market Study: Current Nanosatellites in Orbit	17
2.5.1 Criteria for the orbital height of the satellites	17
2.5.2 New Space: Adapting to new society needs	19
3 Constellation Configuration	20
3.1 Introduction: The Global Positioning System Example	20
3.2 Polar Orbit Constellation	21
3.2.1 Introduction	21
3.2.2 General Configuration	22
3.2.3 The Streets of Coverage Method	23
3.2.4 Results of Streets of Coverage	25
3.3 Walker-Delta Constellation	26
3.3.1 Full Walker-Delta Constellation	26

3.3.1.1	Characteristics	26
3.3.1.2	Notation	28
3.3.1.3	Coverage	28
3.3.2	Semi Walker Delta Configuration	29
3.3.2.1	Advantages	29
3.3.2.2	Disadvantages	30
3.3.3	Other Walker Delta Configurations	31
3.3.3.1	SWDC including an additional polar orbit.	31
3.3.3.2	Mixed Walker Delta.	32
3.4	Testing Method	33
3.4.1	Introduction	33
3.4.2	Method Bases	33
3.4.2.1	Global Coverage Conditions	34
3.4.2.2	Results of Testing Method	35
4	Orbit Perturbations	38
4.1	Sources of Perturbation	38
4.1.1	Introduction to Orbit Perturbations [?].	38
4.1.2	Gravity Potential of Earth	39
4.1.3	Atmospheric Drag	40
4.1.4	3rd Body Perturbations	42
4.1.5	Other Perturbations	42
4.2	Significant Perturbations	43
4.3	Orbit Decay	44
4.3.1	Effects on the Ascension Node	44
4.3.1.1	Introduction	44
4.3.1.2	Perigee Effect	45
4.3.1.3	Ascension Node	45
4.3.1.4	Conclusion	45
4.3.2	Effects of the Solar Cicle	45
4.3.3	Orbital Decay Propagation Results	48
4.3.3.1	Introduction	48
4.3.3.2	Drag Computation Algorithm	48
4.3.4	Dynamic Orbit Decay Computation	50
4.3.4.1	Introduction	50
4.3.4.2	Results	52
4.4	Orbital Station-Keeping	53
4.4.1	Raising the orbit height to increase Lifetime	54
4.4.2	Using Thrusters to increase Lifetime	55
4.4.2.1	Energy equation	55
4.4.2.2	Delta-V	56

4.4.2.3	Time	57
4.4.2.4	Propellant	57
4.4.2.5	Orbit maintenance	57
4.4.2.6	Results	58
5	Constellation Design Decision	62
5.1	Considered Designs	62
5.1.1	Introduction	62
5.1.2	Candidate 1: Polar - Global Coverage	62
5.1.3	Candidate 2: Polar - GS Coverage	63
5.1.4	Candidate 3 and 4: Walker-Delta GS Coverage	63
5.1.5	Candidate 5: Walker-Delta Lat: 0-58	64
5.1.6	Candidate 6: Polar - Walker-Delta J2 + Rotació	64
5.1.7	Candidate 7: Walker-Delta GS Coverage 3	65
5.2	Constellation Performance Analysis	68
5.2.1	Performance Evaluation	68
5.3	Ordered Weighting Average based Decision	70
II	ANNEX II: Constellation Deployment	72
6	Constellation Deployment	73
6.1	Constellation Deployment Department	74
6.2	First Placement	78
6.2.1	First Placement logistics	78
6.2.2	1st Placement In-Orbit Injection Maneuver	79
6.2.3	Orbit Parameters Calculation	82
6.2.3.1	Plane Order	83
6.3	Replacement Strategy	85
6.4	Spare Strategy	88
6.4.1	Spare Strategy Alternatives	88
6.4.2	Major failure deffinition	89
6.4.3	Major failure	90
6.4.3.1	Satellite in range failure	90
6.4.3.2	Ground station failure	92
6.4.3.3	Transmitting time failure	92
6.4.4	Space Debris	94
6.4.5	End-of-Life Types and Analysis	95
6.5	Conclusions	97

III ANNEX III: Communications	98
7 Space Segment Protocol Stack	99
7.1 Layer 2: Data Link	99
7.1.1 Functions of the DLL	99
7.1.2 Working procedure	100
7.1.2.1 Simplest Protocol	100
7.1.2.2 Stop-and-Wait Protocol	101
7.1.2.3 Stop-and-Wait Automatic Repeat Request	102
7.1.2.4 Go-Back-N Automatic Repeat Request	103
7.1.2.5 Selective Repeat Automatic Repeat Request	106
7.1.2.6 Bidirecional links: Piggybacking	109
7.1.2.7 Working procedure ranking	110
7.1.3 Protocols	111
7.1.4 TC Space Data Link Protocol	114
7.1.5 TC Sync and Channel Coding	115
7.2 Layer 3: The Network	116
7.2.1 Functions of the Network Layer	116
7.2.2 Protocols	117
7.2.2.1 Main protocols	118
7.2.2.2 Auxiliary protocols	122
7.2.2.3 Routing protocols	126
7.2.3 Protocol Selection	130
7.2.3.1 Choice of the main protocol	130
7.2.3.2 Choice of routing protocol	131
7.2.3.3 Choice of complementary protocols	132
7.2.3.4 Conclusion	132
7.2.4 Final structure	133
7.3 Layer 4: Transport and Session	134
7.3.1 User Datagram Protocol (UDP)	135
7.3.2 Stream Control Transmission Protocol (SCTP)	135
7.3.3 Transmission Control Protocol (TCP)	135
7.3.3.1 TCP Services	136
7.3.3.2 TCP features	137
7.3.4 Choice of protocol for the transport layer	141
7.4 Global Overview	141
8 Ground Segment	143
8.1 Introduction	143
8.2 Ground Segment protocols	144
8.2.1 File Transfer Protocol (FTP)	144

8.2.2	Secure Shell (SSH)	144
8.2.3	Simple Mail Transfer Protocol (SMTP)	144
8.2.4	Hypertext Transfer Protocol (HTTP)	145
8.2.5	Transport Layer Security (TLS)	145
8.2.6	Hypertext Transfer Protocol Secure (HTTPS)	146
8.3	Conclusions	146
9	Design of the Ground Segment	149
9.1	Study of localization of Ground Stations	149
9.1.1	Latitude analysis	149
9.1.2	Longitude analysis	155
9.2	Study of annual costs	157
9.2.1	Energy and Maintenance	157
9.2.1.1	Mission Control Center	157
9.2.1.2	Ground Stations	158
9.2.2	Salaries	159
9.3	Study of initial investment	161
9.4	List of existing Ground Stations	161
9.4.1	ESA Ground Stations	161
9.4.2	KSAT Ground Stations	163
9.4.3	NASA Ground Stations	164
9.4.4	SSC Ground Stations	165
9.4.5	Other Ground Stations	166
9.5	Decision taking	167
9.5.1	Availability	167
9.5.1.1	Building a ground station	167
9.5.1.2	Renting a ground station	167
9.5.2	Cost	167
9.5.2.1	Building a ground station	167
9.5.2.2	Renting a ground station	168
9.5.3	Position	168
9.5.3.1	Building a ground station	168
9.5.3.2	Renting a ground station	168
9.5.4	Ease to improve	168
9.5.4.1	Building a ground station	168
9.5.4.2	Renting a ground station	169
9.5.5	Decision	169
IV	ANNEX IV: Satellite design	170
10	Satellite design	171

10.1 Structure and mechanics	171
10.1.1 Structure	171
10.1.2 Thermal protection	172
10.1.3 Study of the commercial available options and options chosen	173
10.2 Electrical Power System	174
10.2.1 Estimation of the power required	174
10.2.2 Solar arrays	175
10.2.3 Power management system	176
10.2.4 Batteries	177
10.2.5 Study of the commercial available options and options chosen	178
10.3 Propulsion Systems	179
10.3.1 Requirements	179
10.3.2 Thrusters	180
10.3.3 Study of the commercial available options	181
10.4 Attitude and Orbital Control Systems	182
10.4.1 Orbital Control	183
10.4.2 Study of the commercial available options	183
10.5 Payload	184
10.5.1 Antennas	185
10.5.2 Antenna selection	187
10.5.3 Payload Data Handling Systems	187
10.5.4 Study of the commercial available options and options chosen	189
10.6 Communication module	191
10.7 Link Budget	191
10.7.1 Communications Basics	192
10.7.2 Propagation losses	193
10.7.3 Local Losses	200
10.7.4 Modulation Technique	200
10.7.5 System Noise	201
10.7.6 Link Budget Calculation	202
10.8 Budget	203
10.9 Astrea satellite Final Configuration	204
V ANNEX V: Financial and Other Considerations	206
11 Financial Study	208
11.1 Selling the product	208
11.1.1 Estimation of demand	209
11.1.1.1 Universities	209
11.1.1.2 Particular customers	210

CONTENTS

11.1.1.3 Demand	211
11.1.2 Pricing the service	211
11.2 Economic Feasibility Report	211
11.2.1 Previous costs	212
11.2.1.1 Engineering hours	212
11.2.1.2 Administrarion costs	213
11.2.1.3 Taxes	214
11.2.1.4 Insurance	214
11.2.2 Economic feasibility study	215
11.3 Conclusions of the financial study	217
11.3.1 Pay Back Time (PBT)	217
11.3.2 Updated Pay Back Time (UPBT)	218
11.3.3 Break Even Point (BEP)	219
11.3.4 Net Present Value (NPV)	220
11.3.5 Internal Rate of Return (IRR)	220
11.3.6 Conclusions of the feasibility study	221
12 Marketing Plan	222
12.1 Executive Summary	222
12.2 Target Customers	222
12.3 Unique Selling Proposition	223
12.4 Pricing & Positioning Strategy	223
12.5 Distribution Plan	224
12.6 Marketing Materials	224
12.7 Online Marketing Strategy	224
12.8 Conversion Strategy	225
12.9 Joint Ventures & Partnerships	225
13 Environmental Impact Study	226
13.1 Introduction	226
13.2 Ground Stations	226
13.3 Satellites	226
13.4 Launch system	227
14 Social and Security Considerations	230
14.1 Social and security considerations	230
14.2 Legislation	232
VI ANNEX VI: Matlab Codes	234
14.3 Satellite Footprint	235
14.4 Minimum Plane Inclination	236

CONTENTS

14.5 Satellite Number Computation for Polar Orbits	239
14.6 Orbit Parameters	241
14.7 Walker Delta Testing	247
14.8 Orbit Plotter	248
14.9 Perturbations	255
14.10 Orbit Decay	260
14.11 Performance Evaluator	265
14.12 Thrust	269
14.13 Satellites Datasheet	274
14.14 Ground Station Localization	276
15 Bibliography	280

List of Tables

1.1.1	Eccentricity values depending on the shape of the orbit	4
3.2.1	Streets of Coverage Method main variables	23
3.4.1	Coverage Testing Method main Variables	34
3.4.2	Testing Values for the Coverage Testing Method	35
4.1.1	Exponential Atmosphere Model main Variables	41
4.1.2	Third Body Perturbations Coefficients	42
4.3.1	Selected data to compute orbit decay extracted from figure ??	49
4.4.1	Simulation Thruster Parameters	58
4.4.2	Station-Keeping with Thrusters Simulation 1 Results	60
4.4.3	Station-Keeping with Thrusters Simulation 2 Results	60
5.2.1	Constellation parameters for the Example Constellation	69
5.2.2	Performance Parameters for the Example Constellation	70
5.3.1	Constellation Configuration OWA Decision	71
6.1.1	List of Launchers	75
7.1.1	OWA of the DLL protocols.	111
7.1.2	Ranking of working procedures	111
7.1.3	Reliability of CCSDS protocols	112
7.1.4	Identifiers of TC and Proximity-1 Space Data Link Layer Protocols	113
7.2.1	IP address notation	120
9.1.1	Equivalent coordinates	156
9.2.1	Costs per year for the control centre	158
9.2.2	Annual costs	159
9.2.3	Total annual cost of the ground segment consumption and maintenance .	159
9.2.4	Salaries according to country	160
9.2.5	Salaries in Spain	160
9.5.1	OWA of the GS	169
10.1.1	Options studied for the structure and thermal protection	173
10.1.2	Options chosen for the structure and thermal protection	173

LIST OF TABLES

10.2.1	Estimation of the power consumption under typical working conditions	175
10.2.2	Options studied for the Electric Power System	179
10.2.3	Options studied for the Electric Power System	179
10.3.1	Main features of BGT-X5	181
10.3.2	Options studied for the propulsion system	181
10.3.3	Option chosen for the propulsion system	182
10.4.1	Main ADACS features	183
10.5.1	Main features of the patch antenna	186
10.5.2	Main features of the turnstile antenna	187
10.5.3	Main inter-satellite communication transceivers features	188
10.5.4	Main space to ground communication transceivers features	188
10.5.5	Main PDHS computers features	189
10.5.6	Options studied for the payload	190
10.5.7	Options chosen for the payload	191
11.1.1	Table. List of Universities with Aerospace Degrees	209
11.2.3	Feasibility Study	216

List of Figures

1.0.1	Geocentric-equatorial frame. Extracted from [1].	3
1.1.1	Geocentric-equatorial frame and the Classical Orbital Elements. Extracted from [1].	5
2.1.1	Single satellite coverage geometry	8
2.2.1	Elevation angle cone. Source: NOAA	9
2.2.2	Minimum elevation angle as function of latitude. Source: [a general evaluation criterion]	14
2.3.1	Minimum Inclination to provide coverage at different latitude for different orbit apogees.	15
2.5.1	Distribution of the currently in orbit nanosatellites.	18
3.1.1	Distribution of the expanded 24-slot GPS constellation. [?]	21
3.2.1	Distribution of the 66 Iridium constellation satellites. Generated using [?]	22
3.2.2	Distribution of the planes for Polar Orbits design.	22
3.2.3	Single plain street of coverage. The footprints of the satellites superpose leading to a street. [?]	23
3.2.4	Two plains streets of coverage. An optimum phasing needs to be obtained. [?]	24
3.2.5	Variation of number of satellites for different heights and elevation angles	25
3.2.6	Variation of number of satellites for different heights between 500 and 600km.	26
3.3.1	Definition of the inclination δ . Extracted from [2]	27
3.3.2	Delta pattern as seen from the North Pole. Extracted from [3]	27
3.3.3	Delta pattern 65° : 30/6/1	28
3.3.4	Minimum altitude for continuous global coverage. Comparison between polar patterns and Walker delta patterns. Extracted from [4]	29
3.3.5	12 plane SWDC. Note the gap and the equidistant planes	30
3.3.6	This geometry distribution induces a large anti-symmetric gap	31
3.3.7	Added polar orbit to the 11 plane based SWDC	32
3.3.8	8 plane based MWDC generated for 210 degrees	33

LIST OF FIGURES

3.4.1	Geometrical conditions needed to fulfill global coverage. On the left: Condition between satellites of different planes. On the right: Condition between satellites of the same plane	34
3.4.2	Possible satellite configurations for a 210° Walker Delta configuration	36
3.4.3	Ground track and spherical representation for a 180° Walker Delta configuration	36
3.4.4	Ground track and spherical representation for a 210° Walker Delta configuration	36
3.4.5	Ground track and spherical representation for a 360° Walker Delta configuration	37
4.2.1	Logarithmic plot of the modulus of the increases in Angular Arguments of the orbit	43
4.3.1	Ascention node perturbation On the left: Perigee deviation in terms of time. On the right: Ascending node deviation in terms of time	44
4.3.2	Deviation of densities in the upper atmosphere due to the 19th solar cycle	46
4.3.3	Measured intensities of the 23rd and 24th solar cycles. Source: NOAA	47
4.3.4	Orbit Decay computed for several values of	49
4.3.5	Algorithm of resolution used to solve the orbital propagation.	51
4.3.6	Orbital decay of the satellite.	53
4.4.1	Increase in the Lifetime obtained by setting the constellation in a higher orbit	54
4.4.2	Hohmann transfer. Extracted from [4]	56
4.4.3	Height variation of the satellite	59
4.4.4	Height variation of the satellite with a more restrictive minimum height	61
5.1.1	Candidate 1. Full Polar constellation with global coverage. h= 560km; Np=20; Npp=21; Tsat=420	65
5.1.2	Candidate 2. Full Polar constellation with total ground station coverage. h= 550km; Np=18; Npp=20; Tsat=288	66
5.1.3	Candidate 3. 210° Walker-Delta constellation configuration. h= 542km; in=72; Np=8; Npp=21; Tsat=168	66
5.1.4	Candidate 4. 225° Walker-Delta constellation configuration. h= 542km; in=72; Np=9; Npp=17; Tsat= 153	66
5.1.5	Candidate 5. 210° Walker-Delta constellation configuration with total coverage of the lattitudes from 0 to 52 degrees. h= 560km; in=72; Np=9; Npp=17; Tsat= 153	67
5.1.6	Candidate 6. 225° Walker-Delta constellation configuration. h= 542km; in=72; Np=9; Npp=21; Tsat= 189	67
5.1.7	Candidate 7. Full Walker-Delta constellation configuration.	67
5.2.1	Length of the passes on the example GS.	70

LIST OF FIGURES

5.3.1	Astrea Constellation Final Configuration.	71
6.1.1	Electron Rocket	75
6.1.2	Second Stage	75
6.1.3	Electron Rocket Fairing	76
6.1.4	Rocket Lab Facilities	76
6.1.5	ISIPOD	77
6.1.6	GPOD	77
6.2.1	Launch Range Operations Flow/Schedule	78
6.2.2	Countdown Operations Flow	78
6.2.3	Rocket's trajectory from lift-off to final orbit.	80
6.2.4	Half of a revolution of the rocket in the elliptical spacing orbit.	80
6.2.5	Deployment of the second satellite.	81
6.2.6	Half of a revolution of the rocket after the deployment of the second satellite.	81
6.2.7	Deployment of the third satellite.	82
6.3.1	Old Constellation	86
6.3.2	Old and New Constellations	86
6.3.3	New Constellation	87
6.4.1	1 communication range failure	90
6.4.2	3 communication range failure	91
6.4.3	7 communication range failure	91
6.4.4	View of the Space Debris around the Earth	94
7.1.1	Sender algorithm for the simplest protocol.	100
7.1.2	Receiver algorithm for the simplest protocol.	101
7.1.3	Sender algorithm for the Stop-and-Wait Protocol.	101
7.1.4	Receiver algorithm for the Stop-and-Wait Protocol.	102
7.1.5	Flow diagram of the Stop-and Wait ARQ.	103
7.1.6	Flow diagram of the Go-Back-N ARQ.	104
7.1.7	Receiver algorithm for the Go-Back-N ARQ.	105
7.1.8	Sender algorithm for the Go-Back-N ARQ.	106
7.1.9	Flow diagram of the Selective Repeat ARQ.	107
7.1.10	Sender algorithm for the Selective Repeat ARQ.	108
7.1.11	Receiver algorithm for the Selective Repeat ARQ.	109
7.1.12	DLL of the CCSDS.	112
7.1.13	Transfer frame structure of the TC Space DL Protocol with SDLS.	114
7.1.14	Transfer frame primary header.	114
7.1.15	Procedure at the sending end.	115
7.1.16	Procedure at the receiving end.	116
7.2.1	CCSDS Recommended Protocols	117

LIST OF FIGURES

7.2.2	Combination of CCSDS Recommended Protocols	118
7.2.3	SPP header	119
7.2.4	IPv4 header	120
7.2.5	IPv6 header	121
7.2.6	Encapsulation header	123
7.4.1	Overall space communication protocol stack	141
9.1.1	Links vs time for latitudes from 0° to 90°	150
9.1.2	Links vs time for latitudes from 0° to -90°	151
9.1.3	Links vs time for latitudes from 70° to 90°	152
9.1.4	Links vs time for latitudes from 45° to 75°	152
9.1.5	Links vs time for latitudes from 55° to 75°	153
9.1.6	Links vs time for latitudes from 57.5° to 67.5°	153
9.1.7	Links vs time for latitudes from 57.5° to 67.5° with 30 seconds time-step	154
9.1.8	Links vs time for latitudes from -62.5° to -57.5° with 30 seconds time-step	154
9.1.9	Links vs time for longitudes from 0° to 270°	155
9.1.10	Links vs time for longitudes of 0°, 120° and 240°	156
10.1.1	Dimensions of a 1U CubeSat	172
10.2.1	Basic schematics of the EPS	174
10.7.1	Principal losses in the received signal [5]	193
10.7.2	Specific attenuation for different frequencies [5]	195
10.7.3	Galaxy noise influence in noise temperature [5]	197
10.7.4	Noise temperature variation with frequency [5]	198
10.7.5	Probability of bit error for common modulation methods [6]	201
14.1.1	Orbital Launch Summary by Year	232

Part I

ANNEX I: Orbit Design

Chapter 1

Orbit Geometry

Throughout this chapter, the bases of orbital geometry will be explained in order to correctly understand the parameters that will later be exposed when dealing with the constellation orbits (or the position of the satellites in them). However, long theoretical explanations will be avoided so as not to distract the reader from the main objective of the project.

To understand the movement in space is enough to apply the Newton's laws. These, however, need an inertial non-rotating frame to be correctly described. When dealing with Earth-orbiting, one usually chooses a reference system called *geocentric-equatorial system* which is shown in the figure 1.0.1 As can be seen, the XY plane coincides with the plane Equatorial with the X axis pointing in the direction of the vernal equinox ¹. The Z axis correspond the axis of rotation of the earth and points to the north (following the right-hand rule).

¹an imaginary line found by drawing a line from the Earth to the Sun on the first day of spring

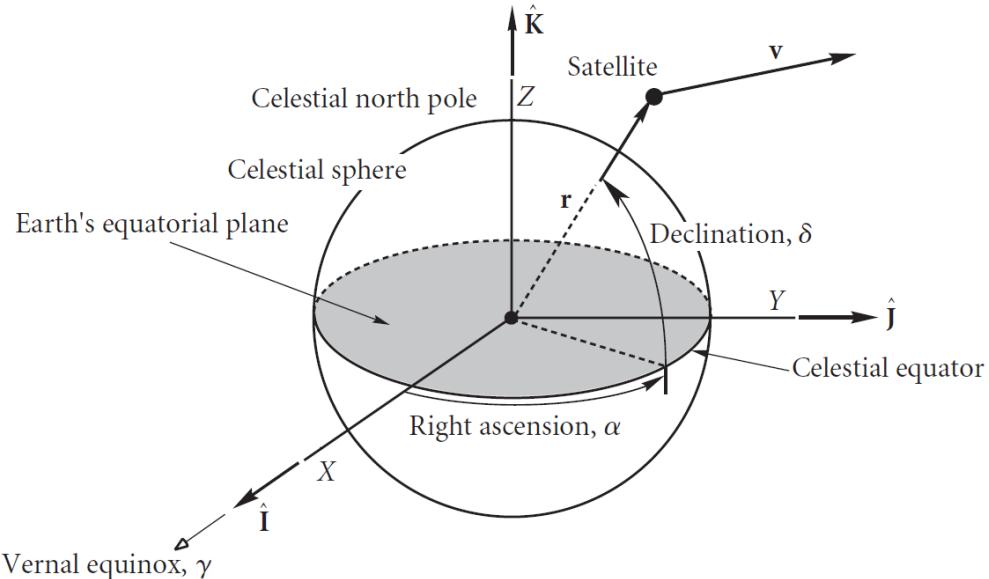


Figure 1.0.1: Geocentric-equatorial frame. Extracted from [1].

By defining this system, any point in the space can be depicted by its position vector r and we can study its movement by the velocity vector \dot{r} . These elements are useful especially for computational work but they nearly do not provide information about the orbit. For these reason, the orbital elements were developed.

Keplerian Geometry

The *Classical Orbital elements*, also known as the *Keplerian elements* as an attribution to Johannes Kepler, are six independent quantities which re sufficient to describe the size, shape and orientation of an orbit. This set of elements are shown in the figure 4.3.6 and are defined as follows:

- **Semi-major axis (a):** It is related to the size of the orbit and its defined by the sum of the apogee (furthest point) and the perigee (closest point) divided by two.
- **Eccentricity (e):** It defines the shape of the orbit with respect to that of a circle. Thus, the eccentricity of a circular orbit is null while hyperbolic orbits have an eccentricity greater than one.

Circular	$e = 1$
Elliptical	$0 < e < 1$
Parabolic	$e = 1$
Hyperbolic	$e > 1$

Table 1.1.1: Eccentricity values depending on the shape of the orbit

- **Inclination (i):** the inclination is the angle between the positive Z axis and the angular momentum vector (\mathbf{h}) which is perpendicular to the orbital plane. The inclination of the orbit can take a value from 0 deg to 180 deg. For $0 \text{ deg} \leq i \leq 90 \text{ deg}$ the motion *posigrade* and for $90 \text{ deg} \leq i \leq 180 \text{ deg}$ the motion is *retrograde*.
- **Right ascension of the ascending node - RAAN (Ω):** This parameter, along with the inclination define the orientation of the orbital plane. It is the angle between the positive X axis and the intersection of the orbital plane with the equatorial plane XY in counterclockwise direction. The intersection mentioned is called the node line and the point where the orbit passes through the node line (from south to north) is the ascension node ($0 \text{ deg} \leq \Omega \leq 360 \text{ deg}$).
- **Argument of perigee (ω):** Is defined as the angle between the ascending node and the perigee. It describes the orientation of the ellipse with respect to the frame ($0 \text{ deg} \leq \omega \leq 360 \text{ deg}$).
- **True Anomaly (ϕ):** This last quantity is used to describe the satellite's instantaneous position with respect to the perigee. Is the angle, measured clockwise, between the perigee and the satellite position. From all the orbital elements, the true anomaly is the only that changes continuously. Sometimes, true anomaly is substituted by the mean anomaly, which can be calculated using another auxiliary angle called the eccentric anomaly.

$$\cos E = \frac{e + \cos \theta}{1 + e \cos \theta} \quad (1.1.1)$$

$$M = E - e \sin E$$

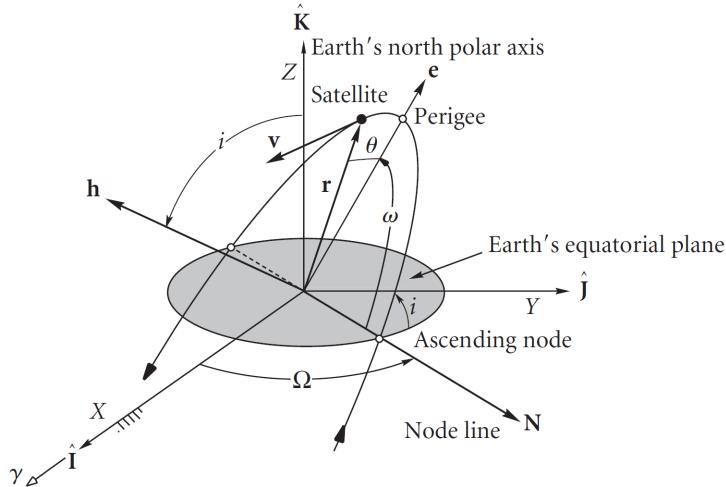


Figure 1.1.1: Geocentric-equatorial frame and the Classical Orbital Elements. Extracted from [1].

Dynamic equations

As aforementioned, the motion of an object in the space can be described using the Newton's laws. The basic idea developed by Newton is to study the Cubesat and the Earth as a spherical bodies in mutual gravitational attraction and neglect the gravitational forces caused by other objects (this is called the *two body* problem). The forces balance is simple since we only have the Earth gravitational attraction, which must compensate the centripetal acceleration of the satellite. Thus, using the law of universal gravitation,

$$-G \frac{M_E m_{sat}}{r^3} \vec{r} = m_{sat} \vec{a}_{sat} \quad (1.2.1)$$

Where G is the gravitational constant and r represents the distance between the satellite and the Earth. From the last equation, we only want to obtain the acceleration, therefore:

$$-G \frac{M_E}{r^3} \vec{r} = \vec{a}_{sat} = \frac{d^2 \vec{r}}{dt^2} \quad (1.2.2)$$

For simplicity, it is usual to denote $\mu = GM_{earth}$ resulting in the following equation:

$$-\frac{\mu}{r^3} \vec{r} = \frac{d^2 \vec{r}}{dt^2} \quad (1.2.3)$$

This expression is a second order equation that models the motion of the Cubesat relative to the Earth and it can be analytically solved. The only problem is that several hypotheses

Dynamic equations

have been applied that make the case different from reality. The formulation should be modified to take into account the effects due to:

- More bodies attracting the satellite (Sun, Moon, Venus, etc.)
- The existence of more forces like the drag, the solar radiation pressure, etc.
- The earth is not an spherical body.

The corrections for considering these things are called perturbations and they are explained in the Chapter ?? of this part of the report.

Chapter 2

Orbital Coverage

Satellite Footprint

Introduction

The first step to build a satellite network with global coverage is to compute a single satellite footprint.

The footprint of a satellite is defined as the region of Earth where a single satellite can be seen. This Earth coverage surface provided is spherical and depends on some orbital parameters such as:

- Height

When increasing height the footprint of a satellite grows.

- Elevation angle

When increasing the elevation angle, which is the angle between the satellite and the horizontal plane of an arbitrary point of the Earth, the surface seen by the satellite decreases. (This parameter will be later studied in detail)

Footprint Computation

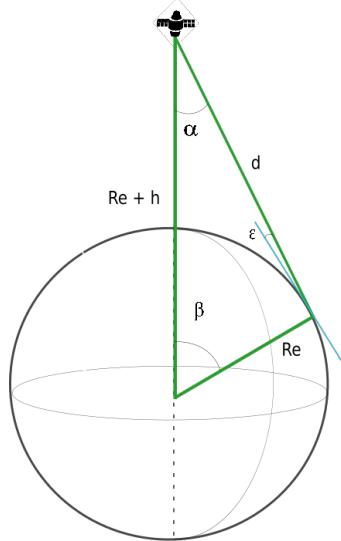


Figure 2.1.1: Single satellite coverage geometry

In order to compute the coverage area we must solve the triangle depicted in figure 2.1.1 where the basic geometry of a satellite footprint is shown.

The most needed parameters are the distance from a random point on Earth (where we can suppose our ground station to be) to the satellite denoted by d and the central angle, denoted with a β .

Applying cosines law to the triangle shown in figure 2.1.1, we obtain the following expression:

$$r^2 = R_{\text{earth}}^2 + d^2 - \cos(90 + \epsilon) \quad (2.1.1)$$

Isolating d from the equation above and changing $r = R_{\text{earth}} + h$, where h is the actual height of the satellite regarding the Earth surface, we arrive at:

$$d = R_{\text{earth}} \left[\sqrt{\left(\frac{h + R_{\text{earth}}}{R_{\text{earth}}} \right)^2 - \cos^2 \epsilon} - \sin \epsilon \right] \quad (2.1.2)$$

From the figure 2.1.1 we can also extract a relation between the central angle, the distance d and the elevation angle. This relation together with the equation 2.1.2 allow us to find β .

$$d\cos\epsilon = (R_{earth} + h) \sin\beta$$

$$\beta = \frac{1}{R_{earth} + h} \arcsin [d(\epsilon)\cos\epsilon] \quad (2.1.3)$$

Once the central angle β has been computed we are able to obtain the footprint satellite's are using the equation below:

$$S = 2\pi R_{earth}^2 (1 - \cos\beta) \quad (2.1.4)$$

The size of the footprint will determine the level of coverage our constellation provides, therefore when deciding the value of the orbital parameters it has to be a factor to consider.

Elevation Angle

The angle of elevation is essential to calculate the geometry of our constellation. As discussed previously, our aim in this project report is to justify how global coverage will be fulfilled. First, we define for a given groundstation the angle between its beam pointing right to the satellite and the horizontal local plane as the elevation angle. Secondly, a study is conducted in order to relate the height of the satellite, the elevation angle and the coverage of the Earth. Finally, we complete our orbital design by configuring a constellation that will securely define a global coverage fulfillment. Next, we will be defining how these parameters are related.

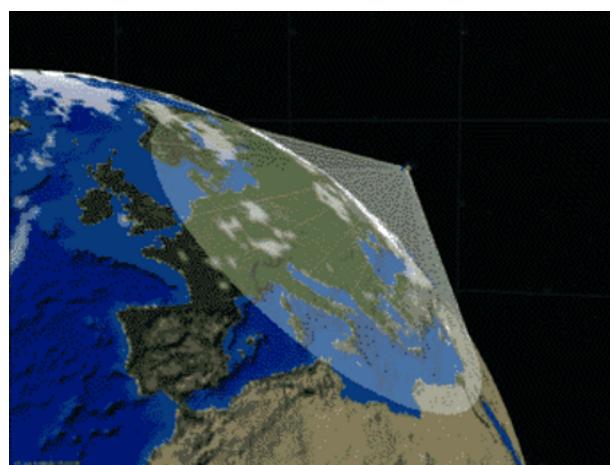


Figure 2.2.1: Elevation angle cone. Source: NOAA

Elevation angle cone

Global coverage will be discussed considering the elevation angle and its resulting footprint on Earth. The elevation angle is described by the angular orientation of the antennas in the ground station. However, this angle is also perceived by the satellite in a similar way - it will vary depending on the orientation of the satellite and the angle between horizontal local planes. In order to describe the footprints we must define a cone which vertex is set at the antennas of the satellite, pointing down to Earth, and which generatrix is given by the angle of elevation. This elevation angle based cone is the description of the paths that our communications can take place. In other words, the generatrix of this cone is setting the limits in which the antenna will operate as function of the elevation angle. This implies that our satellite will be able to communicate to all the points contained in the cone. Finally, this cone will be describing a circular surface on top of the Earth which we will call the footprint of the satellite. Additionally, this footprint is the coverage that a single satellite can generate, hence we will be distributing satellites all around the Earth in order to fulfill global coverage.

Atmospheric restrictive conditions

In order to obtain the final restrictive angle of elevation needed to contact the ground stations some considerations have to be made. First, a description of the different atmospheric conditions will be defined. Then, we will relate these to our bandwidth in order to analyse if they must be taken into account when communicating with ground stations. [elec2013cantero]

- **Atmospheric gases:** water vapour and oxygen absorptions; important when frequencies are above 3 GHz. More information [64] and [07328546]
- **Precipitations and Clouds:** these conditions are relevant for signals above 10GHz.
- **Cross Polarization Discrimination:** direct consequence of both terrestrial links and rain. Related to non-spherical rain drops which have a polarization rotated towards the component of the major axis, and hence may attenuate a signal wave.
- **Scintillation** is a rapid fluctuation in signal amplitude at low elevations.

– **Radio Refracting Index:** for elevation angles below 3 degrees (especially those below 1 degree) and depending on the latitude of our satellite we may find big signal losses due to the resulting differential ray bending.

– **Ionosphere layers:**

D layers: 60-90km. Considerable signal absorptions for 10 MHz and below, with progressively less absorption at higher frequencies and oblique incidences.

E layers: 90-150 km. Absorptions relevant for frequencies lower than 10 MHz, although for sporadic E propagations this value may be increased to 50MHz.

Sporadic E layers: Reflections of radio waves in this thin-cloud small layer may reach to frequencies up to 225MHz. These layers are usually formed following the E layers altitudes.

F layers: 150-500 km and higher. No absorptions or reflections for these layers. The F2 region allows the longest communication paths, above 210km of altitude.

By means of these physical phenomena we can subtract the elevation angle as function of the latitude. However, we must take into account that these physical conditions give a value for the elevation angle which may not be the most restrictive. Global coverage conditions, bandwidths, inclination and the final distribution of our constellation will be considering this elevation angle and viceversa, iteratively.

The ASTREA CONSTELLATION was designed and optimized in order to fulfill global coverage for a constant elevation angle - respect to the latitude - of 20 degrees.

Our constellation will be operating at S-band for telemetry and X-band for data relay. Therefore, the satellites need to be operating up to 10 GHz. This directly implies that physical conditions such as atmospheric gases, precipitations and clouds must be studied when determining the elevation angle needed.

The minimum elevation angle is applied in low latitude regions for constellations based on

polar orbits whereas this value is also applied out of the low-latitude region for inclined orbit constellations [a general evaluation criterion]. The minimum elevation angle is a specific value which is equivalent to the maximum elevation angle needed to fulfill coverage at a given latitude, considering that the distance between planes is maximum at the equator and that it is reduced for higher latitude positions.

This elevation angle is maximum in a Walker Delta constellation when the latitude is equal to the orbital inclination angle[a general evaluation criterion]. This means that the limiting restrictive elevation angle that we need in order to fulfill global coverage is defined at latitude equal to 72 degrees, which is the inclination of our constellation. Otherwise, we can define a constant elevation angle that will apply to the equator, which will then be, for this model, the restrictive condition.

Accordingly, the approach considered is that of a constant elevation angle to fulfill global coverage at 20 degrees. This implies that our constellation is configured and distributed in order to optimize coverage both at the equator and at the maximum elevation angle latitude. This value has been contrasted and discussed considering the atmospheric conditions and analysing experimental data, which contemplates also the rotation of the Earth among others.

This constant elevation angle model will be very useful in order to analyse and calculate the distribution of the constellation. Nevertheless, we need to describe in an accurate way the minimum elevation angle respect to the latitude. This is why a different model must be approached.

Thus, we need to describe the elevation angle respect to the latitude of our constellation taking into account all considerations above. First, for a latitude of 0 degrees the value of the minimum elevation angle will be of 10 degrees. In our model we have considered that this value was of constant 20 degrees, so in fact we have redundant global coverage. At latitudes between the equator and 45 degrees our second model increases linearly to 15 degrees. From 45 to 60 degrees the elevation angle also increases linearly to 22 degrees. Then, from 60 to 70 the value increases highly reaching a peak at 70 degrees, where the elevation angle will be of 30 degrees. Finally, from 70 to 80 degrees this model is reduced linearly to 15 degrees, and from 80 to the north and south poles it falls to 0 degrees. This is a simple model that will guarantee global coverage, especially at the latitudes of our ground stations

For the distribution of ground stations we need to guarantee that these will be covered either by one satellite or two at any given moment. As discussed before, the model used was based on a constant 20 degree constant elevation angle. However, for this last model that we have described - which is more realistic - we obtain more coverage than for the constant model except for those regions next to the peak. The most restrictive latitude is now 60 degrees - where all the ground stations are set - and has a 22 degree restriction of the angle of elevation, which is higher than the constant model described previously. These facts imply the following:

- At low latitudes (between 0 and 30 degrees) the constellation fulfills global coverage generously.
- At ground station latitude (60 degrees) the constellation is covering the station successfully. As discussed before, our first model considered a constant 20 degree elevation angle instead of the 22 degrees that now must be corrected. For the previous model coverage was well established with margin. For the latter, the margin has decreased but coverage is still complete. Note: each orbit could be reduced by a number of satellites per plane, but this would endanger the correct and stationary working of the constellation. In this case we would not be able to control possible incidences such as unoperative satellites with enough margin.
- The ground stations are covered at all time for at least one satellite.

Elevation angle of other current constellations

Analysing the minimum elevation angle needed in order to fulfill global coverage requieres, as mentioned before, the understanding first of the restrictive conditions of the atmosphere and how these will alter it. As a consequence of the different physical conditions given before we will be able to determine a relation between latitude and elevation angle. All the same, the elevation angle depends on the bandwidth in which the satellites operate, hence different distributions of this angle respect to the latitude will be described depending on the bandwidths used.

- Celestri: 18.8 to 20.2 GHz at 48 degree inclination.
- GlobalStar: 2.4 GHz at 52 degree inclination.
- Iridium: 20 to 30 GHz at 90 degree inclination - polar orbits.

Comparing our configuration to other present constellations some clarifications can be made:

- The minimum elevation angle peak is proportional to the bandwidth at which the satellite is communicating with Earth. For instance, Iridium's peak of elevation angle is the highest relative to the other configurations since it is also working with the highest frequency signals.
- The latitude position of the peaks is related to the inclination of the constellation. Iridium, - a polar orbit based configuration - describes a peak at 90 degrees of latitude whereas Celestri and GlobalStar are near 40 to 50 degrees.

With these tendencies our model can be confirmed as function of the frequencies of the signals and related to the inclination of the orbits.

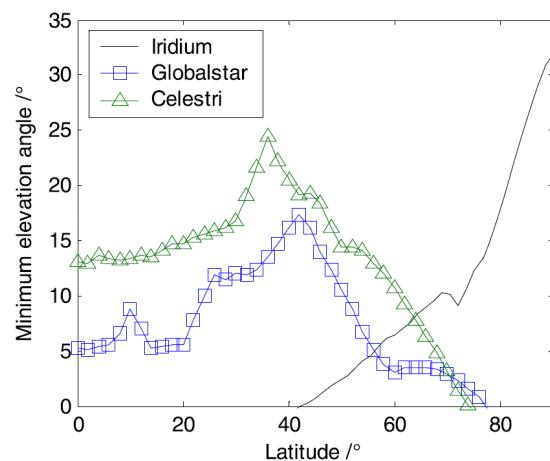


Figure 2.2.2: Minimum elevation angle as function of latitude. Source: [a general evaluation criterion]

Minimum Plane Inclination

As it has been pointed before, there are several factors to take into account in order to design a constellation that provides global coverage on Earth. In this section the minimum inclination to achieve that purpose is assessed. Using the theory previously developed, we can observe the following results:

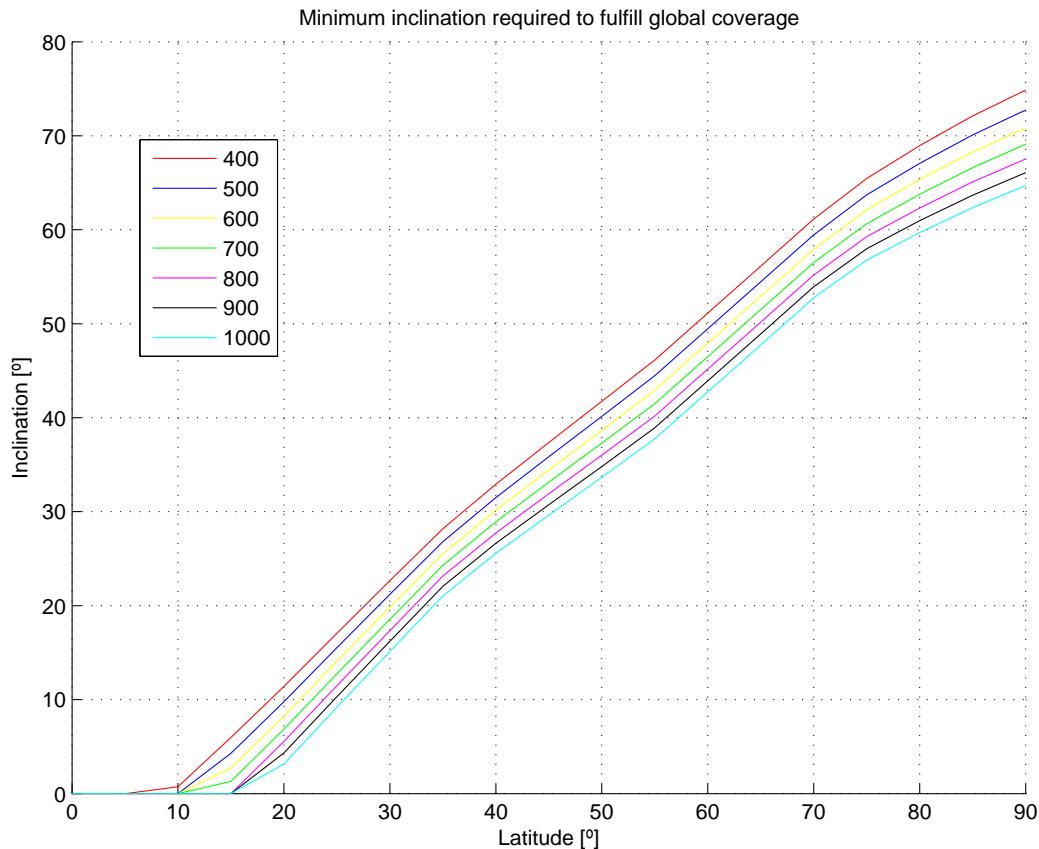


Figure 2.3.1: Minimum Inclination to provide coverage at different latitude for different orbit apogees.

As it can be observed, if the goal of the design is to provide full global coverage, the distribution of elevation angles with latitude is not significant, since the inclination is required to be higher than approximately 75° . In the other cases, the change of minimum elevation angle distribution causes changes of tendency in the distribution of inclination required.

In conclusion

The main point is that there is a limit inclination for a Walker-Delta constellation configuration in order to provide global coverage at the desired latitude. With this study, this limits in the design algorithms can be set.

Satellite to Satellite Visibility

One of the restrictive conditions that we must take into account is the visibility between satellites. Communications among different satellites is they key point of our constellation. Therefore, this has to be guaranteed considering a model which will

represent the conditions of the atmosphere for LEO communications.

In order to fulfill communications among satellites we must consider that a straight beam can be described between two consecutive satellites, which will then communicate with others. These two satellites will need to be at a distance such that the Earth itself doesn't interfere in this straight beam. Depending on the bandwidth of our constellation we will also have to consider that this communication beam will not interfere with a given element of the atmosphere such as the upper layers of the ionosphere. Thus, a model will be developed in order to limit the minimum altitude at which this beam is guaranteed to pass through safely.

This model is a restrictive condition that we need to satisfy when designing our constellation. The highest restrictive conditions are the upper layers of the ionosphere, specifically the E layers at 150 km above the surface of the Earth. Reflections and absorptions can occur for both E layers and sporadic E layers. E layers may reflect signals of frequencies below 10 MHz whereas Sporadic E layers can be a problem up to 225 MHz. Working for S bands and X bands implies that neither of these layers will alter the signals of our constellation.

Operating and computing with these conditions a maximum distance is obtained which defines how far these satellites can be from each other. A simple equation is used to calculate this distance considering the height of the satellites and the height of the E layers in the atmosphere.

$$d = 2\sqrt{(R + h_{sat})^2 - (R + h_{atm})^2}$$

$$h_{sat} = 550 \text{ km}$$

$$h_{atm} = 150 \text{ km}$$

$$R = 6371 \text{ km}$$

The final expression for the distance between two satellites indicates that distance between two satellites has to be smaller than 4640 km approximately. For this result we conclude

that this restrictive condition is actually less restrictive than the 9 planes needed for our constellation. Thus, satellite to satellite visibility is a parameter which will not affect the design of our constellation after all.

Market Study: Current Nanosatellites in Orbit

Criteria for the orbital height of the satellites

Satellites currently in Orbit

If only geometric considerations were to be applied in the design of a satellite constellation, it is clear that the higher the orbit the broader is the footprint in the surface leading to a smaller number of satellites. However, if the service of communications is to be offered, the satellites currently in orbit or in design phases need to be at higher orbit than the one of the constellation. The purpose of that requirement is to intersect the field of view of the satellites that nowadays point to Earth.

From source [?] we can study how the currently on orbit satellites are launched and specially, in which orbits. The results of the study of this source is presented below. All of them are in Low Earth Orbits, and half of them above 550km. In total, there are 203 operational satellites.

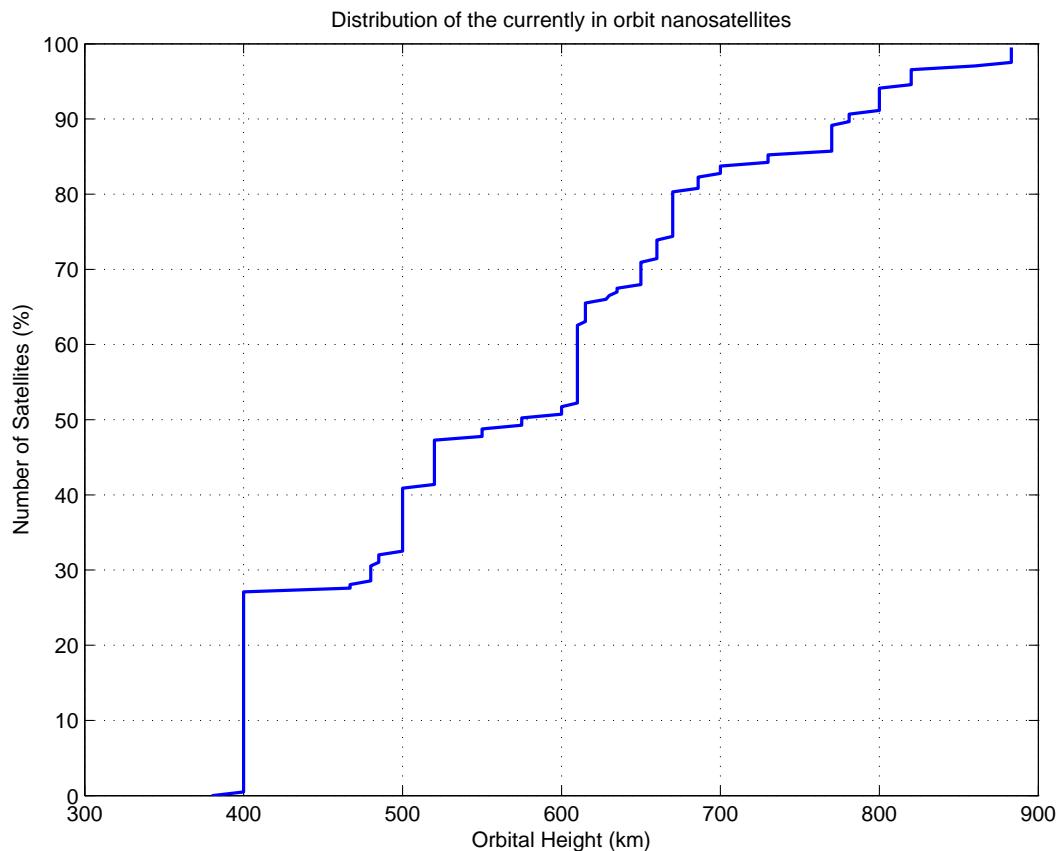


Figure 2.5.1: Distribution of the currently in orbit nanosatellites.

The most interesting potential clients

Lots of satellites are orbiting at heights lower than 500km, mainly because one of the most feasible way of launching a small satellite is from the International Space Station. However, these very low LEOs are related to very high speeds and specially to low lifetimes, since drag affects them in a more significant way. To the interest of the constellation, the satellites at higher altitudes are a better commercial target, since they are going to be in orbit for longer missions. In addition, the same orbit decay problems are avoided for the constellation satellites.

New Space: Adapting to new society needs

Nowadays new satellites willing to provide services to Earth are being positioned closer than ever. Where closer can be applied in many points of view. Physically, the satellites are placed every time at lower orbits, since the energetic requirement is lower. Technically, the space certified materials and hardware are becoming more feasible, and new launchers are smaller. In the end, everything comes down to an economic approach, launching satellites is becoming cheaper every time and this means closer to the private pocket.

In the future, the possibility of using the Astrea constellation to contact Earth can reduce the requirements for the antennas and AOCSSs to communicate with ground, leading to a whole new level of resources for the satellite payload. For instance, by communicating to the constellation pointing to outer space instead of pointing down to Earth. That is just a way in which Astrea is in the New Space Generation.

In conclusion, In the decision process one of the statistics considered with certain weight will be the following: the ratio of satellites at which the constellation will be able to provide service considering that nowadays all of them point down to Earth.

Chapter 3

Constellation Configuration

"Our two greatest problems are gravity and paperwork. We can lick gravity, but sometimes the paperwork is overwhelming."

Werner von Braun, 1958

Introduction: The Global Positioning System Example

Depending on the application the Space Segment of a mission can vary in an infinite number of ways. Probably the most famous and widely used satellite constellation is the Global Positioning System satellite network. In this case, it uses an irregular geometry.

The GPS Constellation: An example of irregular distributed orbits [?]

The GPS is a constellation property of the U.S. It provides positioning, navigation and timing. The constellation was designed with a 24-slot arrangement to ensure a visibility of at least four satellites from any point on the planet. Nowadays the constellation has expanded to a total operative number of 27-slot since June 2011. Some characteristic parameters of the satellites are the following:

- Orbit: Almost Circular
- Height = 20,200 km (MEO);
- Lifetime = 12.5 years;

Polar Orbit Constellation

- Satellite Cost = 166 million USD;
- Inclination = 55° ;
- Number of planes = 6;
- Phasing: 30° - 105° - 120° - 105° ;

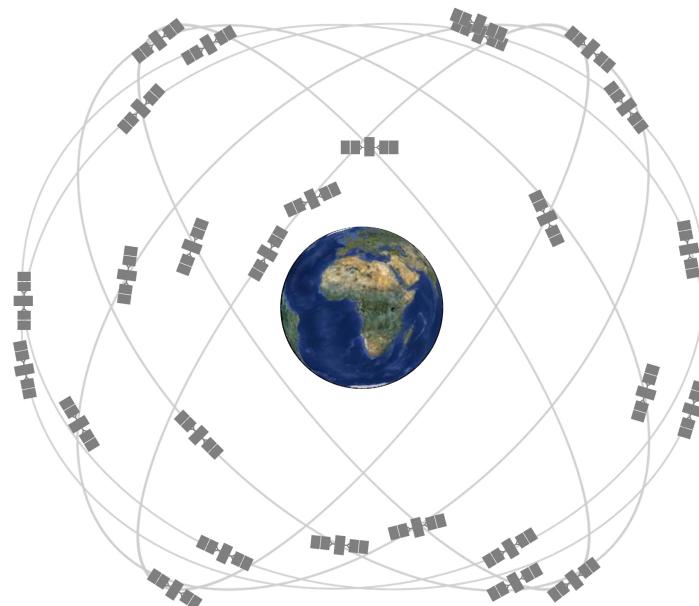


Figure 3.1.1: Distribution of the expanded 24-slot GPS constellation. [?]

Polar Orbit Constellation

Introduction

Polar Orbits are probably the simplest way to configure an evenly spaced constellation. As we will see in the section **Orbit Perturbations** when the inclination is the same for all the planes, the deviations tend to be the same for all the satellites. In addition, the computation of the number of satellites required is also easier.

The Iridium Constellation: An example of near polar orbits [?]

The Iridium constellation is a private constellation. It provides voice and data coverage to satellite phones among other services. The constellation was designed with 77 satellites, giving name to the constellation by the chemical element. The constellation was reduced to a number of 66. Sadly, Dysprosium is not such a good commercial name. Some characteristic parameters of the satellites are the following:

- Orbit: Almost Circular
- Height = 781 km (LEO);
- Satellite Cost = 5 million USD;
- Inclination = 86.4° ;
- Number of planes = 11;
- Phasing: Regular;

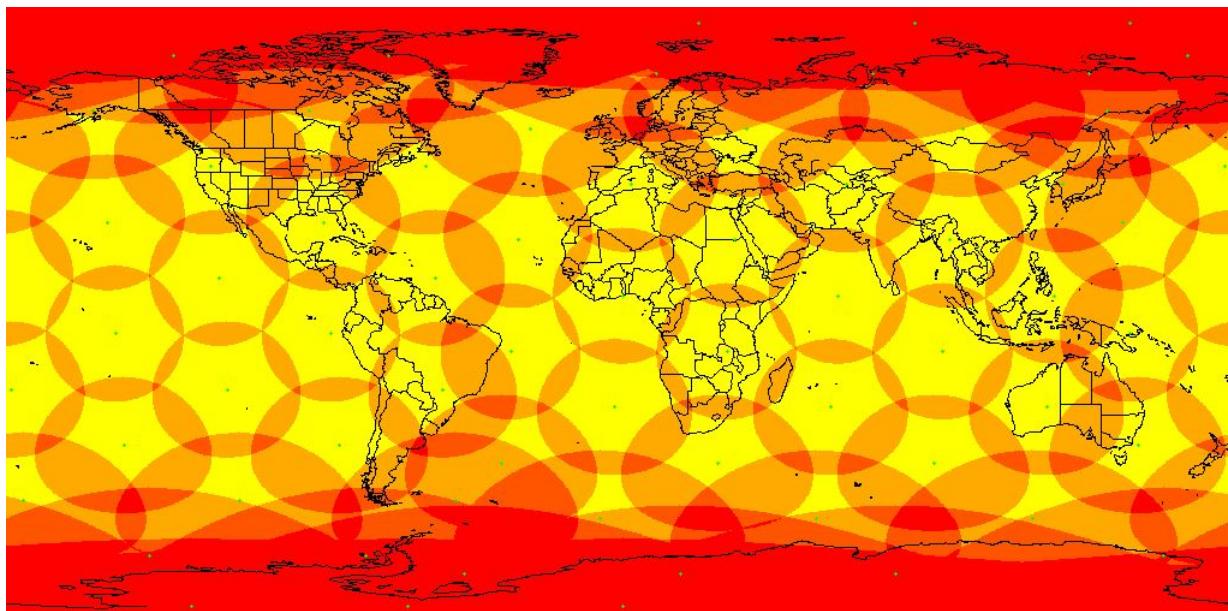


Figure 3.2.1: Distribution of the 66 Iridium constellation satellites. Generated using [?]

General Configuration

The Polar Orbits configuration consists in the distribution of plains with inclination equal to 90 degrees. Note that the satellites will be travelling parallel to the satellites of the next plain except for the communications between the first and the last plane.

The communications between satellites in antiparallel directions require less space between plains to be fulfilled. In order to solve this inconvenience the separation between the first and the last plain is reduced.

The plains are splitted in the following pattern:

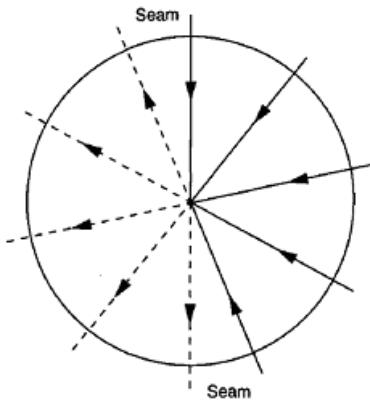


Figure 3.2.2: Distribution of the planes for Polar Orbits design.

The Streets of Coverage Method

This Street of Coverage Method is obtained from [4]. As you can see in the figure below, the relations between angles seen from different satellites can be easily computed. The main variables are the following:

Streets of Coverage Method Variables	
N	Number of Satellites
n_p	Number of Planes
N_{pp}	Number of Satellites per plane
S	Separation between satellites of the same plane
D	General space between planes [$^{\circ}$]
D_0	Space between antiparallel planes [$^{\circ}$]
ε	Elevation angle [$^{\circ}$]
λ_{street}	Street of coverage Width [$^{\circ}$]
λ_{max}	Maximum footprint Radius [$^{\circ}$]

Table 3.2.1: Streets of Coverage Method main variables

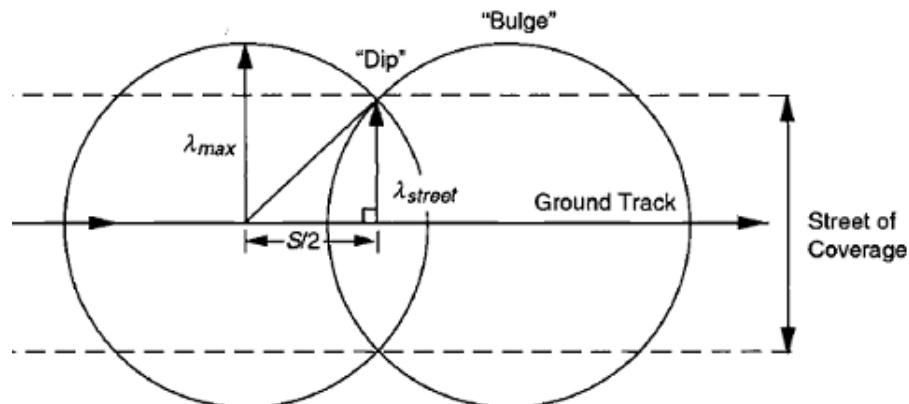


Figure 3.2.3: Single plain street of coverage. The footprints of the satellites superpose leading to a street. [?]

From the figure it can be inferred:

$$S < 2\lambda_{max}$$

$$\cos(\lambda_{street}) = \cos(\lambda_{street})/\cos(S/2)$$

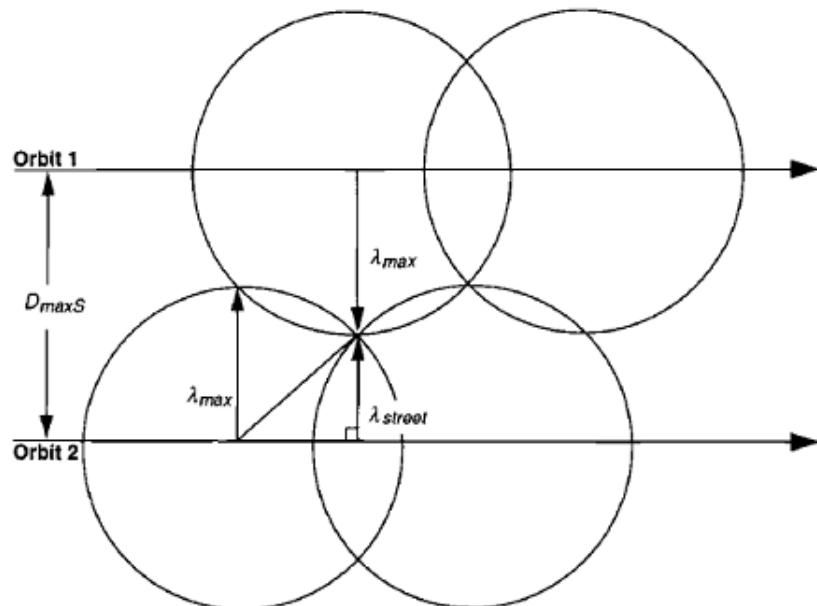


Figure 3.2.4: Two plains streets of coverage. An optimum phasing needs to be obtained. [?]

From this point of view, in general:

$$D = \lambda_{street} + \lambda_{max}$$

n For the antiparallel planes:

$$D_0 = 2\lambda_{street}$$

And the overall relationship between planes sums:

$$180 = (n_p - 1)D + D_0$$

The algorithm for computing the Streets of Coverage Results is defined in the following way:

Inputs: Height, elevation, inclination... $\rightarrow \lambda_{max} \rightarrow N_{pp} = \left\lceil \frac{360}{2\lambda_{max}} \right\rceil \rightarrow S = 360/N_{pp} \rightarrow \lambda_{street} \rightarrow n_p \rightarrow N = N_{pp} * n_p$

Results of Streets of Coverage

A MATLAB routine has been designed to compute the previously described algorithm. In this conceptual design phase, different heights are computed in order to see the evolution of the number of satellites.

General Solution

The program is run in a broad range of parameters to see the evolution of the number of satellites. As it can be predicted, as the height increases the number of satellites is reduced. The reason is that the footprint of the satellites increases with the height. In addition, as the minimum elevation over the horizon to contact the satellites is reduced, the number of satellites is also reduced for the same reason.

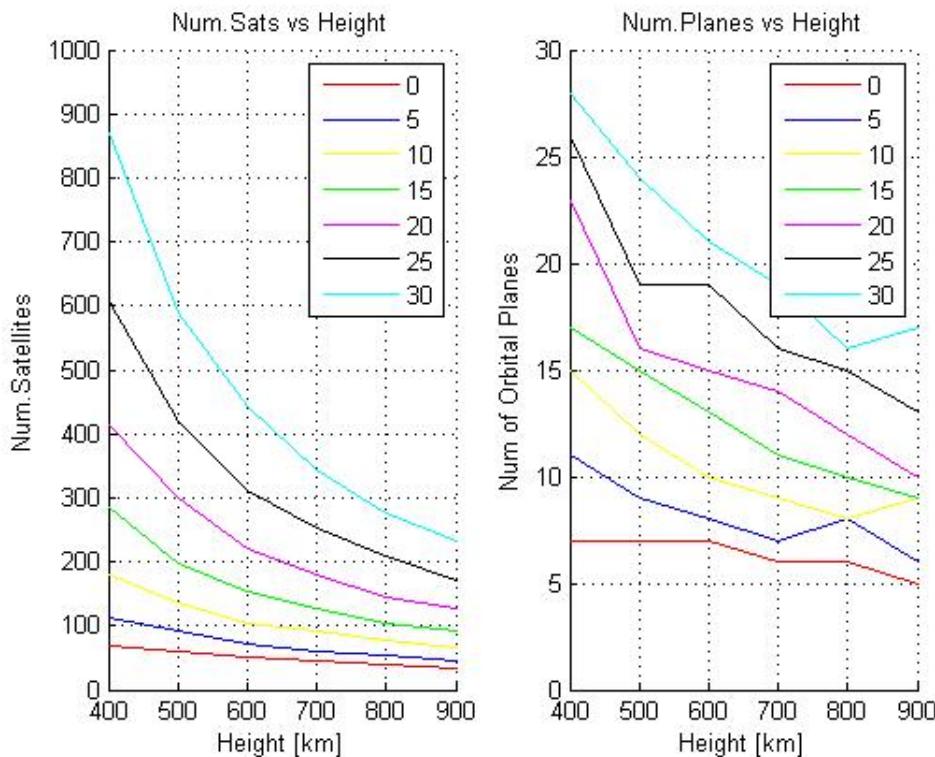


Figure 3.2.5: Variation of number of satellites for different heights and elevation angles

Detailed Solution

Given the previously justified assumptions, the same simulation is computed for a more reasonable range of results. In this case, the elevation is set as:

$$\varepsilon = 20\check{z}$$

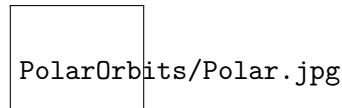


Figure 3.2.6: Variation of number of satellites for different heights between 500 and 600km.

Conclusion

The computation and the design of this constellation requires small computational and conceptual effort. However, the number of satellites and planes is greater than expected. Even though the technical complexity can be reduced, the availability of small launchers to reach this particularly inclined orbit is also small. In conclusion, more constellation configurations need to be assessed to compare and select the most feasible one.

Walker-Delta Constellation

Walker Delta Pattern constellations are a type of symmetric, inclined constellation made of equal-radius circular orbits, with an equal number of satellites each one. There are several ways to construct a Walker-Delta Constellation:

- Full Walker-Delta Configuration
- Semi Walker-Delta Configuration
- Custom Walker-Delta Configuration

Full Walker-Delta Constellation

Characteristics

A typical delta pattern has the following characteristics:

- The constellation contains a total of T satellites evenly spaced in each of the P orbital planes. All planes have the same number of satellites, defined as S , equally distributed. Thus:

$$T = SP \quad (3.3.1)$$

$$\Delta\varphi = \frac{2\pi}{S} \quad (3.3.2)$$

Where $\Delta\varphi$ is the angle between satellites in the same plane.

- All orbits have equal inclinations δ to a reference plane. If this plane is the Equator (it usually is), then the inclination δ equals the orbital parameter inclination i [2].

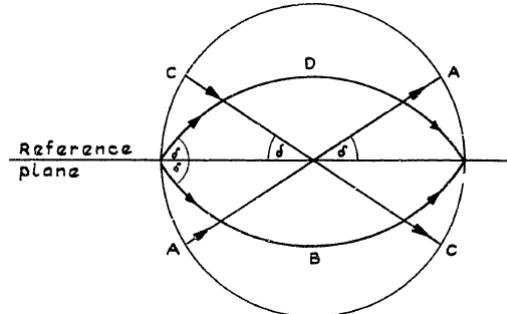


Figure 3.3.1: Definition of the inclination δ . Extracted from [2]

- The ascending nodes of the orbits are equally spaced across the full 2π (360° of longitude) at intervals of:

$$\Delta\Omega = \frac{2\pi}{P} \quad (3.3.3)$$

- The position of the satellites in different orbital planes is measured through the factor F . When a satellite is at its ascending node, a satellite in the most easterly adjacent plane has covered a relative phase difference F . The real phase difference is defined as:

$$\Delta\Phi = F \frac{2\pi}{P} \quad (3.3.4)$$

In order to have the same phase difference between all orbital planes, F is defined as an integer, which may have any value from 0 to $(P-1)$.

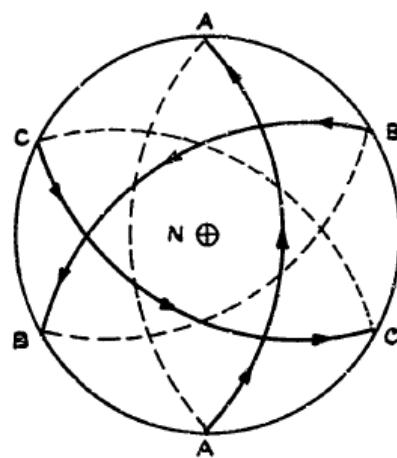


Figure 3.3.2: Delta pattern as seen from the North Pole. Extracted from [3]

With these characteristics, delta constellations are more complex than polar constellations. Because of the inclination of the orbits, the ascending and descending planes and the

coverage of the satellites continuously overlap. This characteristic is a constraint on intersatellite networking because the relative velocities between satellites in different orbital planes are larger than in a polar constellation. Consequently, tracking requirements and Doppler shift are increased [?].

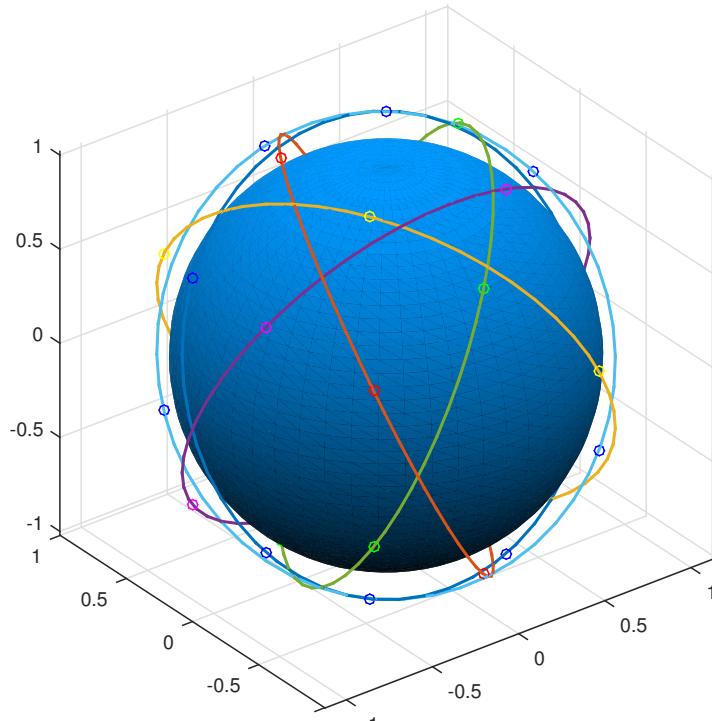


Figure 3.3.3: Delta pattern 65°: 30/6/1

Notation

J.G. Walker developed a notation to define this constellations with only 4 parameters [3]:

$$i : T/P/F$$

Since all satellites are placed at the same altitude, with these notation the shape of the pattern is completely determined. However, to determine all the orbital parameters it is necessary to know the radius of the orbits.

Coverage

The previous section has shown that in polar orbits the coverage of the constellation could be determined with the streets of coverage method. On the other hand, in delta patterns it is necessary to study each configuration to verify its coverage. J.G. Walker determined that delta patterns gave better coverage than polar orbits, but not substantially better

in the case of single coverage. This kind of patterns are more useful for double or triple coverage constellations, as it can be seen in Figure 3.3.4. However, his calculations were for a low number of satellites, so it is necessary to compute new results for the number of satellites of the Astrea constellation.

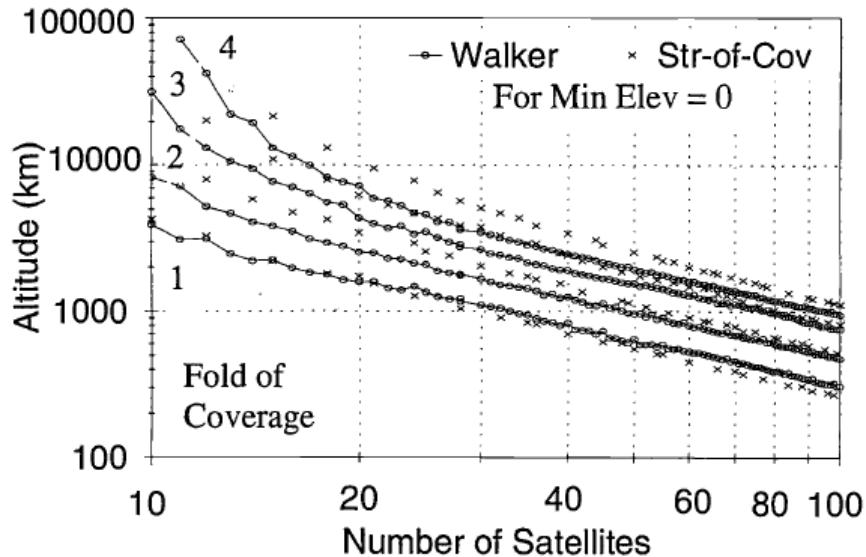


Figure 3.3.4: Minimum altitude for continuous global coverage. Comparison between polar patterns and Walker delta patterns. Extracted from [4]

Semi Walker Delta Configuration

In order to reduce the necessary costs to design this satellite-based constellation some other configurations will be discussed. The Walker Delta Configuration (WDC) represents the most general constellation for a given inclination different to 90 degrees, i.e. 75 degrees. The WDC is a uniform based 360 degree generated configuration with equidistant orbits, which implies a certain redundant Earth coverage as described in the previous chapter. However, this can and will be solved by generating a 180 degree constellation - Semi Walker Delta Configuration (SWDC) - which will also fulfill global coverage although having some inconveniences.

Advantages

- **Distance between planes reduced.** With the SWDC constellation the redundant orbits are directly corrected, thus the distance between planes is reduced to half, as results from the geometry itself.

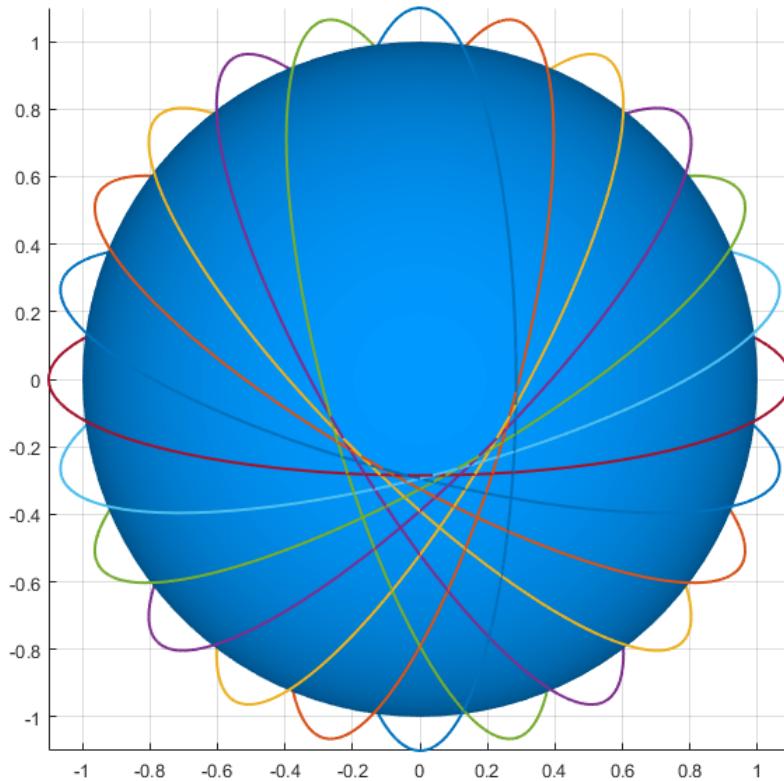


Figure 3.3.5: 12 plane SWDC. Note the gap and the equidistant planes

- **Less number of planes needed.** This means that in order to approach global coverage fewer planes will be required due to the decrease in distance between planes.
- **Satellites following the same direction - sense** With the SWDC constellation the orbits have no interaction with each other, thus the satellites for each orbit can be set following the same direction. This will significantly improve the communications among satellites from different planes; also, we will be avoiding the Doppler Effect.

Disadvantages

- **Gap configuration.** With the SWDC constellation the main problem is the gap that results from configuring the constellation at a given inclination and describing equidistant orbits. In order to fulfill global coverage this gap will have to be covered by means of auxiliary orbits.

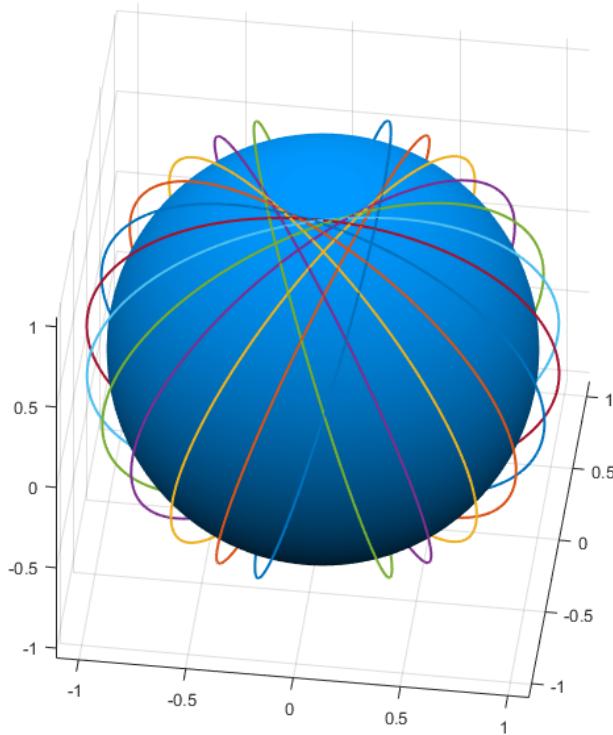


Figure 3.3.6: This geometry distribution induces a large anti-symmetric gap

Other Walker Delta Configurations

As we have discussed for the SWDC, the main disadvantage respect to the Walker Delta Configuration is the fact that a gap is obtained, thus a global coverage network cannot be described. In order to cover the entire Earth we have analysed some ways of covering the gap with auxiliar orbits.

SWDC including an additional polar orbit.

This polar orbit would be set directly on top of the gap described by the SWDC. The main issue with polar orbits, as discussed before in this report, is the complex reorientation and decay in inclination that takes place. We must take into account these considerations when covering the entire Earth, especially if we only have one polar orbit

in our constellation.

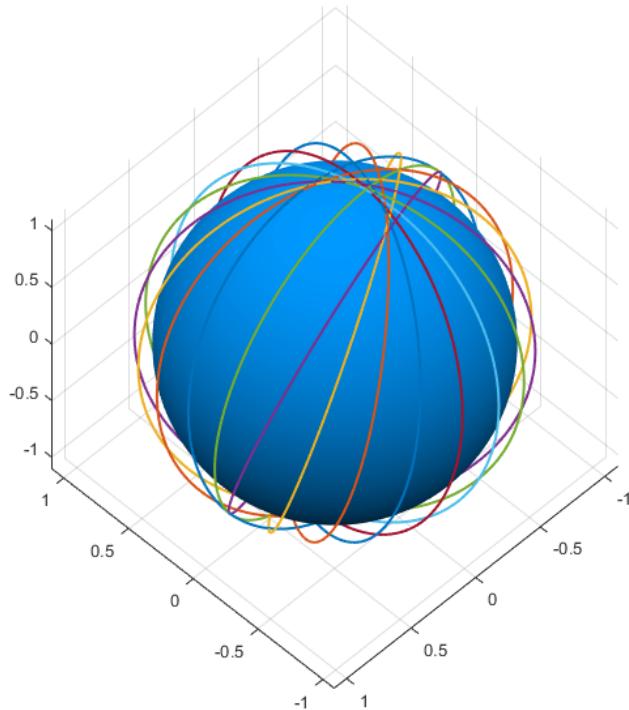


Figure 3.3.7: Added polar orbit to the 11 plane based SWDC

Mixed Walker Delta.

In order to avoid using polar orbits and their complex reorientations, we can contemplate adding planes to the SWDC. In result, different configurations distributed around the Earth can be described and set in order to fulfill global coverage. As discussed before, the SWDC constellation is generated around 180 degrees whereas the Walker Delta Constellation is a 360 degree generated configuration. This Mixed Walker Delta (MWDC) is the result of adding some planes to the SWDC, thus a constellation can be generated for different degree values, such as 200, 225, 240, etc.

After different mathematical approaches and optimal solutions, the department of Orbital Design considered that the best option in order to have a global coverage constellation with the least economic and strategic issues - exposed and discussed in previous chapters - would be that of a 225 degree generated MWDC, defined by 9 planes and 21 satellites per plane. This configuration was found optimizing the whole Earth in order to have full coverage without gaps (except for the limitations of this model at high latitudes). An important consideration is that we also analysed other Mixed Walker

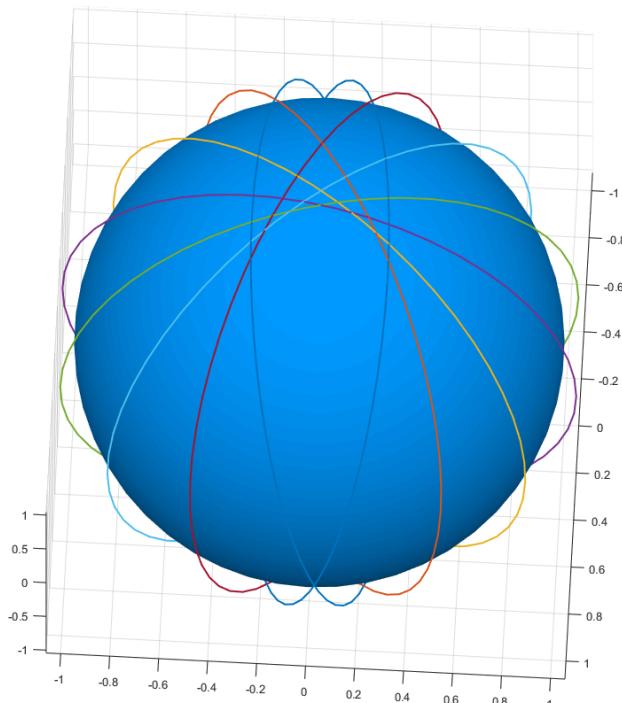


Figure 3.3.8: 8 plane based MWDC generated for 210 degrees

Delta Configurations for 210 and 240 degrees, but these resulted in a more expensive distribution of satellites.

Testing Method

Introduction

To design Astrea constellation the orbit parameters must be decided following the established requirements. As seen in the previous sections, there are different types of constellation that must be considered when selecting those parameters.

The main requirement in the bases of this chapter is to fulfill global coverage of the Earth. Therefore all the possible solutions have to be tested to ensure they pass this specification.

Method Bases

The testing method is designed to evaluate the achievement of global coverage. The main variables needed for the development of it are the following:

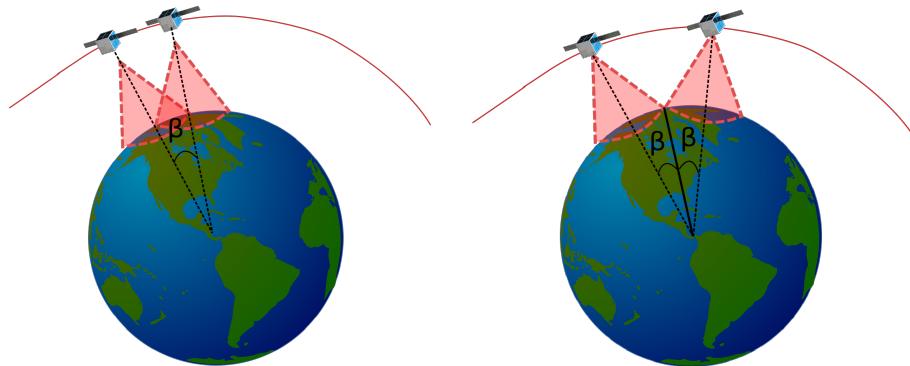


Figure 3.4.1: Geometrical conditions needed to fulfill global coverage.
On the left: Condition between satellites of different planes.
On the right: Condition between satellites of the same plane

Coverage Testing Method Variables	
typeC	Type of constellation
ε	Elevation angle [$^{\circ}$]
h	Height [km]
in	Inclination angle [$^{\circ}$]
n_p	Number of Planes
N_{pp}	Number of Satellites per plane

Table 3.4.1: Coverage Testing Method main Variables

It consist in evaluating all the possible variables combinations within established margins and testing them to know if they fulfill the determined conditions than ensures global coverage.

Global Coverage Conditions

Same plane condition

In order to fulfill the desired coverage, the distance between two satellites on the same plane must not be more than two times the central angle β . This condition is visually represented in Figure 3.4.1 .

Different plane condition

To accomplish the coverage requirements, the distance between two satellites on different planes must not be more than the central angle β . This condition is visually represented in Figure 3.4.1 .

Results of Testing Method

A MATLAB routine has been designed to compute the describe algorithm. In this phase different values of all the variables have been computed in order to found the most suitable solution. The values tested are the following:

Coverage Testing Method Variables	
typeC	[180 210 225 240 360] [°]
ε	[20] [°]
h	[540-550] [km]
in	[70-80] [°]
n_p	[5-12]
N_{pp}	[10-24]

Table 3.4.2: Testing Values for the Coverage Testing Method

General Solution

The program has been runned for all the range specified above to see the evolution of a satellite network configuration regarding the variation of the orbital parameters in order to find the best constellations options.

As it can be deduced both the number of planes and satellites decreases when increasing height because as explained before the footprint of the satellites gets incremented with height. If height is left as a constant, a less intuitive results are obtain. We have now different configurations in terms of number of satellites an planes due to the variation of the inclination angle of the planes. In the Figure 3.4.5 is shown the results obtained for one of the analysed configurations.

Once all the possible configurations have been computed, the ground track of three of them has been ploted to visualy check the coverage obtained.

Conclusions

From the developed code that runs all the parameters needed to define a Walker Delta configuration it is possible to obtain for a chosen requirement which are the optimum configuration. Therefore defining the criteria in function of the constellation needs it will be possible to optimize the design. The configurations that will be later considered to perform an analysis of weighted weights are extracted from this routine.

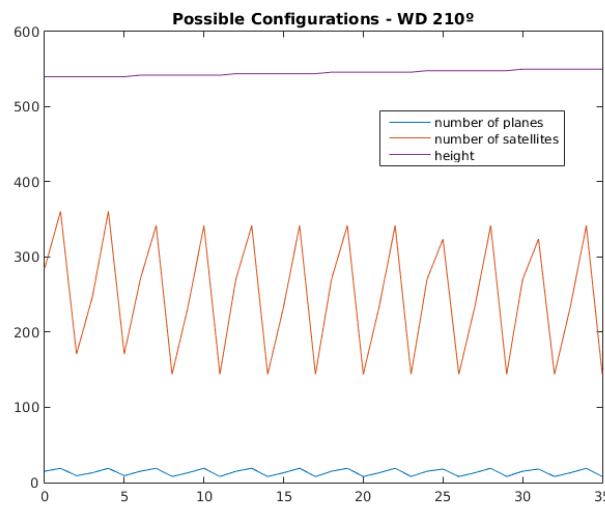


Figure 3.4.2: Possible satellite configurations for a 210° Walker Delta configuration

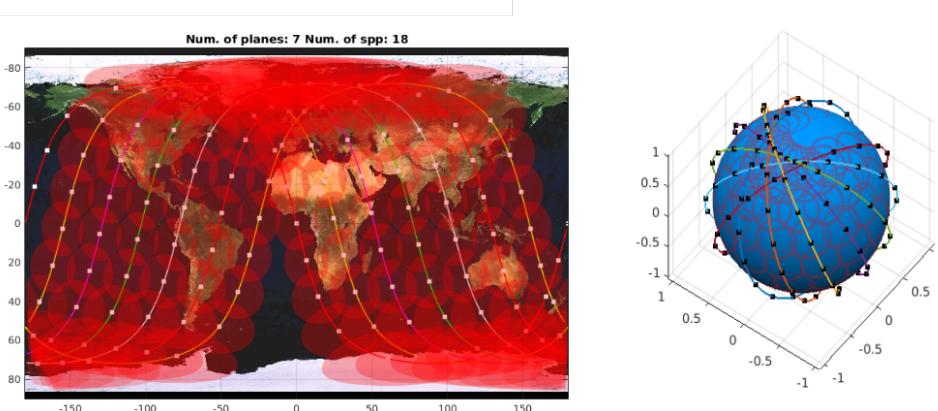


Figure 3.4.3: Ground track and spherical representation for a 180° Walker Delta configuration

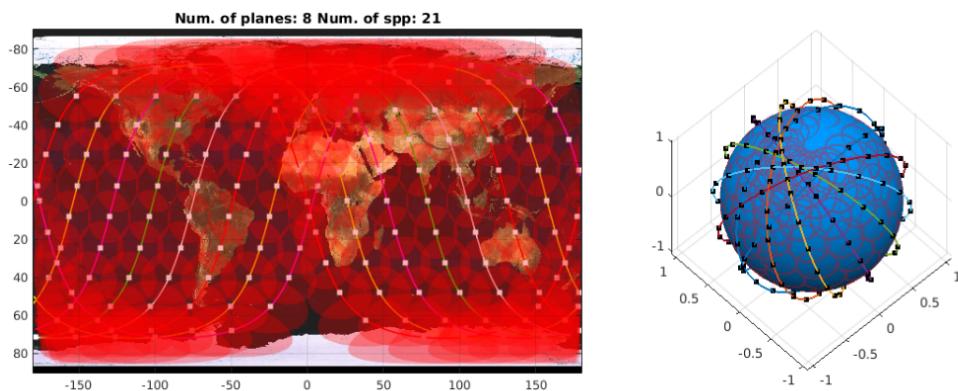


Figure 3.4.4: Ground track and spherical representation for a 210° Walker Delta configuration

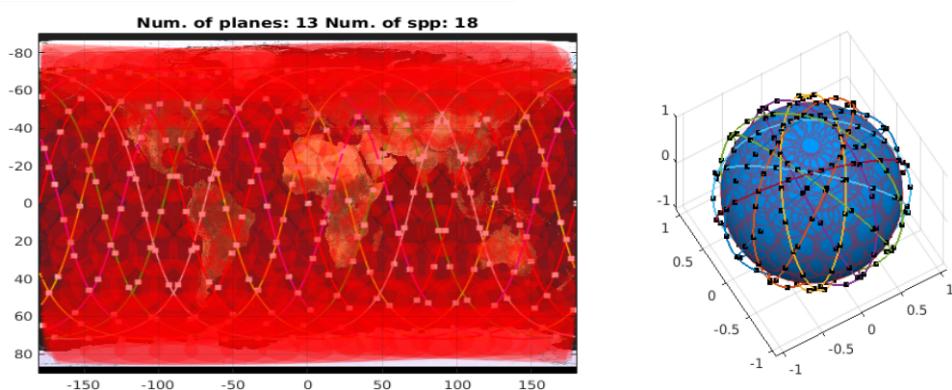


Figure 3.4.5: Ground track and spherical representation for a 360° Walker Delta configuration

Chapter 4

Orbit Perturbations

Sources of Perturbation

Introduction to Orbit Perturbations [?]

In this chapter it is seen how the designed orbit configuration varies in time due to external perturbation sources. While some of them can be neglected, there are other of major importance to the future of the constellation. For instance, atmospheric drag determines in plenty of cases the lifetime of the constellation. A first classification of perturbations depending on the time in which their effects are present is the following:

- Secular terms (Sec): They depend on the semimajor axis, the excentricity and the inclination.
- Short Period terms (SP): They depend on the anomalies, this leads to a strong variation in each period.
- Long Period terms (LP): They depend on the argument of the periapsis or the ascendent node.

Even though most of the outer space is vacuum, there ideal models need to consider some factors that escape the typical two body problem. For instance, we can no longer consider Earth as a punctual mass, neither the atmospheric density equal to 0. To enumerate, here is a typical list of the main perturbation sources:

Sources of perturbation:

- Gravity Field of the Central Body

- Atmospheric Drag
- Third Body perturbations
- Solar-Radiation Pressure
- Other Perturbations

All the perturbations can be deeply studied. Consequently, analytical solutions are very hard to find, and even they were found, they do not show clearly a meaning or are not really useful. Instead, there are two mainly used approaches:

- Special Perturbation: Step-by-step numerical integration of the motion equations with perturbation.
- General Perturbation: Through analytical expansion and integration of the equations of variation of orbit parameters.

The Approach of the Perturbations Study For the purposes of these study the different approaches will be assessed. The first analysis will discuss which of the perturbations are the most significant to the study. This analysis will be done considering General Perturbation Techniques. In a deeper second analysis, the two approaches for the perturbations will be assessed and compared considering only the most significant perturbation sources.

Gravity Potential of Earth

Earth's aspherical shape can be modelled as a sum of terms corresponding to the Legendre polynomials. These polynomials can be empirically measured and consider radial symmetry. If one would like to compute also variations in longitude, then should use associated Legendre polynomials.

$$V(r, \delta, \lambda) = -\frac{\mu}{r} \left[\sum_{n=1}^{\infty} \left(\frac{R_e}{r} \right)^n \sum_{m=0}^n P_{nm} \cos(\delta) (C_{nm} \cos m\lambda + S_{nm} \sin m\lambda) \right] \quad (4.1.1)$$

General Legendre associated polynomials developed Gravitational Potential

$$V(r, \delta) = -\frac{\mu}{r} \left[1 - \sum_{n=2}^{\infty} J_n \left(\frac{R_e}{r} \right)^n P_n(\sin \delta) \right] \quad (4.1.2)$$

General Legendre polynomials developed Gravitational Potential

For Earth, the J_n coefficients are the following:

$$J_2 = 0.00108263 \quad J_3 = -0.00000254 \quad J_4 = -0.00000161$$

Given this distribution, the only significant term J_2 .

$$V(r, \delta) = -\frac{\mu}{r} \left[1 - \frac{1}{2} J_2 \left(\frac{R_e}{r} \right)^2 (1 - 3\sin^2 \delta) \right] \quad (4.1.3)$$

Aproximated Gravitational Potential

If we integrate the force that derives from this potential we can afterwards compute the effect of J_2 On the different orbital elements:

- $\Delta a = 0$

- $\Delta e = 0$

- $\Delta i = 0$

-

$$\Delta\Omega = -3\pi \frac{J_2 R_e^2}{p^2} \cos i \text{ [rad/orbit]} \quad (4.1.4)$$

-

$$\Delta\omega = \frac{3}{2}\pi \frac{J_2 R_e^2}{p^2} (4 - 5\sin^2 i) \text{ [rad/orbit]} \quad (4.1.5)$$

Atmospheric Drag

In order to compute the effect of the remaining atmosphere we use the typical definition of atmospheric drag knowing a drag coefficient:

$$\vec{a}_{drag} = \frac{1}{2} \frac{C_d A}{m} \rho v_{rel}^2 \frac{\vec{v}_{rel}}{|\vec{v}_{rel}|} \quad (4.1.6)$$

The **ballistic coefficient** B_c is defined as $\frac{m}{C_d A}$, characterizing the behaviour of the satellite against atmospheric drag.

Modelling the Atmosphere

There are several models for the atmosphere. For instance, the most commonly used, the exponential model:

$$\rho = \rho_0 e^{-\frac{h-h_0}{H}} \quad (4.1.7)$$

$$H = \frac{kT}{Mg} \quad (4.1.8)$$

Where:

Exponential Atmosphere Variables	
ρ	Density at given height
ρ_0	Density at a reference height
h	Height over the ellipsoid
h_0	Reference height
H	Scale Height
k	Boltzmann Constant
T	Temperature
M	Molecular Weight
g	Gravity

Table 4.1.1: Exponential Atmosphere Model main Variables

In addition, other models for the exospheric temperature and the molecular weight need to be used. For this study the ones proposed by The Australian Weather Space Agency are used.

In addition, it is important to note that the following phenomena interfere with the previsions:

- Diurnal Variations
- 27-day solar-rotation cycle
- 11-year cycle of Sun spots
- Semi-annual/Seasonal variations
- Rotating atmosphere
- Winds
- Magnetic Storm Variations
- Others: Tides, Winds,...

Again, if we integrate this force in a period of time, considering the orbit nearly circular, we obtain:

$$\Delta r = -2\pi\rho r^2/B \text{ [/orbit]} \quad (4.1.9)$$

3rd Body Perturbations

The effects of this extra bodies in the system can be computed considering the motion equations. However, some approximations can be found in the reference as:

$$\dot{\Omega} = \frac{A_m + A_s}{n} \cos i \text{ [z/day]} \quad (4.1.10)$$

$$\dot{\omega} = \frac{B_m + B_s}{n} (4 - 5 \sin^2 i) \text{ [z/day]} \quad (4.1.11)$$

Where n stands for the rate of rotation in orbits/day. In that case, the A_m, A_s, B_m and B_s coefficients take as values:

	$A_m + A_s$	$B_m + B_s$
Moon	-0.00338	0.00169
Sun	-0.00154	0.00077

Table 4.1.2: Third Body Perturbations Coefficients

Other Perturbations

In this bag the following low-intensity can be classified:

- Solar Radiation Pressure
- Solid-Earth and Ocean Tides
- Magnetic Field
- South Atlantic Anomaly

Significant Perturbations

Propagation Algorithm

Given the definitions and approximations to compute perturbations described in the previous section, a propagation in time for the change in orbital parameters is solved. The results are plotted in the graph below:

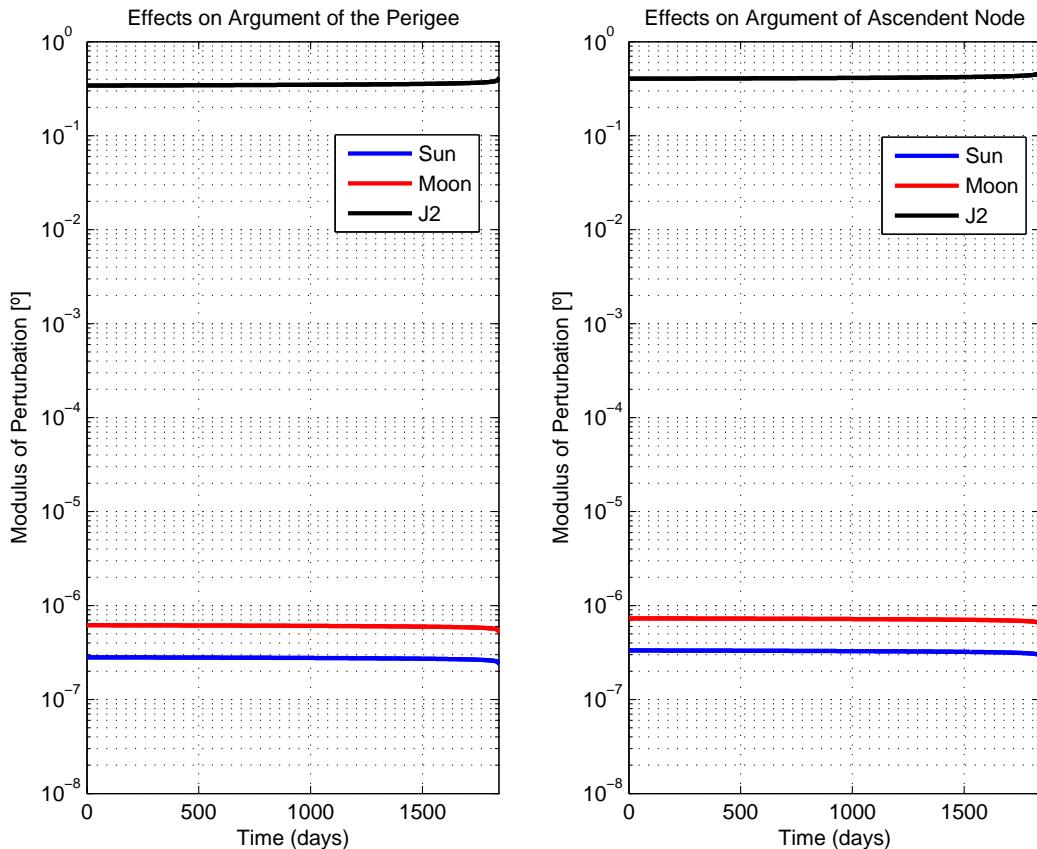


Figure 4.2.1: Logarithmic plot of the modulus of the increases in Angular Arguments of the orbit

As it can be seen, the perturbations caused by 3rd bodies are several orders of magnitude below the order of magnitude of the variation caused by Earth's oblateness. It is also remarkable that the moon has a higher effect than the sun given the relative distance to Earth, even if the sun is way more massive.

Another important observation is that given the very low eccentricity we are considering, the deviation of the argument of the perigee does not affect the performance of the constellation. In other words, since the orbits are considered almost circular there is not a defined Perigee for the orbit.

In conclusion

The effects of the Moon and the Sun are neglected in comparison with the effects of J2 for the Argument of the ascendent node as well as for the argument of the Perigee.

Orbit Decay

In this chapter the effects of the main perturbations are deeply studied. Firstly, an introduction on the effects of Earth's oblateness on the orbital parameters. Secondly and in more detail, the effects of Atmospheric drag. This is significant because it deviates the power and mass budget to engines and propellant.

Effects on the Ascention Node

Introduction

Due to the non sphericity of the Earth, two deviations exist in terms of perigee and ascendent node. This perturbations are related to the J2 effect described before. Both effects are related to the orbital planes inclination angle, so depending in which inclination they are positioned, the perturbation will be more or less significant.

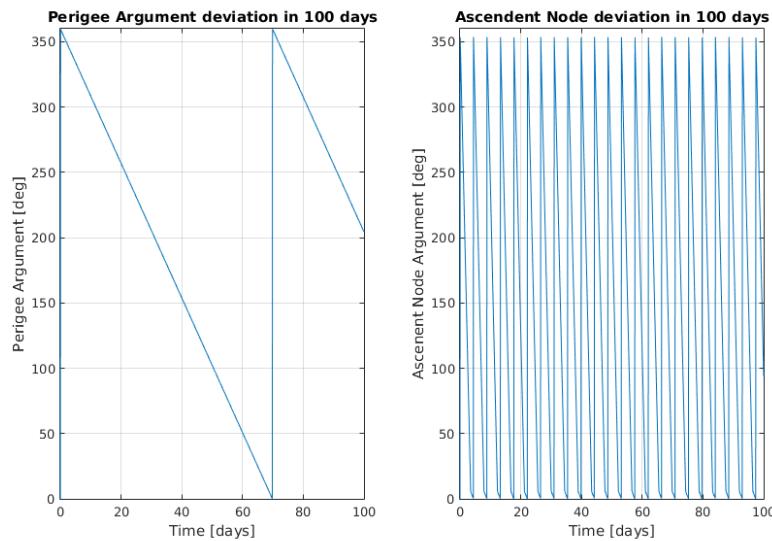


Figure 4.3.1: Ascention node perturbation
 On the left: Perigee deviation in terms of time.
 On the right: Ascending node deviation in terms of time

Perigee Effect

The Perigee effect is the responsible of the rotation of the orbit regarding the Earth and is found inside the orbital plane itself. Therefore the perigee of an elliptical orbit is not static in an Earth's point but moves around it.

This effect is noticed when having elliptical orbits. Consequently Astrea constellation will not be affected because the satellites describe almost circular orbits.

Ascention Node

In this case the perturbation affects the rotation of the orbital plane. So the plan longitude variates with time. That means, that if we had just one orbital plane it would not cover always the same fraction of Earth.

This effect is noticed when having planes with different inclinations. That is not Astrea's constellation case since all its planes are positioned in the same inclination angle.

Conclusion

As explained, both perturbations do not affect Astrea's constellation so they will not be considered as active agents on the orbit decay process.

The Figure 4.3.1 shows the propagation in time of both effects which are periodic due to the constant velocity of orbits.

Effects of the Solar Cycle

It is important to consider many parameters when calculating the orbital decay of a satellite. The most important of these parameters for LEO based constellations is drag. As discussed in other chapters, the drag of a satellite depends on the coefficient of drag, its surface, the density of the air and the velocity at which operates. Solar cycles will directly affect the density of the upper atmosphere. This phenomena is relevant when calculating the drag of the satellite and therefore is essential to compute the orbital decay.

Solar cycles are periodic changes in the Sun's activity of approximately 11 years. In each period a solar maximum and minimum can be determined, referring to the amount of periods of sunspot counts. The intensities for these periods vary from cycle to cycle.

Different studies have been made throughout the 20th century cycles. In order to understand the change density of the air changes as consequence of these solar cycles we considered the result data of an old study regarding the 19th solar cycle, which had a duration of 10.5 years between 1958 and 1968. This solar cycle had the highest maximum smoothed sunspot number ever recorded (since 1755), which was of 201.3. This maximum value was recorded in March 1958. This value is high in comparison to other cycles, especially when comparing it to the current 24th solar cycle. In this chapter an analysis will be developed in order to study the influence of the solar cycles on the drag of our satellites.

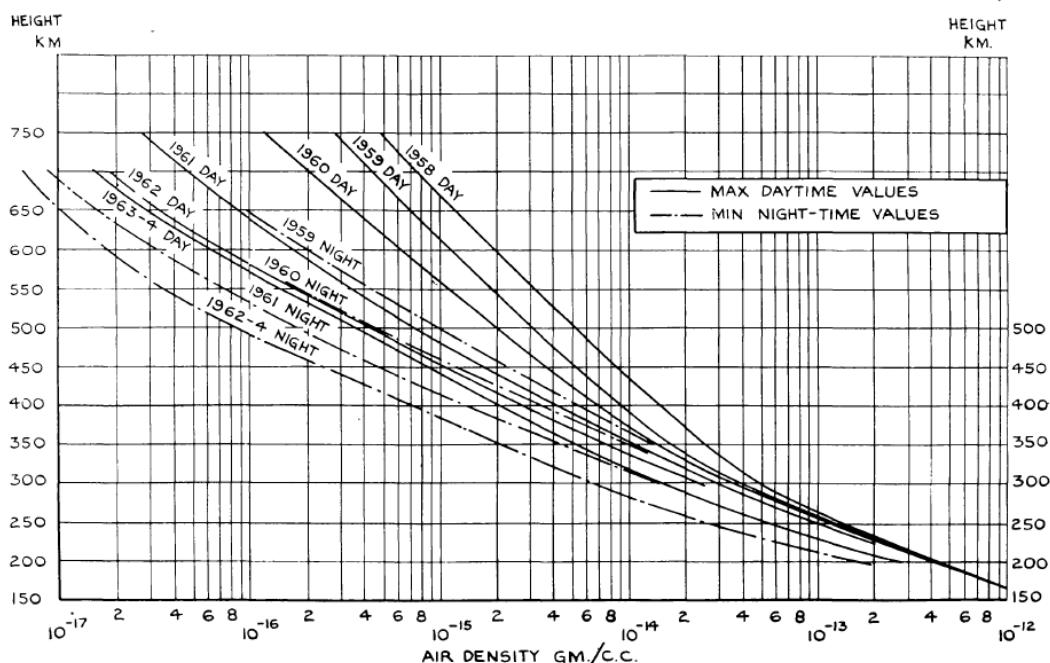


Figure 4.3.2: Deviation of densities in the upper atmosphere due to the 19th solar cycle

At 550 km:

Year	D/N	Density at 550km [g/cc]
1958	Day	3.2E-14
1958	Night	5.0E-15
1964	Day	1.35E-15
1964	Night	3.35E-16

These values referring to day and night are the densities of the upper atmosphere at 550 km of altitude respect to the surface of the Earth. The upper atmosphere densities

rise during the day following the increase of temperature caused by the radiation of the Sun whereas these values are reduced at night. The orbital decay is on the order of several years whereas these deviations appear every few hours. Thus, in order to compute the orbital decay we will not be taking into account these daily deviations but rather a main value. Therefore the mean density for 1958 will be of 1.85E-14 g/cc and the solar minimum's density of 1964 will be of 8.4E-16 g/cc.

In order to analyse how these values may apply to our constellation we first must adjust these - which belong to the 19th solar cycle - to those of the current 24th cycle, which is noticeable less intense. A way of operating this adjustment is comparing the mean solar maximum achieved by each cycle. The maximum monthly smoothed sunspot number of the 19th cycle had a value of 201.3 and a minimum of 9.6 whereas the current 24th ranges between 11.7 and 81.9 approximately. This means that for the 19th cycle a total deviation of 191.7 was measured whilst for the 24th cycle this deviation was only of 70.2. This is crucial if we want to analyse the solar maximum densities.

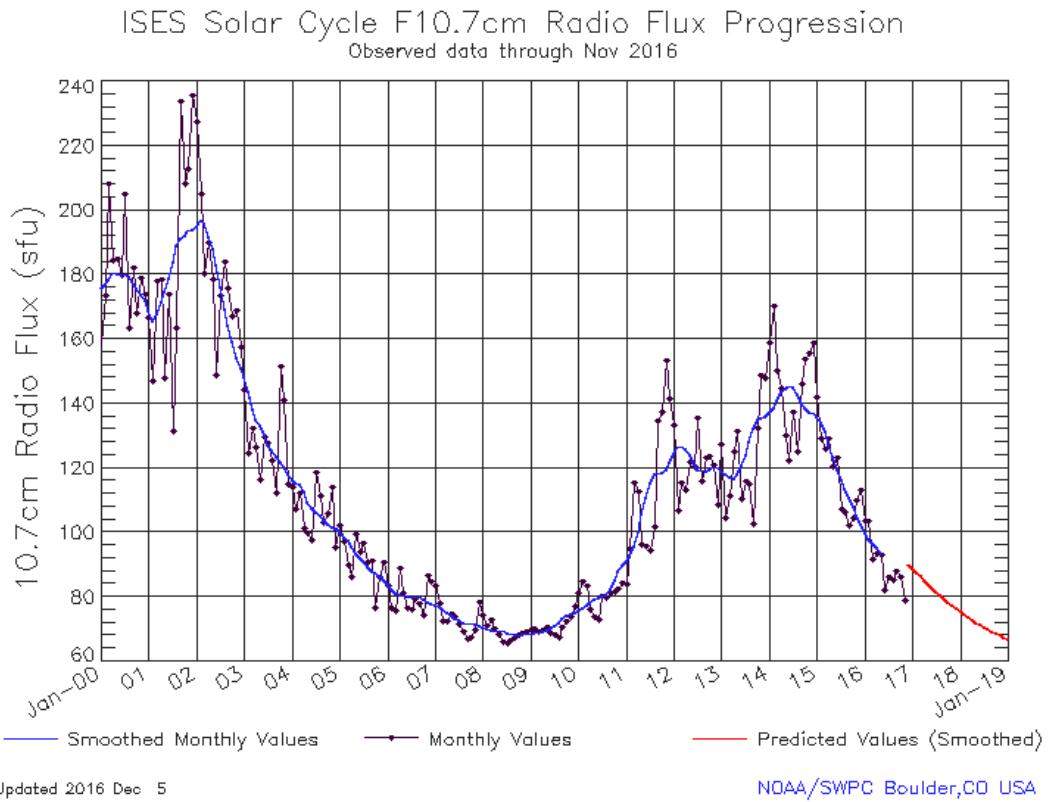


Figure 4.3.3: Measured intensities of the 23rd and 24th solar cycles. Source: NOAA

We must now adjust the mean constant density defined initially to the conditions that this 24th cycle imposes. It is important to note that our satellites will be launched in

2017, and that the 24th cycle is currently decreasing its intensity. Thus, our calculations will be near the conditions of solar minimum, meaning that the drag of our satellite will be smaller than first considered.

Our new approach to the density of the atmosphere at 550 km is near the first approximation, but will consider that we are now entering the solar minimum which will remain more or less constant until 2022. As discussed before, the solar minimum represents a singularity with a minimum density of 8.4E-16 g/cc. The approximation taken will be the resulting constant value which represents the mean smoothed densities between 2017 and 2022.

The final density at 550 km considering the solar minimum during 2017 to 2022 will be of 2.0E-15 g/cc.

Orbital Decay Propagation Results

Introduction

In this section a first aproach of the drag computation have been done in order to determine the orbit decay and consequently compute how much time a satellite last untill it reenters the Earth atmosphere.

Drag Computation Algorithm

Given the definitions to calculate orbital perturbations described in ?? a computation of the atmosphere drag has been done together with the computation of the other main perturbations that have been discussed in previous sections.

As explained in the last section the atmospheric drag depens on the drag's coefficient and it surface, that are constant values, on the velocity at which the satellite operates and on the air density.

So in orther to see the effects of variations in air density the orbit decay has been estimated and plotted for several F10 Radio Flux values corresponding to different moments of a solar cycle. (This data has been extracted from the figure ??).

The data selected and the results obtained are shown in 4.3.1 and 4.3.4 respectively.

Table 4.3.1: Selected data to compute orbit decay extracted from figure ???

Selected Values	
Year	F10 Radio Flux
2002	195
2004	115
2009	70
2013	120
2016	100

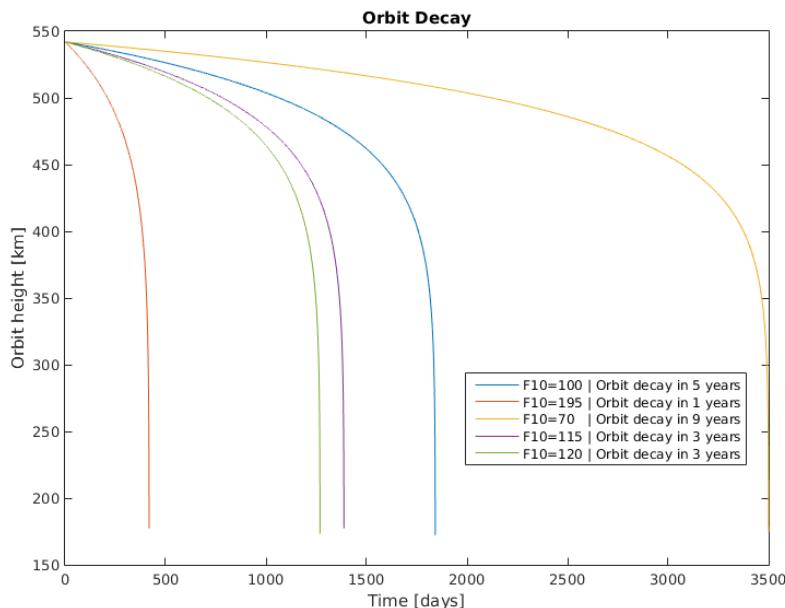


Figure 4.3.4: Orbit Decay computed for several values of

As it can be seen, the orbit decay strongly depends on the positioning in time of a solar cycle. (In 7 years the difference in lasting time of the satellite is reduced in 4 years).

In conclusion The lasting time in orbit of satellites is affected by period of the the solar cycle we are in. According to the data then Astrea's satellites will have an approximated orbit decay of 5 years.

Dynamic Orbit Decay Computation

Introduction

In this part of the chapter the orbital is studied using the model of special perturbations, which as previously defined, is the one that uses a numerical step-by-step integration. There are three manly used methods to study the dynamic propagation of an orbit, which are:

Cowell's method: This is the simplest method since it does not require any assumption or approximation. It is based on quantifying the accelerations produced by the perturbations and adding them to the dynamic equation of a Keplerian orbit (see Orbit Design: Chapter 1 equation 1.2.3) leading to:

$$\frac{d^2\vec{r}}{dt^2} = -\frac{\mu}{r^3}\vec{r} + \vec{a}_p \quad (4.3.1)$$

Where \vec{a}_p is the acceleration produced by the perturbations. This second order differential equation is the one that must be integrated in order to propagate the orbit. Although the formulas and application of this method are simple, this does not imply that it lacks robustness or precision. Its results are as good as any of the following two methods but the major drawback of *Cowell's method* is that it requires smaller time-steps being therefore slower (in terms of computation speed).

Encke's Method: This method is based on correcting the defects of the previous method. Encke uses a schema based on what is called *predictor-corrector*. First, it evaluates the orbit as if it were a Keplerian orbit (i.e. without perturbations) and then it integrates only the perturbations to correct the deviation caused by considering the unperturbed orbit. Its advantage over Cowell's method is clear, since it only integrates perturbations, and since these vary less over time than the position itself, we can relax the integration by increasing the time step. In short, this scheme is faster but also more complex to program than the one proposed by Cowell.

Variation of the parameters: This method, developed by Lagrange, is based on considering the orbit as a succession of Keplerian orbits, each of them being tangent to the satellite orbit at a certain point. Thus we can obtain differential equations that model the variation of the orbital parameters as a function of time.

The formulations and schemes followed by each of these methods can be found in any

reference dealing with orbital mechanics. For example, the reader can refer to [7] or the chapter 20 of [8] to obtain more detailed information about these methods.

For the purposes of this study, implementing the simplest method is enough. As it has already mentioned, it is based on adding the perturbations (discussed at the beginning of this chapter) to the dynamics equation. A *Matlab* routine has been developed that follows the next scheme:

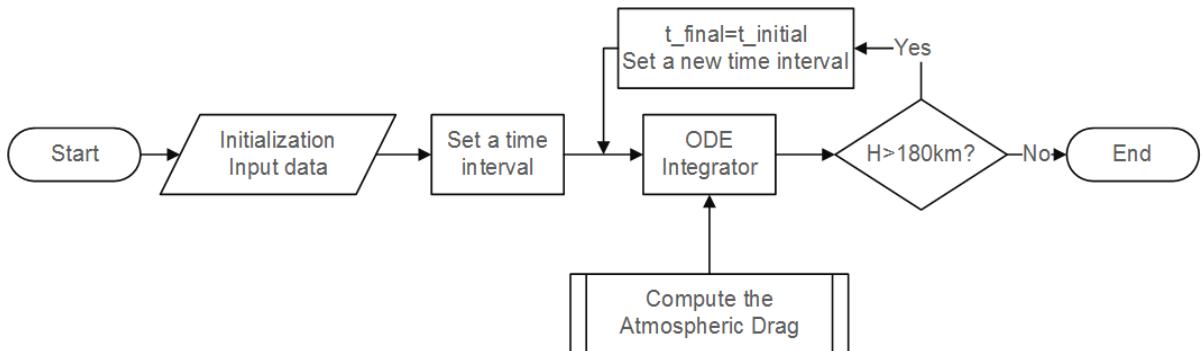


Figure 4.3.5: Algorithm of resolution used to solve the orbital propagation.

The disturbances that the routine includes are:

- The potential field of the earth.
- The Atmospheric drag.
- The influences of 3 bodies.
- Solar Radiation Pressure.

As it has been seen in previous sections, the only truly significant perturbation for the orbital decay at the altitude in which the constellation is located is the one caused by the atmospheric drag. Thus, other contributions have been deactivated to speed up the calculation. Therefore, explaining the formulation used to obtain the accelerations caused by these perturbations is not of interest for the development of the study. However, the following are the sources from which they were obtained:

- The calculation of the Earth gravity Potential uses the equation 4.1.1. Following the indications of [8] both the Legendre polynomials and the parameters C_{nm} and S_{nm} can be obtained.
- the equations present in ?? have been used to compute the perturbations due to other bodies,

- For Solar Radiation pressure the formulation used is the one presented in [?] including a 'shadow factor' (if the earth is between the sun and the satellite, the latter will not receive direct radiation from the Sun) modeled by a normal statistical distribution.
- For the calculation of Drag, the equation 4.1.6 and the atmosphere model presented in the same section have been used.

To be able to integrate the system we must take into account that, in fact, as we work in Cartesian coordinates, it is a system of three equations. Moreover, since it is a second-order equation we must rewrite it as a first-order system. Let $x_1 = r = (x, y, z)$ and $x_2 = \dot{r} = (vx, vy, vz)$. Therefore:

$$X = \begin{pmatrix} x \\ y \\ z \\ vx \\ vy \\ vz \end{pmatrix} \Rightarrow \dot{X} = \begin{pmatrix} v_x \\ v_y \\ v_z \\ \ddot{x} \\ \ddot{y} \\ \ddot{z} \end{pmatrix} = \begin{pmatrix} v_x \\ v_y \\ v_z \\ a_{p,x} - \frac{\mu}{r^3}x \\ a_{p,y} - \frac{\mu}{r^3}y \\ a_{p,z} - \frac{\mu}{r^3}z \end{pmatrix} \quad (4.3.2)$$

To integrate this system, you can use the *Matlab* built-in function **ode45**, which is a runge-kutta 4-5 with a variable step control that basically modifies the time step if the error is too large. Also, the **juliandate.m** function (included in the Matlab Aerospace module) have been used. It calculates the Julian Date, that is the number of days since noon Universal Time on January 1, 4713 ECB (On the Julian calendar).

Results

A simulation has been executed with the same parameters as in the previous section. After 932 seconds of computation, the results obtained are shown below:

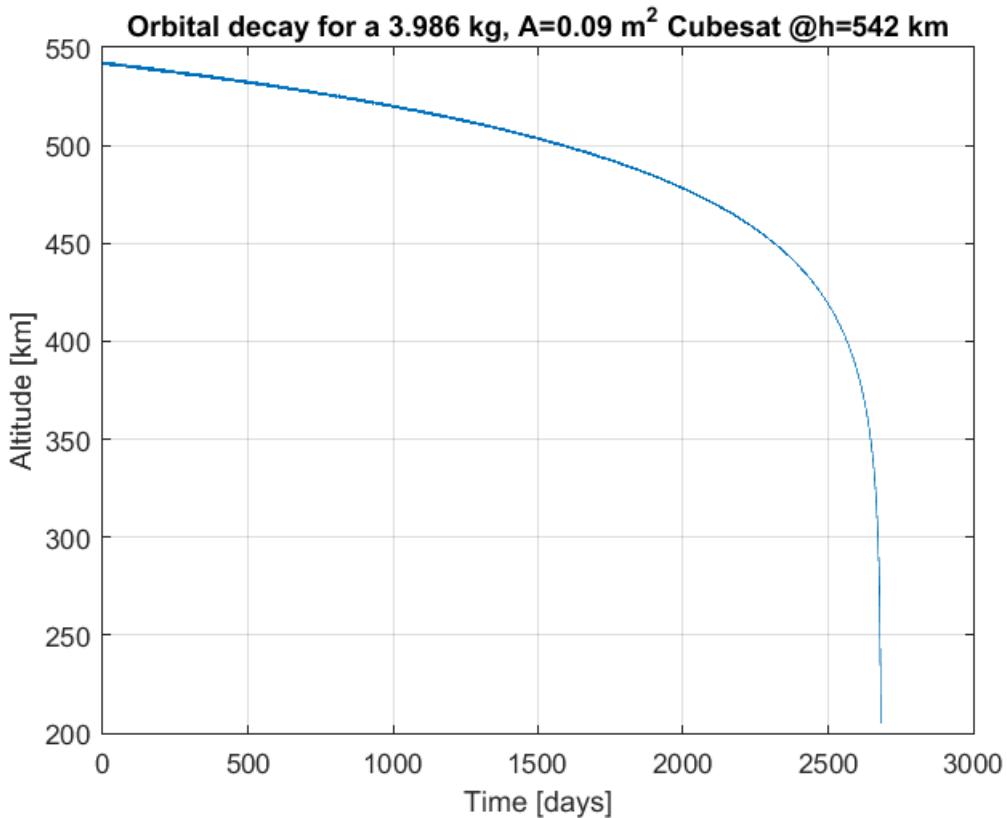


Figure 4.3.6: Orbital decay of the satellite.

As it can be seen, the estimated orbital decay for a satellite like Astrea's Cubesat is about 2700 days or, what is the same, 7.4 years. This estimation and the temporal evolution of the altitude is in agreement with the results obtained by the semi-analytic method. It is therefore verified that for a preliminary analysis and the respective modifications that it can present (i.e. changes in weight, changes in area, initial height, geometry of the orbit) it is enough with the results obtained by the semi-analytic study, which do not require almost computation time (only a few seconds), avoiding the expense of computing resources that would produce a dynamic simulation for every modification.

Orbital Station-Keeping

We will study:

- Increased height
- Thrusters

Raising the orbit height to increase Lifetime

The key to understand this solution is to see from another point of view the atmospheric drag phenomena. Once we have designed the constellation to provide certain coverage to specific points of the globe, the action of increasing the height of the orbit has the effect of increasing the footprint area on the surface of the earth. As the constellation is set, the time that take the satellites to reach the design height is extra lifetime.

From this point of view, the atmospheric drag phenomena can be recomputed and plotted it in this new way:

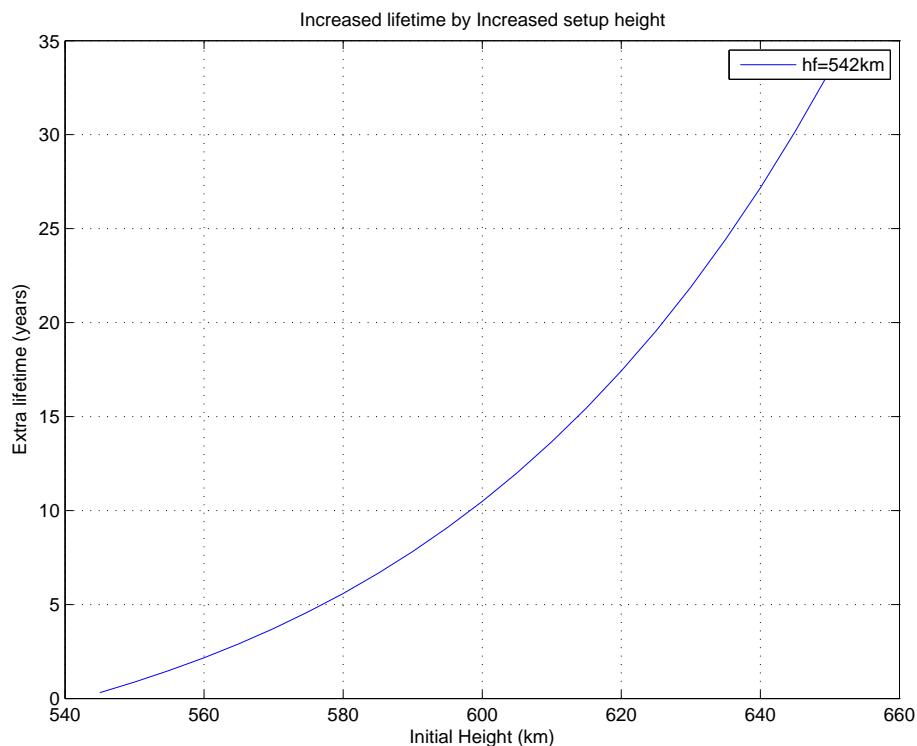


Figure 4.4.1: Increase in the Lifetime obtained by setting the constellation in a higher orbit

As it can be seen, the lifetime increases radically with time. However, this is a dangerous solution, since the coupling with another design parameters is compromised. To list the complications that can lead to:

- **Clients:** With the current technology, the satellites currently in orbit are set to point towards Earth. This means, if the constellation's satellites are at a higher orbit, the contact is impossible. As the market study reveals, it is important to place the satellites as low as possible.
- **Spacecraft Subsystems:** A higher orbit means a higher gain for the antennas and

therefore an increase in the required power.

- **Constellation Reconfiguration:** The overall time to reconfigure the constellation increases with height, since the period of the transition orbits is higher.

In conclusion

This tool is a very powerful option to deal with the orbit decay, even though it is not exactly an operation of Station Keeping itself. Given the high correlation it shows with other subsystems, the possibility of using it needs to be considered while the other design decisions are taken.

Using Thrusters to increase Lifetime

In order to maintain the configuration of the constellation for a longer time, a thruster is installed in each satellite to correct the decrease in altitude due to the orbit decay. The most optimal way to maintain the altitude is through a low-thrust maneuver. However, since this is a preliminary study, the calculations will be computed for a Hohmann transfer maneuver, which is simpler and more effective, but requires more propellant and greater increases of velocity. That is, by computing the velocity and propellant needed for a Hohmann maneuver, the results will be safe for a low-thrust maneuver, because the latter one requires less energy.

Energy equation

The deduction of the equations needed to solve the Hohmann maneuver begins with the energy equation:

$$\frac{V^2}{2} - \frac{\mu}{r} = -\frac{\mu}{2a} \quad (4.4.1)$$

where V is the orbital velocity of the satellite, r is the distance from the focus, a the semimajor axis of the orbit and μ the gravitational constant of the attracting body, in this case, the Earth. This expression shows that the total energy of the satellite equals the sum of its kinetic and potential energy (per mass unit).

This equation can be arranged to obtain the velocity of the satellite. In the case of a circular orbit, the radius is constant, and equal to the semimajor axis. Replacing $a = r$ in the energy equation and after some operations, the expression of the velocity of a circular orbit is obtained:

$$V_c = \sqrt{\frac{\mu}{r}} \quad (4.4.2)$$

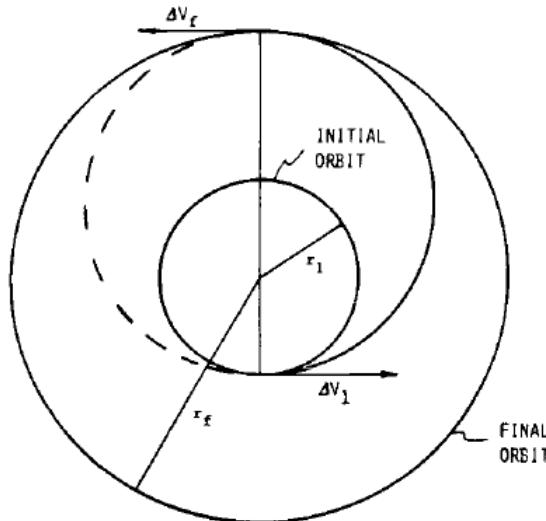


Figure 4.4.2: Hohmann transfer. Extracted from [4]

As it can be deduced from the energy equation, a change in orbital velocity leads to a change in the value of the semimajor axis. This property is used in satellites to change their orbit through a velocity increment ΔV . This process is called an orbital maneuver.

Delta-V

If the velocity increment ΔV is done instantaneously, the maneuver is called an impulsive maneuver. The Hohmann transfer is a two-impulse transfer between coplanar circular orbits. From an initial circular orbit, a tangential velocity increment ΔV_1 is applied to change the orbit to an ellipse. This ellipse is the transfer orbit, in which the perigee radius is the radius of the initial circular orbit and the apogee radius equals the radius of the final circular orbit. When the satellite reaches the apogee, a second velocity increment ΔV_2 is applied, so that the satellite reaches the final circular orbit with the apogee radius. If this second velocity is not applied, the satellite will remain in the elliptic orbit.

With the energy equation defined above, it is easy to determine the velocity of the satellite in each orbit. The first orbit and the final ones are circular:

$$V_1 = \sqrt{\frac{\mu}{r_1}} \quad (4.4.3)$$

$$V_f = \sqrt{\frac{\mu}{r_f}} \quad (4.4.4)$$

The velocity in the transfer orbit can be easily calculated with the energy equation applying the definition of the semimajor axis of an ellipse:

$$a = \frac{r_1 + r_f}{2} \quad (4.4.5)$$

The velocities in the perigee and apogee are:

$$V_p = \sqrt{\frac{2\mu r_f}{r_1(r_1 + r_f)}} \quad (4.4.6)$$

$$V_a = \sqrt{\frac{2\mu r_1}{r_f(r_1 + r_f)}} \quad (4.4.7)$$

Therefore the velocity increments are:

$$\Delta V_1 = V_p - V_1 = \sqrt{\frac{2\mu r_f}{r_1(r_1 + r_f)}} - \sqrt{\frac{\mu}{r_1}} \quad (4.4.8)$$

$$\Delta V_2 = V_f - V_a = \sqrt{\frac{\mu}{r_f}} - \sqrt{\frac{2\mu r_1}{r_f(r_1 + r_f)}} \quad (4.4.9)$$

Time

It is also necessary to know the time needed to do the maneuver. This time is equal to half of the period of the transfer ellipse:

$$t = \frac{T}{2} = \frac{1}{2} \sqrt{\frac{4\pi^2 a^3}{\mu}} \quad (4.4.10)$$

Propellant

In order to know the mass of propellant needed in the maneuver, the Tsiolkovsky rocket equation is applied:

$$\Delta V = g_0 I_{sp} \ln \frac{m_1}{m_f} = g_0 I_{sp} \ln \frac{m_1}{m_1 - m_{prop}} \quad (4.4.11)$$

where $\Delta V = \Delta V_1 + \Delta V_2$ is the total velocity increment of the maneuver, g_0 is the Earth's gravity, I_{sp} is the specific impulse of the thruster used, m_1 is the initial mass of the satellite, m_f is its final mass and m_{prop} is the mass of propellant used in the maneuver.

$$m_{prop} = m_1 \left(1 - \exp \left(- \frac{\Delta V}{g_0 I_{sp}} \right) \right) \quad (4.4.12)$$

Orbit maintenance

As explained at the beginning of the section, the orbital maneuvers exposed are intended to maintain the altitude of the satellite for a longer time and, consequently, lengthen its life. The method proposed begins when the satellite is deployed at a given height. This

Thrust	100 μN
Specific Impulse	2150 s

Table 4.4.1: Simulation Thruster Parameters

height will decrease due to the orbit decay, reaching a critical value, the limit altitude in which the constellation provides global coverage or another given height. Once this critical altitude is achieved, the satellite is put once again at its initial height through a Hohmann maneuver. The process is repeated several times until the satellite runs out of propellant or until it reaches its desired lifetime.

In reality the satellite will perform a low-thrust maneuver, which is more practical for an electric thruster. In this non-impulsive maneuvers, the thruster is constantly providing a velocity increment to the satellite, but it is so small that the whole transfer maneuver requires a lot of time. This means that it is not necessary to wait until the satellite reaches the critical altitude. The maneuver will start when the satellite is deployed or when it reaches a given altitude (higher than the critical altitude) so that it counteracts the effect of the orbital decay.

Results

The results are computed for a 3U CubeSat with an ion thruster. The characteristics of the thruster are the following ones (for more characteristics of the thruster refer to the section ??.):

The first parameters to be defined are the maximum and minimum height of the orbit, measured from the surface of the Earth. The maximum height is the altitude at which the satellite is deployed, and minimum height is the altitude at which the Hohmann transfer maneuver is applied. The satellite has to be above the minimum height to be functional.

Figure 4.4.3 is an example of the height variation of the satellite using the Hohmann maneuver to reach the maximum height once the satellite is in the minimum height. The results of this maneuver are:

Since the thruster used is an ion thruster, the specific impulse is big, and the mass propellant is very low. In this case, the variation of height due to the orbit decay is approximately 3 km per year, so the thruster needs to do a Hohmann maneuver per year. With only 10 g of propellant, the lifetime of the satellite is over 30 years.

Figure 4.4.4 is another example of the Hohmann maneuver with the same amount of propellant but with a more restrictive range of operational heights, only 80 m. It should have the same shape as Figure 4.4.3, but since a lot of maneuvers are applied, the lines

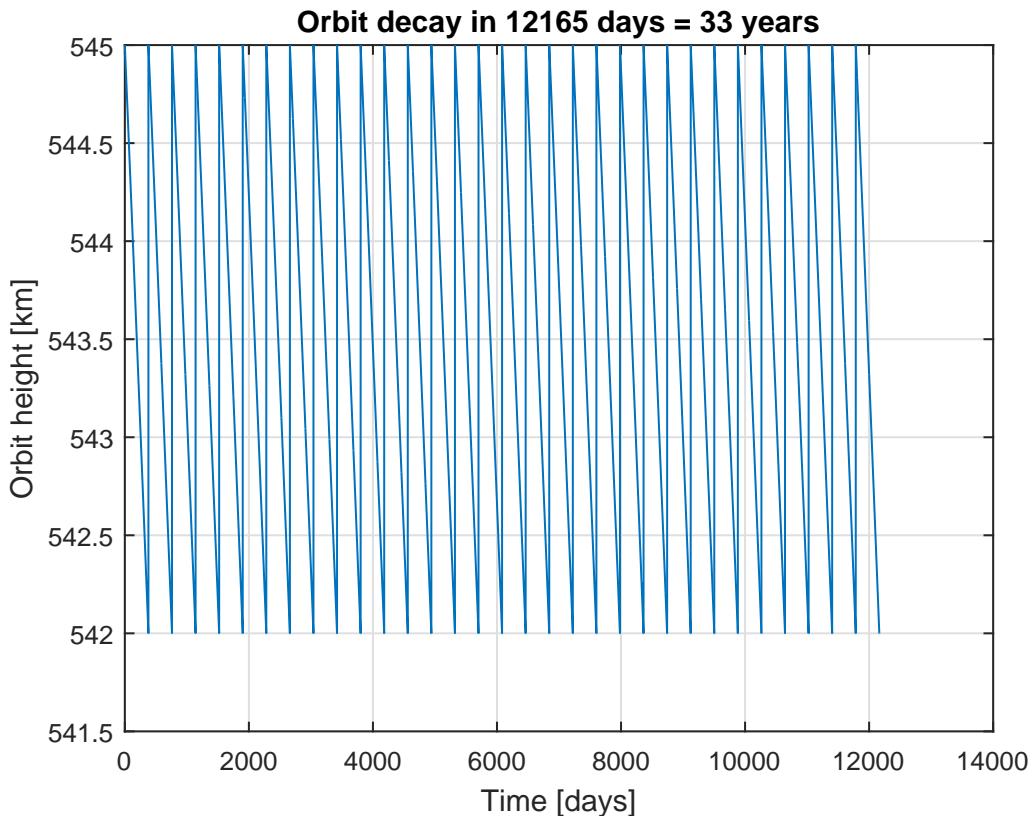


Figure 4.4.3: Height variation of the satellite

have overlapped. The characteristics of this maneuver are:

Comparing these results with the previous ones, it can be seen that with a more restrictive range of heights, the lifetime of the satellite is practically the same. The velocity increments are lower because the difference in the heights is extremely low, but at the same time, the satellite reaches before the minimum height and the maneuvers needed to maintain the satellite in this range are many more than on the other case. Since the ΔV budget is practically the same in both cases, it can be assured that the only difference between them is the number of maneuvers computed.

As mentioned earlier, the results obtained are for a Hohmann maneuver when in reality the satellite will compute a low-thrust maneuver, that requires less velocity increments and less propellant. In conclusion, taking into account these results, it can be stated that the lifetime of the satellite will not be determined by its orbit decay but for the failure of its systems or other external causes. It can also be assured that the satellite is capable of carrying enough propellant to maintain its altitude and to compute other maneuvers if necessary.

Maximum height	545 km
Minimum height	542 km
Number of Hohmann Maneuvers	32
Maximum ΔV_1	0,8237 m/s
Maximum ΔV_2	0,8236 m/s
Total ΔV Budget	52,7116 m/s
Propellant mass	10 g
Lifetime of the satellite	33,3288 years

Table 4.4.2: Station-Keeping with Thrusters Simulation 1 Results

Maximum height	545 km
Minimum height	544,92 km
Number of Hohmann Maneuvers	1200
Maximum ΔV_1	0,0221 m/s
Maximum ΔV_2	0,0221 m/s
Total ΔV Budget	52,7570 m/s
Propellant mass	10 g
Lifetime of the satellite	34,5726 years

Table 4.4.3: Station-Keeping with Thrusters Simulation 2 Results

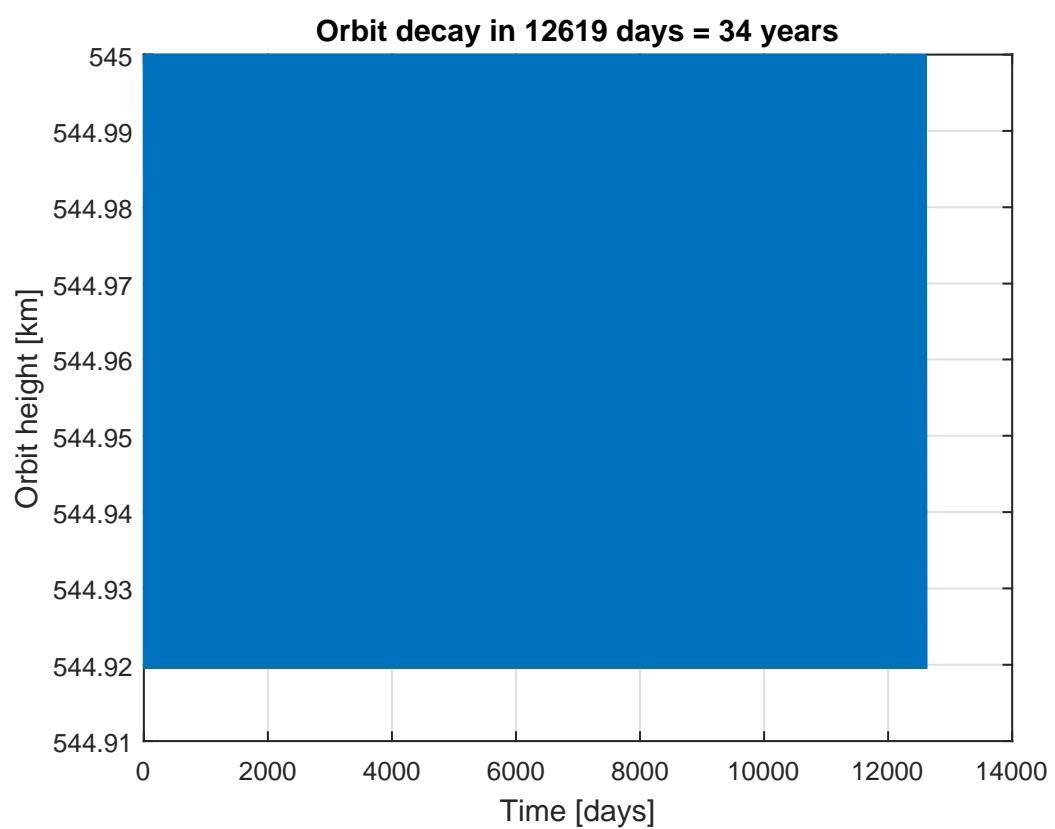


Figure 4.4.4: Height variation of the satellite with a more restrictive minimum height

Chapter 5

Constellation Design Decision

*"Aerospace Engineering is the way to
the universe."*

Marc Cortés Fargas, 2012

Considered Designs

Introduction

In this chapter it is seen how the final constellation decision is made. To do that an analysis of weighted weights will be performed.

The constellations candidates selected to their later evaluation are the following:

Candidate 1: Polar - Global Coverage

This polar constellation (Figure 5.1.1) came from the street coverage method explained in [??.](#) It is a network of polar orbits that provides global coverage. Its characteristics orbit parameters are the following:

- Height: 560 km
- Inclination of the planes: 90 °

Considered Designs

- Number of planes: 20
- Number of satellites per plane: 21
- Total number of satellites: 420
- Range of argument of ascending node: 360 °

Candidate 2: Polar - GS Coverage

The second candidate that will be compared is a polar orbit extracted from the coverage method explained in ??(Figure 5.1.2). This constellation provides total coverage to the Astrea's team ground stations. The network orbits parameters are:

- Height: 550 km
- Inclination of the planes: 90 °
- Number of planes: 18
- Number of satellites per plane: 16
- Total number of satellites: 288
- Range of argument of ascending node: 360 °

Candidate 3 and 4: Walker-Delta GS Coverage

Two Walker-Delta constellation configurations have been also chosen due to their reduced number of planes and satellites while being able of providing total coverage on the latitudes where the ground stations are located.(Figures 5.1.3 and 5.1.4). This constellations have been obtained with the algorithm explained in ??

Candidate 3

- Height: 542 km
- Inclination of the planes: 72 °
- Number of planes: 8
- Number of satellites per plane: 21

Considered Designs

- Total number of satellites: 168
- Range of argument of ascending node: 210 °

Candidate 4

- Height: 542 km
- Inclination of the planes: 72 °
- Number of planes: 9
- Number of satellites per plane: 17
- Total number of satellites: 153
- Range of argument of ascending node: 225 °

Candidate 5: Walker-Delta Lat: 0-58

Another Walker-Delta constellation has been selected with the criteria of total coverage of a range of latitudes going from 0 to 58 (Figure 5.1.5). Therefore the parameters needed to fulfill this particular condition of the constellation obtain from ?? are the following:

- Height: 560 km
- Inclination of the planes: 72 °
- Number of planes: 14
- Number of satellites per plane: 19
- Total number of satellites: 226
- Range of argument of ascending node: 210 °

Candidate 6: Polar - Walker-Delta J2 + Rotació

With the goal of providing constant coverage at the Ground Stations we can design a constellation that takes profit of the rotation of the Earth. If we also consider Earth's oblateness that causes another Ω derivative with time, we can exactly compute the longitudinal position of a plane after an orbit has passed. Now, if we design the constellation in a way that this deviation after an orbit matches the separation between planes, a line of satellites will always be on the GS. (Figure 5.1.6)

Considered Designs

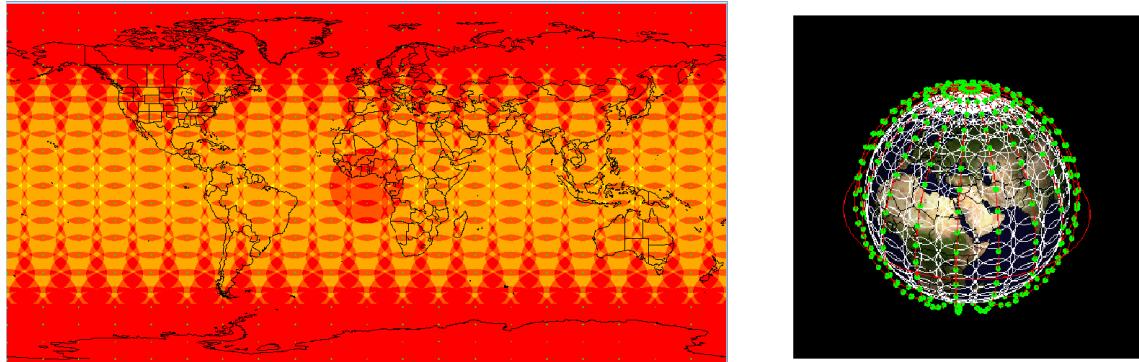


Figure 5.1.1: Candidate 1. Full Polar constellation with global coverage. $h = 560\text{ km}$; $N_p = 20$; $N_{pp} = 21$; $T_{sat} = 420$

- Height: 560 km
- Inclination of the planes: 72 °
- Number of planes: 14
- Number of satellites per plane: 19
- Total number of satellites: 226
- Range of argument of ascending node: 210 °

Candidate 7: Walker-Delta GS Coverage 3

The last configuration to be studied is a Walker-Delta constellation configuration designed to provide total coverage to the ground stations (Figure 5.1.7). It came up from candidate 3 constellation adding one more plane in order to increase its global coverage and minimize the gaps. As can be seen below, its parameters are the same as candidate 3 adding a single plane.

- Height: 542 km
- Inclination of the planes: 72 °
- Number of planes: 9
- Number of satellites per plane: 21
- Total number of satellites: 189
- Range of argument of ascending node: 225 °

Considered Designs

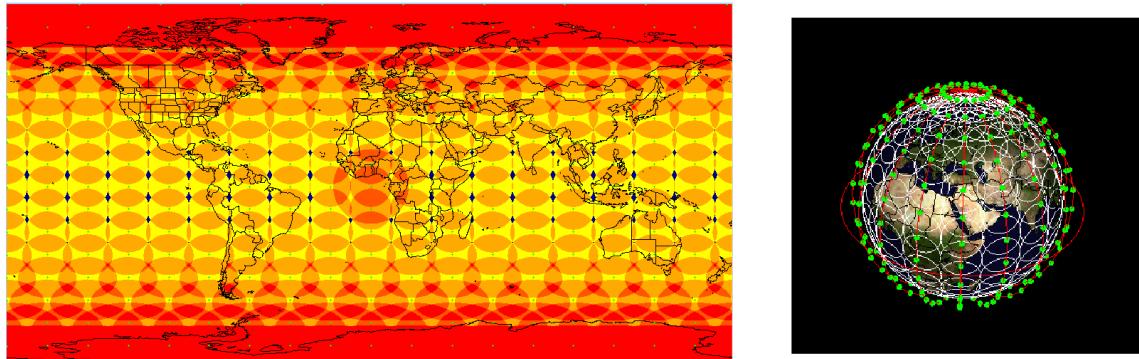


Figure 5.1.2: Candidate 2. Full Polar constellation with total ground station coverage. $h = 550\text{km}$; $N_p=18$; $N_{pp}=20$; $T_{sat}=288$

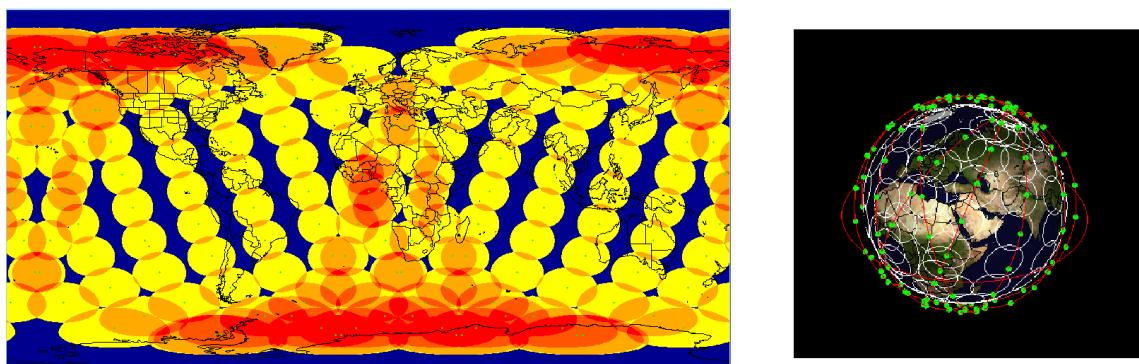


Figure 5.1.3: Candidate 3. 210° Walker-Delta constellation configuration. $h = 542\text{km}$; $i_n=72$; $N_p=8$; $N_{pp}=21$; $T_{sat}=168$

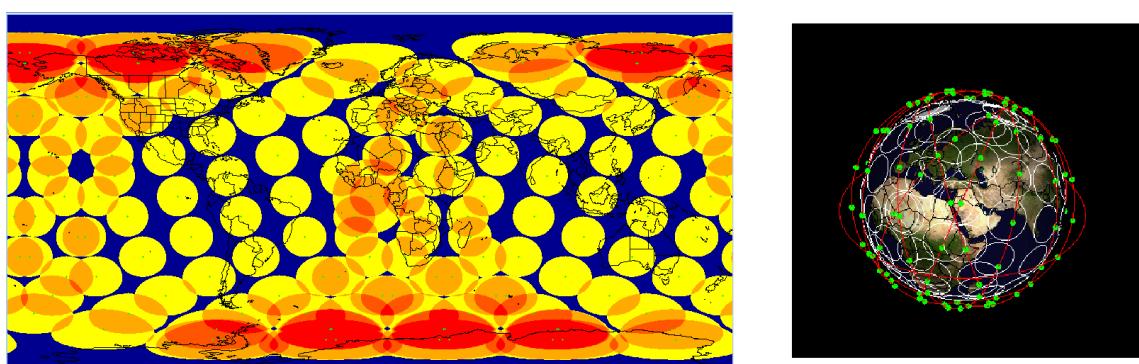


Figure 5.1.4: Candidate 4. 225° Walker-Delta constellation configuration. $h = 542\text{km}$; $i_n=72$; $N_p=9$; $N_{pp}=17$; $T_{sat}=153$

Considered Designs

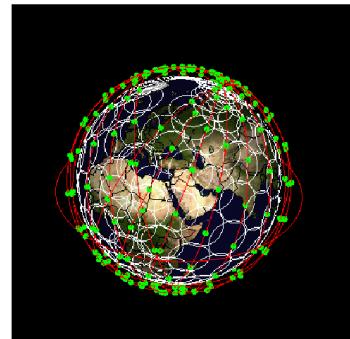
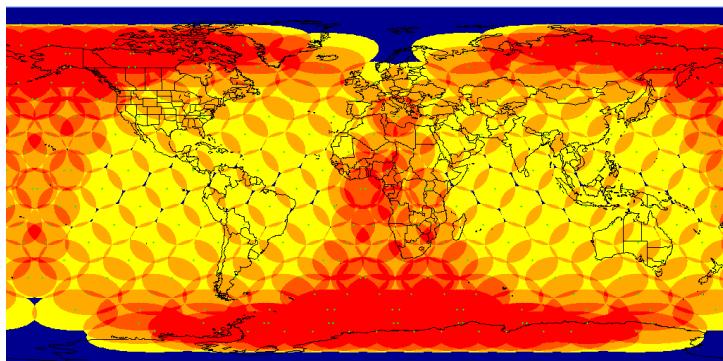


Figure 5.1.5: Candidate 5. 210° Walker-Delta constellation configuration with total coverage of the latitudes from 0 to 52 degrees. $h = 560\text{km}$; $in=72$; $Np=9$; $Npp=17$; $Tsat= 153$

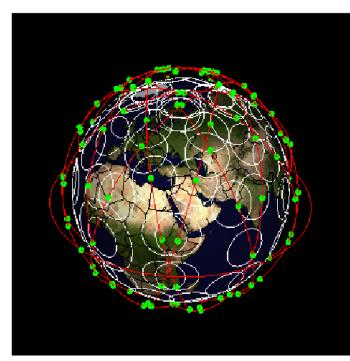
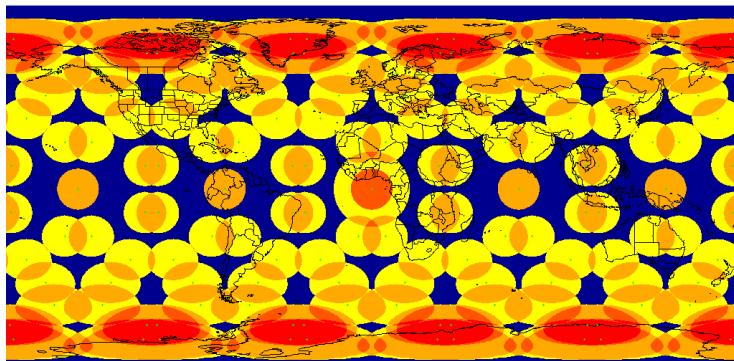


Figure 5.1.6: Candidate 6. 225° Walker-Delta constellation configuration.
 $h = 542\text{km}$; $in=72$; $Np=9$; $Npp=21$; $Tsat= 189$

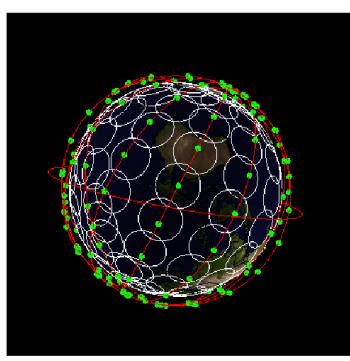
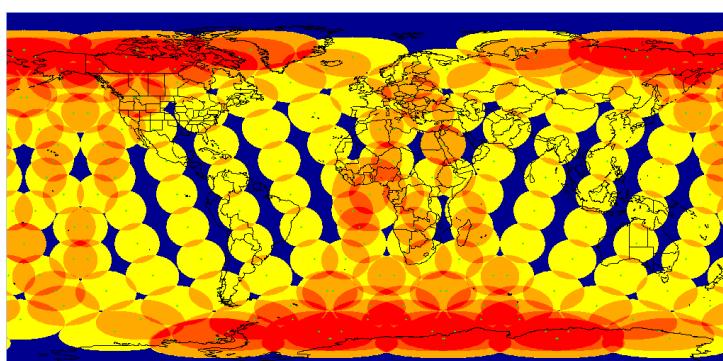


Figure 5.1.7: Candidate 7. Full Walker-Delta constellation configuration.

Constellation Performance Analysis

Even though the design requirements are included in the computation of the different configurations, it is necessary to evaluate how does the constellation perform when deployed. With this purpose, another MATLAB routine was developed.

Time factor

It is important to remark that the design methods used so far did not consider coverage in a certain period of time, but the coverage at a given instant. This section summarizes a method to compute this variation.

Quality Time

Another factor that was not considered in the design process was the pass times of the satellites. If a pass is too short the contact with the satellite cannot be produced.

Performance Evaluation

In order to determine if the performance of the Constellation is good enough and to compare different constellations, we define the following parameters that are to be used in the weighted ordered average decision5.3.1.

Simulation parameters important to clarify:

- Simulation time: 25h. This time is enough to observe the motion of the whole constellation on Earth considering its rotation and the rotation of the plains due to the Earth's oblateness.
- Minimum contact time: 3 minutes. Time enough to download data, tracking and Telecommanding the satellite.
- Time precision: 10 seconds. It is empirically observed to be precise enough.

The computed parameters:

- Fraction of time with flybys on the GS: Ratio between the time in which there is any satellite in the field of view of the Ground Station and the total simulation time. (Referred in table 5.3.1 as % Coverage)
- Mean number of links with the satellite

- Fraction of time with flybys longer than 3 minutes: In this case the ratio is with the time in which there is a satellite doing a useful pass, since a full contact can be done. (Referred in table 5.3.1 as %Quality Time)
- Mean pass time: This parameter is used to guarantee a minimum of quality and to compare different configurations. (Referred in table 5.3.1 as Average Pass Time)
- Number of gaps: Gaps are in this chapter defined as periods of time without a pass that is lasting/will last more than 3 minutes. (Referred in table 5.3.1 as Num Gaps)
- Maximum gap time: At high latitudes all the Walker-Delta configurations show a characteristic gap that can last even for hours, which is not admissible. This parameter will tell us if we exceed a maximum defined as 3 minutes for this study. (Referred in table 5.3.1 as Max Gap Time)
- Mean gap time: As it is obvious, a minimum or a 0 is desired.

You can find below an example of the analysis, for a constellation in a Semi Walker-Delta configuration.

Constellation	Full WD
Number of Planes	$p = 8$
Satellites per plane	$spp = 18$
Inclination	$i = 75^\circ$
GS Latitude	$\lambda = 80^\circ$
GS Longitude	$\phi = 0^\circ$

Table 5.2.1: Constellation parameters for the Example Constellation

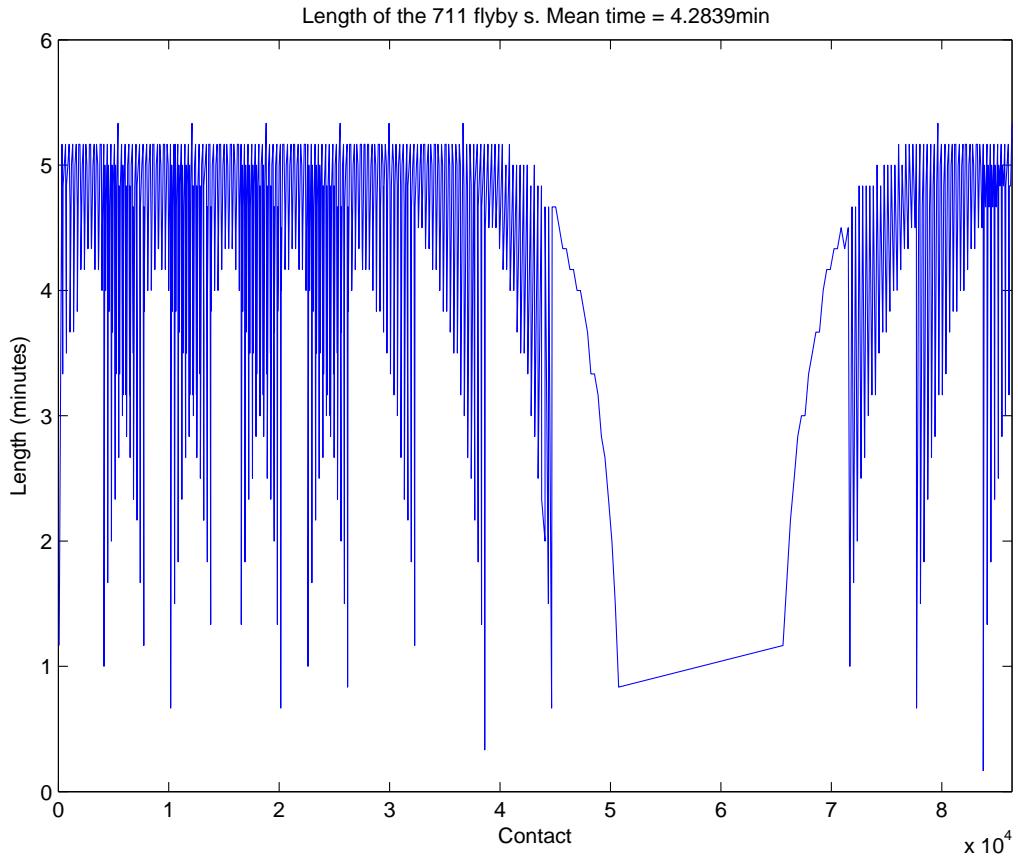


Figure 5.2.1: Length of the passes on the example GS.

Pass Time Ratio	77.53%
Quality Time Ratio	75.77%
Mean Pass Time	4.28min
Number of gaps	37
Maximum Gap Time	314.33min

Table 5.2.2: Performance Parameters for the Example Constellation

Given the high latitude of the Ground Station plus the Semi Walker-Delta Configuration there is an enormous gap. In addition, between planes some gaps are also observed.

Ordered Weighting Average based Decision

The Described Constellations are weighted and averaged in the table below. The detailed explanation of the parameters can be found in 5.2.1:

Criteria	W	Candidates						
		1	2	3	4	5	6	7
Price	15	1	2.35	5	4.94	3.21	3.92	4.67
% Coverage	4	5	4.77	2.94	2.14	4.43	1	3.86
Max Gap Time	3	3.12	3.62	1	2.88	3.51	5	4.75
% Quality time	5	4.91	4.49	4.05	1	3.19	5	4.98
Average Pass Time	5	1.21	1.14	1.14	1	1.90	5	4.72
Num Gaps	2	4.73	4.44	4.23	1	3.03	4.99	5
% Sats above	6	1	1	5	5	1	5	5
SUM (p*g)	40	90.42	108.17	154.19	133.29	113.94	167.71	188.21
OWA		0.452	0.541	0.771	0.666	0.570	0.838	0.941

Table 5.3.1: Constellation Configuration OWA Decision

With this comparison table, the optimum Constellation is option number 7:

The Astrea Constellation

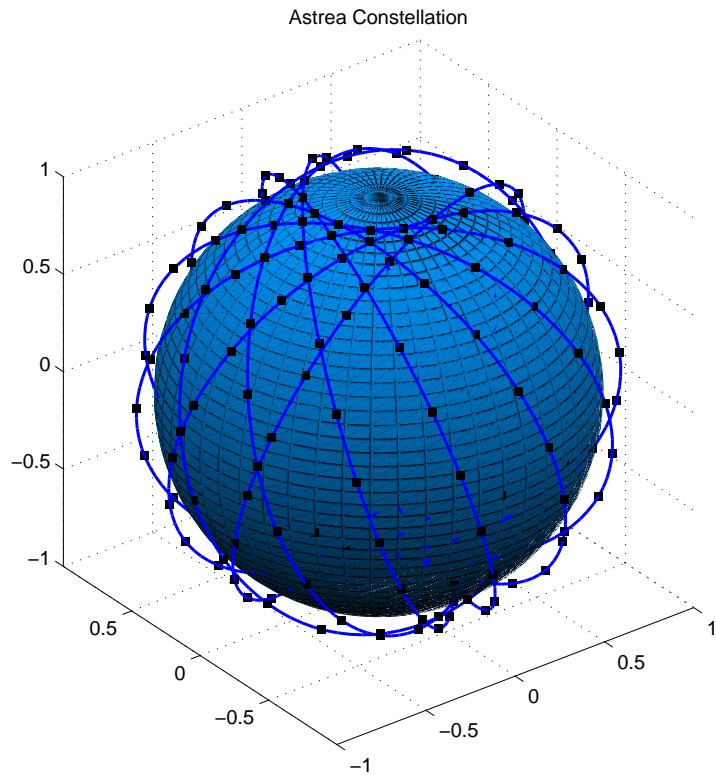


Figure 5.3.1: Astrea Constellation Final Configuration.

Part II

ANNEX II: Constellation Deployment

Chapter 6

Constellation Deployment

Constellation Deployment Department

This introductory section aims to present the Constellation Deployment Department and its duty.

The mentioned department is composed of four members of the Astrea Constellation. It is created in order to asses all the issues related to the launcher which will put the constellation into orbit and the different strategies to be followed to ensure the adequate set up and posterior maintenance of the constellation. In the Project Charter document, four tasks are assigned to the department:

- A comparison among the existing launching platforms to find one that fulfills the requirements of the constellation at a reasonable economic conditions.
- The book of a launching date if the selected launcher requires it.
- The follow of the current legislation referred to launchers and deployers.
- The design of an End of Life and a Replacement strategy.

In order to simplify the accomplishment of this assignments, the department decides to divide its tasks into six parts each of one is a section of this report:

- Launching System
- Deployer
- First Placement
- Replacement Strategy
- Spare Strategy
- End of Life Strategy

The following table displays the first seven candidates.

ENTERPRISE	ROCKET	LAUNCHING SITE	TYPE
Rocket Labs	Electron	North Island (New Zealand)	Light
Kosmostras	Dpner	Baikonur Cosmodrome (Kazakhstan)	Light
Arianespace	Ariane V	Guiana Space Center (French Guiana)	Heavy
Arianespace	Vega	Guiana Space Center (French Guiana)	Light
SapceX	Falcon 9	USA	Heavy
PLDSpace	ARION-2	Huelva and Cape Canaveral	Light
LEO Launch and Logistics	-	USA	Light

Table 6.1.1: List of Launchers



Figure 6.1.1: Electron Rocket



Figure 6.1.2: Second Stage



Figure 6.1.3: Electron Rocket Fairing

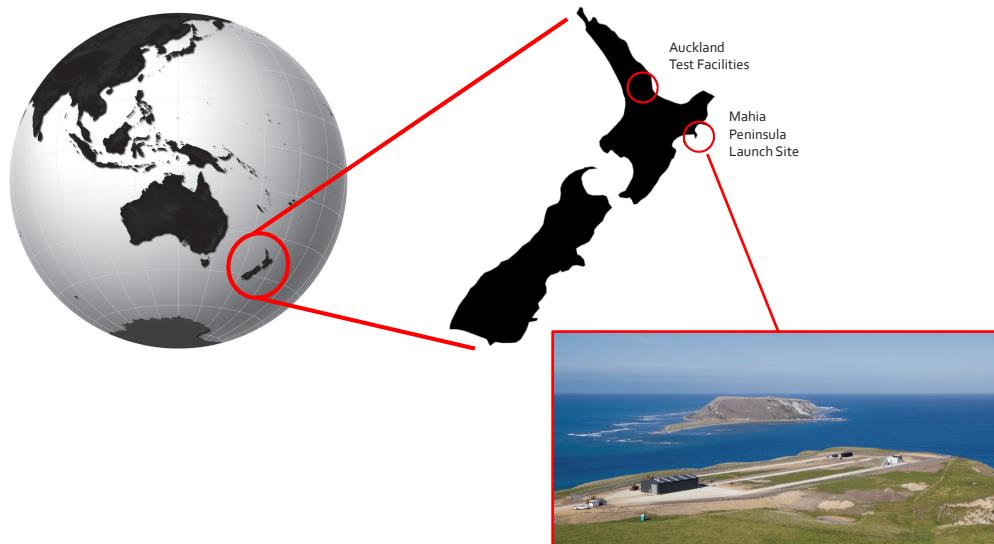


Figure 6.1.4: Rocket Lab Facilities

Characteristics of GPOD and ISIPOD. First, the main ones that both have in common are shown, secondly, the few differences between them are listed:

- Main features
 - Provide deployment status signal.
 - No battery needed nor external power source
 - No pyrotechnics
 - Protect the CubeSat from external environment
 - Mechanically interfaces with the CubeSats by means of guidelines
 - Mechanically interfaces with the launch vehicle by means of standard fasteners
 - Qualified for multiple of launch vehicles
- ISIPOD

- The satellites are fully enclosed inside the deployer, once the CubeSat is fit in, there is no access to it (see image 6.1.5)
 - Electrically interfaces with launch vehicle for telemetry
- GPOD
 - Accessible panels: all the side panels allow the access to the integrated CubSat (see image 6.1.6). This means that the entire area between the guide rails over the entire CubeSat length may be freely accessed.
 - The price for a single deployer 3U is 16000 euros.



Figure 6.1.5: ISIPOD

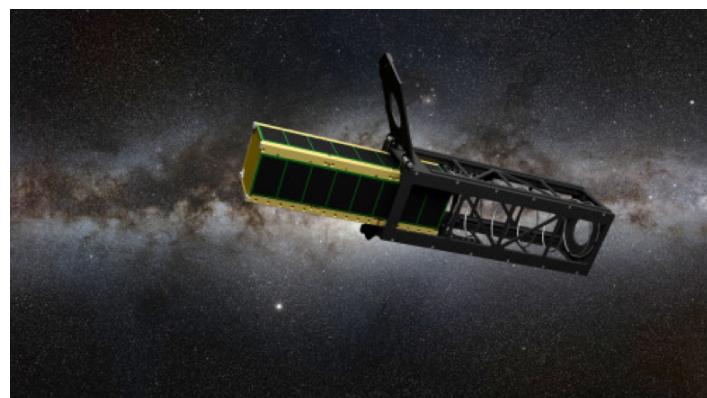


Figure 6.1.6: GPOD

First Placement

The aim of this part is to explain the first placement of the constellation. It is divided in two parts, the first one is intended to give a first approach to the logistics involved in the first placement. The second one is focused on the maneuver required so as to deploy the satellites into orbit.

First Placement logistics

Gantt diagrams provided by Rocketlab USA:

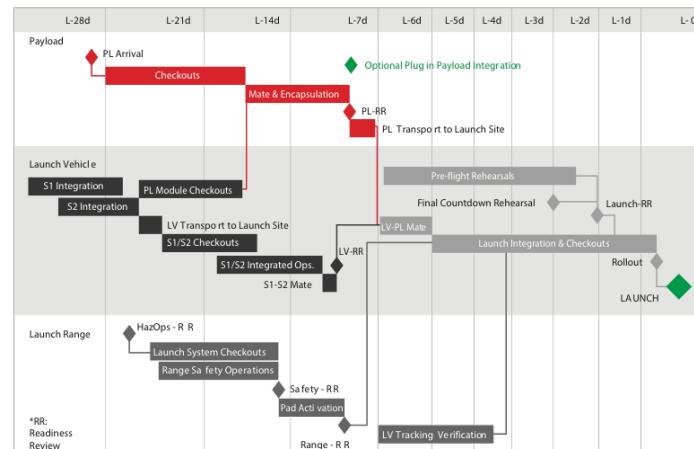


Figure 6.2.1: Launch Range Operations Flow/Schedule

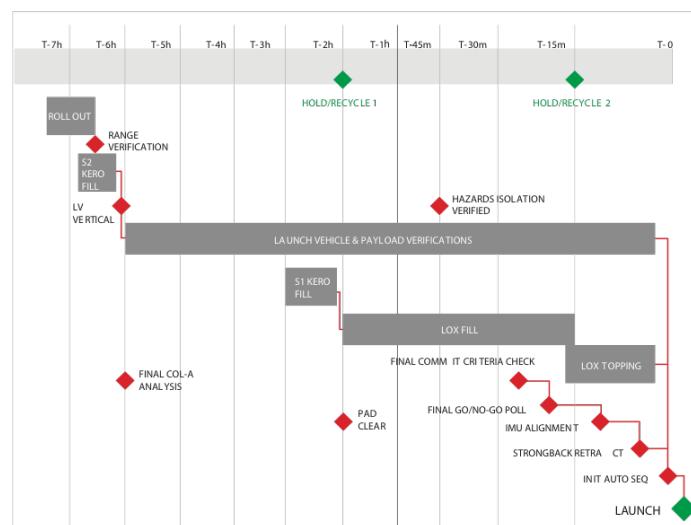


Figure 6.2.2: Countdown Operations Flow

1st Placement In-Orbit Injection Maneuver

In a more schematic way, the procedure goes as follows:

1. The rocket goes through the procedure designed by Rocketlab USA to get to the destination orbit. The approximate trajectory during this stage is represented in 6.2.3. Right after entering into the destination orbit, the first satellite is deployed into it as seen in 6.2.3 represented with a red dot.
2. Once the latter is completed, the rocket's engine gives it the necessary ΔV in order to get to the elliptical spacing orbit. In 6.2.4 half a revolution of the rocket is represented along with the orbit of the first deployed satellite at the same point in time.
3. After one full revolution of the rocket in the elliptical orbit, the first satellite will have left the right phase spacing with respect to the rocket. At this point the rocket's engine gives the same ΔV as in 2 but negative. This will cause it to enter again into the circular orbit of the satellites. At this point the rocket deploys the second satellite as shown in 6.2.5. Right after this deployment the rocket enters into the elliptical orbit again.
4. 6.2.6 represents again half a revolution of the rocket in the elliptical orbit along with the deployed satellites so far.
5. Finally, the rocket reduces its velocity again to enter into the circular destination orbit in order to deploy the third satellite (6.2.7).
6. The procedure is iterated until the orbital plane is full.

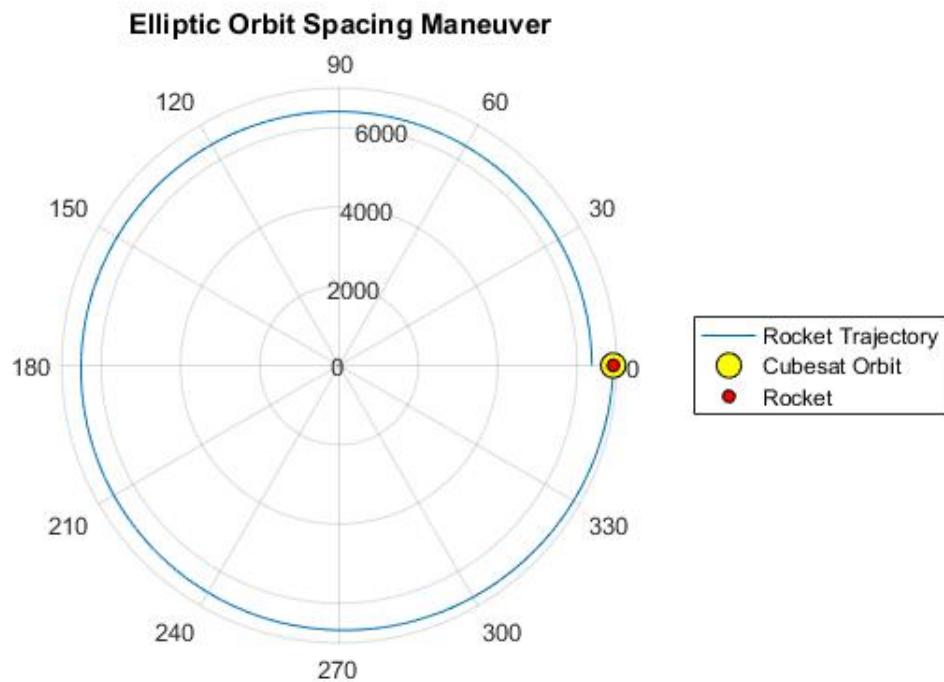


Figure 6.2.3: Rocket's trajectory from lift-off to final orbit.

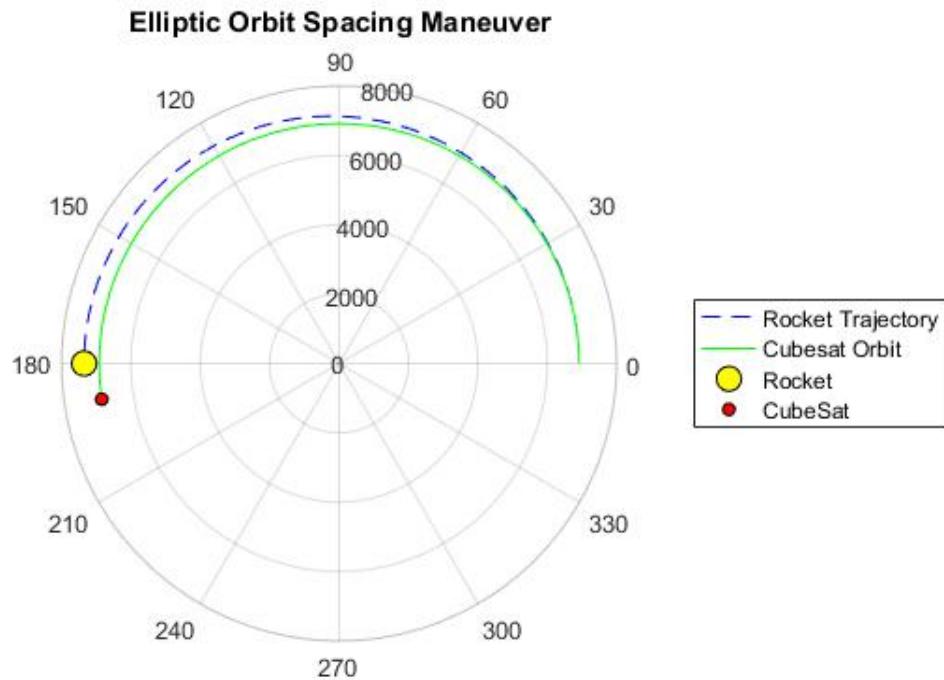


Figure 6.2.4: Half of a revolution of the rocket in the elliptical spacing orbit.

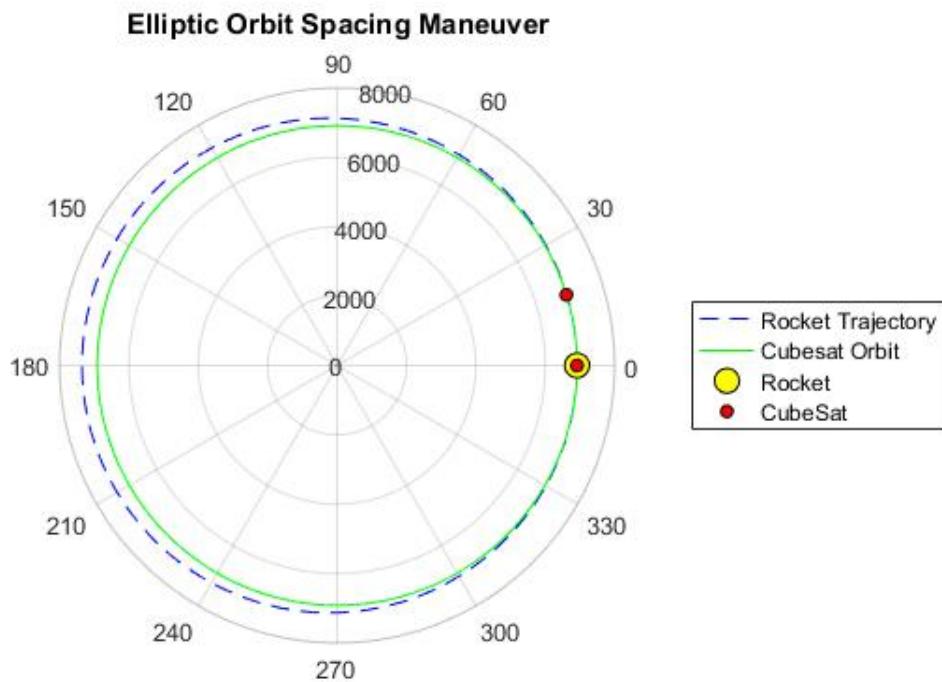


Figure 6.2.5: Deployment of the second satellite.

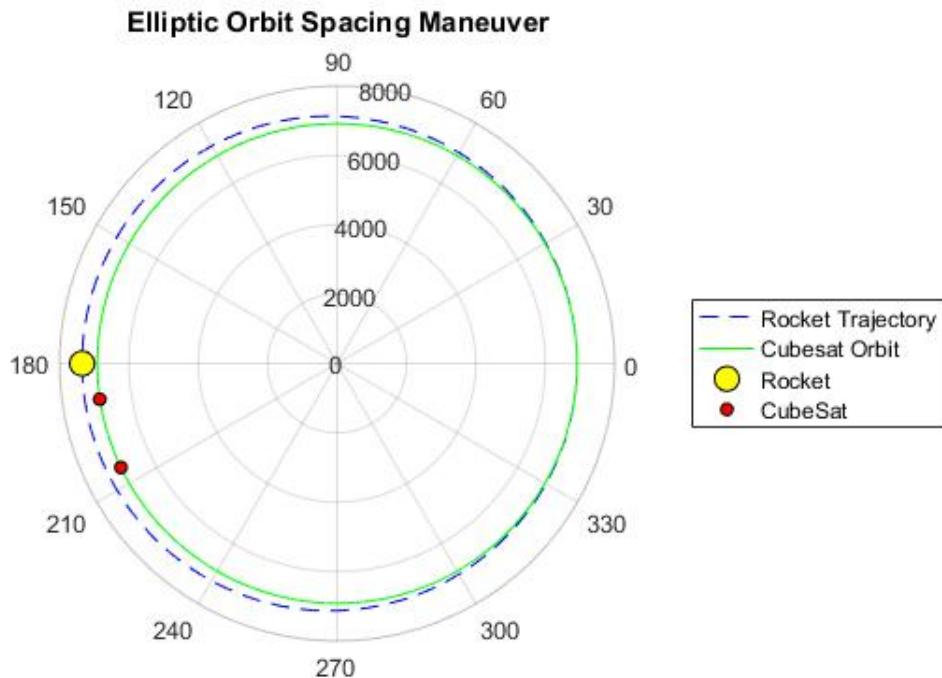


Figure 6.2.6: Half of a revolution of the rocket after the deployment of the second satellite.

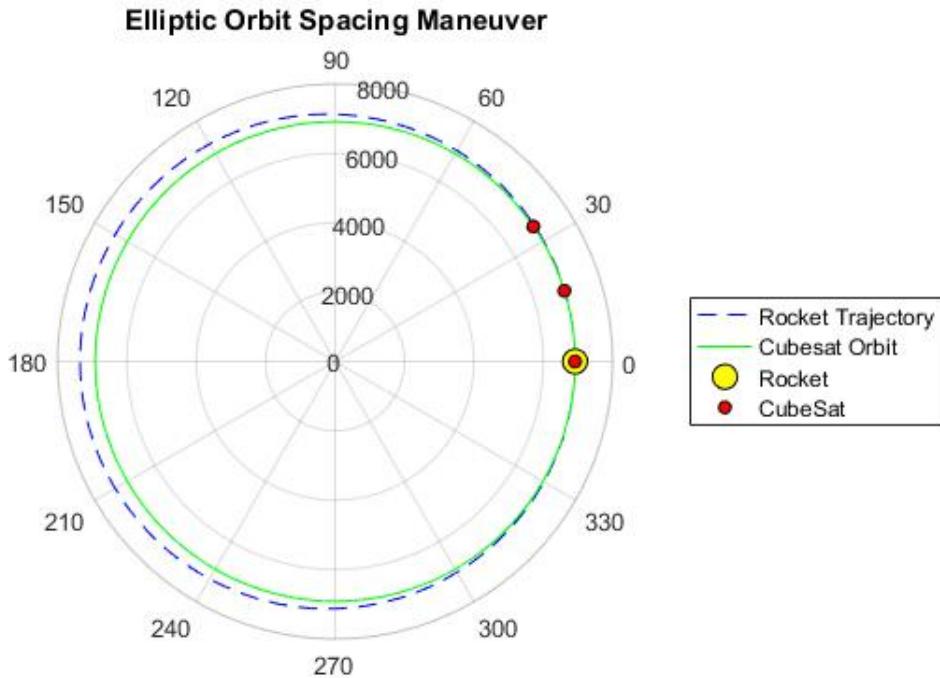


Figure 6.2.7: Deployment of the third satellite.

Orbit Parameters Calculation

$$V_s = \sqrt{\frac{GM_t}{R_t + h}}$$

$$T_s = \frac{2\pi*(R_t + h)}{V_s}$$

Where R_t and h are Earth's radius and height above Earth's surface respectively. For $h = 542 \text{ km}$, the values obtained are $V_s = 7,589.6 \text{ m/s}$ and $T_s = 5,723.1 \text{ s}$. Let's call the spacing between satellites $\theta = \frac{360^\circ}{21} = 17.14^\circ$ and $R = R_t + h$. Using these values it is possible to compute the period of the elliptical orbit, T_r , along with the rest of the parameters:

$$T_r = T_s + \frac{\theta R}{V_s} = 5,995.6 \text{ s}$$

$$a = \left(\frac{T_r}{2\pi}\right)^2 GM_t^{\frac{1}{3}} = 7,130.8 \text{ km}$$

$$R_1 = R; \quad R_2 = 2a - R_1$$

$$c = a - R_1; \quad b = \sqrt{a^2 - c^2}$$

$$\epsilon = \sqrt{1 - \frac{b^2}{a^2}} = 0.0305$$

$$\Delta V = \sqrt{\frac{GM_p}{R_1}} \left(\sqrt{\frac{2R_2}{R_1 + R_2}} - 1 \right) = 115.01 \text{ m/s}$$

Plane Order

The aim of this section is to describe the order in which all of the 9 planes are put into orbit. The fact that establishes one path or another is the fact that satellites can only communicate with neighbours, that is, one satellite can only communicate with its neighbours from the same plane and the neighbours from the neighbour planes.

When it comes to the order in which the planes are put into orbit, there are two main ways that come to mind. The first one is putting the planes consecutively into orbit. The second one is to put the planes into orbit leaving space between them for future planes. For example plane number one is put into orbit. The second plane to be put into orbit leaves space for one plane in between them. Then the third leaves space for one plane from the second, and so on. Leaving more space than for one plane could also be an option.

On the one hand, when using the first way the satellites from each plane could communicate with the ones from their neighbourhood. Therefore the range of communication would start being narrower but as new planes are put into orbit, the range would become wider. For instance, when three planes are already working, a given satellite from a customer could communicate with satellites that are at the other side of the planet in a determined range given by the width of signal that those three orbital planes could cover. When new planes are put into orbit this width becomes bigger up until the full globe is covered. Of course the main drawback of using this consecutive way of putting planes into orbit would be the long time of inactivity right at the beginning when few planes are working.

On the other hand, when using the second described way, the satellites can't communicate with other satellites from neighbour planes but the time of inactivity for customer's satellites would be less as a gap between planes is left for future ones. Nevertheless, this kind of configuration has a huge drawback and it's that when a satellite communicates with one given plane, this one can only communicate with other satellites that are in the

range of signal emission of that given plane. This is due to the fact that as neighbour planes are further apart they can't communicate with each other and therefore the range of communication is affected.

. Having pointed out all of the advantages and drawbacks of each configuration it is time to choose and it all comes down to Astrea's preferences. The configuration that fulfils these preferences for the most part is the consecutive .It allows the satellites to communicate in a broader range as the constellation grows and progressively conquer the sky.

Replacement Strategy

Due to the lifespan of the CubeSats, the whole constellation is replaced every five years, hence, a replacement strategy has to be designed. As stated in the First Placement section, the orbital planes are deployed consecutively, thus, the replacement has to be so also. One simple solution could be waiting for a plane to de-orbit and then place a new one into the same position, however, this procedure would spend too much time by the fact that the satellites approach the atmosphere in a very slow rate. Additionally, the replacement of different planes would probably overlap. Since the first placement has been carefully designed, it is thought to adapt the same procedure to the replacement process, that means, to consider the replacements as a first placement. Obviously, some differences have to be taken into account given that at this point there is a constellation providing full service to the customers. The problem remains on the fact that in order to use the same strategy, the replacement needs to be achieved in eight weeks, therefore, the new orbital planes cannot be situated into the same position than the old ones. A rapid replacement is also interesting regarding the need of providing full service to the customers without interruption. The solution adopted consists on placing the new planes between the old ones consecutively, following the order of the first placement. In order to clarify the process, a detailed explanation is shown below:

First of all, since different orbital planes are going to be taken into account in this explanation a nomenclature is set: old planes are the ones that have to be replaced, the new ones are the planes that will substitute them. If a plane is named with the number 1, it means that is the first one to be placed (old or new) and so on (2,3,...,21).

- The new plane 1 is placed between the old plane 1 and the old plane 21.
- The new plane 2 is placed between the old plane 1 and the old plane 2 to ensure that at the very moment the first old plane begins to decay, it does not appear a gap.
- At this point, the following new planes are deployed consecutively between the old ones until the constellation is fully renovated. This maneuver is repeated every five years to ensure the continuity of the Astrea Constellation. The following images show the process explained above.

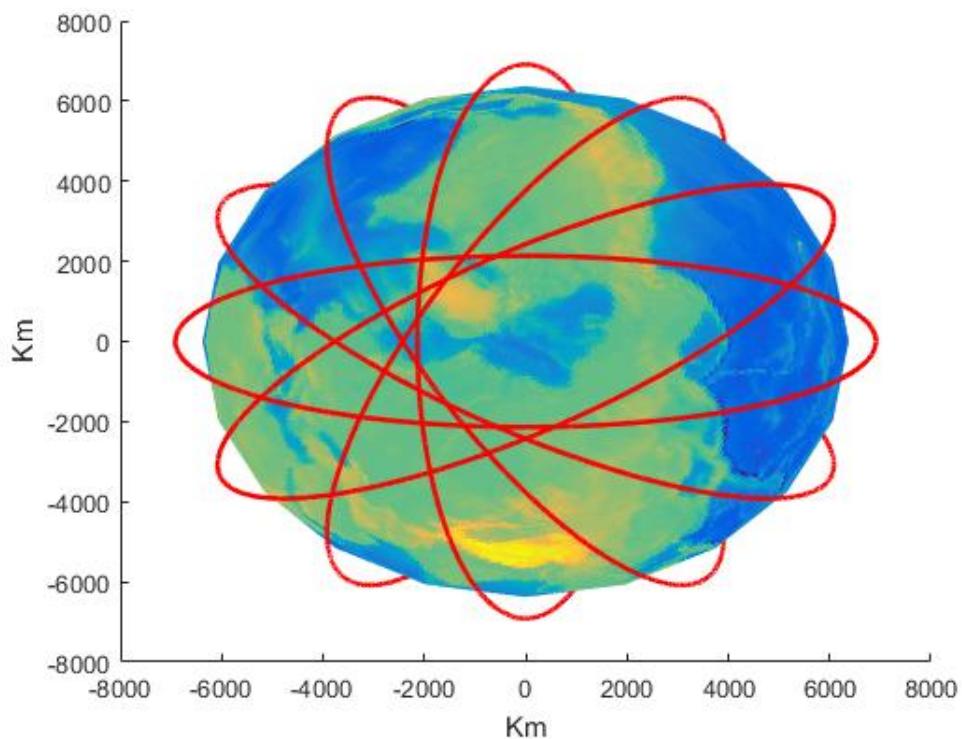


Figure 6.3.1: Old Constellation

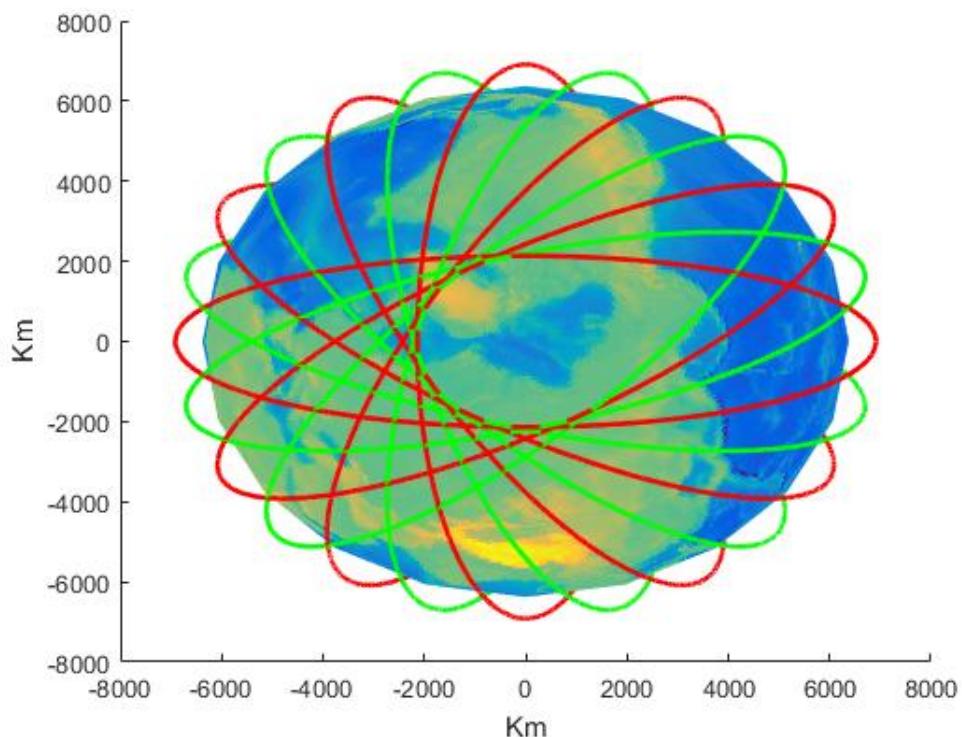


Figure 6.3.2: Old and New Constellations

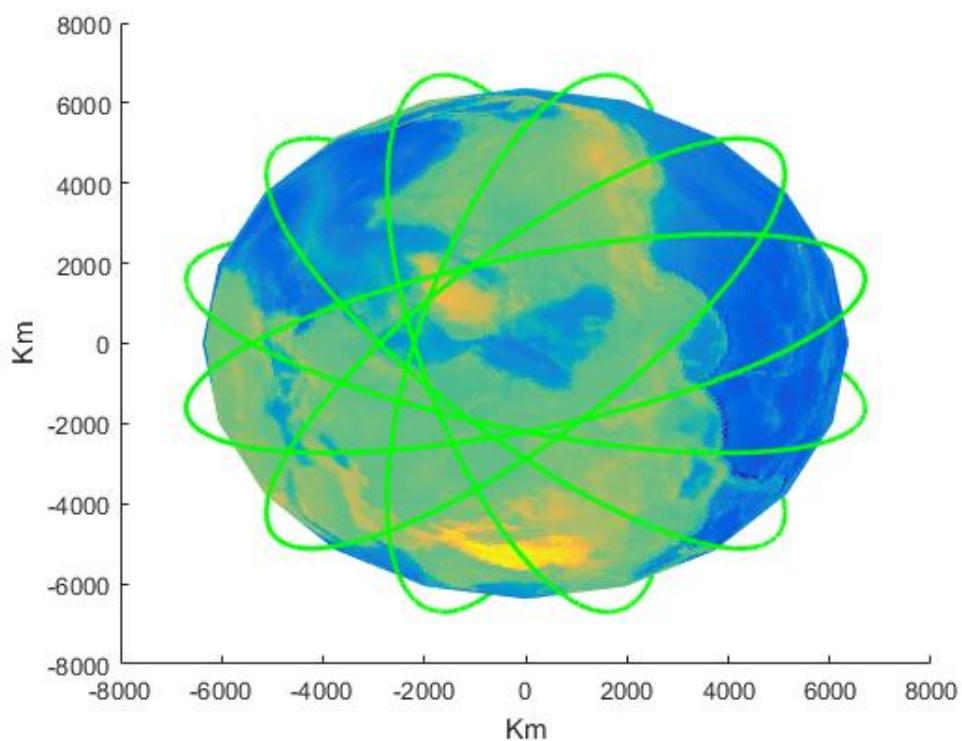


Figure 6.3.3: New Constellation

Spare Strategy

Spare Strategy Alternatives

Spare satellites in constellation:

This configuration consists on designing the constellation to be "*overpopulated*". As it sounds, this means that the system is established with *extra* operative satellites already orbiting within the constellation. For instance, only two overpopulating configurations had been pictured: overpopulated by one satellite or overpopulated by two satellites per orbital plane.

- ONE EXTRA SATELLITE:

By adding an extra satellite to the primary design of the orbital plane configuration, one satellite failure is covered with little time delay to recover the plan. In this way, the constellation continues to work at maximum capacity after a short interruption and at a suitable cost.

- TWO EXTRA SATELLITES:

Usually, by adding two extra satellites per orbital plane the reliability of the service achieves values around the 99.99%. This configuration increases considerably the cost of the project and it is mainly necessary in cases where the availability of the satellite is essential for the proper operation of the constellation.

Therefore, when designing an overpopulated constellation, the first decision to be made is the number of extra satellite per orbital plane. To guarantee the most optimal configuration a feasibility study is needed.

In-orbit spare:

The main difference between this strategy and the previous one is that in this case spare satellites are not operative. So the idea is to put some spare satellites in a orbit close to the principal one of the constellation in order to avoid possible collisions between operative satellites and spares.

A few things have to be taken into account when using this method. Firstly, even though the spare satellites are not operative, by being in orbit they deteriorate and by the time they are needed their operative lifetime and performability will not be such as the ones of brand new satellites. Secondly, as they are non-controlled satellites their orbital decay has to be predicted to be aware of possible collisions and avoid them. Thirdly, once any spare satellites is needed, it has to be able to do a two Hohmann transfer to achieve the performance orbit; the first one to reach a phasing orbit and the second one to end in

the operational altitude.

Spare satellites in parking orbits:

By making this choice it has to be assumed that the spare satellites can be kept in parking orbit until they are needed. Two different options are valid: keeping the rocket in a "*parking*" orbit and then trying to send it to the corresponding orbit; or keeping it in in-orbit satellites parkings such as the ISS. The main drawback is that the performance takes a long time until the constellation is recovered and depending on the orbit parameters and the launcher it is not possible to use this strategy.

Spare satellites in parking orbits:

The simplest and easiest one; the only thing that has to be done is to build extra satellites. The spares will remain on ground when the constellation is launched. Only in case the structure collapses due to a satellites failure, an emergency launch will put the spares in orbit. Moreover, this method is expensive because every extra launch has a high cost and it can take weeks to recover the constellation performance.

Major failure definition

In Project Charter, it has been stated that a major failure can be defined as the loss of a client's satellite coverage because of a failure in the network. However, this definition is not enough precise. For example, during a communication, it can happen that a data packet is lost, or has an error and it is discarded. This means that, for that packet, the communication was lost, but it does not mean that the communication with the client was lost. Another aspect to take into account is that a satellite may fail, but an alternative path can still exist and, therefore, the communication can continue. Moreover, if the client satellite loses all communication with all satellites in range, due to the different orbital velocities of the client satellite and the network satellites, the client satellite will eventually be in range of a functional network satellite.

For all these reasons, a more specific criteria is needed. In Project Charter it has also been stated that the network will provide communication between a client satellite and a ground station with a latency lower than 5 minutes (300 seconds, or 300,000 milliseconds). A major failure will consist in a failure in the network that causes a message to arrive from a client satellite to a client ground station with more than 5 minutes of delay, or not arrive at all. Derived from this definition, a minor failure can also be defined. It can be defined as a delay of more than 5 minutes in a communication between a client satellite and a ground station without any failure in the network.

Major failure

Because of the different height of the client satellite and the network satellites, if all the network satellites in range of the client satellite fail, the client satellite may come in range of a working network satellite if enough time passes. In some cases, this can happen in less than 5 minutes and, therefore, it will not be considered a major failure. For this reason, a more critical situation will be considered. It will be considered that the client satellite moves at the same speed as the network satellites, in the same orbital plane. In this situation, a major failure can happen because for three reasons: all network satellites in range of the client satellite fail, all ground stations fail, or some satellites fail but the alternative path takes more than 5 minutes to transmit the information.

Satellite in range failure

The first reason will be evaluated in the following lines. Depending on the location of the satellite and the distribution of the satellites in the constellation, the number of adjacent satellites may vary. A satellite over the equator can have up to six adjacent satellites. If a client satellite only communicates with this network satellite, a major failure will be the failure of this satellite, as it can be seen in Figure 6.4.1. It can also be the failure of a group of satellites surrounding the transmitting satellite, but this number is larger and, therefore, it would not be considered since the failure of the transmitting satellite is more restrictive.

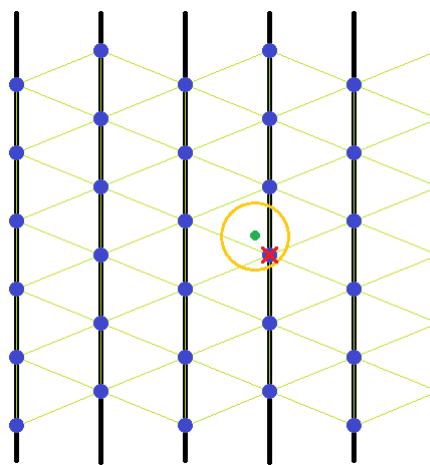


Figure 6.4.1: Failure due to the loss of the only satellite in range of the client satellite.

For antennas with almost half-spherical patterns (an angle of 10° over their horizontal plane has been considered as the minimum angle capable of receiving and transmitting),

the minimum height over the satellite network orbit in order to always see more than one satellite is, approximately, 400 km, considering that our constellation is at 550 km height over the Earth's surface. This means that a significant portion of clients would be in that zone.

For clients that have more than one network satellite in range, the critical failure would be similar as the ones in Figure 6.4.2 and Figure 6.4.3.

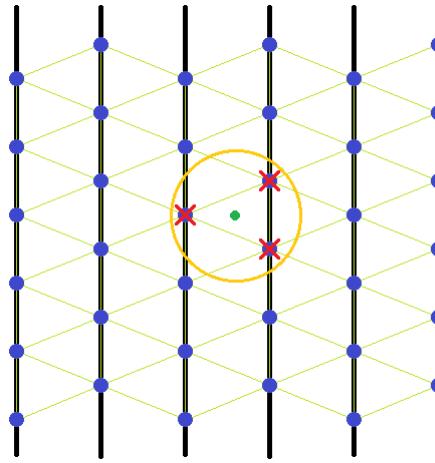


Figure 6.4.2: Failure due to the loss of all possible communication satellites if the client can communicate to three network satellites.

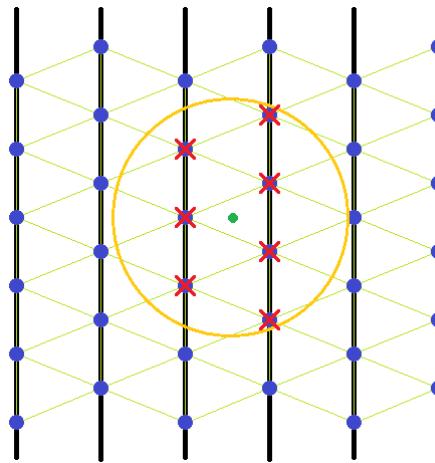


Figure 6.4.3: Failure due to the loss of all possible communication satellites if the client can communicate to seven network satellites.

As it can be seen, the critical failure depends on the communication range of the client satellite. Taking the more restrictive one would mean considering the failure of only one

satellite. As this affect a significant amount of potential clients, it can not be neglected.

Ground station failure

Since any satellite in the network is able to communicate with any ground station, in order to have a critical failure due to a ground station failure, all ground stations must fail. It will not be considered a failure the loss of connection to a ground station caused by bad weather conditions or radio-frequency interference, since it is not a failure in the network but an anomaly in the medium.

Therefore, for a critical failure caused by ground station failures to happen, all ground stations must fail. Since at least three ground stations will be used, the three of them must fail. As the previous case, the time of failure does not matter, but the fact that they remain unoperative at a given time.

Transmitting time failure

In the following lines, a major failure due to a delay superior to 5 minutes originated by a failure will be evaluated. First of all, it is needed to evaluate the transmission time. The minimum data rate that will handle the satellites is 25 Mbit/s. Therefore, it will be considered 25 Mbit/s as the data rate of the satellites, since it is the most restrictive. The protocols chosen, by default, cannot handle data units of more than 62,500 bytes, approximately. This is 500.000 bits. With the data rate chosen, the time to transmit this information is 0.02 seconds. For a path of 20 nodes, and considering that a satellite receives the entire packet before sending it again, the transmission time will be 0.4 seconds. The transmission is done using electromagnetic waves, which move at the speed of light. For this short distances, it can be considered to be instantaneously. The time used to process each data packet has to be taken into account. If each node needs 1 second to process the packet, the total processing time will be 20 seconds.

Finally, the time to recognize a fallen satellite and the time to compute an alternative route is required. By default, OSPF protocol requires 40 seconds of no response to label an adjacent node as dead. When this time expires, the fallen link state will be transmitted. When a node receives this update, it will wait 5 seconds and then it will calculate new routes. If the process requires 100 seconds, the total time until a failure happens and a new route is calculated is 145 seconds. With the processing time of 20.4 seconds, if one node fails, the time to deliver the message is 165.4 seconds. But if another node fails while

the message is still being delivered, the total time to deliver the message would be 310.4 seconds, which is superior to 5 minutes.

Therefore, for a critical failure to happen because of a delay of more than 5 minutes in the communication due to a failure in the network, two satellites must fail in less than 160 seconds, and both of them must be in a communication path between a client and a ground station.

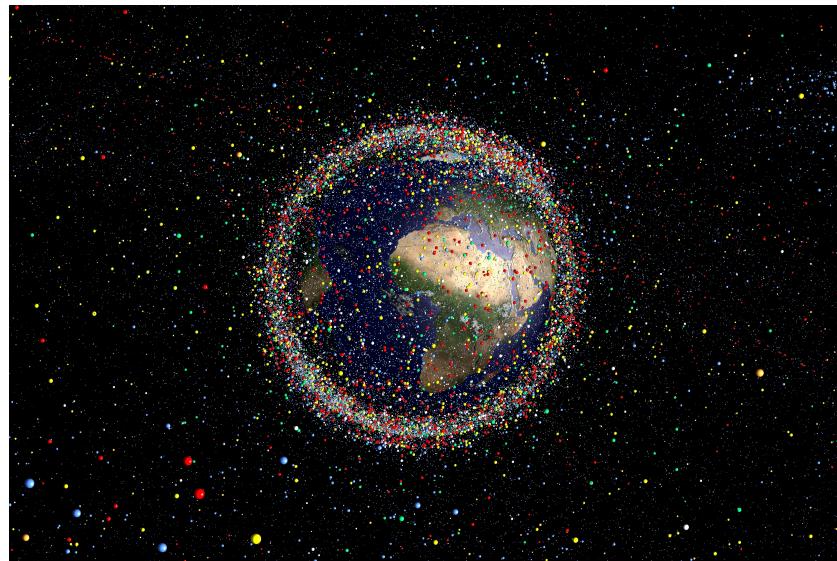


Figure 6.4.4: View of the Space Debris around the Earth

Space Debris

The Space had been a virgin environment until the middle of the twentieth century. However, it has already been exploited by humanity. During the last sixty years many space research centers –such as NASA, ESA or ROSCOSMOS- have been sending rockets and satellites to explore and understand its foreign environment without thinking on the consequences it could have. Fortunately, at the twenty-first century the concern about space debris has appears. Due to this fact, all those space research centers have begun to develop end-of-life strategies for all the missions that generate debris to restrict its lifetime.

The term Space Debris implicates all man-made objects that are orbiting with no human control. The problem arises from the fact that depending on the orbital parameters this space stuff is subject to more or less perturbations from either the Earth, the Moon, the Sun or the atmospherically drag and, after their operability's death, they might never disappear or completely disintegrate. As the quantity of space debris is huge and varied, they have been classified in four categories: fragmentation debris, non-functional spacecraft, rocket bodies and mission related debris.

The category that concerns the project is the non-functional spacecraft because it refers to all intact structures which have completed their mission. It is noticed that once satellite's operative lifetime arrives to its end, the satellites stop maneuvering and counteracting perturbations to maintain the current orbit. Consequently, they tend to deviate from their nominal orbital parameters, starting an unknown trajectory and

important repercussions.

Therefore, by increasing the number of uncontrolled “dead” satellites the probability of collision between working satellites and space debris increases at LEO as it is overcrowded. Space debris is small usually and its location can be followed from earth but is impossible to control it. Meanwhile, it is essential for space assets to be free of any impact because avoidance maneuvers are too complicated to have real success. Thereby, the increasing risk of collision becomes the big threat everyone is fighting against.

End-of-Life Types and Analysis

End-of-life strategies were implemented taking into account three factors: the time the satellite can orbit, the technical feasibility of active de-orbiting in terms of propellant and sub-systems enhancements and the altitude of its nominal orbital plane.

The first one is related to the fact that the current recommendations say that any space asset that can become a non-functional spacecraft must de-orbit and disintegrate at its twenty-fifth birth on orbit. The second refers to the magnitude of the maneuver that can be developed with the power the thruster system can achieve. The third one is relevant because perturbations in space change according to the distance to the Earth’s surface. The closer it is the more perturbations from Earth and drag forces from the atmosphere the satellite suffers and perturbations help to de-orbit and disintegrate space assets.

Based on these premises, two different end-of-life groups had been determined:

- CONTROLLED DE-ORBIT:

It consists on carrying out a maneuver that leads to steep, controlled re-entry and burn-up in the atmosphere or ground impact. It must be done in a relatively short period of time, usually 1 revolution and it involves significantly high ΔV . This sophisticated maneuver is initiated by a large increment of potential energy to make change the orbital altitude to a lower one well into the atmosphere where the satellite burns. A few calculations are useful to have a numerical result of that ΔV : The velocity in the initial orbit is:

$$V1 = \sqrt{\frac{GM_t}{R_t + h}} = 7593.4 \text{ m/s}$$

Then the semi major axis of the elliptical orbit is obtained:

$$a = \frac{r_1 + r_2}{2} = 6672 \text{ km}$$

The speed at apogee of the elliptical orbit is:

$$V_2 = \sqrt{GM_t\left(\frac{2}{r} - \frac{1}{a}\right)} = 7455 \text{ m/s}$$

Finally, the ΔV is computed:

$$\Delta V = V_1 - V_2 = 138.4 \text{ m/s}$$

- UNCONTROLLED DE-ORBIT:

A simpler and cheaper way to de-orbit satellites is to induce a reduction of the orbit altitude in order to cause a decay and, finally, a re-entry to the atmosphere. The process is initiated by one or several arc maneuvers at apogee passes and it is carried out without controlling the trajectory. This procedure is appropriate for low-thrust systems and small satellites.

In addition, when considering satellites placed at LEOs, this strategy takes advantages of the perturbations present in this altitudes (atmospheric drag). This force contributes to the decay increasing the rate of approach to the atmosphere.

Conclusions

This final section is intended to put and end to the Constellation Deployment Department activities. First of all, a brief summary of the work done is carried out, secondly, the compliance of the tasks assigned to this department in the Project Charter document is verified. Accomplished tasks:

- Launching System: a launching platform has been chosen regarding all the important parameters. Electron, from the enterprise Rocket Lab is the rocket that will bring Astrea Constellation to life.
- Deployer: a suitable deployer has been selected according to the standards of CubeSat deployment. GPOD deployer, developed by the enterprise GAUSS is in charge of the separation of the CubeSats from the rocket.
- First Placement: the assembly of the satellites will begin approximately 420 days before the first launching. The first placement will consist on eight launchings (one per orbital plane) and will last eight weeks.
- Replacement Strategy: similar to the first placement strategy, new orbital planes are placed between the old ones avoiding the formation of gaps during the decay of the satellites that are being renewed.
- Spare Strategy:
- End of Life Strategy: an uncontrolled de-orbit procedure has been chosen.

The summary shown above demonstrates that the Constellation Deployment Department has fulfilled the requested duties. According to the legislation, both the chosen launcher (Electron) and deployer (GPOD) are certified. Their enterprises designed them strictly following the international requirements.

Part III

ANNEX III: Communications

Chapter 7

Space Segment Protocol Stack

"The wonder is, not that the field of stars is so vast, but that man has measured it."

Anatole France, 1894

Layer 2: Data Link

Functions of the DLL

The explained functions are:

- **Framing:** Data-link layer takes packets from Network Layer and encapsulates them into Frames. Then, it sends each frame bit-by-bit on the hardware. At receiver end, data link layer picks up signals from hardware and assembles them into frames.
- **Addressing:** Each device on a network has a unique number, usually called a hardware address or MAC address, that is used by the data link layer protocol to ensure that data intended for a specific machine gets to it properly.
- **Synchronization:** When data frames are sent on the link, both machines must be synchronized in order to transfer to take place.
- **Error control:** Sometimes signals may have encountered problem in transition and the bits are flipped. These errors are detected and attempted to recover actual data bits.

- **Flow control:** Stations on same link may have different speed or capacity. Data-link layer ensures flow control that enables both machine to exchange data on same speed.

Working procedure

Working procedure is explained deeply now. All the images have been extracted from [9].

Simplest Protocol

This protocol has no error or flow control. It is supposed that the frames are traveling only in one direction, from the sender to the receiver. It is also supposed that the receiver can immediately handle the frames received, so there is no overwhelming. The DLL of the sender site gets data from its network layer, makes a frame out of the data and sends it. The DLL at the receiver site receives a frame from its physical layer, extracts data from the frame and delivers the data to its network layer. The problem here is that the sender site cannot send a frame until its network layer has a data packet to send and the receiver site cannot deliver a data packet to its network layer until a frame arrives. There is the need to introduce the idea of events in the protocol. The procedure at the sender site is constantly running; there is no action until there is a request from the network layer. The procedure at the receiver site is also constantly running, but there is no action until notification from the physical layer arrives.

1	<code>while (true)</code>	<i>// Repeat forever</i>
2	<code>{</code>	
3	<code> WaitForEvent()</code>	<i>// Sleep until an event occurs</i>
4	<code> if(Event(RequestToSend))</code>	<i>//There is a packet to send</i>
5	<code> {</code>	
6	<code> GetData()</code>	
7	<code> MakeFrame()</code>	
8	<code> SendFrame()</code>	<i>//Send the frame</i>
9	<code> }</code>	
10	<code>}</code>	

Figure 7.1.1: Sender algorithm for the simplest protocol.

```

1 while(true)           // Repeat forever
2 {
3   WaitForEvent();i      // Sleep until an event occurs
4   if(Event(ArrivalNotification)) // Data frame arrived
5   {
6     ReceiveFrame();i
7     ExtractData();i
8     DeliverData();i        // Deliver data to network layerz
9   }
10 }
```

Figure 7.1.2: Receiver algorithm for the simplest protocol.

Stop-and-Wait Protocol

If data frames arrive at the receiver site faster than they can be processed, the frames must be stored until their use. Normally, the receiver does not have enough storage space, especially if it is receiving data from many sources. This may result in either the discarding of frames or denial of service. To prevent the receiver from becoming overwhelmed with frames, we somehow need to tell the sender to slow down. There must be feedback from the receiver to the sender.

In the Stop-and-Wait Protocol the sends one frame, stops until it receives confirmation from the receiver and then sends the next frame. We still have unidirectional communication for data frames, but auxiliary ACK frames (simple tokens of acknowledgment) travel from the other direction. We add flow control to our previous protocol. In this case the algorithms of the sender and the receiver are the following ones.

```

1 while(true)           // Repeat forever
2 canSend = true          // Allow the first frame to go
3 {
4   WaitForEvent();i      // Sleep until an event occurs
5   if(Event(RequestToSend) AND canSend)
6   {
7     GetData();i
8     MakeFrame();i
9     SendFrame();i        // Send the data frame
10    canSend = false;      // I/cannot send until ACK arrives
11  }
12  WaitForEvent();i      // Sleep until an event occurs
13  if(Event(ArrivalNotification)) // An ACK has arrived
14  {
15    ReceiveFrame();i        // Receive the ACK frame
16    canSend = true;
17  }
18 }
```

Figure 7.1.3: Sender algorithm for the Stop-and-Wait Protocol.

```

1  while (true)           IIRepeat forever
2  {
3      WaitForEvent();      II Sleep until an event occurs
4      if(Event(ArrivalNotification)) II Data frame arrives
5      {
6          ReceiveFrame();
7          ExtractData();
8          Deliver(data);        /IDeliver data to network layer
9          SendFrame();         IISend an ACK frame
10     }
11 }
```

Figure 7.1.4: Receiver algorithm for the Stop-and-Wait Protocol.

The two protocols explained are protocols that can be suitable for noiseless channels. However, noiseless channels are nonexistent. There is a need to add error control to the protocol. Three protocols are discussed with the aim of doing so.

Stop-and-Wait Automatic Repeat Request

The Stop-and Wait ARQ adds a simple error control mechanism to the Stop-and-Wait Protocol. To detect and correct corrupted frames, we need to add redundancy bits to our data frame. When the frame arrives at the receiver site, it is checked and if it is corrupted, it is silently discarded. The detection of errors in this protocol is manifested by the silence of the receiver. Frames are also numbered so if the receiver receives a data frame that is out of order, this means that frames were either lost or duplicated. What is done to solve the error is that when the sender sends a frame, it keeps a copy of the sent frame. At the same time, it starts a timer. If the timer expires and there is no ACK for the sent frame, the frame is resent, the copy is held, and the timer is restarted. Since the protocol uses the stop-and-wait mechanism, there is only one specific frame that needs an ACK even though several copies of the same frame can be in the network. Since an ACK frame can also be corrupted and lost, it too needs redundancy bits and a sequence number. In the following figure is possible to see more clearly what is going on with this protocol.

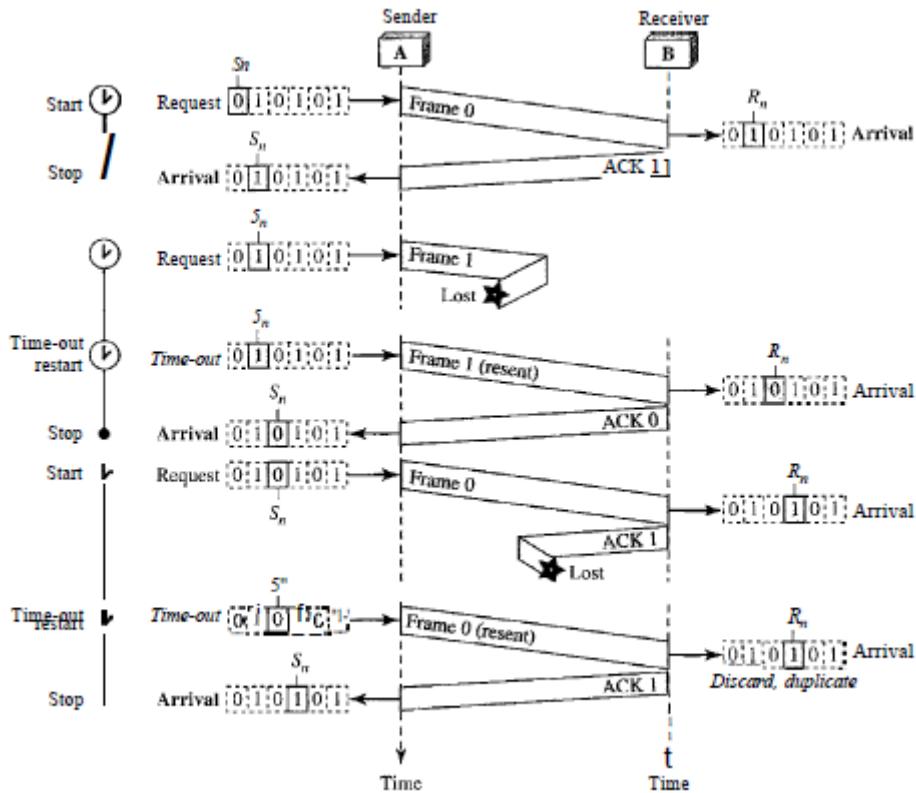


Figure 7.1.5: Flow diagram of the Stop-and Wait ARQ.

The main problem of this protocol is its efficiency. The Stop-and-Wait ARQ is very inefficient if our channel is thick and long. The product of thickness and length is called the bandwidth-delay product. We can think of the channel as a pipe. The bandwidth-delay product then is the volume of the pipe in bits. The pipe is always there. If we do not use it, we are inefficient.

Go-Back-N Automatic Repeat Request

To improve the efficiency of transmission (filling the pipe), multiple frames must be in transition while waiting for acknowledgment. In other words, we need to let more than one frame be outstanding to keep the channel busy while the sender is waiting for acknowledgment. In the Go-Back-N Automatic Repeat Request the sender sends several frames before receiving acknowledgments. It also keeps a copy of these frames until the acknowledgments arrive. Although there can be a timer for each frame that is sent, in this protocol only one is used. The reason is that the timer for the first outstanding frame always expires first and then all outstanding frames when this timer expires are sent again. The receiver sends a positive acknowledgment if a frame has arrived safe and sound and

Layer 2: Data Link

in order. If a frame is damaged or is received out of order, the receiver is silent and will discard all subsequent frames until it receives the one it is expecting. The silence of the receiver causes the timer of the unacknowledged frame at the sender site to expire. This, in turn, causes the sender to go back and resend all frames, beginning with the one with the expired timer. The receiver does not have to acknowledge each frame received. It can send one cumulative acknowledgment for several frames. That is the reason why the protocol is called Go-Back-N. The flow diagram and the algorithms of the sender and the receiver are shown next.

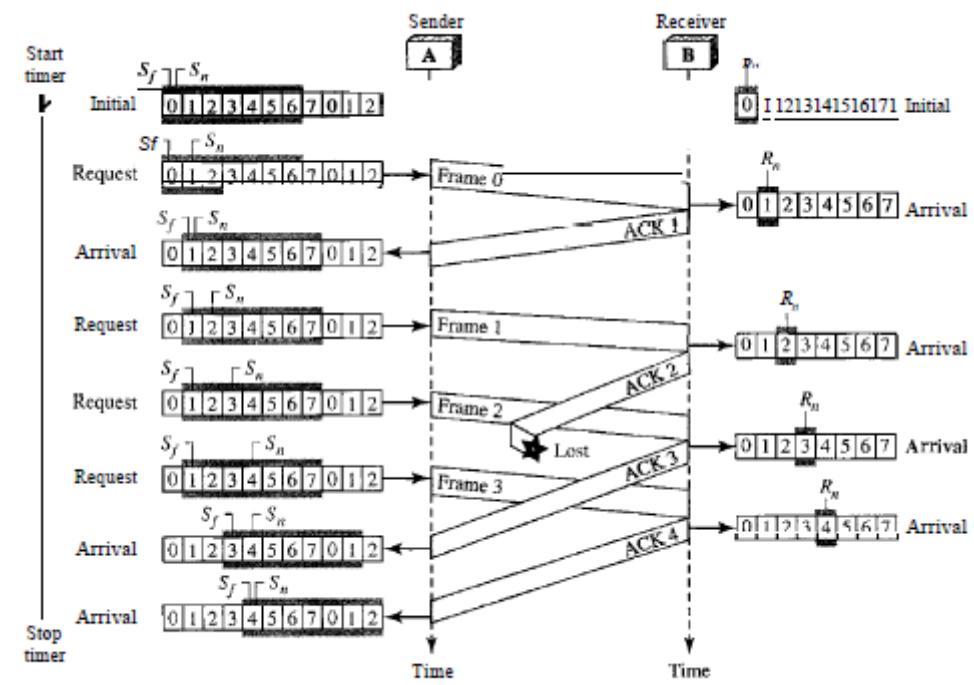


 Figure 7.1.6: Flow diagram of the Go-Back-N ARQ.

```
1 Rn = 0;
2
3 while (true)           IIRepeat forever
4 {
5   WaitForEvent();
6
7   if(Event{ArrivalNotification}) /Data frame arrives
8   (
9     Receive(Frame);
10    if(corrupted(Frame))
11      Sleep();
12    if(seqNo == Rn)           IIIIf expected frame
13    {
14      DeliverData();          IIDeliver data
15      Rn = Rn + 1;          IISlide window
16      SendACK(Rn);
17    }
18  }
19 }
```

Figure 7.1.7: Receiver algorithm for the Go-Back-N ARQ.

```

1 Sw = 2m - 1;
2 Sf = 0;
3 Sn = 0;
4
5 while (true)           //Repeat forever
6 {
7   WaitForEvent();
8   if(Event{RequestToSend}) //A packet to send
9   {
10     if(Sn-Sf == Sw)      //If window is full
11       Sleep();
12     GetData();
13     MakeFrame(Sn);
14     StoreFrame(Sn);
15     SendFrame(Sn);
16     Sn = Sn + 1;
17     if(timer not running)
18       StartTimer();
19   }
20
21   if(Event{ArrivalNotification} //ACK arrives
22   {
23     Receive(ACK);
24     if(corrupted(ACK))
25       Sleep();
26     if((ackNo>sf)&&(ackNO==Sn) //If a valid ACK
27     While(sf == ackNo)
28     {
29       PurgeFrame(sf);
30       sf = sf + 1;
31     }
32     StopTimer();
33   }
34
35   if(Event{TimeOuts}        //The timer expires
36   {
37     StartTimer();
38     Temp = sf;
39     while(Temp < Sn);
40     {
41       SendFrame(sf);
42       sf = sf + 1;
43     }
44   }
45 1

```

Figure 7.1.8: Sender algorithm for the Go-Back-N ARQ.

Selective Repeat Automatic Repeat Request

Go-Back-N ARQ simplifies the process at the receiver site. The receiver keeps track of only one variable, and there is no need to buffer out-of-order frames; they are simply discarded. However, this protocol is very inefficient for a noisy link. In a noisy link a frame has a higher probability of damage, which means the resending of multiple frames. In the case of these protocol, the Selective Repeat ARQ, the processing at the receiver is more complex but is more efficient for noisy links. The Selective Repeat Protocol allows a number of frames to arrive out of order and be kept until there is a set of in-order frames to be delivered to the network layer. The handling of the request event is similar to that of the previous protocol except that one timer is started for each frame sent. The arrival event is more complicated here. An ACK or a NAK frame may arrive. If a valid NAK frame arrives, the corresponding frame is resent. If a valid ACK arrives the corresponding timer stops. When the time for a frame has expire, only this frame is resent.

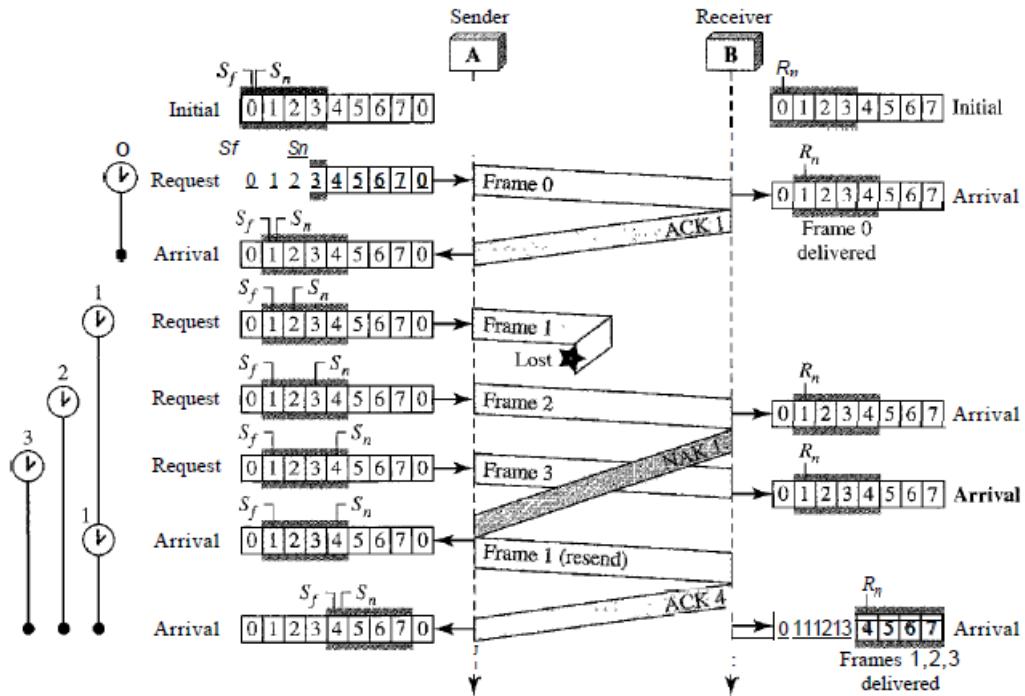


Figure 7.1.9: Flow diagram of the Selective Repeat ARQ.

```

1   = 2m-1 i
2   = Oi
3   = Oi
4
5   while (true)           //Repeat forever
6   {
7     WaitForEvent(i)
8     if(Event(RequestToSend)) //There is a packet to send
9   {

```

```

10     if(Sn-S;E >= Sw)           I/If window is full
11         Sleep();
12         GetData();
13         MakeFrame(Sn);
14         StoreFrame(Sn);
15         SendFrame(Sn);
16         Sn = Sn + 1;
17         StartTimer(Sn);
18     }
19
20     if(Event{ArrivalNotification}» ACK arrives
21     {
22         Receive(frame);          I/Receive ACK or NAK
23         if{corrupted(frame)}
24             Sleep();
25         if (FrameType == NAK)
26             if (nakNo between Sf and So)
27             {
28                 resend(nakNo);
29                 StartTimer(nakNo);
30             }
31         if (FrameType == ACK)
32             if (ackNo between Sf and So)
33             {
34                 while(sf < ackNo)
35                 {
36                     Purge(sf);
37                     stopTimer(Sf);
38                     Sf = Sf + 1;
39                 }
40             }
41     }
42
43     if(Event{TimeOut{t}})        If the timer expires
44     {
45         StartTimer(t);
46         SendFrame(t);
47     }
48 }
```

Figure 7.1.10: Sender algorithm for the Selective Repeat ARQ.

```

1 Rn = 0;
2 NakSent = false;
3 AckNeeded = false;
4 Repeat(for all slots)
5   Marked(slot) = false;
6
7 !while (true)                                //Repeat forever
8 {
9   WaitForEvent();
10
11  if(Event{ArrivalNotification})           //Data frame arrives
12  {
13    Receive(Frame);
14    if(corrupted(Frame)&& (NOT NakSent)
15    {
16      SendNAK(Rn);
17      NakSent = true;
18      Sleep();
19    }
20    if(seqNo <> Rn)&& (NOT NakSent)
21    {
22      SendNAK(Rn);
23      NakSent = true;
24      if ((seqNo in window)&&(IMarked(seqNo))
25      {
26        StoreFrame(seqNo)
27        Marked(seqNo)= true;
28        while(Marked(Rn)
29        {
30          DeliverData(Rn);
31          Purge(Rn);
32          Rn = Rn + 1;
33          AckNeeded = true;
34        }
35        if(AckNeeded);
36        {
37          SendAck(Rn);
38          AckNeeded = false;
39          NakSent = false;
40        }
41      }
42    }
43  }
44 }
```

Figure 7.1.11: Receiver algorithm for the Selective Repeat ARQ.

Bidirectional links: Piggybacking

Piggybacking is not a protocol, is a technique. All que protocols explained until now are all unidirectional: data frames flow in only one direction although control information such as ACK and NAK frames can travel in the other direction. In real life, data frames are normally flowing in both directions: from node A to node B and from node B to node A. This means that the control information also needs to flow in both directions. Piggybacking is used to improve the efficiency of the bidirectional protocols. When a frame is carrying data from A to B, it can also carry control information about arrived (or lost)

frames from B; when a frame is carrying data from B to A, it can also carry control information about the arrived (or lost) frames from A.

Working procedure ranking

Now its time to choose the working procedure that best fits the needs of the mission. To do so, an OWA (Ordered Weighted Average) will be used. The criteria to consider is the following one:

- Efficiency: This fact deals with how the channel is being used. Protocols will be classified as non-efficient or efficient.
- Time: This fact deals about the time needed to transmit the data satisfactory.
- Error correction: Deals about whether a protocol can correct an error of transmission or not.

It is important also to take into account that the protocol to use should have a flow control, that is, should know if the receiver is available or not to receive the data. For this reason the Simplest Protocol is rejected and won't be studied in the OWA. Regarding the factors of the OWA, all of them will be rated from 0 to 1. In this project the fact of transmitting the data without errors is more important than transmitting it fast, as is possible to appreciate in the project charter (the latency can be relative high, but incorrect information is useless). The efficiency of the protocol is very important too, because the less the efficiency the less power provided by the CubeSat is being used. Since the CubeSat has limited space, ideally all the power it can give for transmission will be used for it. Then, the weights of the different factors are the following ones:

- Efficiency: 40
- Time: 30
- Error correction: 60

In the following table the rating of each protocol together with the corresponding OWA is shown.

Layer 2: Data Link

Protocol	Efficiency	Time	Error correction	OWA
Stop-and-Wait Protocol	0	0	0	0
Stop-and-Wait ARQ	0	0	1	0,46
Go-Back-N ARQ	1	0	1	0.69
Selective Repeat ARQ	1	1	1	1

Table 7.1.1: OWA of the DLL protocols.

Then, the ranking of working procedures is the following one:

1	Selective Repeat ARQ
2	Go-Back-N ARQ
3	Stop-and-Wait ARQ
4	Stop-and-Wait Protocol

Table 7.1.2: Ranking of working procedures

It has to be said that when dealing with bidirectional links piggybacking technique will be used if possible.

Protocols

The standards of the CCSDS will be followed in order to allow interoperability with other satellites such as the one of the client. The CCSDS has developed four protocols for the Data Link Protocol Sublayer of the Data Link Layer [10]:

- TM Space Data Link Protocol
- TC Space Data Link Protocol
- AOS Space Data Link Protocol
- Proximity-1 Space Link Protocol-Data Link Layer

These protocols provide the capability to send data over a single space link. TM, TC, and AOS can have secured user data into a frame using the Space Data Link Security (SDLS) Protocol.

CCSDS has also developed three standards for the Synchronization and Channel Coding Sublayer of the DLL:

- TM Synchronization and Channel Coding

Layer 2: Data Link

- TC Synchronization and Channel Coding
- Proximity-1 Space Link Protocol—Coding and Synchronization Layer

TM Synchronization and Channel Coding is used with the TM or AOS Space Data Link Protocol, TC Synchronization and Channel Coding is used with the TC Space Data Link Protocol and the Proximity-1 Space Link Protocol—Coding and Synchronization Layer is used with the Proximity-1 Space Link Protocol—Data Link Layer. This can be seen better in the following image.

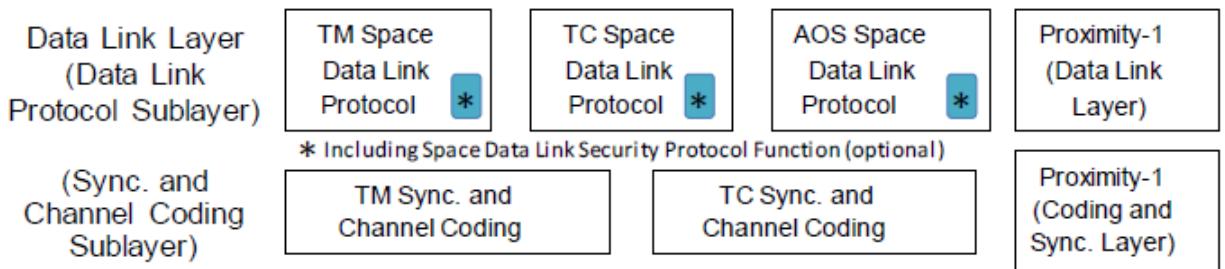


Figure 7.1.12: DLL of the CCSDS.

Now the reliability of each of the protocols of the Data Link Protocol Sublayer will be compared in order to know which one is the best of them. This will be done because reliability is the most important feature of the DLL.

Protocol	System used for reliability
TM	Stop-and-Wait Protocol
TC	Type-A: Go-Back-N ARQ, Type-B: Stop-and-Wait Protocol
AOS	Stop-and-Wait Protocol
Proximity-1	Go-Back-N ARQ

Table 7.1.3: Reliability of CCSDS protocols

According to the table and to the ranking of working procedures done previously, only TC Type-A and Proximity-1 will be considered from now on. Security is another important feature to take into account when taking this decision. TM Space Data Link Protocol has provision for inserting secured data into a frame using the Space Data Link Security (SDLS) Protocol. However, there have been no security requirements to date established for Proximity-1. The SDLS protocol can provide security services, such as authentication and confidentiality for TC Transfer Frames (it can also do it with TM and AOS, that have been previously discharted). Both the TC and the Proximity-1 use variable-length

Transfer Frames to facilitate reception of short messages with short delay. Another key feature to take into account when deciding a protocol, is the concept of "Virtual Channels". The Virtual Channel facility allows one Physical Channel (a stream of bits transferred over a space link in a single direction) to be shared among multiple higher-layer data streams, each of which may have different service requirements. A single Physical Channel may therefore be divided into several separate logical data channels, each known as a Virtual Channel (VC). The TC has the following identifiers: the Transfer Frame Version Number (TFVN), the Spacecraft Identifier (SCID), and the Virtual Channel Identifier (VCID). It also uses an optional identifier, called the Multiplexer Access Point Identifier (MAP ID), that is used to create multiple streams of data within a Virtual Channel. In contrast, the Proximity-1 uses a triad of multiplexing capabilities, which is incorporated for specific functionality within the link. The Spacecraft Identifier (SCID) identifies the source or destination of Transfer Frames transported in the link connection based upon the Source-or-Destination Identifier. The Physical Channel Identifier (PCID) provides up to two independently multiplexed channels. The Port ID provides the means to route user data internally to specific logic ports, such as applications or transport processes, or to physical ports, such as onboard buses or physical connections. Now a table with the identifiers of the TC and the Proximity-1 will be shown:

Identifiers	TC Space Data Link Protocol	Proximity-1 Space Link Protocol- Data Link Layer
TFVN	00	10
SCID	0 to 1023	0 to 2013
PCID	N/A	0 to 1
VCID	0 to 63	N/A
MAP ID	0 to 63	N/A
Port identifier	N/A	0 to 7

Table 7.1.4: Identifiers of TC and Proximity-1 Space Data Link Layer Protocols

Having Virtual Channels is important for the mission that is exposed in this project because it allows having more than one stream of bits to take place at the same time, that is to say that more than one client can communicate with their satellite without having to wait for another client to finish.

The decision taken is to use the TC Space Data Link Protocol with the TC sync. and channel coding together with the Space Data Link Security Protocol. The reasons for doing so are mainly:

- Security: Incorporating the SLDS authentication and confidentiality is provided.
- More virtual channels: This feature allow more clients communicating with their satellites at the same time.

TC Space Data Link Protocol

Now some specifications of the chosen protocol will be exposed in order to know how it is structured and how many bits it adds to the original data. Further information of the protocol can be found in [11]. The protocol specifications will be explained when it is used with the support of the SDLS protocol. In this section is important to know that 1 octet is an eight-bit word. The structure of the transfer frame in this protocol is the following one:

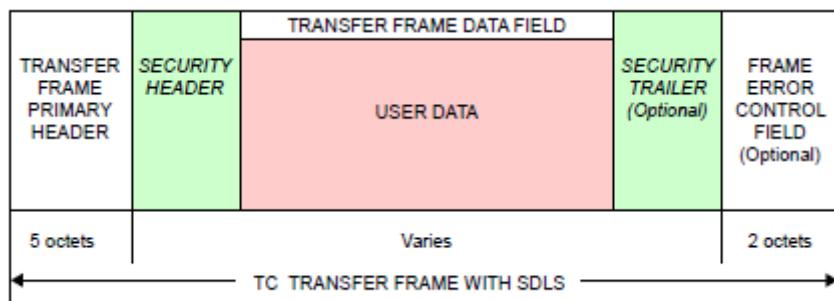
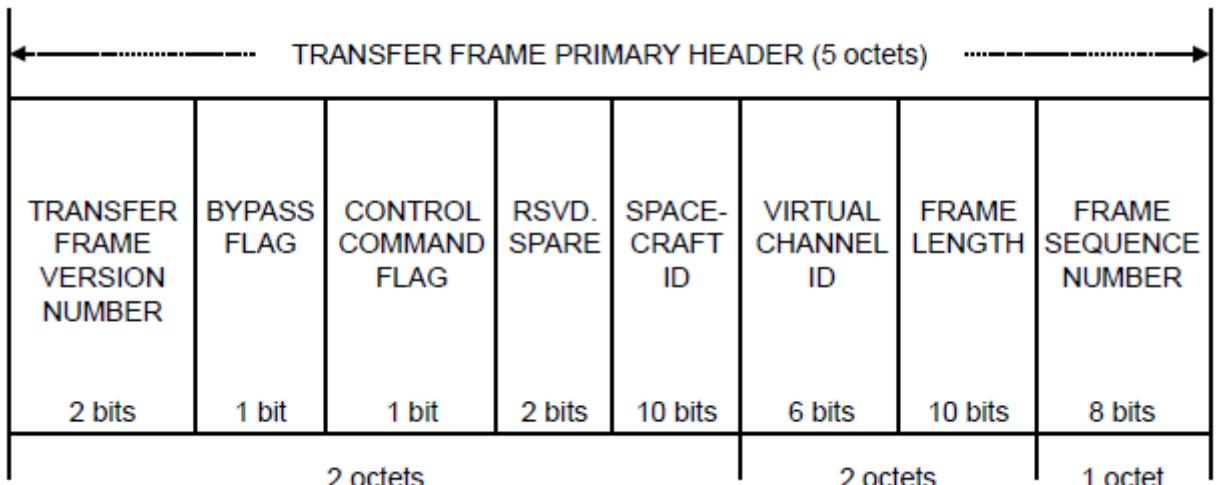


Figure 7.1.13: Transfer frame structure of the TC Space DL Protocol with SDLS.

In the transfer frame primary header, the following information is contained:



TRANSFER FRAME PRIMARY HEADER (5 octets)							
TRANSFER FRAME VERSION NUMBER	BYPASS FLAG	CONTROL COMMAND FLAG	RSVD. SPARE	SPACE- CRAFT ID	VIRTUAL CHANNEL ID	FRAME LENGTH	FRAME SEQUENCE NUMBER
2 bits	1 bit	1 bit	2 bits	10 bits	6 bits	10 bits	8 bits
				2 octets	2 octets		1 octet

Figure 7.1.14: Transfer frame primary header.

With this data, is possible to say that the TC Space Data Link Protocol will add to data coming from the Network layer at least 5 octets (40 bits).

TC Sync and Channel Coding

This protocol is the corresponding to the Synchronization and Channel Coding Sublayer that has been used with the TC Space and Data Link Protocol. It has functions as for example, encapsulate the data units so that the start and end can be detected by the receiving end, ensure there are sufficient bit transitions in the transmitted bit stream so that the receiver can maintain bit synchronization during the reception of the data unit, etc. In a nutshell, one instance of the Synchronization and Channel Coding Sublayer processes the data stream for a single Physical Channel, making it a stream of bits that can be transferred over a space link in a single direction. The procedures can be differentiated between the ones that occur in the sending end and the one that occur in the receiving end. The procedures are the following ones:

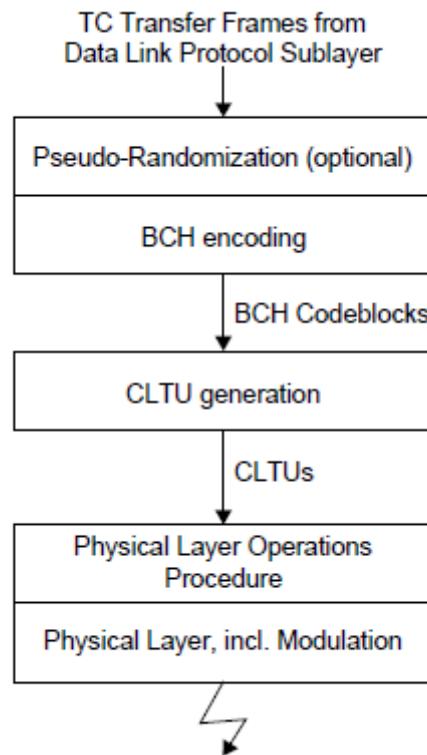


Figure 7.1.15: Procedure at the sending end.

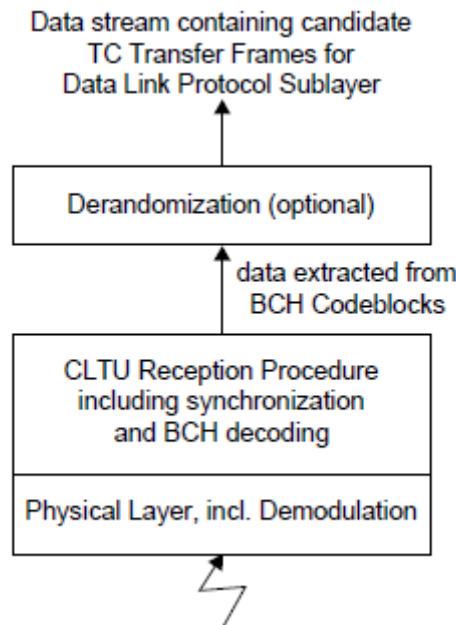


Figure 7.1.16: Procedure at the receiving end.

Is possible to see that two packets of data are created, BCH Codeblocks and CLTUs. From the point of view of the Synchronization and Channel Coding Sublayer, the content of the Frames parameter is a single block of data. For a single Channel Access request, the Synchronization and Channel Coding Sublayer generates a set of BCH Codeblocks, and that set of BCH Codeblocks is placed in a single CLTU. One of the managed parameters for the Physical Channel is the maximum length of a CLTU. The lenght of the CLTU can be calculated as follows (in octets):

$$\text{Length of the CLTU} = 10 + 8 \cdot \left(\frac{\text{Total lenght of the frames} + 6}{7} \right) \quad (7.1.1)$$

Since with the TC Space Data Link protocol the frames can have different sizes, the CLTU can also have different sizes. More information about this sublayer of the DLL can be found in reference [12]

Layer 3: The Network

Functions of the Network Layer

The Network layer provides the following functions:

- **Routing:** Selects the best path between two nodes in a network, often using intermediate nodes called routers.

- **Network flow control:** Routers may indicate a transmitting node to reduce its transmission when the router's buffer becomes full.
- **Package fragmentation:** If the message to be transmitted is too large to be transmitted in the Data link layer, the network may split it into several packages in one node, send them independently and reassemble them in another node. Optionally, it can provide error control.
- **Logical-physical address allocation:** Translates the logical address (or names) of the network nodes into a unique physical address.
- **Message forwarding:** A network may be divided into subnetworks, connected through specialized hosts, called gateways or routers, that forward packets between those subnetworks.

Protocols

The Consultive Committee for Space Data Systems (CCSDS) [13] has two standards for using in the Network layer in conjunction with the Space Data Link Layer Protocols recommended by the CCSDS. Those two standards are the Space Packet Protocol (SPP) [14] and the Encapsulation Service [15]. With the Space Packet Protocol, application processes generate and consume Protocol Data Units (PDU). The Encapsulation Service encapsulates PDU of recognized protocols defined in a Space Assigned Number Authority (SANA) [16] registry into two types of packets, either Space Packets or Encapsulation Packets. External protocols data units, such as the Internet Protocol datagrams, can be transmitted by CCSDS Space Data Link Protocols, although they cannot be directly encapsulated by the Encapsulation Service, and an intermediate service, such as IP over CCSDS (IPoC) [17], must be used.

Figure 7.2.1, shows the recommended protocols by the CCSDS for Space Communications. In Figure 7.2.2 those protocols are rearranged in some possible combinations. As it can be seen, IP cannot be directly used neither by the protocols in the Data Link layer nor the Encapsulation Service.

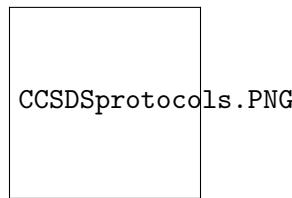


Figure 7.2.1: Protocols recommended by the CCSDS, classified in their respective OSI layers. Extracted from [13].

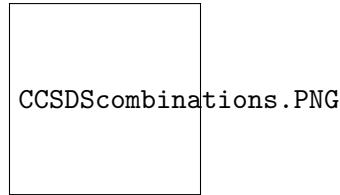


Figure 7.2.2: Possible Combinations of the CCSDS recommended protocols. Extracted from [13].

Protocols in the Network Layer can be classified according if they are the main protocol (SPP or IP, for example) or they provide additional features so that the main protocol can work efficiently. An example of the latter are routing protocols, and also for IP, IPoC and Encapsulation Service.

In the following pages, a brief review of distinct protocols on the Network layer will take place. Since CCSDS recommends using SPP or Encapsulation Service, only SPP and protocols that can be encapsulated by the Encapsulation Service, either directly or indirectly, will be reviewed. The protocols reviewed will be classified according if they are the main protocol, auxiliary protocols, or routing protocols.

Main protocols

Space Packet Protocol (SPP) [14]

The Space Packet Protocol (SPP) is a protocol designed to efficiently transfer application data over a network of space links. SPP provides a unidirectional data transfer service from a single source user application to one or more destination user applications through one or more subnetworks. The path from the source user application to the destination user application is called a Logical Data Path (LDP). Every LDP is uniquely identified by a Path Identifier (Path ID). The protocol data unit used by this protocol is the Space Packet. Each Space Packet is defined by a header section and a data section.

Each LPD is uniquely identified by a Path ID. A Path ID consists of an Application Process Identifier (APID) and an optional APID Qualifier. APID Qualifiers identify the naming domain for an APID. APIDs are unique in a single naming domain. The APID is part of the header of the Space Packet, but the APID Qualifier must be carried by a protocol of an underlying layer.

The following features are common to the services of the SPP:

- Pre-configured Services. The user can send or receive data only through a preconfigured LDP established by management.
- Unidirectional Services. One end of an LDP can send, but not receive, data through the LDP, while the other end can receive, but not send. This means A can send to B through a LPD, but for B to send to A has to use a different LDP
- Asynchronous Services. There are no predefined timing rules for the transfer of service data units supplied by the service user. The user may request data transfer at any time it desires, but there may be restrictions imposed by the provider on the data generation rate.
- Unconfirmed Services. The sending user does not receive confirmation from the receiving end that data has been received.
- Incomplete Services. The services do not guarantee completeness, nor do they provide a retransmission mechanism.
- Non-sequence Preserving Services. The sequence of service data units supplied by the sending user may not be preserved through the LDP.

The following services are assumed from the underlying layers:

- Addressing and routing capabilities for establishing LDPs
- Capability for associating an APID Qualifier for each Space Packet.

The structure of a Space Packet consists of a Packet Primary Header, and a Packet Data Field, which can contain an optional Secondary Header. Figure 7.2.3 shows the structure of the SPP primary header:

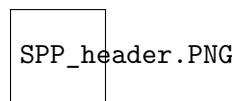


Figure 7.2.3: Example of a header for an SPP Space Packet.

Internet Protocol version 4 (IPv4) [18]

The Internet Protocol version 4 (IPv4) is the fourth version of the Internet Protocol (IP). It is one of the core protocols of standards-based internetworking methods in the Internet. Despite the ongoing deployment of a successor protocol (IPv6), the IPv4 still

routes most of the Internet traffic. IPv4 is a connectionless protocol and does not guarantee delivery, nor does it assure proper sequencing or avoidance of duplicate delivery. These aspects are addressed by a transport layer protocol.

One of the features of IPv4 are addresses. Network addresses are the identification number of any device that is part of a network. IPv4 uses 32-bit (4 byte) addresses. Therefore, the address space is limited to 4294967296 (2^{32}) addresses. A IPv4 address is usually represented in two ways: in binary notation, where each group of 8 bits is separated by a dot, or in decimal notation, where each 8-bit binary number is translated to decimal, as it can be seen in Table 7.2.1.

IP address	10101100000100001111111000000001
Dot-binary notation	10101100.00010000.1111110.00000001
Dot-decimal notation	172.16.254.1

Table 7.2.1: IP address notation in dot-decimal and dot-binary.

Packets in the IPv4 consist of a header section and a data section. There is no footer at the end of the data section since the protocols in the data link layer and the transport layer provide error correction controls. Headers in a IPv4 packet contain 14 fields, one of them being optional. The fields are packed with the most significant byte first, and the most significant bit is also the first. Headers have a length between 20 and 60 bytes. The data section comes after the header, and its format depends on the protocol used (for example, ICMP, IGMP, TCP, etc.). Figure 7.2.4 shows the structure of a IPv4 header.

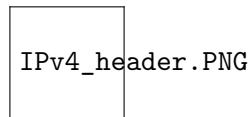


Figure 7.2.4: Example of a header for an IPv4 packet. In this case, it has a length of 36 bytes.

IPv4 provides fragmentation of packets. If size of the packet is bigger than the maximum transmission unit (MTU) of the destination, and the message allows fragmentation (the option of Do not Fragment in the header of the packet is set to 0) the transmitting router will divide the packet in fragments smaller than the MTU.

Internet Protocol version 6 (IPv6) [19]

The Internet Protocol version 6 (IPv6) is the most recent version of the Internet Protocol, developed to solve the problem of the exhaustion of IP addresses of the IPv4. IPv6 is intended to replace IPv4. The new features of the IPv6 compared to those of the IPv4 are the following:

- Larger address space: The length of IPv6 addresses is 128 bits, which is four times the length of IPv4 addresses. It offers a capacity of 2^{128} addresses.
- Multicasting: IPv6 accomplishes multicasting without using other protocols (such as IGMP for IPv4)
- Stateless address autoconfiguration (SLAAC): IPv6 hosts can configure themselves automatically when they are connected to a IPv6 network using the Neighbor Discovery Protocol via Internet Control Message Protocol version 6 (ICMPv6) router discovery messages. When a host connects for the first time, it sends a link-local router solicitation multicast request for its configuration parameters. Then, routers respond to the request with a router advertisement packet that contains Internet Layer configuration parameters.
- Network-layer security: Internet Protocol Security was developed for IPv6 before it was adapted for IPv4.
- Simplified processing by routers: Packet headers and the process of packet forwarding have been simplified, so packet processing by routers is more efficient. Headers now have a fixed length of 40 bytes, and may have an optional section aimed for options between the header section and the data section. Figure 7.2.5 shows the structure of an IPv6 header. IPv6 routers do not perform fragmentation.
- Mobility: Mobile IPv6 avoids triangular routing (unlike IPv4) and is as efficient as native IPv6.
- Options extensibility: IPv6 headers have a structure capable of extending the protocol in the future without affecting the core packet structure.
- Jumbograms: IPv4 limits packets to $(2^{16}) - 1$ octets per payload. A IPv6 node can handle packets of $(2^{32}) - 1$ octets (called jumbograms).

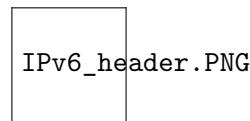


Figure 7.2.5: Example of a header for an IPv6 packet.

Auxiliary protocols

Encapsulation service [15]

The Encapsulation Service is a service used to transfer data units that can not be directly transferred by the CCSDS Space Data Link Protocols. In order to be directly transferred by a Space Data Link Protocol, a data unit must have a Packet Version Number authorized by the CCSDS (a list of PVN authorized by CCSDS is contained in [20]). With the Encapsulation Service, data units that do not have an authorized VPN can be transmitted with Space Data Link Protocols. The data unit to be transmitted must be of an integral number of octets.

A user of the Encapsulation Service is identified by the combination of the following:

- A Packet Version Number (PVN) that indicates whether Space Packets (PVN=1) or Encapsulation Packets (PVN=8) are used for encapsulation,
- An Encapsulated Protocol Identifier (EPI), which is either:
 - An Application Process Identifier (APID) defined in reference (if Space Packets are used).
 - a Protocol ID defined in section 4 of this document (if Encapsulation Packets are used).

The APIDs used by the Encapsulation Service must be registered as ‘reserved APIDs’ in [21]. The Protocol IDs used by the Encapsulation Service must be registered as ‘defined Protocol IDs’ in [22].

If the Data Unit is encapsulated in a Space Packet, the header format of the Space Packet is the same as the one used by Space Packet Protocol, only that the values of the parameters are restricted to some values. On the other hand, if the Data Unit is encapsulated in an Encapsulation Packet, a different header format will be used. This header has a length of 1-8 octets, and for the case of 8 octet it can be shown in Figure 7.2.6

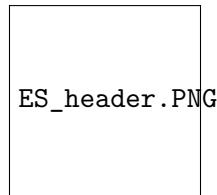


Figure 7.2.6: Example of a header for an Encapsulation Packet of maximum length. Some parameters may vary its length in other cases.

IP over CCSDS (IPoC) [17]

The IP over CCSDS is used to transfer IP Data Units over CCSDS Space Data Link Protocols. IP Data Units are encapsulated in Encapsulation Packets and sent through Space Data Link Protocols. IPoC uses the CCSDS Internet Protocol Extension (IPE) convention in conjunction with the CCSDS Encapsulation Service. The IPE convention is used to add IPE octets at the beginning of a IP Data Unit, encapsulate the result in an Encapsulation Packet, and transmit it with a CCSDS Space Data Link Protocol. It is used because not all protocols that use an IP datagram have a Protocol ID used by the Encapsulation Packet.

IPoC adds a header at the beginning of the IP Data Unit, called IPE header. The sum of the IP Data Unit and the IPE header is the Data Unit used by the Encapsulation Service. In other words, for the Encapsulation Service, the IPE header and the IP Data Unit are a whole.

The structure of the IPE header will be the following. It must be of a length of an integral number of octets, with a minimum length of 1 octet. Each octet will be divided into two parts: the first seven bits (bits 0-6), and the least significant bit (LSB, bit 7). If more octets are added, the LSB of all octets except the last octet are set to '0'. The value of the IPE header is the decimal value of all the octets. The value of the IPE header must be one of the possible values in [23].

Internet Control Message Protocol (ICMP) [24]

The Internet Control Message Protocol (ICMP) is one of the main protocols of the TCP/IP protocol suite. It is used to send error messages to the source IP of the data packet. It is assigned IP protocol number 1. ICMP messages are typically used for diagnostic, control purposes or generated in response to errors in IP operations. They are processed differently than normal IP processing.

There are many types of control messages that the ICMP can send:

- Source quench: Used to request the sender to decrease the rate of messages sent to a router.
- Redirect: Used to request the sender to send the data to another router.
- Time exceeded: Used by a gateway to inform the sender of a discarded datagram due to the time to live field reaching zero. It is also used to inform the sender that a fragment of a message has not been reassembled within the time limit
- Timestamp: Used for time synchronization. The sender sends the timestamp it last touched the packet (in milliseconds since midnight)
- Timestamp reply: Used to reply a timestamp. The receiver of the timestamp message replies the sender with the original timestamp, the timestamp when the message was received, and the timestamp when the reply was sent.
- Address mask request: Used by a host to obtain the subnet mask of a router
- Address mask reply: Used to reply the address mass request returning the subnet mask.
- Destination unreachable: Used by the host or its inbound gateway to inform the client that the destination is unreachable.

Internet Control Message Protocol version 6 (ICMPv6) [25]

The Internet Control Message Protocol version 6 (ICMPv6) is the implementation of the ICMP for IPv6. Several extensions have been published that define new types of ICMPv6 messages, as well as new options for existing message types. One of those is the Neighbor Discovery Protocol (NDP), a node discovery protocol for IPv6 that replaces and enhances the features of the Address Resolution Protocol (ARP). Secure Neighbor Discovery (SEND) is, respectively, an extension of NDP with extra security. Multicast Router Discovery (MRD) allows discovery of multicast routers.

Internet Group Management Protocol (IGMP) [26]

The Internet Group Management Protocol (IGMP) is used by hosts and adjacent routers on IPv4 networks to establish multicast group memberships. It is a part of IP multicast, and it is used in one-to-many networking applications such as online streaming video. IGMP operates between the client computer and a local multicast router. IGMP messages are carried in bare IP packets with protocol number 2.

Internet Protocol Security (IPsec) [27]

The Internet Protocol Security (IPsec) is a protocol suite for secure Internet Protocol (IP) communications. It authenticates and encrypts each IP packet of a communication session. IPsec includes protocols for establishing mutual authentication between agents at the beginning of the session and negotiation of cryptographic keys to be used during the session. IPsec can be used in protecting data flows between a pair of hosts (host-to-host), between a pair of security gateways (network-to-network), or between a security gateway and a host (network-to-host). It supports network-level peer authentication, data origin authentication, data integrity, data confidentiality (encryption), and replay protection.

IPsec uses the following protocols to perform various functions;

- Authentication Headers (AH): Provides connectionless data integrity and data origin authentication for IP datagrams, and provides protection against replay attacks.
- Encapsulating Security Payloads (ESP): Provide confidentiality, data-origin authentication, connectionless integrity, an anti-replay service, and limited traffic-flow confidentiality.
- Security Associations (SA): Provides the bundle of algorithms and data that provide the parameters necessary for AH and ESP operations.

Protocol Independent Multicast (PIM) [28] [29]

The Protocol Independent Multicast (PIM) is a family of multicast routing protocols for Internet Protocol (IP) networks that provide one-to-many and many-to-many distribution of data. PIM does not include its own topology discovery mechanism, but instead uses routing information supplied by other routing protocols.

There are four variants of PIM:

- PIM Sparse Mode (PIM-SM): It builds unidirectional shared trees rooted at a rendezvous point (RP) per group, and optionally creates shortest-path trees per source. It is called sparse-mode because it is suitable for groups where low percentage of the nodes will subscribe to the multicast session.
- PIM Dense Mode (PIM-DM): It uses dense multicast routing. It builds shortest-path trees by flooding multicast traffic domain wide, and then pruning back branches of

the tree where no receivers are present. Dense mode is ideal for groups where many of the nodes will subscribe to receive the multicast packets.

- Bidirectional PIM: It builds shared bi-directional trees. It never builds a shortest path tree, so may have longer end-to-end delays than PIM-SM.
- PIM Source-Specific Multicast (PIM-SSM): It builds trees that are rooted in just one source, offering a more secure model for a limited amount of applications (mostly broadcasting of content). In SSM, an IP datagram is transmitted by a source S to an SSM destination address G, and receivers can receive this datagram by subscribing to channel (S,G).

Routing protocols

Enhanced Interior Gateway Routing Protocol (EIGRP) [30]

The Enhanced Interior Gateway Routing Protocol (EIGRP) is a routing protocol used on a computer networks for automating routing decisions and configuration. This protocol was designed by Cisco Systems and it was only available for Cisco routers. In 2003, partial functionality of EIGRP was converted to an open standard and in 2016 was published with informational status. EIGRP is used on a router to share routes with other routers in the same autonomous system.

All routers contain a routing table that lists the routes to network destinations. If a router cannot find a valid path to the destination, the traffic is discarded. EIGRP is a dynamic routing protocol, which means that routers automatically exchange information about routes and, therefore, the administrator does not have to change the routing table manually. Besides the routing table, routers additionally have two more tables.

- Neighbour table. It stores the IP address of the routers that have a direct connection with this router. If a router is connected to another with an intermediate router, it will not be recorded in this table.
- Topology table. It keeps record of routes that has learned from neighbouring router tables, and also records the distance (number of intermediate routers) of each route, the feasible successor and the successors (other routes that have the same destination and are loop free). Routes in this table are either labelled as "passive" or "active". Passive means that EIGRP has determined the path for the specific route and has finished processing. Active means that EIGRP is still trying to calculate the best path for the specific route. The router does not use the routes in this table. A

route in this table will be inserted in the routing talbe when is marked as passive, is not a feasible successor and does not have a higher distance than an equivalent path

If there is a change in the network (a link fails, or a router is disconnected), the path becomes unavailable, and is removed from the routing table. The routing table of a router will be updated, and only the changes since the previous update will be transmitted to the neighbouring routers. The information about the changes in the routing table is not transmitted periodically, but only when a change actually occurs.

EIGRP supports the following features:

- Support for Classless Inter-Domain Routing (CIDR) and variable length subnet masking. Routes are not summarized at the classful network boundary unless auto summary is enabled.
- Support for load balancing on parallel links between sites.
- The ability to use different authentication passwords at different times.
- MD5 authentication between two routers.
- Sends topology changes, rather than sending the entire routing table when a route is changed.
- Periodically checks if a route is available and propagates routing changes to neighboring routers if any changes have occurred.
- Runs separate routing processes for Internet Protocol (IP), IPv6, IPX and AppleTalk through the use of protocol-dependent modules (PDMs).

EIGRP does not operate using the Transmission Control Protocol (TCP) or the User Datagram Protocol (UDP). This means that EIGRP does not use a port number to identify traffic. Rather, EIGRP is designed to work on top of layer 3. Since EIGRP does not use TCP for communication, it implements Cisco's Reliable Transport Protocol (RTP) to ensure that EIGRP router updates are delivered to all neighbors completely.

Open Shortest Path First (OSPF) [31] [32]

The Open Shortest Path First (OSPF) is a routing protocol for Internet Protocol (IP) networks that operates in a single autonomous system. OSPF version 2 is designed

for IPv4, while OSPF version 3 is designed for IPv6. It works by gathering link state information from available routers and constructing a topology map of the network. The topology is presented as a routing table to the Internet layer which routes packets based solely on their destination IP address. OSPF detects changes in the topology, such as link failures, and creates a new loop-free routing structure. It computes the shortest-path tree for each route using a method based on Dijkstra's algorithm. OSPF does not use a transport protocol, such as UDP or TCP, but encapsulates its data directly in IP packets with protocol number 89. It implements its own transport layer error detection and correction functions. OSPF uses multicast addressing for distributing route information within a broadcast domain.

OSPF supports complex networks with multiple routers, including backup routers, to balance traffic load on multiple links to other subnets. Routers form adjacencies when they have detected each other. This detection is initiated when a router identifies itself in a Hello protocol packet. Upon acknowledgment, this establishes a two-way state and the most basic relationship. The routers in an Ethernet or Frame Relay network select a Designated Router (DR) and a Backup Designated Router (BDR) which act as a hub to reduce traffic between routers. OSPF establishes and maintains neighbor relationships for exchanging routing updates with other routers. The neighbor relationship table is called an adjacency database. Two OSPF routers are neighbors if they are members of the same subnet and share the same area ID, subnet mask, timers and authentication. OSPF adjacencies are formed between selected neighbors and allow them to exchange routing information. Two routers become adjacent if at least one of them is Designated Router or Backup Designated Router (on multiaccess type networks), or they are interconnected by a point-to-point or point-to-multipoint network type.

OSPF does not carry data via a transport protocol. Instead, OSPF forms IP datagrams directly, packaging them using protocol number 89 for the IP Protocol field. OSPF defines five different message types, for various types of communication:

- Hello: It is used to allow a router to discover other adjacent routers on its local links and networks. The messages establish adjacencies between neighboring devices. During normal operation, routers send hello messages to their neighbors at regular intervals. If a router stops receiving hello messages from a neighbor, after a set period the router will assume the neighbor has gone down.
- Database Description: It contains descriptions of the topology of the autonomous system or area. They convey the contents of the link-state database (LSDB) for the area from one router to another. Communicating a large LSDB may require several messages to be sent.

- Link State Request: These messages are used by one router to request updated information about a portion of the LSDB from another router. The message specifies exactly which link about which the requesting device wants more current information.
- Link State Update: These messages contain updated information about the state of certain links on the LSDB. They are sent in response to a Link State Request message, and also broadcast or multicast by routers on a regular basis. Their contents are used to update the information in the LSDBs of routers that receive them.
- Link State Acknowledgment: These messages provide reliability to the link-state exchange process, by explicitly acknowledging receipt of a Link State Update message.

Routing Information Protocol (RIP) [33] [34]

The Routing Information Protocol (RIP) is a routing protocol. It uses a hop count to establish the distance between two routers and, in order to prevent loops, establishes 15 as the limit number of hops in a route. If the number of hops is 16, the distance between the two routers is considered infinite. Each router has a routing table with all the routes to each possible destination, and the number of hops to get there. There are 3 versions of RIP: RIPv1, which is the original, RIPv2, which is an updated version of RIPv2, and RIPvng, which is the new generation of RIP compatible with IPv6.

The operating principle of the RIP is the following: When a RIP router comes online, it sends a broadcast message to all of its RIP enabled interfaces. All the neighbouring routers that receive the Request message respond back with the Response Message containing their Routing table. The Response Message is also gratuitously sent when the Update timer expires (by default, 30 seconds). On receiving the Routing table, the router processes each entry of the routing table as per the following rules:

- If there are no route entries matching the one received then the route entry is added to the routing table automatically, along with the information about the router from which it received the routing table.
- If there are matching entries but the hop count metric is lower than the one already in its routing table, then the routing table is updated with the new route.
- If there are matching entries but the hop count metric is higher than the one already in its routing table, then the routing entry is updated with hop count of 16 (infinite hop). The packets are still forwarded to the old route. A Hold-down timer is started

and all the updates for that route from other routers are ignored. If after the Hold-down timer (per default 180 seconds) expires and still the router is advertising with the same higher hop count then the value is updated into its routing table. Only after the timer expires, the updates from other routers are accepted for that route.

If the Invalid timer (per default 180 seconds) expires and a routing entry has not been updated, the hop counter of that route will be set to 16, marking the route as invalid. Then, if the Flush timer (per default 240 seconds) expires, the invalid route entry will be removed

Protocol Selection

Choice of the main protocol

The choice of the main protocol will be between SPP, IPv4 and IPv6. To make the choice, it is important to take into account that the Astrea constellation is a network that can be of more than two hundred satellites, which will communicate point-to-point. Each node can be the source, the destination or an intermediate node of a communication route.

SPP has the advantage of being designed to work easily with the protocols of the adjacent layers, while IP needs IP over CCSDS and Encapsulation Service. However, SPP requires a parameter called Path ID, which is the identifier of a Logical Data Path. Since each satellite of Astrea constellation can be the source or the destination of a data path, this means that for a network of 200 nodes, there are $200 \times 199 = 39800$ possible routes. The parameter to indicate the Path ID has a length of 11 bits, which can identify 2048 different routes, which is not enough. Another issue to take into account is that since the ground station nodes of the constellation are moving respect the satellite nodes, their relative position changes and, therefore, paths also change. If the path associated to a Path ID changes during a transmission, or if it is not updated for all nodes at the time of the transmission, errors can occur. This does not happen with IP, since instead of Path ID it uses the IP address of the source and destination node. For this reason, SPP is discarded.

The main differences between IPv4 and IPv6 are the header of the datagram and the IP addresses of the nodes. Since our network is private and it is not intended to be connected to the Internet, nodes can have an arbitrary IP address assigned. For this reason, IPv4 addresses are better, since they are shorter than IPv6 addresses. The size of the header would also be smaller in IPv4 than IPv6. However, for long datagrams, the extra length of IPv6

headers is irrelevant. Another difference is that IPv6 datagrams require less processing power, however, since the processing power is very small compared to the power required by the antennas this factor also has little importance in terms of power. However, it is important in terms of time, since less processing means less time to process. Other features of IPv6 that, in Astrea network, do not provide benefits are the multicast and mobility features, which the network will not have. Additionally, due to the changing nature of the constellation, jumbograms will not be used because a packet so long may be interrupted when the path changes.

The real benefits of IPv6 over IPv4 is that there are less additional protocols compared to IPv4 to perform the same features, since ICMPv6 provide the features of ICMP, ARP and IGMP, and some features of IPv6 itself and its additional protocols have been eliminated since they were already performed by other layer protocols and were redundant. All of this helps to reduce the time required to process the data and this, in long paths, is a significant factor.

If reliable adjacent layer protocols are provided, IPv6 is the best option, due to less processing in routers and more simple additional protocols. Additionally, IPv6 is progressively replacing IPv4 and, therefore, using IPv6 has no risk of being obsolete.

Choice of routing protocol

The choice of the routing protocol will be between EIGRP, OSPF and RIP.

EIGRP is a protocol compatible with either IPv4 and IPv6. Contrary to other protocols, it only sends topology changes instead of the whole routing table, allowing for less data transmitted. It also contains more information about routes than other routing protocols, and provides authentication processes.

RIP is a protocol that, compared to EIGRP and OSPF, has the drawback that its time to converge and its scalability are poor. Additionally, RIP uses the User Datagram Protocol (UDP) as its transport protocol. On the other, it is easier to configure than other protocols.

OSPF is a protocol also compatible with IPv4 and IPv6. Unlike EIGRP, each router exchanges its adjacency links with adjacent routers and then, each router creates its

own map of the network and, using this map, each router creates its own routing table. However, it has mechanisms to ensure that there are not loops in the network.

Taking into account that nodes in the Astrea network have an order of magnitude of 200 and are continuously changing the data paths. Also, since Astrea is a network where a node can be the beginning or the end of a communication, this means that for a given node there has to be a route to every other node in the network, and for a network of 200 nodes, there are 199 possible routes for the 200 nodes, which is a total of 39800 different entries in the routing table only for the satellite nodes. Since RIP has longer time to converge compared to other protocols, and due to the huge size of the routing table, RIP is discarded.

EIGRP does not have this problem because it does not transmit the whole routing table, but only the changes. Although the network is continuously moving, the paths between the satellite nodes remain the same. The problem happens with the ground nodes, which are continuously changing its position respect the satellite nodes due to Earth's rotation. And since each satellite node can communicate with every ground station, the number of entries in the routing table that will be updated for a network of 200 satellite nodes and 5 ground stations is 200x5, which is 1000 entries that will be updated frequently. Since OSPF does not transmit the routing table but only the adjacencies, only 205 entries will be transmitted. This reduces the time to share the updated information to the whole network. For this reason, OSPF is chosen.

Choice of complementary protocols

The choice of which protocols include will depend on the main protocol of the network layer and the degree of services featured by the communication process.

Since IPv6 has been chosen, IP over CCSDS and Encapsulation Service are necessary. Additionally, ICMPv6 greatly expand the features of IPv6 such as flow control. Security features are already provided in the Data Link layer and, therefore, IPsec is not necessary. Also, no multicast features are required, so no multicast protocols will not be used.

Conclusion

It has been decided that IPv6 will be the network layer protocol, complemented with IPoC, Encapsulation Service and ICMPv6, and with OSPF as the routing protocol.

Final structure

As the protocols have already been chosen, it is time to establish how will be the headers of the different protocols.

The IPv6 header will depend greatly on the protocol of the upper layers, or the auxiliar protocol (OSPF, ICMPv6). The main parameters of the IPv6 header, that can be seen in Figure 7.2.5, are the following:

- **Version** Current version of IP, which for IPv6 is 6 (bit sequence 0110).
- **Traffic Class**. The bits of this field hold two values. The 6 most-significant bits are used for differentiated services, which is used to classify packets. The remaining two bits are used for ECN; priority values subdivide into ranges: traffic where the source provides congestion control and non-congestion control traffic.
- **Flow Label**. The flow label when set to a non-zero value now serves as a hint to routers and switches with multiple outbound paths that these packets should stay on the same path so that they will not be reordered.
- **Payload Length**. The size of the payload in octets, including any extension headers. The length is set to zero when a Hop-by-Hop extension header carries a Jumbo Payload option.
- **Next Header**. Specifies the type of the next header. This field usually specifies the transport layer protocol used by a packet's payload. When extension headers are present in the packet this field indicates which extension header follows. The values are shared with those used for the IPv4 protocol field, as both fields have the same function (see List of IP protocol numbers in [35]).
- **Hop Limit**. This value is decremented by one at each intermediate node visited by the packet. When the counter reaches 0 the packet is discarded.
- **Source Address**. The IPv6 address of the sending node.
- **Destination Address**. The IPv6 address of the destination node.

It has been stated that, since Astrea network is a private network that will not be connected to the Internet, IP addresses will be arbitrary assigned to the nodes of the network.

For the IPoC header, the value for IPv6 datagrams is 87, so the header of OPoC will be 01010111

For the Encapsulation Service, depending of the length of the data unit transmitted, the header will vary. For data units up to 65531 octets, the Encapsulation Service header will be the following: 11101010-00000000-XXXXXXX-XXXXXXX, where XXXXXXXX-XXXXXXX is the binary number of the total length of the Encapsulation Packet, including the Encapsulation Packet header.

Layer 4: Transport and Session

This layer is the one in charge of the free-of-error transference of data from one process to another. Therefore, its goal is to provide and guarantee a reliable and cheap flow of the data.

Whereas the network layer oversees source-to-destination delivery of individual packets, it does not recognize any relationship between those packets. It treats each one independently, as though each piece belonged to a separate message, whether or not it does. The transport layer, on the other hand, ensures that the whole message arrives intact and in order, overseeing both error control and flow control source-to-destination level.

A transport layer can be either connectionless or connection-oriented. A connectionless transport layer treats each segment as an independent packet and delivers it to the transport layer at the destination machine. A connection-oriented transport layer makes a connection with the transport layer at the destination machine first before delivering the packets. After all the data is transferred, the connection is terminated.

In the transport layer, a message is normally divided into transmittable segments. A connectionless protocol, such as UDP, treats each segment separately. A connection-oriented protocol, such as TCP and SCTP, creates a relationship between the segments using sequence numbers.

The transport layer is responsible for process-to-process delivery, i.e., the delivery of a packet, part of a message, from one process to another. Two processes communicate in a client/server relationship.

Regarding addressing, at the transport layer, it is necessary a transport layer address,

called a port number, to choose among multiple processes running on the destination host. The destination port number is needed for delivery, whereas the source port number is needed for the reply.

The addressing mechanism allows multiplexing and demultiplexing by the transport layer.

User Datagram Protocol (UDP)

The User Datagram Protocol (UDP) is a connectionless, unreliable transport protocol. The only new feature regarding IP is that it provides process-to-process communication instead of host-to-host communication, and performs a very limited error checking. It might seem a powerless protocol, but its main point is that is a very simple protocol using a minimum of overhead. Therefore, if a process wants to send a small message and no extremely reliability is required, UDP is a good choice.

Nevertheless, regarding the aim of this project, it is unacceptable to use UDP, since reliability is a key factor and must be taken into account.

Stream Control Transmission Protocol (SCTP)

The Stream Control Transmission Protocol is a new reliable, message-oriented transport layer protocol. Nevertheless, it has been designed and implemented mostly for Internet applications, such as IUA or SIP. But precisely it does not fit the goal of this project.

Therefore, as there is a better choice (which will be deeply and widely explained in the following section), this protocol will not be considered.

Transmission Control Protocol (TCP)

The Transmission Control Protocol is again a process-to-process protocol. Consequently it uses port numbers. The main difference with the UDP is that TCP is a connection-oriented protocol, which means that creates a virtual connection between two TCP's in order to send data. Moreover, TCP uses flow and error control mechanisms. It is then a more reliable protocol than UDP. It adds connection-oriented and reliability features to the services of IP.

This will be the protocol chosen for this project, so it will be explained in detail in this section.

TCP Services

Process-to-process communication: Like UDP, TCP provides this type of communication, using port numbers. In the following image there are the main well-known port numbers used by TCP.

<i>Port</i>	<i>Protocol</i>	<i>Description</i>
7	Echo	Echoes a received datagram back to the sender
9	Discard	Discards any datagram that is received
11	Users	Active users
13	Daytime	Returns the date and the time
17	Quote	Returns a quote of the day
19	Chargen	Returns a string of characters
20	FIP, Data	File Transfer Protocol (data connection)
21	FIP, Control	File Transfer Protocol (control connection)
23	TELNET	Tenninal Network
25	SMTP	Simple Mail Transfer Protocol
53	DNS	Domain Name Server
67	BOOTP	Bootstrap Protocol
79	Finger	Finger
80	HTTP	Hypertext Transfer Protocol
111	RPC	Remote Procedure Call

Stream Delivery Service: as has been mentioned before, TCP, unlike UDP, is a stream-oriented protocol. UDP does not recognize any relationship between the datagrams. TCP, in contrast, allows the sending process to deliver data as a stream of bytes and allows the receiving process to obtain data as a stream of bytes. A way of explaining this would be an environment in which the two processes seems to be linked by an imaginary "tube" that carries the data across the Internet. The sending process produces the stream of bytes and the receiving process consumes them. This is, the first writes and the last reads.

Sending and Receiving Buffers: Since the sending and receiving processes might not write or read data at the same speed, there is a need for storage in TCP. Therefore, TCP includes two buffers, the sending buffer and the receiving buffer. A deeper look into those buffers can be performed by looking at the bibliography.

Full-Duplex Communication: TCP allows full-duplex service, so that data can flow in both directions at the same time. Each TCP has a sending and receiving buffer, and segments move in both directions. This feature is very important for the goal of this project.

Segments: Although buffering solves the problem of different speeds of producing and consuming, there is still one important feature to be discussed. The data needs to be sent in packets, not as an endless stream of bytes. Therefore, TCP groups a number of bytes together into a packet called a segment. A header is added to each segment for control purposes.

TCP features

In order to provide the services that have been explained, TCP has some features that will be briefly discussed.

Numbering Systems

TCP keeps track of the segments being transmitted or received, using the header previously discussed. There are in addition two fields, the sequence number and the acknowledgement number, which refer to the byte number, not the segment number.

TCP numbers all data bytes that are transmitted in a connection. Numbering is independent in each direction. When TCP receives bytes of data from a process, it stores them in the sending buffer and numbers them. Typically, it generates randomly a number between 0 and $2^{32} - 1$ for the number of the first byte. For example, if the random number happens to be 1427 and the total data to be sent are 5000 bytes, the bytes are numbered from 1427 to 6426. This system is used for flow and error control.

After the bytes have been numbered, TCP assigns a sequence number to each segment that is being sent. The sequence number for each segment is the number of the first byte carried in that segment. This is, the value in the sequence number field of a segment defines the number of the first data byte contained in that segment.

The value of the acknowledgement field in a segment defines the number of the next byte a party expects to receive. It is a cumulative number.

Flow Control

TCP provides flow control, which means that the receiver can control the amount of data that is to be sent by the sender. The purpose of this is to avoid over-whelmed receivers.

Error Control

In order to provide a reliable service, TCP implements an error control mechanism. It considers a segment as the unit of data for error detecting, even though there is also a byte-oriented control mechanism.

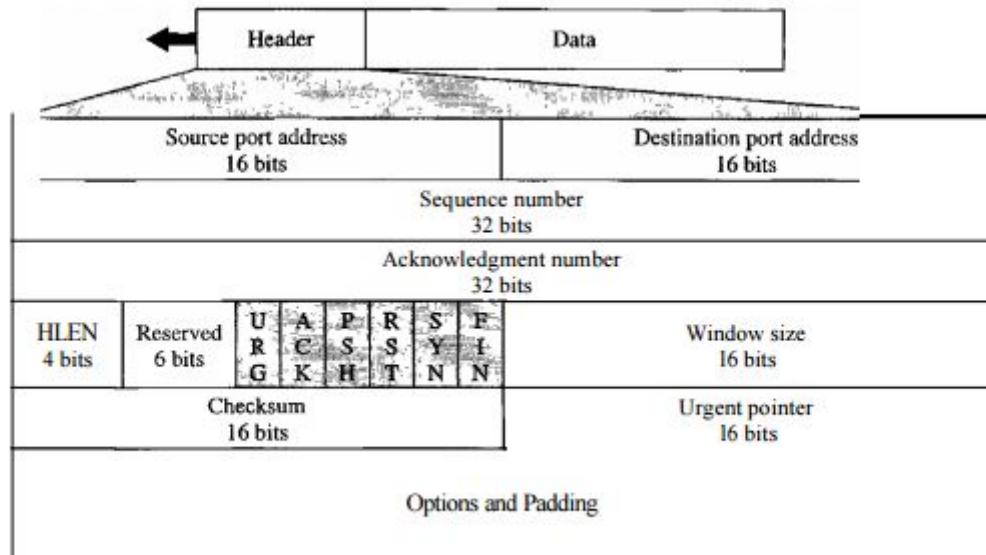
Congestion Control

TCP also takes into account congestion in the network, by the detennining of the flow depending on the level of congestion in the network.

Segment

As has been explained before, a packet in TCP is called a segment. The aim of this point is to explain in detail what a segment is and how its structure is.

The typical format of the segment is shown in the next figure.



The segment consists of a 20 to 60-byte header, followed by data from the application

program. The byte is 20-byte long if there are no options, and up to 60-bytes if there are options.

The main parts of the format are to be discussed in the following lines.

Source Port Adress

This is a 16-bit field that states the port number of the application program in the host that is sending the segment.

Destination Port Adress

It is also a 16-bit that defines the port number of the application program in the host that is receiving the segment.

Sequence Number

This 32-bit field defines the number assigned to the first byte of the data contained in the segment considered. This numeration has been previously explained.

Acknowledgement Number

This is a 32-bit field that defines the byte number that the receiver of the segment is expecting to receive from the other party. If the receiver of the segment has successfully received byte number x , it defines $x + 1$ as the acknowledgement number.

Header Length

A 4-bit field that indicates the number of 4-byte words in the TCP header. As seen, the length of the header can be between 20 and 60 bytes. Then, the value of this field can be between 5 and 15 (since $5 \times 4 = 20$, and $15 \times 4 = 60$).

Reserved

This is a 6-bit field reserved for future usage.

Control

This field defines 6 different control bits or flags. One or more of those bits can be set at a time.

Window Size

This field defines the size of the window, in bytes, that the other party must maintain. Since the length of this field is 16 bits, the maximum size of the windows is $2^{16} = 65535$ bytes.

Urgent Pointer

Another 16-bit field, which is only valid if the urgent flag is set, which means that the segment contains urgent data. It actually defines the number that must be added to the sequence number to obtain the number of the last urgent byte in the data section of the segment.

Options

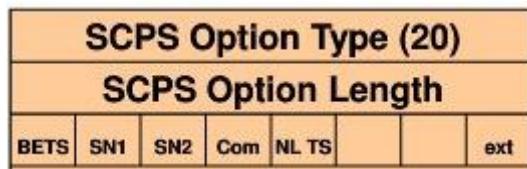
As has been explained, there can be up to 40 bytes of optional information in the TCP Header. This is the purpose of this last field.

Adaptation to space needs

TCP was established for wired connections initially. Therefore, in order to be eligible for the purpose of this project, it is highly recommended that some slight modifications are done. The Space Communications Protocols Specification (SCPS) defines a set of revisions to the protocols to enable them to operate properly. This is, SCPC-TCP becomes an "upgraded" TCP, specially designed for space application.

With SCPS, TCP the bandwidth of an existing link will be utilized to a significantly higher percentage and more efficiently. It also supports end-to-end communications between applications and is designed to meet the needs of a broad range of space missions.

This is all achieved because of an extension that is added to the header shown before. This extension header is shown next. Each line is a octet of bits; i.e., 8 bits:



Choice of protocol for the transport layer

Three protocols have been discussed, the UDP, the SCTP and the TCP. The first one has some disadvantages which make it not suitable for the purpose of the project, such as the fact that no reliability is guaranteed, for example, amongst others. The second one is designed mostly for Internet applications, which does not fit the goals of this project. Therefore, the only candidate suitable for the project is the TCP, Transmission Control Protocol, which has already been widely explained and analyzed. As it has the required features that the project demands, it is the chosen protocol for this layer. Also, as it has been established, it is very recommended to use the extension SCPS, due to adaptation to space needs.

Global Overview

For the sake of clarification, all the elected options are going to be put together obtaining the desired fully designed **protocol stack**.

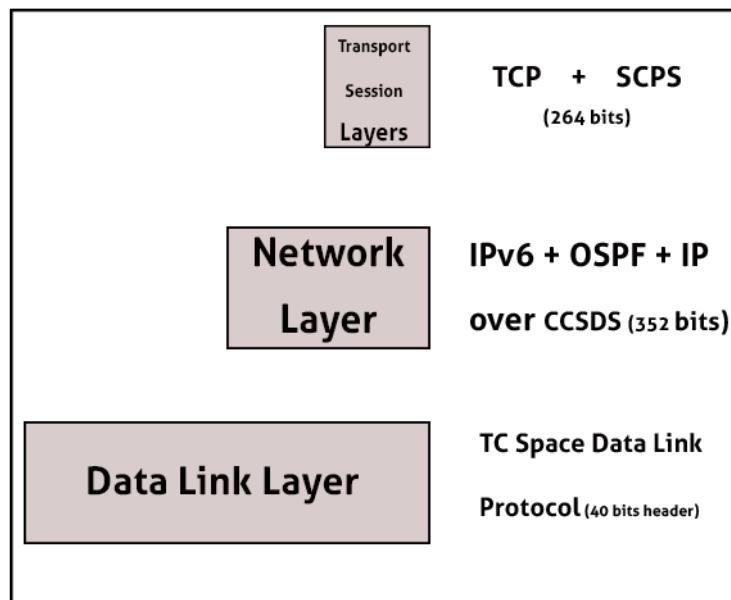


Figure 7.4.1: Overall space communication protocol stack

In total, the overhead is **656 bits**, whith conservative calculations. Hence, the quantity is negligible in comparison to the data rate.

Chapter 8

Ground Segment

Introduction

In the previous chapter the space protocols have been selected, so in this one the focus will be on the ground segment protocols. The information will be transmitted to the client using the Internet, so a part of the protocol is already established by the system. However, a secure protocol has to be defined above the Internet protocol to assure confidentiality to the client. The protocol used in the Internet is the TCP/IP protocol suite, that provides an end-to-end data communication specifying how data should be packeted, addressed, transmitted, routed and received. The layer of this protocol that can be adjusted to our needs is the application layer. The application layer is an abstraction layer that specifies the shared protocols and interface methods used by hosts in a communications network. In TCP/IP, the application layer contains the communications protocols and interface methods used in process-to-process communications across an Internet Protocol (IP) computer network. The application layer only standardizes communication and depends upon the underlying transport layer protocols to establish host-to-host data transfer channels and manage the data exchange in a client-server or peer-to-peer networking model. That means that the application layer is very important in Astrea project because it will define how the information is received by the client.

In the following lines the different available protocols for the application layer depending on the presentation of data are explained.

Ground Segment protocols

File Transfer Protocol (FTP)

The File Transfer Protocol (FTP) is a standard network protocol used to transfer computer files between a client and server on a computer network.

FTP is built on a client-server model architecture and uses separate control and data connections between the client and the server. FTP users may authenticate themselves with a clear-text sign-in protocol, normally in the form of a username and password, but can connect anonymously if the server is configured to allow it. For secure transmission that protects the username and password, and encrypts the content, FTP is often secured with SSL/TLS (FTPS). SSH File Transfer Protocol (SFTP) is sometimes also used instead, but is technologically different.

Setting up an FTP control connection is quite slow due to the round-trip delays of sending all of the required commands and awaiting responses, so it is customary to bring up a control connection and hold it open for multiple file transfers rather than drop and re-establish the session afresh each time.

See more about FTP in [?]

Secure Shell (SSH)

Secure Shell (SSH) is a cryptographic network protocol for operating network services securely over an unsecured network. The best known example application is for remote login to computer systems by users.

SSH provides a secure channel over an unsecured network in a client-server architecture, connecting an SSH client application with an SSH server. Common applications include remote command-line login and remote command execution, but any network service can be secured with SSH.

See more about SSH in [?]

Simple Mail Transfer Protocol (SMTP)

Simple Mail Transfer Protocol (SMTP) is an Internet standard for electronic mail (email) transmission. Email is submitted by a mail client (mail user agent, MUA) to a mail server (mail submission agent, MSA). The MSA delivers the mail to its mail transfer agent (mail

transfer agent, MTA). Often, these two agents are instances of the same software launched with different options on the same machine. Local processing can be done either on a single machine, or split among multiple machines; mail agent processes on one machine can share files, but if processing is on multiple machines, they transfer messages between each other using SMTP, where each machine is configured to use the next machine as a smart host. Each process is an MTA (an SMTP server) in its own right.

SMTP is a connection-oriented, text-based protocol in which a mail sender communicates with a mail receiver by issuing command strings and supplying necessary data over a reliable ordered data stream channel. An SMTP session consists of commands originated by an SMTP client (the initiating agent, sender, or transmitter) and corresponding responses from the SMTP server (the listening agent, or receiver) so that the session is opened, and session parameters are exchanged.

See more about SCTP in [?]

Hypertext Transfer Protocol (HTTP)

The Hypertext Transfer Protocol (HTTP) is an application protocol for distributed, collaborative, hypermedia information systems. HTTP is the foundation of data communication for the World Wide Web.

HTTP functions as a request-response protocol in the client-server computing model. A web browser, for example, may be the client and an application running on a computer hosting a website may be the server. The client submits an HTTP request message to the server. The server, which provides resources such as HTML files and other content, or performs other functions on behalf of the client, returns a response message to the client. The response contains completion status information about the request and may also contain requested content in its message body.

Transport Layer Security (TLS)

Transport Layer Security (TLS) is a cryptographic protocol that provides communications security over a computer network. Several versions of the protocol find widespread use in applications such as web browsing, email, Internet faxing, instant messaging, and voice-over-IP (VoIP). Major websites use TLS to secure all communications between their servers and web browsers.

The Transport Layer Security protocol aims primarily to provide privacy and data integrity between two communicating computer applications. When secured by TLS, connections

Conclusions

between a client and a server have one or more of the following properties:

- The connection is private (or secure) because symmetric cryptography is used to encrypt the data transmitted. The keys for this symmetric encryption are generated uniquely for each connection and are based on a shared secret negotiated at the start of the session. The server and client negotiate the details of which encryption algorithm and cryptographic keys to use before the first byte of data is transmitted.
• The negotiation of a shared secret is both secure (the negotiated secret is unavailable to eavesdroppers and cannot be obtained, even by an attacker who places themselves in the middle of the connection) and reliable (no attacker can modify the communications during the negotiation without being detected).
- The identity of the communicating parties can be authenticated using public-key cryptography. This authentication can be made optional, but is generally required for at least one of the parties (typically the server).
- The connection ensures integrity because each message transmitted includes a message integrity check using a message authentication code to prevent undetected loss or alteration of the data during transmission.

Hypertext Transfer Protocol Secure (HTTPS)

HTTPS is a protocol for secure communication over a computer network which is widely used on the Internet. HTTPS consists of communication over Hypertext Transfer Protocol (HTTP) within a connection encrypted by Transport Layer Security. The main motivation for HTTPS is authentication of the visited website and protection of the privacy and integrity of the exchanged data.

See more about HTTP and HTTPS in [?]

Conclusions

At first, it has to be take in account that this layer provides the platform in which the client will make contact with the service. At this point, not only the technical criteria should be considered, but also how do the service is presented. It has to be found a friendly use method for the client keeping the technical efficiency.

Analazying the previous protocols, avoiding the techincal details of each one, there are considered tthis 3 ways of working, with its advantages and drawbacks:

Conclusions

- **Web.** This system would be based in HTTP and implemented with the corresponding security protocols in order to ensure the privacy of the data. In this case the client would enter with its computer a https address where he/she would sign in with an account. When the user is verified, the client could request to download information of his satellite.
 - Advantages:
 - * It would have a really friendly use for the customer.
 - * It could include friendly information for the user such as who we are, how to contact, FAQs, etc.
 - * It could be very automatized.
 - * The information could be protected with the adequate security protocols.
 - * The client would not need any special software.
 - Disadvantages:
 - * The web would be vulnerable to some type of attacks or problems that would compromise the data. This could avoid the communication between the user and the network.
 - * It would need several maintenance.
 - * There would be some type of data, like videos and photos, which the client would want to download as a file. So the web would have to be complemented with a file transfer protocol.
 - * The web would have to be designed.
- **Mail.** This method would be implemented over a SMTP with the corresponding security protocols. If the client wants to download data of his satellite, he/she would have to send a mail specifying the request. Then the client will receive an email with the information.
 - Advantages:
 - * It would be very secure and stable.
 - * The mail could not fail as a web does.
 - * The client would not need any special software.
 - * The information could be sent and received as a text or as a file.
 - Disadvantages:
 - * It could not be automatized, and this make it inefficient.
 - * It is not very friendly to use for a client.
 - * If there is some information missing in the request the client would have to wait for an answer and then complete the information.

Conclusions

- **Application.** The idea is that the client would operate in his computer with this software, and when he/she wants to upload or download something, the program would use a secure internet channel to transfer the information. This system would be implemented over a FTP or a SSH. For using this method it has to be implemented a platform for the client use.

- Advantages:

- * It would be really friendly use for the customer.
- * It would be really secure and stable.
- * It could include friendly information for the user as: who we are, how to contact, FAQs, etc.
- * The information could be sent and received as a text or a files.

- Disadvantages:

- * It would need to be downloaded and installed.
- * It would need some maintenance.
- * It would need to be designed.

Taking into account the advantages and disadvantages of each method it is concluded that an application is the method with the better security, efficiency and friendly-use relationship. The application will ensure a high security of the data, a robust access to it, and a friendly interface for the user.

This system could work with a FTP or with a SSH. Both would work properly in the system and have very similar characteristics, but SSH is more secure than FTP, so the system would be ruled by a SSH protocol.

Chapter 9

Design of the Ground Segment

Study of localization of Ground Stations

In the following lines, a study of the location of the Ground Stations will be carried in order to know the optimal location for them. As it has been stated in the report, the study has been done using a Matlab code that can be found in Annex VI.

Latitude analysis

Is easy to see that the effect of changing the latitude is practically independent for the longitude. For this reason, the links during the day for a given longitude are studied independently of the latitude and viceversa. Doing the analysis for latitudes between 0° and 90° during 2 days, with 5 minutes time-step, this are the results:

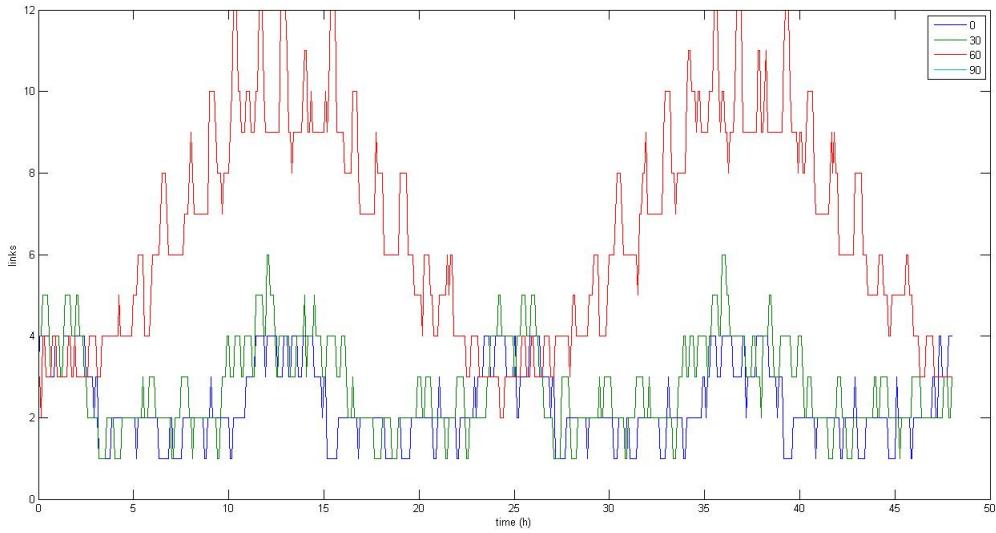
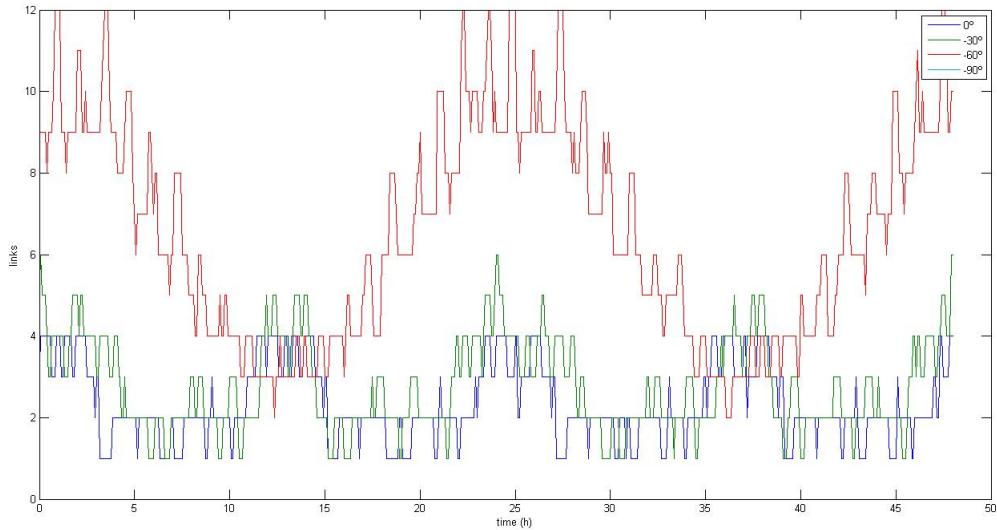


Figure 9.1.1: Links vs time for latitudes from 0° to 90°

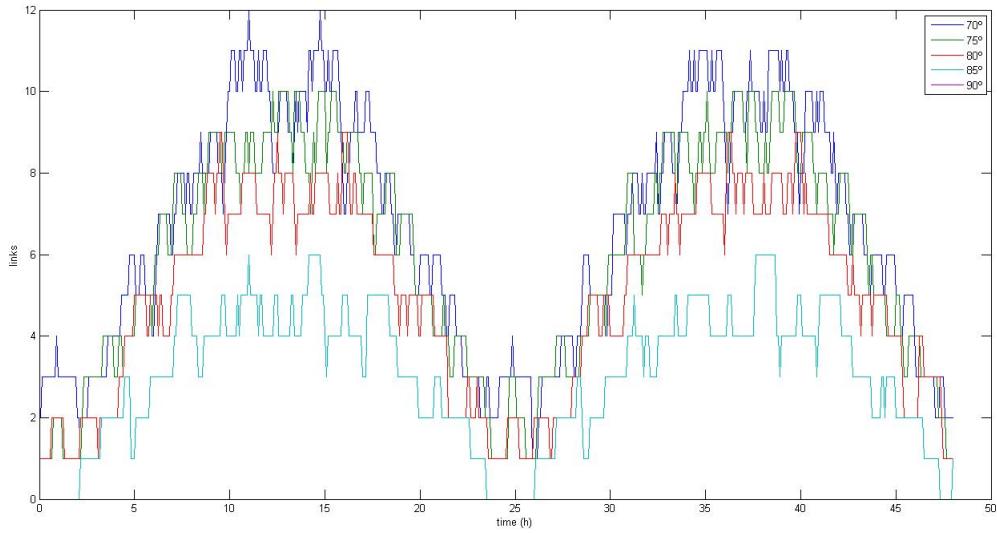
As is shown in Figure 9.1.1, the behaviour is not constant during the day. For every day there is a peak and a valley. This is produced for the cylindrical asymmetry of the constellation. It can also be seen that the pole is not covered. This fact was considered and assumed at the design of the constellation since it doesn't involve any problem at the performance of the system. It can also be seen that for an equatorial latitude there is always 1 link, at least. The equator is the most critical place because is where satellites from different planes are more separated. Global coverage can be ensured, but is important to appreciate that for higher latitudes the coverage is better.

Doing the same analysis but for negative latitudes, the following results are obtained:


 Figure 9.1.2: Links vs time for latitudes from 0° to -90°

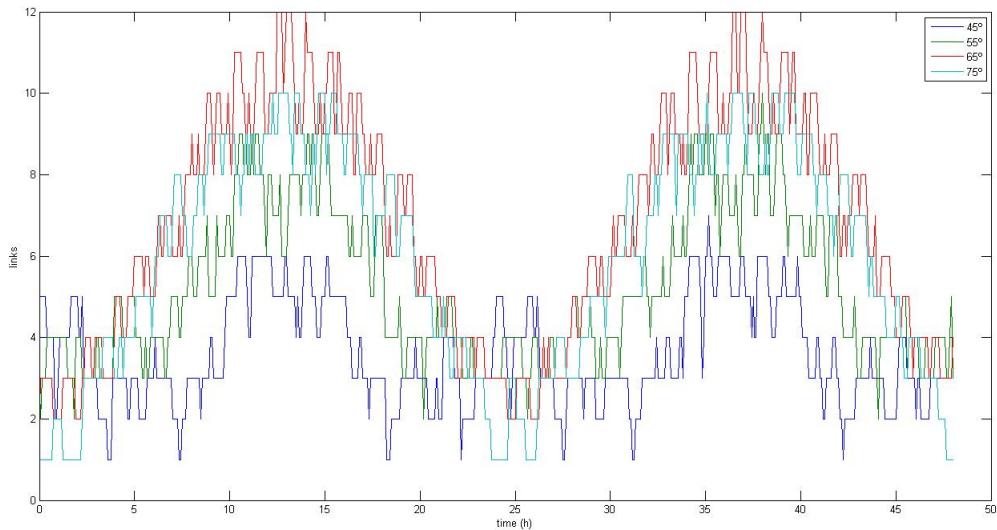
Comparing the results of Figure 9.1.2 with the ones of Figure 9.1.1 it is seen that they are practically the same but with an offset of 12 hours. They are also seen small local deviations, but these are not much significant because of the time-step. This time-step is of 5 minutes for a first sight of the tendencies, and it do not allow extremely precise results.

Taking into account that the results of positive latitudes can be extrapolated to negative ones, the rest of the analysis will be done only for positive latitudes. Is important to know at which latitude, close to the poles, the coverage is lost due to the geometry of the constellation.


 Figure 9.1.3: Links vs time for latitudes from 70° to 90°

It is seen that over 80° of latitude the system starts to lose coverage. It does not cause any problem because there are not inhabited zones over $+80^\circ$ or under -80° . For situating the Ground Stations it has to be considered this restriction.

Now, the latitudes that can provide more links are, around 60° :


 Figure 9.1.4: Links vs time for latitudes from 45° to 75°

As it can be seen in Figure 9.1.4, the optimal latitude must be between 55° and 75° . Expanding the analysis:

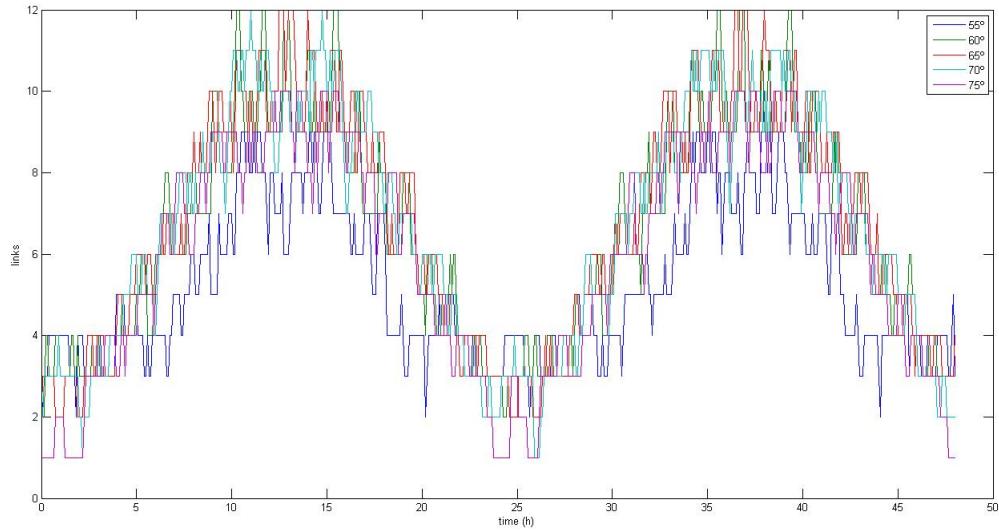


Figure 9.1.5: Links vs time for latitudes from 55° to 75°

The better performance is registered around 60° and 65° . Figure 9.1.5 suggest that between 50° and 60° there is always at least 1 link. But looking it carefully, at the hour 37, there is a local deviation to 0 links. This requires a more accurate analysis decreasing the time-step. For 30 seconds time-step:

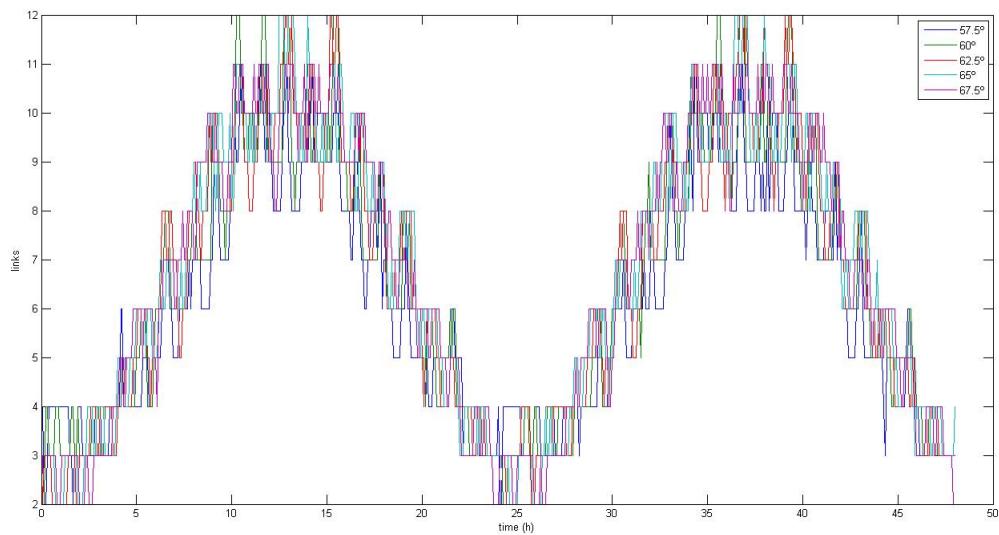


Figure 9.1.6: Links vs time for latitudes from 57.5° to 67.5°

In Figure 9.1.6 there is no problem with the coverage. For ensuring the results and to avoid possible loses of links locally in time, the same range of latitudes is analyze with a smaller time-step.

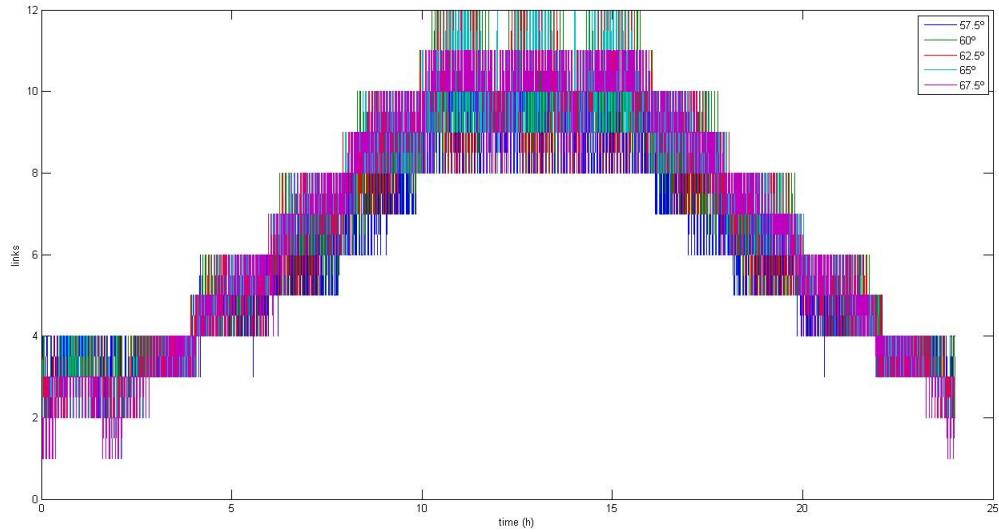


Figure 9.1.7: Links vs time for latitudes from 57.5° to 67.5° with 30 seconds time-step

It can be seen that between 65° and 67.5° the system loses the 2nd link and for a while the station would be connected only to 1 satellite. It is optimum to place the stations between $+57.5^\circ$ and $+62.5^\circ$ of latitude. In order to verify the results for the opposite latitudes:

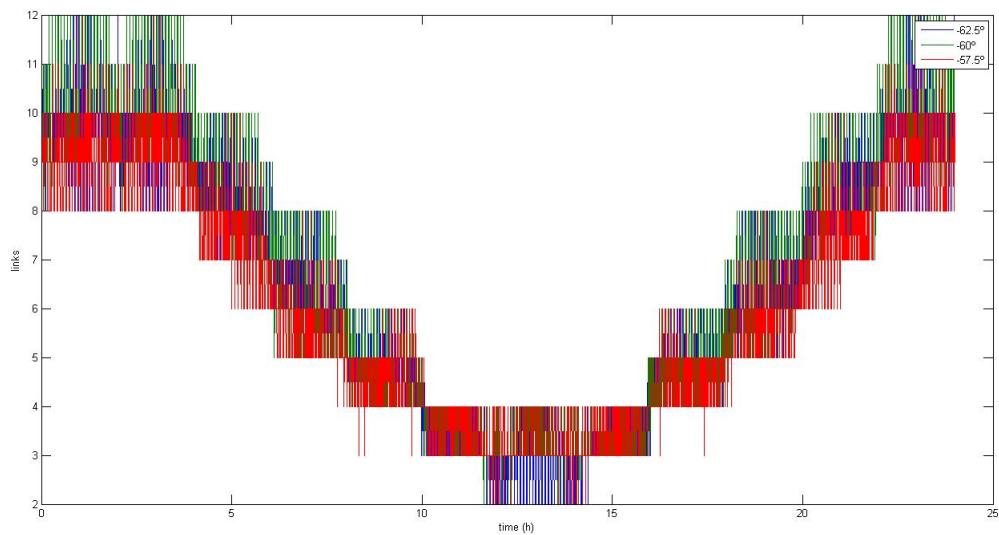


Figure 9.1.8: Links vs time for latitudes from -62.5° to -57.5° with 30 seconds time-step

In conclusion, the optimum latitudes for the Ground Station are:

- Between -62.5° and -57.5°
- Between $+57.5^\circ$ and $+62.5^\circ$

Longitude analysis

It is intuitive to think that the effect of changing the longitude is delaying the evolution of the coverage. This effect is verified by the algorithm:

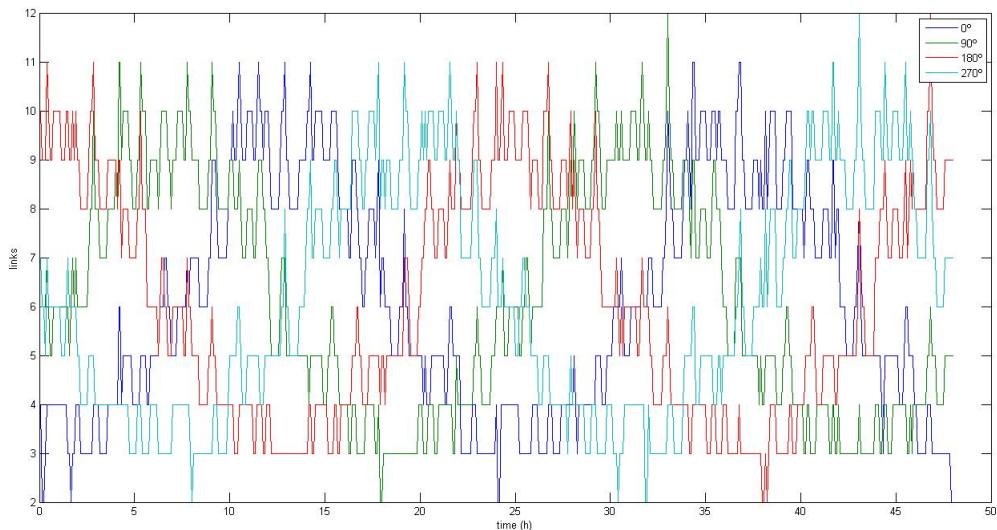
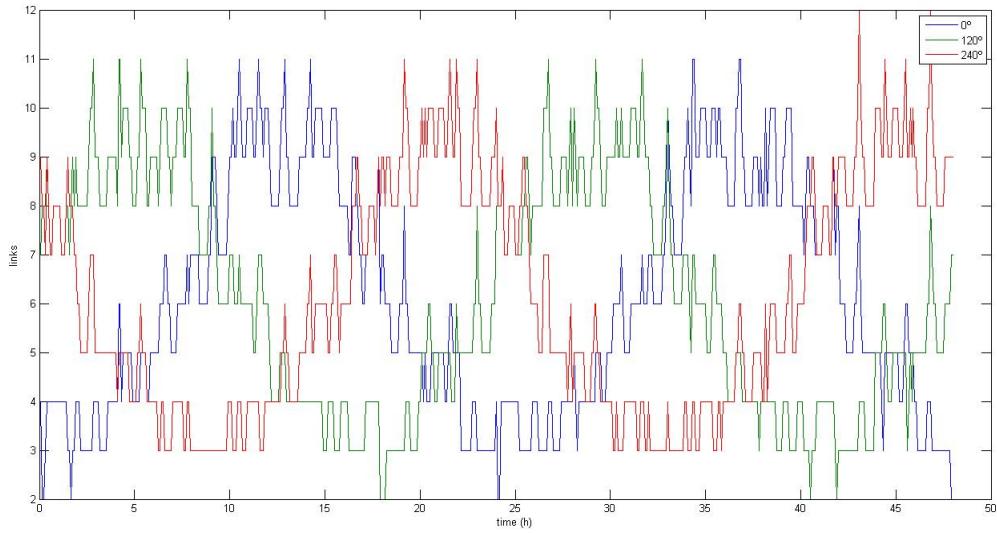


Figure 9.1.9: Links vs time for longitudes from 0° to 270°

As it is seen in Figure 9.1.9 the delay has a reason of 3 hours for every 45° of longitude. This effect can be used in order to optimize the performance of the Ground Stations. During the day every station will have a peak and a valley in the coverage. Placing the stations with a relative longitude of 120° would ensure that when one is at the valley another one is at the peak:


 Figure 9.1.10: Links vs time for longitudes of 0° , 120° and 240°

In conclusion, the Ground Stations should be separated 120° longitude between them. It has to be taken into account that this analysis is done for stations at the same latitude. A Ground Station in a given latitude has the same coverage behaviour as another one at the opposite latitude and 180° of longitude away. To exemplify, in the following table coordinates of equivalent places from the Ground Station point of view are showed.

	GS1		GS2		GS3	
	Latitude	Longitude	Latitude	Longitude	Latitude	Longitude
Option 1	55	0	55	120	55	240
Option 2	-55	180	55	120	55	240
Option 3	55	0	-55	300	55	240
Option 4	55	0	55	120	-55	60
Option 5	-55	180	-55	300	55	240
Option 6	-55	180	55	120	-55	60
Option 7	55	0	-55	300	-55	60
Option 8	-55	180	-55	300	-55	60

Table 9.1.1: Equivalent coordinates

Study of annual costs

Energy and Maintenance

In this section the maintenance of the ground stations and the control center, which is located in Terrassa, will be explained and its costs will be approximated. Is important to notice that the prices are not exact numbers, but just an approximation of the real value of the costs. For these reasons, some of the calculations as for example the cost of Internet in Scotland or Canada, is done using the value of the Internet cost in Spain, as they will be of the same order but can have a slow variation.

Mission Control Center

The control center will be located in Terrassa and it will act as a center from which the activity of the Astrea group will be monitored. The most important cost in this building will be the energy consumption. To approximate the energy consumption the energy use intensity (EUI) can be used. The EUI is a recommended benchmark metric for all type of buildings and tells the amount of energy used in buildings per meter square during one year. The EUI is calculated depending on the type of building (hospital, school, etc). The type of building of the control center can be considered as a set of offices, because the most important features of it will be the computers and the internet communications. Taking as a reference an usual office floor from a building, the average surface it occupies is 500 m^2 . The EUI has been obtained from [36] and is 212 kWh/m^2 . The cost of a kWh according to [37] is of $0,141033\text{ €/kWh}$, taking into account that the main type of consumption is of electricity. Then, doing the calculation:

$$212 \cdot 500 \cdot 0,141033 = 14960 \quad (9.2.1)$$

This is the cost of the energy consumed. However, the fixed term has also to be taken into account. This term is of $3,170286\text{ €/month/kW}$. It does not depend on the kW consumed, but the ones that have been contracted. Considering a tariff of $11,5\text{ kW}$, the cost per year will be of 440 € . Then, the total cost of electricity per year is 15400 € . This is the cost without taxes. Taxes applied to the consume of electricity in Spain are the excise duty on electricity (4,864%) and the value added tax (21%). With these data, the resulting cost is of 20540 € .

Another important cost is the one of the maintenance. The maintenance include cleaning service, industrial maintenance and possible failures of the systems that would need to be repaired. There are companies that offer these services, so to know the cost of the maintenance a research on the market will be done. In most of these companies, no

available information about the cost can be found if no information about the exact needs is provided. However, there are some of them that have few standards tariff that can be used. The maintenance will be divided into two: informatic maintenance and cleaning service. The cost of informatic maintenance for a business extracted from [38] is of 206 € per month. So in one year the cost will be of 2500 €. For the cleaning service, the average market cost is of 10 € per hour according to [39], for contracted maintenance. If there are 250 laborable days and every day there is 2 hour of cleaning service, the total cost of it is of 5000 €.

The other cost that has to be taken into account is the Internet connexion. To give an approximation of this cost, some Internet providers are consulted and the resulting price is of 55 €/month, that are 660 € per year.

In the following table the results are exposed:

Concept	Cost€
Energy:	20540
Maintenance:Informatics	2500
Maintenance:Cleaning	5000
Internet connexion	660
Total cost	28700

Table 9.2.1: Costs per year for the control centre

Ground Stations

The same procedure as the previous one will be done. The costs of maintenance (informatics and cleaning) and of the Internet connexion will be the same, but the difference will be on the energy consumed. The EUI of the site itself, without taking into account the antennas, will also be the same: 212 kWh/m². The surface of the building of the ground station will be of approximately 100 m², enough for the comfortability of 4 people working there. Then, the energy consumption per year will be of 21200kWh. The consumption of the antennas has also to be taken into account. Each antenna consumes 770 W approximately and each GS has four antennas, considering that they will be working 24 h/day during the whole year, the consumtion during one year can be calculated.

$$\frac{4 \cdot 770 \cdot 24 \cdot 365}{1000} = 26981 \text{ kWh/year} \quad (9.2.2)$$

Then the total consumption in kWh of one ground station is:

$$26981 + 21200 = 48181 \text{ kWh/year} \quad (9.2.3)$$

Now the cost of the kWh is needed, and it depends on the countries, so in the following lines the cost will be calculated for each of the ground stations. The cost of kWh supplied has been extracted from [40] and is an average because it depends on many factors as for example the company selected, the type of tariff, the fixed term, taxes, etc.

Canada In Canada, the average cost of 1kWh is of 10 US cents, that are 0,0945 €. Doing the calculation:

$$48181 \cdot 0,0945 = 4550 \quad (9.2.4)$$

The total cost of energy will be of 4550 €.

United Kingdom and Falkland Islands As the other two ground stations are located under the administration of the United Kingdom, its costs will be used. In the UK the average cost per kWh is of 20 US cents, that are 0,189 €. Doing the calculation:

$$48181 \cdot 0,189 = 9100 \quad (9.2.5)$$

The total cost of energy will be of 9100€.

Total annual cost In the following table all the data that has been calculated is exposed in order to know the annual cost of the control centre (MCC) and the ground stations (GS).

Concept	MCC	GS Canada	GS Scotland	GS Malvinas
Energy	20540€	4550€	9100 €	9100 €
Maintenance	7500€	7500€	7500€	7500€
Internet	660€	660€	660€	660€
Total	28700€	12710€	17260€	17260€

Table 9.2.2: Annual costs

Total annual cost	75930 €
--------------------------	----------------

Table 9.2.3: Total annual cost of the ground segment consumption and maintenance

Salaries

In order to work properly, each ground station will require an electrical engineer, a computer technician, a manager and a secretary. Due to the nature of the constellation,

the GS will need to be always functioning and, therefore, it can potentially fail at any moment. For this reason, the presence of an electrical engineer and a computer technician is required all the time. Four engineers and four computer technician will be hired so that for each job three of them will work all the day in 8 hours shifts while the other has the day off.

The salaries for each employee will be the average salary for each job in their respective countries. Those can be seen in Figure 9.2.4.

	Canada	United Kingdom	Argentina
Electrical engineer	47,700€	36,900€	12,300€
Computer technician	30,100€	21,800€	7,100€
Manager	34,500€	28,800€	14,100€
Secretary	28,000€	22,300€	9,500€

Table 9.2.4: Salaries for the different jobs according to the country.

Taking into account that each GS will have a manager, a secretary, four electrical engineers and four computer technicians, and that everyday will be an engineer and a technician working during night, the total cost per ground station would be the following:

- Canada: 381,500€
- United Kingdom: 226,400€
- Argentina: 81,800€

The Mission Control Centre will consist of a building with a manager, a secretary and three aerospace engineers working. Because of the same reason as the ground station, it will be needed to hire twelve engineers, so as to have always three of them working all the time. Taking into account the average salary of each job in Spain, the cost of the salaries can be seen in Figure 9.2.5:

	Spain
Aerospace engineer	30,600€
Manager	30,500€
Secretary	23,000€

Table 9.2.5: Salaries for the different jobs in Spain.

The annual cost of all the salaries can be seen below:

Study of initial investment

- Annual cost of all Ground Stations salaries: 689,700€
- Annual cost of the Mission Control Centre salaries: 429,900€

Study of initial investment

The following items are needed:

- S-band system: 46,500€
- X-band system: 100,000€
- Computers and office material: 13,000€
- Building: 50,000€

Because of the time interval in which an antenna will be reorientating itself to point to the next satellite when the current satellite gets out of range, that antenna will not function until it finishes the reorientation. For this reason, two S-band and X-band systems are required for each ground station to be always operative. Therefore, each ground station needs two X-band systems, two S-band systems, computers and office material and a building.

The initial investment of one ground station will be 356,000€. The initial investment of the three ground stations will be 1,070,000€.

For the Mission Control Centre, the following costs are assumed:

- Computers and office material: 50,000€
- Building: 100,000€

The initial investment of the mission control centre will be 150,000€. The initial investment of all the ground segment will be 1,220,000€.

List of existing Ground Stations

ESA Ground Stations

- Kiruna Station

List of existing Ground Stations

- Coordinates: $67^{\circ} 51' 25.66''$ N, $20^{\circ} 57' 51.57''$ E.
- Number of antennas: 2.
- Size of the antennas: 15 meters. 13 meters.
- Frequencies: S band transmission and S and X band reception. S band transmission and S and X band reception.

• Kourou Station

- Coordinates: $5^{\circ} 15' 05.18''$ N, $52^{\circ} 48' 16.79''$ W.
- Number of antennas: 1.
- Size of the antennas: 15 meters.
- Frequencies: S and X band transmission and reception.

• Maspalomas Station

- Coordinates: $27^{\circ} 45' 46.40''$ N, $15^{\circ} 38' 01.68''$ W.
- Number of antennas: 1.
- Size of the antennas: 15 meters.
- Frequencies: S band transmission and S and X band reception.

• Redu Station

- Coordinates: $50^{\circ} 00' 01.64''$ N, $5^{\circ} 08' 43.24$ E.
- Number of antennas: 3.
- Size of the antennas: 15 meters. 13.5 meters. 2.4 meters.
- Frequencies: S band reception and transmission. Ka band reception and transmission. S band reception and transmission.

• Santa Maria Station

- Coordinates: $36^{\circ} 59' 50.10''$ N, $25^{\circ} 08' 08.60''$ W.
- Number of antennas: 1.
- Size of the antennas: 5.5 meters.
- Frequencies: S band reception.

• Villafranca Station

- Coordinates: $40^{\circ} 26' 33.23''$ N, $03^{\circ} 57' 05.70''$ W.
- Number of antennas: 2.
- Size of the antennas: 15 meters. 15 meters.
- Frequencies: S band transmission and reception. S band transmission and reception.

KSAT Ground Stations

- **Svabard Satellite Station**

- Coordinates: 78° N, 15° E.
- Number of antennas: More than 30
- Size of the antennas: -
- Frequencies: C, L, S, X and Ka band.

- **Tromsø Satellite Station**

- Coordinates: 69° N, 18° E.
- Number of antennas: More than 30
- Size of the antennas: -
- Frequencies: L, S and X band.

- **Troll Satellite Station**

- Coordinates: 72° S, 2° E.
- Number of antennas: 3
- Size of the antennas: 7.3 meters.
- Frequencies: S and X band.

- **Grimstad**

- Coordinates: 58° N, 8° E.
- Number of antennas: 1.
- Size of the antennas: 3.2 meters.
- Frequencies: X band.

- **Hartebeesthoek**

- Coordinates: 25° S, 27° E.
- Number of antennas: 1
- Size of the antennas: -
- Frequencies: S and X band.

- **Dubai**

- Coordinates: 25° N, 55° E.
- Number of antennas: 1

List of existing Ground Stations

- Size of the antennas: -
- Frequencies: S and X band.
- **Mauritius**
 - Coordinates: 20° S, 57° E
 - Number of antennas: 1
 - Size of the antennas: -
 - Frequencies: S and X band.
- **Singapore**
 - Coordinates: 1° N, 103° E.
 - Number of antennas: 1
 - Size of the antennas: -
 - Frequencies: S and X band.

- **NASA Ground Stations**
- **Alaska Satellite Facility**
 - Coordinates: 64° N, 147° W.
 - Number of antennas: 3.
 - Size of the antennas: 11 meters. 11 meters. 10 meters.
 - Frequencies: S and X band. S and X band. S and X band.
- **McMurdo Ground Station**
 - Coordinates: $77^{\circ} 50' 20.87''$ S, $193^{\circ} 19' 58.50''$ W.
 - Number of antennas: 1.
 - Size of the antennas: 10 metes.
 - Frequencies: S band transmission and S and X band reception.
- **Wallops Ground Station**
 - Coordinates: 35° N, 75° W.
 - Number of antennas: 1.
 - Size of the antennas: 18.3 meters.
 - Frequencies: UHF.
- **White Sands Ground Station**

- Coordinates: 33° N, 107° W.
- Number of antennas: 2.
- Size of the antennas: 18.3 meters. 18.3 meters.
- Frequencies: VHF, S and Ka band. VHF, S and Ka band.

SSC Ground Stations

- **Clewiston Satellite Station**

- Coordinates: 26.7° N, 81.0° W.
- Number of antennas: 1.
- Size of the antennas: -
- Frequencies: S and X band.

- **Esrangle Satellite Station**

- Coordinates: $67^{\circ} 53''$ N, $21^{\circ} 04''$ E.
- Number of antennas: 12.
- Size of the antennas: -
- Frequencies: 6x S band. 6x S and X band.

- **Inuvik Satellite Station**

- Coordinates: $68^{\circ} 24''$ N, $133^{\circ} 30''$ W.
- Number of antennas: 1.
- Size of the antennas: 13 meters.
- Frequencies: S and X band.

- **North Pole Satellite Station**

- Coordinates: $64^{\circ} 48'$ N, $147^{\circ} 30'$ W.
- Number of antennas: 2.
- Size of the antennas: -
- Frequencies: S band transmission and S and X band reception. S band transmission and S and X band reception.

- **Punta Arenas Satellite Station**

- Coordinates: 53° S, 71° W.
- Number of antennas: 1.

List of existing Ground Stations

- Size of the antennas: 7.3 meters.
- Frequencies: S and X band.
- **Santiago Satellite Station**
 - Coordinates: $33^{\circ} 08'$ S, $70^{\circ} 40'$ W.
 - Number of antennas: 3.
 - Size of the antennas: -
 - Frequencies: S band transmitting and receiving.
- **South Point Satellite Station**
 - Coordinates: 19° N, 156° W.
 - Number of antennas: 2.
 - Size of the antennas: -
 - Frequencies: S, X and Ku band transmitting and receiving. S, X and Ku band transmitting and receiving.
- **Dongara Satellite Station**
 - Coordinates: $29^{\circ} 03'$ S, 115° E.
 - Number of antennas: 3.
 - Size of the antennas: -
 - Frequencies: S, X, Ku and Ka band transmitting and receiving. S, X, Ku and Ka band transmitting and receiving. S, X, Ku and Ka band transmitting and receiving.
- **Yatharagga Satellite Station**
 - Coordinates: 29° S, 115° E.
 - Number of antennas: 1.
 - Size of the antennas: 13.56 meters
 - Frequencies: S band transmitting and S, X and Ka band reception.

Other Ground Stations

- **Goonhill Earth Station**
 - Coordinates: 50° N, 5° W.
 - Number of antennas: 28.
 - Size of the antennas: 3.7 meters – 32 meters.
 - Frequencies: L, S, X, C, Ku and Ka band.

Decision taking

In the following lines the factors to take into account to decide the ground stations will be explained. After doing so, an OWA will be done if needed.

Availability

Building a ground station

If the decision to build a ground station is taken, it will be available as soon as it is constructed. The time taken to construct the ground stations depend on the efforts employed, but the three ground stations will be surely completed at the time the satellite network is completely deployed. From the moment the ground stations are built, they are totally available to accomplish the missions of Astrea constellation.

Renting a ground station

The sections regarding the renting of a ground station will be done considering LeafSpace (as it has been already said). LeafSpace is a company that does not work only with Astrea constellation, so total availability of the antenna's and its transmissions can not be assured. For this reason, is not possible to assure that the communication rate established in the project charter will be accomplished. Moreover, LeafSpace's Ground Stations are still non-existent, and they predict that the first ones will be available next year.

Cost

Building a ground station

The costs of building a ground station can be divided into an initial investment and a maintenance. The initial investment have been estimated in 190940 € and the maintenance in 30000€/year. The Net Present Cost (NPC) in 10 years will be calculated in order to compare this option with the option of renting a ground station. The discount rate used to do so will be 12%.

$$NPC = +I_o + \sum_{i=1}^{10} \frac{CF_i}{(1+r)^i} \quad (9.5.1)$$

$$NPC = 190940 + \sum_{i=1}^{10} \frac{30000}{(1+0.12)^i} = 360500 \quad (9.5.2)$$

Renting a ground station

In this case maintenance is not needed as it is carried out by the owners of the ground station. The cost, however, comes from the amount of data that is transferred from the satellites to the client. The estimation of the Mbyte transferred over a whole year is difficult to calculate. LeafSpace provides a minimum cost per month of 2400 €. This has been calculated for small communications with X-band. To calculate an approximation, this number will be increased a 40% because Astrea constellation will probably have quite higher transfer of data. The cost per year is, then 40320 €. The NPC will be calculated too:

$$NPC = \sum_{i=1}^{10} \frac{40320}{(1 + 0.12)^i} = 227820 \quad (9.5.3)$$

Position

Building a ground station

In the case the ground station is constructed and operated for the Astrea constellation, there is the possibility of building them in latitudes close to the ideal ones (from 45° to 70°), so more links will be available during more time. Moreover, there is also the possibility to build them in different longitudes (approximately with a difference of 120°).

Renting a ground station

In the case the ground station is rented, there is no possibility to choose the position of the ground station. In the case of LeafSpace, most of the ground stations that will be built in 2017 are located at 45° north. This can seem quite good from the point of view of visibility and links. However, all of them are more or less in the same longitude, so at the same time the links at the different ground stations are the same. With ground stations at different longitudes, the performance of the constellation would be better than having them in the same longitude.

Ease to improve

Building a ground station

The fact of building a ground station implies that it can be improved and adapted to the constellation and the needs of the clients along the development of the mission.

Renting a ground station

If the ground station is rented, it can not be improved according to the needs of the constellation, and maybe the constellation will have to be adapted to the ground station in order to accomplish the mission. The improvement in this case is, then, difficult and probably impossible.

Decision

The factors used to decide will be the ones presented previously. They will be rated from 1 to 2, being 2 the best option and 1 the worst option. As there are only two options, no linear interpolation is needed. Taking into account the requirements and needs of the project, the weights are the following ones:

- Availability: 6
- Cost: 9
- Position: 6
- Ease to improve: 5

The rating and the OWA of the decision between building a ground station or renting an existent one is:

	Availability	Cost	Position	Ease to improve	OWA
Build	2	1	2	2	0.83
Rent	1	2	1	1	0.67

Table 9.5.1: OWA of the GS

Part IV

ANNEX IV: Satellite design

Chapter 10

Satellite design

Structure and mechanics

The design and operation of a CubeSat is a complex process that must be completed keeping in mind the different subsystems as well as the role they will play during the lifetime of the mission. And since these systems will operate in space, they have to be prepared and certified to withstand extreme temperature and radiation conditions.

The satellite used by Astrea must have high compatibility between all the systems to avoid potential problems and has to be tested (either all the systems together or one by one) and their correct functioning has to be ensured. Given that the lifetime of the mission should be greater than four years, the critical systems such as the solar arrays, batteries and antennas should be fully operational until the end of the mission.

Structure

The mission of the structure is to sustain and protect all the electronic devices carried by the satellite in order to fulfill the mission requirements. In order to ensure that all the electronic and mechanic systems can be mounted upon the structure, a high compatibility between these systems is required. Given that the configuration of the current CubeSat is not as common as other configurations of actual commercial or operational CubeSats, it is a really important point that the structure is highly flexible regarding the arrangement of the subsystems.

The structure chosen is manufactured by **Innovative Solutions In Space (ISIS)**. Among its features it is worth mentioning that it can withstand the high range of temperature it will face in the space (from -40°C to 80°C) and it is highly compatible; almost every physical system used can be placed within the structure or on its faces (such as the antennas or the deployable solar arrays). Finally, the mass of the structure is relatively low, and given that the mass of the other subsystems is sometimes a drawback, it is plus point.

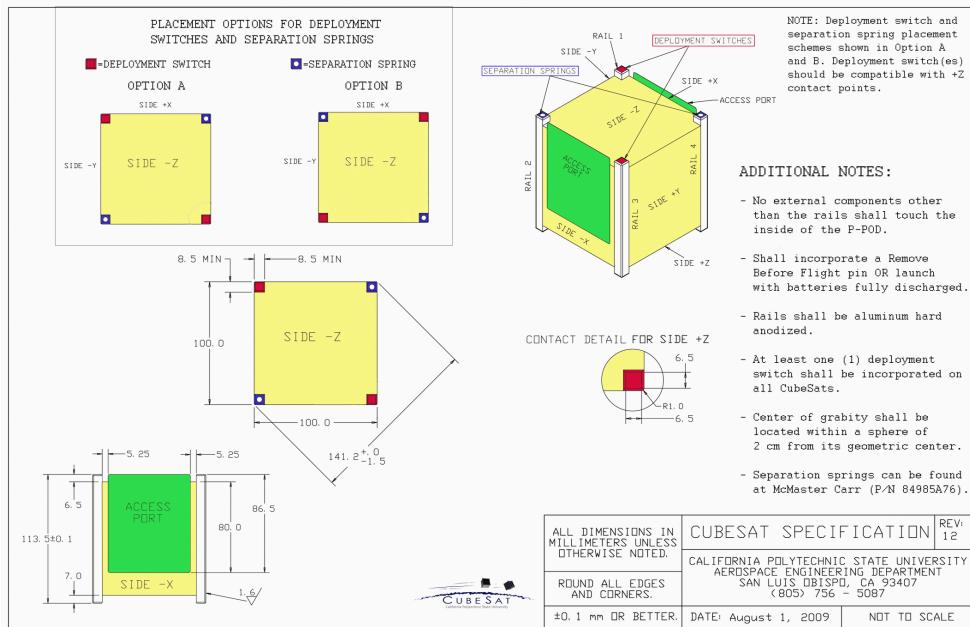


Figure 10.1.1: Dimensions of a 1U CubeSat

[41]

Thermal protection

The thermal protection system consists of various insulating materials that aim to protect the CubeSat from potential thermal shocks. The satellite must remain within an optimal range of temperature, despite of the variation of the external temperature, in order to work properly. Operating in space, the CubeSat is vulnerable to suffer extreme temperatures, both below zero and above zero, and thermal protection must guarantee that all subsystems are protected. Furthermore, the thermal protection system should also dissipate the heat produced by the other systems.

Currently, the most used element as thermal protection in the aerospace industry is the multilayer insulation (MLI), a set of multiple thin insulation layers. The MLI fulfills all the requirements that were previously stated and its main objective is to reduce the heat

generated by radiation since the heat generated by convection or conduction does not have such a high impact on the on-board systems.

After a market study, *Dunmore Aerospace* company has been chosen to provide us its MLI product. Specially, the product is the **Dunmore Aerospace Satkit** and it is made for small satellites for LEO and it will provide the CubeSat with the protection required during operation

Study of the commercial available options and options chosen

A broad marked study is needed since all the options have to be considered. For this reason, and with the aim to show all the information and features of each system that has been considered in this section, the table 10.1.1 is presented below.

Brand and model	Features	Total price (€)
Structure		
ISIS 3U structure	Low mass (304.3g) Highly compatible High temperature range	3900
Gomspace GOMX-Platform	High mass (1500g) Comes fully equipped (basic systems) High temperature range	11000
Thermal protection		
Dunmore Aerospace Satkit	Lightweight Durability Made for small satellites	1000
Dupont Kapton Aircraft Thermal	Lightweight Durability Non-flammable	1400

Table 10.1.1: Options studied for the structure and thermal protection

Finally, the options chosen are presented in the table 10.1.2.

System	Brand and model	Price per unit (€)	N. of units
3U Structure	ISIS	3900	1
Thermal Protection	Dunmore Satkit	1000	1

Table 10.1.2: Options chosen for the structure and thermal protection

Electrical Power System

The electric power system of the satellite must provide and manage the energy generated efficiently in order to have all the systems operating under normal conditions during the lifetime of the mission. The EPS of the Cubesat is, probably, the most fundamental requirement of the satellite, since its failure would result in a mission failure.

The energy collection system and the power management and collection systems compose the EPS and their role is to control and distribute power to the Cubesat, to supply a continuous source of electrical power during the length of the mission, to protect the satellite against electrical bus failures and to monitor and communicate the status of the EPS to the on-board computer.

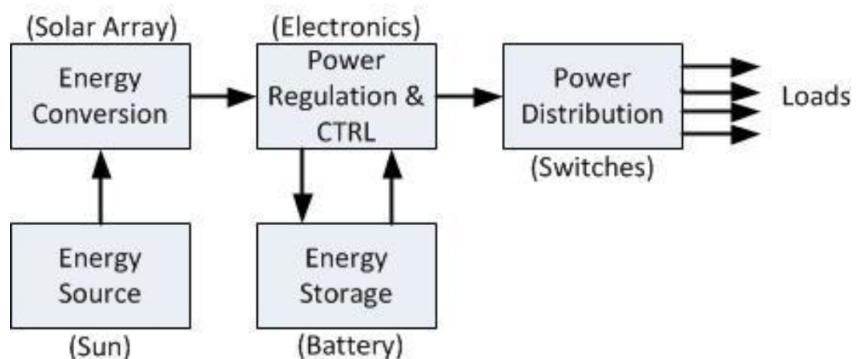


Figure 10.2.1: Basic schematics of the EPS

[42]

Estimation of the power required

To select the adequate electrical power systems it is essential that the power consumed by the CubeSat is known *a priori*. Thus, to select the solar arrays and the batteries, as well as the power management system, an estimation of the power consumed has to be made.

The vast majority of the time the satellite will work under typical operation conditions. However, the estimation of the power consumption provided in the table 10.2.1 has been made for typical-high conditions in order to have a power margin and a more reliable estimation.

System (number of units)	Typical power consumption per unit (W)
Payload	
Patch antenna (8)	4
Payload power consumption	32
Electrical Power System	
NanoPower P60 Power Module (1)	2
Battery (2)	-
Solar arrays (4)	-
EPS power consumption	2
Data Handling Systems	
Transceiver inner-satellite (3)	4
Transceiver space to ground (1)	4
Data handling system (1)	4
DHS power consumption	15
Propulsion and ACDS	
Thruster (1)	20
ADACS (1)	3
OACDS power consumption	3
Estimated total power consumption	52

Table 10.2.1: Estimation of the power consumption under typical working conditions

Additionally, it is worth mentioning that the thrusters are not included in the final estimated power. The thruster will only be active for short periods of time to maintain the orbit, and when it ignites, the other subsystems will not perform in typical conditions. The CubeSat will manage to send only the essential information to the other satellites and, since it is unlikely that their thruster is ignited, the communication is ensured during the maneuver.

Solar arrays

Given that the space of a 3U CubeSat is very limited, the primary source of electrical power has to be photovoltaic cells. The photovoltaic cells will collect and convert the energy of the sun into electrical energy and they have to be correctly selected to prevent failure given their importance.

The solar arrays used must have a decent efficiency and capacity to collect the energy from the sun, have to keep their mass relatively low, must have a protective radiation shield to ensure their full efficiency for at least 4 years, a proper deployment system, the

ability to withstand space conditions and also must be highly compatible with all the other systems used, especially the power management system (the *NanoPower P60*).

The option selected for the mission is a set of deployable solar panels provided by **EXA (Agencia Espacial Civil Ecuatoriana)**. These solar arrays fulfill all the requirements mentioned above: they are low mass (135g per unit), they have a protective radiation shield (NEMEA Anti Radiation Shield protects the solar panels of EM, High Gamma, X-Ray, Alfa, Beta and low neutron radiation) they can withstand a very high temperature range (from -80°C to 130°C) ensuring that they can operate in space, they have a gentle release and deployment system with artificial muscles (developed by EXA) and they provide a power of 16.8W each (19.2V@0.5A).

Every cubesat will come with at least 4 deployable solar panels providing it with 67.2W of power, approximately, to supply peak demands during the lifetime of the mission. Additionally, it is worth mentioning that these solar arrays are compatible with the hardware used (the structure and the power management system).

Note that these 4 deployable solar panels are a basic requirement. If more space is available on the faces of the satellite, additional 1U non-deployable solar arrays (giving an extra power of 2.3W per array, approximately) or 1U deployable arrays (giving an extra power of 16.8W or 10W) will be placed. They are also low mass equipment (about 80g per array) as the deployable solar arrays and highly compatible with the CubeSat. Their current and voltage are different but given that the CubeSat will be equipped with the NanoPower P60, that should not be a problem. The only drawback of these arrays is that they may be only fully operational for 2 years in LEO. However, that does not mean they will not work anymore after these 2 years; it means that they will start losing efficiency.

Power management system

The role of the power management system is to distribute the power and supply the energy to the different systems used in the CubeSat. Since the systems of the CubeSat have different power and energy needs, the power management system has to be highly compatible and have a number of buses high enough to supply the different voltage and intensity required to the systems.

The selected option for the mission is the **NanoPower P60** by **Gomspace**, a high-power EPS for small satellites that comes with 1 motherboard, 1 ACU module (Array Conditioning Unit) and 1 PDU (Power Distribution Unit), allowing multiple configurations in just one motherboard; saving a lot of space.

The motherboard supports up to 4 ACU and PDU modules and has different regulated outputs (3.3V and 5V). It means that with one single motherboard, several conditioning and distributing units can be connected. That ensures that additional equipment (ACU and PDU) could be linked to the motherboard if something failed in the assembly process.

The ACU module 6 different inputs per unit with a high voltage solar input (up to 16V or 32V). Additionally, each input can withstand a maximum current of 2A and current and voltage inputs are measured on each input channel and the measurements can be communicated to the onboard computer.

The PDU module has 9 different outputs per unit that are highly configurable. Each module has 3 configurable output voltages (3.3V, 5V, 8V, 12V, 18V, 24V) and each of the outputs can withstand a maximum current of 1A or 2A (programmable). Additionally, like the ACU module, current and voltage outputs are measured on each output channel and can be effectively communicated to the onboard computer.

All these features make the **NanoPower P60** a very efficient and configurable power management unit that fulfills the mission requirements. Furthermore, given this capacity to configure each input and output channel and the high number of channels that it has, the compatibility between all the systems used in the satellite is ensured. Additionally, the communication between this system and the onboard computer in order to detect potential failures is a really adequate feature.

With the NanoPower P60 we aim to distribute the energy to all of the subsystems of the CubeSat.

Batteries

Batteries are essential for a proper mission operation. They will provide the spacecraft subsystems with the power needed when the solar arrays are working less efficiently or not properly. Astrea is looking for decent capacity batteries that provide a slightly high typical energy and power supply, since all the systems will not usually operate under peak conditions. Additionally, through the lifetime of the mission, the solar arrays will face an important unfavorable condition; in the worst case scenario, the satellite will be in the dark during half of the period of the orbit. So, it is clear that the batteries are a critical system of the CubeSat

Among all the commercial options, Astrea has chosen the **BA01/D** batteries manufactured by **EXA-Agencia Espacial Civil Ecuatoriana**. The CubeSat will have two of these batteries, with a total capacity of 28800mAh or 106,4Wh. Each battery has a total of 16 cells, highly stackable and with a very low mass (155g per unit). They also come with unique thermal transfer bus, that will transfer the heat of the other subsystems to the batteries to keep their temperature under efficient working conditions.

The output voltage can be configured (3.7V and 7.4V) and they are perfectly compatible with the solar arrays. Furthermore, they come with a protective radiation shield (NEMEA) that ensures at least 4 years working under full efficiency conditions in a LEO. It is also worth mentioning that if the company that will assemble the CubeSat faces problems during this part of the process, the batteries can be customized by contacting EXA.

As mentioned above, if the satellite was in the dark during half of the period of the orbit, the estimated energy that it would need would be 50W. Thereby, the capacity of the batteries is more than enough to supply the required energy in the worst case scenario. In fact, they will supply energy when the energy demand of the CubeSat is higher than the energy collected by the solar cells. And logically, they will store the energy collected by the solar arrays when the energy demand of the systems is lower than the energy collected.

Study of the commercial available options and options chosen

A broad marked study is needed since all the options have to be considered. For this reason, and with the aim to show all the information and features of each system that has been considered in this section, the table 10.2.2 is presented below.

Brand and model	Features	Total price (€) per unit
Solar arrays		
EXA-Agencia Espacial Ecuatoriana	Total power of 67.2W (4units) Mass of 270g (p.unit) Included thermal protection At least 4 years lifetime	17000
ISIS	Total power of 30W (4units) Mass of 150g (p.unit) No thermal protection At least 2 years lifetime	9000
Power management		

Crystalspace P1 Vasik	Mass of 80g Full redundancy Low volume 6x outputs Up to 10W input High temperature range	5400
Gomspace NanoPower P60	Mass of 176g 9x configurable outputs 6x inputs per module EMI shielding High temperature range	16000
Batteries		
Gomspace NanoPower BP4	Total capacity of 77Wh (2u) Automatic heat regulation Highly stackable Mass of 270g (p.unit)	3250
EXA-Agencia Espacial Ecuatoriana	Total capacity of 106.4Wh (2u) Automatic heat regulation Highly stackable Total mass of 155g	6300

Table 10.2.2: Options studied for the Electric Power System

Finally, the options chosen are presented in the table 10.2.3.

System	Brand and model	Price per unit (€)	N. of units
Solar arrays	EXA	17000	4
Additional solar arrays	-	4000-12000	depends
Batteries	EXA	6300	2
Power Management	Gomspace NanoPower P60	16000	1

Table 10.2.3: Options studied for the Electric Power System

Propulsion Systems

Requirements

There is a big risk of a collision with space debris while a spacecraft is operating in Low Earth Orbits. The Inter-Agency Space Debris Coordination Committee recommended to the United Nations (section 5.3.2 ‘Objects Passing Through the LEO Region’): “Whenever

possible space systems that are terminating their operational phases in orbits that pass through the LEO region, or have the potential to interfere with the LEO region, should be de-orbited (direct re-entry is preferred) or where appropriate manoeuvred into an orbit with a reduced lifetime. Retrieval is also a disposal option.” and “A space system should be left in an orbit in which, using an accepted nominal projection for solar activity, atmospheric drag will limit the orbital lifetime after completion of operations. A study on the effect of post-mission orbital lifetime limitation on collision rate and debris population growth has been performed by the IADC. This IADC and some other studies and a number of existing national guidelines have found 25 years to be a reasonable and appropriate lifetime limit.” [43]

Thus, a proper propulsion system is needed both for maintaining the satellite’s orbit and for de-orbiting after the mission’s lifetime.

Given the size of the CubeSat, not many effective options are available and a committed solution has to be found in order to follow the recommendations by the IADC.

Thrusters

Thruster is a main part of the structure because it is needed to allow the satellite to realise different maneuvers how incorporate it adequately to the orbit after the deployment of the rocket, can obtain the optimal orientation or to mantain the satellite in the orbital and avoid its fallen.

The main parameters that must consider are thrust, total specific impulse, power required, weight of the propulsion subsystem and its volume.

At the moment, the most used and more modern thrusters for satellites are: ionic, pulsed plasma, electrothermal and green monopropellant thrusters. An important aspect to consider is that the goal is to reduce the mass required although this will cause minor accelerations than conventional engines but it will be suitable for small satellites.

After a market study, the best two options to consider are the green monopropellant thruster BGT-X5 and the ion thruster BIT-1, both from Busek company. These two thruster are among the most used in the aerospace industry for small satellites. The main difference between both are the thrust and the specific impulse. On the one hand, the BIT-1 thruster provides a lower thrust but with a high specific impulse. On the other

hand, BGT-X5 thruster provides a high thrust, around 0.5 N but with a lower specific impulse.

Finally, BGT-X5 has been chosen how the CubeSat thruster. With the high thrust and delta V that BGT-X5 provides, the CubeSat will be able to carry out the necessary actions to keep the satellite in orbit, to relocate the satellite or to change its orbit.

The following table 10.3.1 shows the main parameters of this thruster.

BGT-X5	
PARAMETERS	VALUE
Total thruster power	20 W
Thrust	0.5 N
Specific impulse	225 s
Thruster Mass	1500 g
Input voltage	12 V
Delta V	146 m/s

Table 10.3.1: Main features of BGT-X5

Study of the commercial available options

A broad marked study is needed since all the options have to be considered. For this reason, and with the aim to show all the information and features of each system that has been considered in this section, the table 10.3.2 is presented below.

Brand and model	Features	Total price (€)
Propulsion		
Busek ion thruster BIT-1	Volume 1/2 U High Isp (2150 s) Low thrust (100 uN)	58000
Busek BGT-X5	Volume 1 U High thrust (0.5 N) High delta V (146 m/s)	50000

Table 10.3.2: Options studied for the propulsion system

Finally, the option chosen is presented in the table 10.3.3.

System	Brand and model	Price per unit (€)
Propulsion	Busek BGT-X5	50000

Table 10.3.3: Option chosen for the propulsion system

Attitude and Orbital Control Systems

Attitude and orbital control subsystem is needed to enable the satellite to keep a specific position within its orbit and to control the antennas in order to remain oriented to assigned area, because the satellite tends to change its orientation due to torque. The AOCS receives telecommands from the central computer and acquires measurements (satellite attitude and orbital position) from sensors. We will also refer to the attitude control as ADACS (Attitude Determination and Attitude control system).

Attitude control for CubeSats relies on miniaturizing technology without significant performance degradation. Tumbling typically occurs as soon as a CubeSat is deployed, due to asymmetric deployment forces and bumping with other CubeSats. Some CubeSats operate normally while tumbling, but those that require pointing in a certain direction or cannot operate safely while spinning, must be detumbled. Systems that perform attitude determination and control include **reaction wheels**, **magnetorquers**, **thrusters**, **star trackers**, **Sun sensors**, **Earth sensors**, **angular rate sensors**, and **GPS receivers and antennas**. Combinations of these systems are typically seen in order to take each method's advantages and mitigate their shortcomings. **Reaction** wheels are commonly utilized for their ability to impart relatively large moments for any given energy input, but reaction wheel's utility is limited due to saturation, the point at which a wheel cannot spin faster. Reaction wheels can be desaturated with the use of thrusters or magnetorquers. **Thrusters** can provide large moments by imparting a couple on the spacecraft but inefficiencies in small propulsion systems cause thrusters to run out of fuel rapidly. Commonly found on nearly all CubeSats are **magnetorquers** which run electricity through a solenoid to take advantage of Earth's magnetic field to produce a turning moment. Attitude-control modules and solar panels typically feature built-in magnetorquers. For CubeSats that only need to detumble, no attitude determination method beyond an angular rate sensor or electronic gyroscope is necessary (*wikipedia extract*, [?]).

Pointing in a specific direction is necessary for Earth observation, orbital maneuvers, maximizing solar power, and some scientific instruments. Directional pointing accuracy can be achieved by sensing Earth and its horizon, the Sun, or specific stars. Determination of a CubeSat's location can be done through the use of on-board GPS,

which is relatively expensive for a CubeSat, or by relaying radar tracking data to the craft from Earth-based tracking systems (*wikipedia extract*, [?]).

Orbital Control

Orbital control will be achieved as a combination of two systems. ADCS will orient the thrust, this thrust will be given by the propulsion system and all the operation will be controlled on the On-Board Computer. Principally, the orbit control will be necessary to mitigate orbital debris effect on every satellite.

Study of the commercial available options

Because AOCS involve so many systems working together, full assembled module had been considered in order to avoid compatibility issues.

ADACS options		
Features	CUBE ADCS	MAI-400 ADACS
Power	3.3/5 VDC Peak: 7.045W	5 VDC Peak: 7.23W
Mass	506 g	694 g
Size	90 x 90 x 58 mm	10 x 10 x 5.59 cm
Sensors	3-Axis Gyro Fine Sun & Earth sensor Magnetometer 10x Coarse Sun Sensors Star tracker(optional)	3-axis magnetometer Coarse sun sensor EHS Camera
Actuators	3 reactions wheels 2 torque rods	3 reactions wheels 3 torque rods
Computer	4-48 MHz full ADCS + OBC	4Hz Provides telemetry
Control Board	Works as OBC included	MAI-400 not included

Table 10.4.1: Main ADACS features

Decision After the study of commercial options available, the previous two where the unique that fitted in AstreaSAT requirements, so a decision between these two must be done. Since all the features tabulated on 10.4.1 are critical, the same weights are given. Therefore, we will compare directly the two alternatives for choosing the best alternatives.

Payload

Taking into account that we need: low power consumption, low, weight and size, high pointing accuracy and really versatile systems that can integrate multiple subsystems; **CUBE ADCS** is chosen. It has the lowest mass and power consumption, it also offers a higher attitude determination systems, redundancy is a key fact because we can not loose precision during the life time of each satellite. Finally, the fact that CUBE ADCS integrates also and On-Board Computer (OBC) is the turning point, because we have size and weight limitations, having and integrated, high performance OBC in this system will make able TT&C with the ground stations and the control af every system on board.
<http://www.cubespace.co.za/cubecomputer>

Payload

Aim AstreaSAT payload, needs to provide a radio link to the client satellites, for real time data relay with no less than 25MB/s of data rate. For achieving its porpoise, the payload will consist on a pack of arrays of antennas and data handling computers.

AstreaSAT payload will have to have three types of radio links for transmitting in every condition the data received from the clients:

- **Space to Ground link:** Connection between satellite and Ground Station when it is possible.
- **Inter-satellite Space to Space link:** Communication between Astrea satellites for data relay, looking for the nearest satellite with Ground Station link available, to transmit the data.
- **Client Space to Space link:** Communication between client and Astrea satellites.

The radio frequencies that we can use to establish the previous described links are regulated in [44] by frequency, bandwidth and type of communication . So, for the **Space to Ground link** we can use frequencies from **70MHz to 240GHz**; for **Inter-satellite Space to Space link** plus data relay type of communication, frequencies are **2-2.4GHz, 4-4.4GHz and 22-240GHz**. Finally, **Client Space to Space link**, they exist to cases; on the one hand, the client points towards the Earth like a standard satellite, we capture its signal and make the data relay, since it is like a Space to Ground communication and also like a inter-satellite communication, we can combine the two previous restrictions. On the other hand, if the client satellite is below our constellation, we only had inter-satellite communication, therefore **Inter-satellite Space to Space link** rules are applied.

Payload

Finally, the Payload will consist on a combination of antennas, transceivers and data handling systems which will combine to create a data relay module.

Antennas

The antennas are essential in this mission, since their role is to transmit and receive the data from other satellites as well as the ground stations. In order to provide fast and reliable communication, several options have been studied and information about their main parameters is presented below.

It has to be kept in mind that the mass of the antennas should be as low as possible given that there are already a lot of subsystems in the CubeSat and the mass limitation is about 4kg. Additionally, the power consumption has to be kept as low as possible given the limitations regarding to the power supply of the CubeSat. The antennas must be certified to work under space conditions (high temperature range and radiation protection shield). Preliminary, after a first satellite preliminary design, seems that patch and turnstile antennas will cover the needs of AstreaSAT.

Basic parameters

The **frequency range** is one of the most important parameters, since it is related to an effective satellite-satellite and satellite-ground station communication. The frequency range should be between 1GHz and 10GHz, which is a very demanding condition given that the CubeSat has a limited space and power supply. Those frequencies, assure the desired data rates and negligible atmosphere attenuations.

For an effective communication, the signal has to be able to trespass the atmosphere without a high number of losses and interference. The high frequency range allows the signal to go through this barrier and reach the ground stations.

The **bandwidth** is the frequency range in which the highest power of the signal is found. It is really important to have a high bandwidth to have a great performance and avoid extremely high signal losses.

The **gain** of an antenna is the ratio between the power density radiated in one direction and the power density that would radiate an isotropic antenna. The best option is to have a high gain.

The **polarization** of an antenna is the orientation of the electromagnetic waves when they are leaving it. There are three types of polarization: linear, circular and elliptical. For a high performance, the receiver antenna and the transmitter antenna should have the same polarization. It has been derived that the best option for the project is an antenna with circular polarization; these types of antennas are able to keep the signal constant regardless of the appearance of different adverse situations such as the relative movement of the satellites with respect to the ground station.

Patch antenna

A **patch antenna** is a type of radio antenna with a low profile, which can be mounted on a flat surface. It consists of a flat rectangular sheet or "patch" of metal, mounted over a larger sheet of metal called a ground plane. They are the original type of microstrip antenna described by Howell in 1972. [?, wikipedia]

Patch antenna AntDevCo	
Features	Value
Bands	L,S,C,X
Frequency range	1-12 GHz
Bandwidth	20 MHz
Gain	6 dBi
Polarization	Circular
Maximum power consumption	10 W
Impedance	50 Ohms
Operational temperature range	-65°C to +100°C
Mass	<250 grams

Table 10.5.1: Main features of the patch antenna

Turnstile antenna

A **turnstile antenna**, or crossed-dipole antenna, is a radio antenna consisting of a set of two identical dipole antennas mounted at right angles to each other and fed in phase quadrature; the two currents applied to the dipoles are 90° out of phase.

Turnstile antenna ANT430	
Features	Value
Frequency range	400-480 MHz
Bandwidth	5 MHz
Gain	1.5 dBi
Polarization	Circular

Maximum power consumption	10 W
Impedance	50 Ohms
Operational temperature range	-40°C to +85°C
Mass	30 grams

Table 10.5.2: Main features of the turnstile antenna

Antenna selection

After a market study, the best two antennas to add in the CubeSat are the patch antenna AntDevCov and the turnstile antenna ANT430 Gomspace. The number of units of each antenna are 4 and 2 respectively. The 4 patch antennas will be placed on each side face of the CubeSat and they will occupy a 1U face. The 2 turnstile antennas will be placed on the upper and lower face of the CubeSat and, as they do not occupy space, other systems such as a solar panel or the thruster can be placed on those faces.

Other antenna types, like helicoidal deployable antennas, parabolic antennas or monopole antennas, had been discarded because of their big volume and mass or because they don't accomplish the preliminary requirements stated on the project charter.

Nevertheless, this is only a preselection. After the link budget study and negotiation with communications department changes can be made if it is necessary.

Payload Data Handling Systems

Every AstreaSAT will act as a router to transmit client data to the ground. This initial raw data, should be temporally stored into the satellite in order to process it, if necessary. Since, to down-link the data, first the satellites need to establish connection, data can not be directly retransmitted to other sources (Ground Station or satellite) as it enters to the satellite. Furthermore, non loss compression algorithms can be applied to reduce the data size load and achieve higher data transmission velocities.

To sum up, Payload Data Handling System of every AstreaSAT (PDHS) will be able to receive, process and send the client data, using the integrated transceivers (transmitter + receiver) for sending the data and the PDHS computer to process it. PDHS have a hard disk associated which will temporally store the client data.

Finally, is necessary to find the transceivers and PDHS computers compatible combination in order to achieve the specifications stated on the Project Charter.

Transceivers

A transceiver is a device comprising both a transmitter and a receiver that are combined and share common circuitry or a single housing. For the preliminary design, because we know that they should satisfy all the connectivity options, we are restricted to the S, K or higher bands for **Inter-satellite communication** and not restriction virtually at all for **Space to Ground** communication. Nevertheless, together with the communications department, X band is chosen as the frequency to talk to the floor because several factors: the use in

Transceivers options - Inter-satellite comm.(S band)		
Features	NanoCom TR-600	SWIFT-SLX
Band	70 - 6000 MHz	1.5 - 3.0 GHz
Bandwidth	0.2 - 56 MHz	10+ MHz
Vcc	3.3V	6 - 36V
Max. Power consumption	14W	10.8W
Dimensions	65 x 40 x 6.5 mm	86 x 86 x 25-35mm
Operational temperature range	-40°C to +85°C	-35°C to +70°C
Mass	16,4 grams	250 grams

Table 10.5.3: Main inter-satellite communication transceivers features

NanoCom TR-600 has an additional advantage, GOMspace, the supplier, offers it in combination with the NanoMind Z7000 seen in PDHS computers section. Both integrated on a board able to hold three TR-600 transceivers and one computer. The low dimensions, high bandwidth (associated to high data rates) and low mass of TR-600 versus SWIFT-SLX, makes the first, a great choice for Inter-Satellite communication.

Transceivers options - Space to Ground comm.(X band)		
Features	SWIFT-XTS	ENDUROSAT
Band	7 - 9 GHz	8.025 - 8.4 GHz
Bandwidth	10 - >100 MHz	10+ MHz
Vcc	3.3V	12V
Max. Power consumption	12W	11.5W
Dimensions	86 x 86 x 45mm	90 x 90 x 25mm
Operational temperature range	-40°C to +85°C	-35°C to +70°C
Mass	350 grams	250 grams

Table 10.5.4: Main space to ground communication transceivers features

SWIFT-XTS is pretty similar to ENDUROSAT, but presents some advantages. The higher Bandwidth, will make possible higher communication data rates. The higher mass respect to ENDUROSAT could be a problem, from the link budget analysis a decision will could be made, because the most important factor is the possibility to transmit with low losses to the ground.

PDHS computers

PDHS computers will process and store the clients data before the data relay is done.

PDHS computers options		
Features	NanoMind Z7000	ISIS iOBC
Operating System	Linux	FreeRTOS
Storage	4GB to 32 GB	16GB
Processor	MPCoreA9 667 MHz	ARM9 400 MHz
Vcc	3.3V	3.3V
Max. Power consumption	30W	0.55W
Dimensions	65 x 40 x 6.5mm	96 x 90 x 12.4mm
Operational temperature range	-40°C to +85°C	-25°C to +65°C
Mass	28.3 grams	94 grams

Table 10.5.5: Main PDHS computers features

The main advantage of NanoMind Z7000 over ISIS iOBC is the computing availability, because of its two 667MHz processor Z7000 can handle higher data payloads and processit at higher velocities, reducing in last term delay between communications. Also, Z7000 presents a lower mass, critical think in our mass limitation of 4kg. But the turning point is, as stated before, Z7000 comes integrated on a single board with a maximum of three NanoMind TR-600 transceivers, fact that makes it a perfect option to build a data relay module payload.

Study of the commercial available options and options chosen

A broad marked study is needed since all the options have to be considered. For this reason, and with the aim to show all the information and features of each system that has been considered in this section, the table 10.5.6 is presented below.

Brand and model	Features	Total price (€)
Antennas		

Payload

Patch antenna AntDevCo	High frequency range (L,S,C,X bands) High bandwidth High mass (120 g)	18000 (7000)
ISIS monopole deployable antenna	Low frequency range (10MHz) Higher mass than ANT430 (100 g) Deployable Not occupy space	17000
Turnstile antenna ANT340 Gomspace	Low frequency range (400-480 MHz) Low mass (30 g) Deployable Not occupy space	9500
Transceiver inter-satellite		
NanoCom TR-600	SDR including S band High Bandwidth Low mass and dimensions Integrated with other PDHS	8545
SWIFT-SLX	Low power consumption High mass and dimensions Narrow bandwidth	7800
Transceiver space to ground		
SWIFT-XTS	High bandwidth High mass Standard dimensions	5500
ENDUROSAT	Narrow bandwidth Lower mass Standard size	22500
PDHS Computers		
NanoMind Z7000	LinuxOS High processing velocity High power consumption Low mass and dimensions	5000
ISIS iOBC	FreeRTOS OS Less computing velocity High dimensions and mass	9400

Table 10.5.6: Options studied for the payload

Finally, with the aim to clarify all the information of this section, the chosen systems and components are presented in the table 10.5.7.

System	Brand and model	Price per unit (€)	N. of units
Antenna	Patch antenna AntDevCo	TO REQUEST!	8
Transceiver	NanoCom TR-600	TO REQUEST!	3
Transceiver	SWIFT-XTS	TO REQUEST!	1
PDHS	NanoMind Z7000	TO REQUEST!	1

Table 10.5.7: Options chosen for the payload

Communication module

The telemetry subsystem analyses the information of the ground station and other sensors of the satellite in order to monitor the on-board conditions. With this system, the CubeSat is able to transmit the status of the on-board systems to the ground station.

The command and control subsystem (TT&C) allows the ground station to control the satellite.

Every Astrea satellite (AstreaSAT) of the constellation, will need to report its operating status to the ground and receive commands from the ground. TT&C operations will usually be performed when the satellite flights over the coverage of the constellation ground station, but since the satellites are interconnected, there is the possibility to perform this operations via data relay links between satellites. As a collaboration with the communications department, S band frequency is chosen for TT&C operations, since there is no need for high data rates, the lower band will significantly reduce the power consumption.

Communication to the ground will be perform with a NanoCom TR-600 transceiver module attached to AntDevCo Patch antenna, both configured for S band frequency communication.

Link Budget

Astrea constellation main satellite must be able to stablish three different telecommunications link:

- Space to Ground link for payload and TT&C data.

- Space to Space link between Astrea satellites.
- Space to Space link between client and Astrea satellites.

Communications Basics

When evaluating a wireless link, the three most important questions to be answered are: [6]

1. How much radio frequency (RF) power is available? Up to 2W for S band or up to 12W for Xband.
2. How much bandwidth is available?
Available 400MHz with 28 channels of 14MHz or 228 channels of 1.75MHz for inter-satellite communication at S band. For X band, there's more than 4GHz available [44]. In fact is limited by the TR-600 transceiver at 56MHz for S band and to 100MHz by SWIFT - XTS at X band.
3. What is the required reliability (as defined by Bit Error Rate, or BER)?
Required reliability for space systems $E_b/N_o \geq 10$, so $BER = 5.5 \times 10^{-6}$ for a MSK, PSK (worst case) modulation as shown in Fig.10.7.5.

The upper limit in terms of data rate is given by Shannon's Channel Capacity Theorem:

$$C = B \log_2(1 + S/N) \quad (10.7.1)$$

where:

$$\begin{aligned} C &= \text{channel capacity (bits/s)} \\ B &= \text{channel bandwidth (Hz)} \\ S &= \text{signal strength (watts)} \\ N &= \text{noise power (watts)} \end{aligned}$$

With all data known, the minimum required sensitivity of a receiver using the Eq. 10.7.1 will be stated in the Link Budget calculation.

Transmission Losses In any satellite transmission, there are always losses from various sources. Some of those losses may be constant, others are dependent of statistical data and others vary with the weather conditions, especially with rain.

TRANSMISSION LOSSES	PROPAGATION LOSSES	FREE SPACE LOSSES			
		ATMOSPHERIC LOSSES	Ionospheric effects	Faraday rotation Scintillation effects	
			Tropospheric effects	Attenuation Rain attenuation Gas absorption Depolarization	
				Sky noise	
		Local effects			
		POINTING LOSSES			
		LOCAL LOSSES	EQUIPMENT LOSSES	Feeder losses	
			?????		
		ENVIRONMENT LOSSES			

Figure 10.7.1: Principal losses in the received signal [5]

Propagation losses

Free Space Losses

Range and Path Loss Another key consideration is the issue of range. As radio waves propagate in free space, power falls off as the square of range. For a doubling of range, power reaching a receiver antenna is reduced by a factor of four. This effect is due to the spreading of the radio waves as they propagate, and can be calculated by [6]:

$$L = 20\log_{10}(4\pi D/\lambda) \quad (10.7.2)$$

where:

D = the distance between receiver and transmitter

λ = free space wavelength = c/f

c = speed of light($3 \times 10^8 m/s$)

f = frequency (Hz)

Atmospheric Losses

This kind of losses derives from the absorption of energy by atmospheric gases. They can assume two different types:

- Atmospheric attenuation.
- Atmospheric absorption.

The major distinguishing factor between them is their origin. Attenuation is weatherrelated, while absorption comes in clear-sky conditions. Likewise, these losses can be due to ionospheric, tropospheric and other local effects. [5]

Ionospheric Effects All radio waves transmitted by satellites to the Earth or vice versa must pass through the ionosphere, the highest layer of the atmosphere, which contains ionized particles, especially due to the action of sun's radiation. Free electrons are distributed in layers and clouds of electrons may be formed, originating what is known as travelling ionospheric disturbances, what provoke signal fluctuations that are only treated as statistical data. The effects are:

- **Polarization rotation:** When a radio wave passes through the ionosphere, it contacts the layers of ionized electrons that move according to the Earth's magnetic field. The direction these electrons move will no longer be parallel to the electric field of the wave and therefore the polarization is shifted, in what is called Faraday rotation (θ_F). ;
- **Scintillation effects:** Differences in the atmospheric refractive index may cause scattering and multipath effect, due to the different directions rays may take through the atmosphere. They are detected as variations in amplitude, phase, polarization and angle of arrival of the radio waves. It is often recommended the introduction of a fade margin so atmospheric scintillation can be a tolerated phenomenon.;
- Absorption
- Variation in the direction of arrival
- Propagation delay
- Dispersion
- Frequency change

These effects decrease usually with the increase of the square of the frequency and most serious ones in satellite communications are the polarization rotation and the scintillation effects, and those are the ones that will be treated in this dissertation. [5]

Tropospheric Effects [5] Troposphere is composed by a miscellany of molecules of different compounds, such as hail, raindrops or other atmospheric gases. Radio waves that pass by troposphere will suffer their effects and will be scattered, depolarized, absorbed and therefore attenuated.

Attenuation: As radio waves cross troposphere, radio frequency energy will be converted into thermal energy and that attenuates signal.

Rain attenuation: Ground stations had been chosen in order that the attenuation caused by rainfall will be very punctual. Also, the fact that there are three ground stations makes really difficult that a satellite can not communicate to the ground in all the orbit period.

Gas absorption: Under normal conditions, only oxygen and water vapour have a significant contribution in absorption. Other atmospheric gases only become a problem in very dry air conditions above 70 GHz. Thereby, losses caused by atmospheric absorption vary with frequency and the collection of data already received allows the elaboration of the graphic that follows:

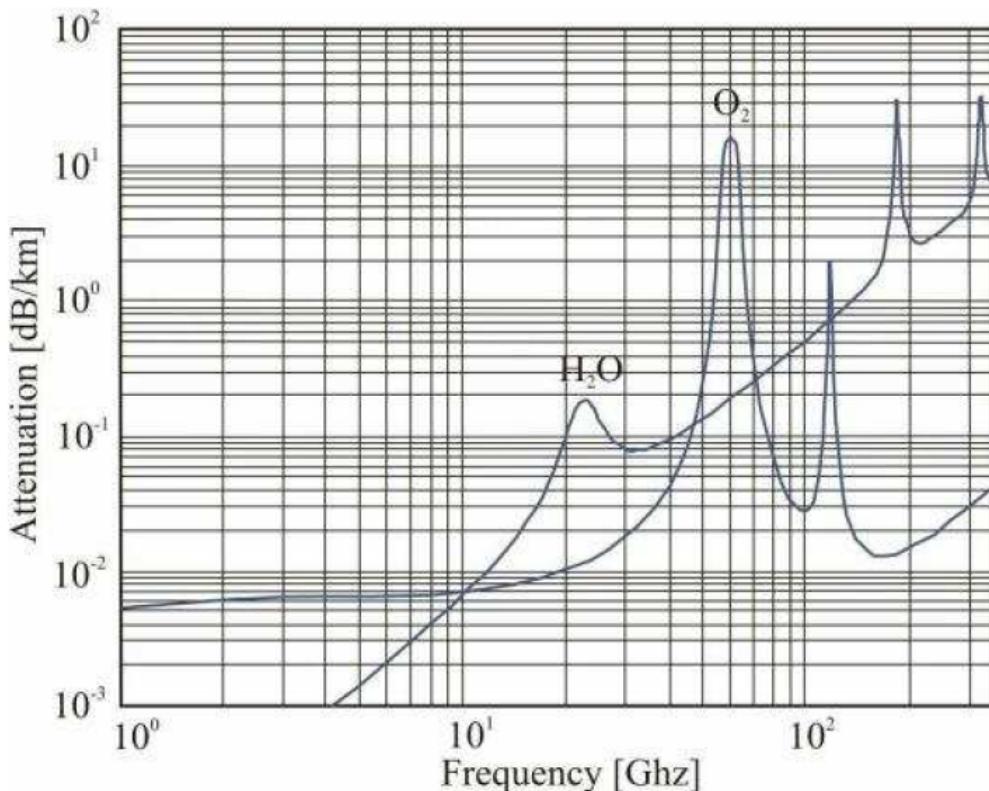


Figure 10.7.2: Specific attenuation for different frequencies [5]

Once these values depend on atmosphere thickness, it becomes necessary to perform all calculations taking into account troposphere's thickest layer (T_{trop}), which has 20 km. It is also mandatory to refer that this graph represents the absorption for a satellite in the zenith, in other words, for an elevation angle of 90° ($\theta = 90^\circ$). For lower angles, the atmospheric absorption (L_{abs}) is given by [5]:

$$L_{abs}(dB) = L_{abs|90^\circ}(dB/km) \operatorname{cosec}(\theta) T_{trop}(km) \quad (10.7.3)$$

For AstreaSAT, $5 \times 10^{-3} dB/km$ attenuation factor is considered for S band due to the O_2 specific attenuation. On the other hand, $4 \times 10^{-3} dB/km$ attenuation factor is considered for X band due to the H_2O and to the O_2 specific attenuations. An study of the critical elevation angle will lately be performed.

For AstreaSAT ground station, communication starts at an elevation angle of $\theta = 10^\circ$ (worst case scenario). Consequently, $\operatorname{cosec}(\theta)$ will go from 5.76 to 1 (best reception case). In that case, we assume:

$$L_{abs} = 2 \cdot 4 \times 10^{-3} \cdot 5.76 \cdot 20 = \mathbf{0.92dB} \quad \text{X band}$$

$$L_{abs} = 5 \times 10^{-3} \cdot 5.76 \cdot 20 = \mathbf{0.58dB} \quad \text{S band}$$

Polarization: Satellite communications use linear and circular polarization, but undesirable effects may transform it into an elliptical polarization. Depolarization may occur when an orthogonal component is created due to the passing of the signal through the ionosphere. There are two ways to measure its effect, cross polarization discrimination (XPD) and polarization isolation (I) [5]. To overcome this attenuation problems a circular polarization is the best option. AstreaSAT patch antennas will mitigate this problem, therefore this losses are considered negligible.

Sky noise: Sky noise is a combination of galactic and atmospheric effects, according as both these factors influence the quality of the signal in the reception. Galactic effects decrease with the increase of frequency. They are due to the addition of the cosmic background radiation and the noise temperature of radio stars, galaxies and nebulae. This value is quite low and a good approximation is **3 K**.

AstreaSAT noise temperature A good approximation based on Fig.10.7.3 is that Galaxy noise is 3K for S band and almost 1K for X band. Furthermore, for the previous

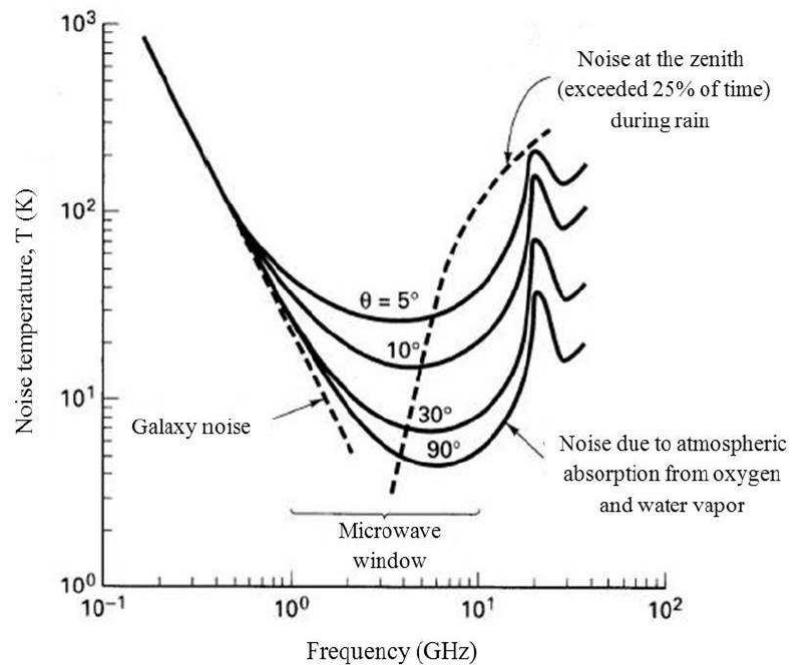


Figure 10.7.3: Galaxy noise influence in noise temperature [5]

worst case scenario stated before $\theta = 10$, noise temperature due to atmospheric absorption is 19K for both bands (S and X).

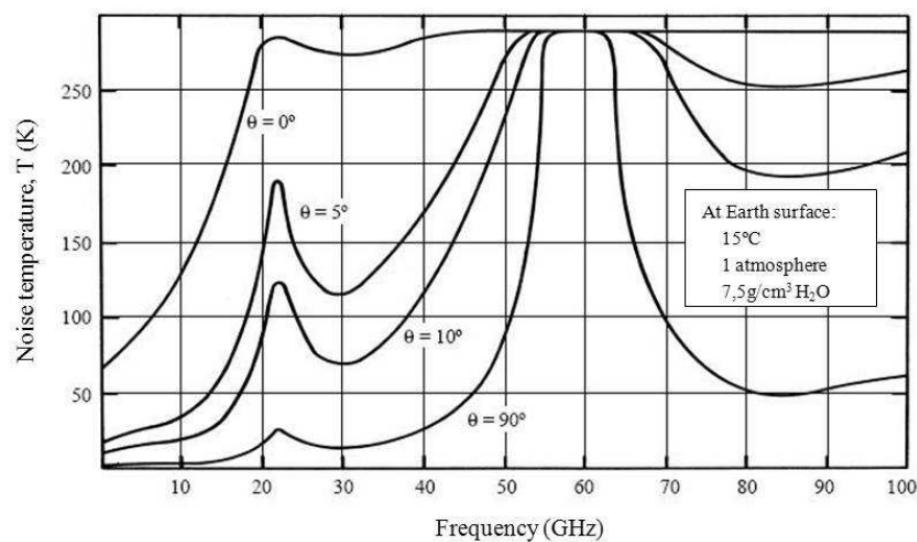


Figure 10.7.4: Noise temperature variation with frequency [5]

Local Effects These effects refer to the proximity of the local ground stations, possible sources that may interfere with the received signal and buildings that may block the signal. If the ground station is on a free external interferences zone, for satellite communications this factor may be negligible.

Pointing Losses

Ideal reception implies that the value for misalignment losses would be 0 dB which means maximum gain at the ground station is achieved when both the transmitter and the receiver antennas are 100% aligned. Realistically it is virtually impossible to achieve a perfect alignment between the antennas of the ground station and the satellite, especially in the case of CubeSats, due to their fast movement of nearly 8000 ms^{-1} .

Antenna misalignment losses (L_{aml}) are calculated using statistical data, so these values are an approximation based on real data observed in several GS. Ergo, these values are not calculated, but estimated. [5]

Based on a estimation from [?] a $L_{aml} = 1dB$ is a good approximation.

Multipath and Fade Margin

Multipath occurs when waves emitted by the transmitter travel along a different path and interfere destructively with waves travelling on a direct line-of-sight path. This is sometimes referred to as signal fading. This phenomenon occurs because waves travelling along different paths may be completely out of phase when they reach the antenna, thereby cancelling each other.

The amount of extra RF power radiated to overcome this phenomenon is referred to as fade margin. The exact amount of fade margin required depends on the desired reliability of the link, but a good rule-of-thumb is 20dB to 30dB.

Local Losses

Equipament Losses

The receiving and emitting equipments also introduces some losses to the signal.

Feeder Losses: Feeder losses occur in the several components between the receiving antenna and the receiver device, such as filters, couplers and waveguides. These losses are similar to the ones which occur also in the emission, between the emitting antenna and the output of the high power amplifier (HPA). [5]

Environment Losses

This item is related to the specific region of the globe where the ground station is placed (equatorial, tropical, polar...). Depending on its latitude, each region has its own characteristics (e.g. temperature, moisture, thickness of atmospheric ice layer...), which may provoke variation in signal reception. [5]

Communications department, had chosen the best locations over the globe, with stable good weather conditions to neglect this fact.

Modulation Technique

Modulation technique is a key consideration. This is the method by which the analogue or digital information is converted to signals at RF frequencies suitable for transmission. Selection of modulation method determines system bandwidth, power efficiency, sensitivity, and complexity. Most of us are familiar with Amplitude Modulation (AM) and Frequency Modulation (FM) because of their widespread use in commercial radio. Phase Modulation is another important technique. It is used in applications such as Global Position System (GPS) receivers and some cellular telephone networks. [6]

For the purposes of link budget analysis, the most important aspect of a given modulation technique is the Signal-to- Noise Ratio (SNR) necessary for a receiver to achieve a specified level of reliability in terms of BER.

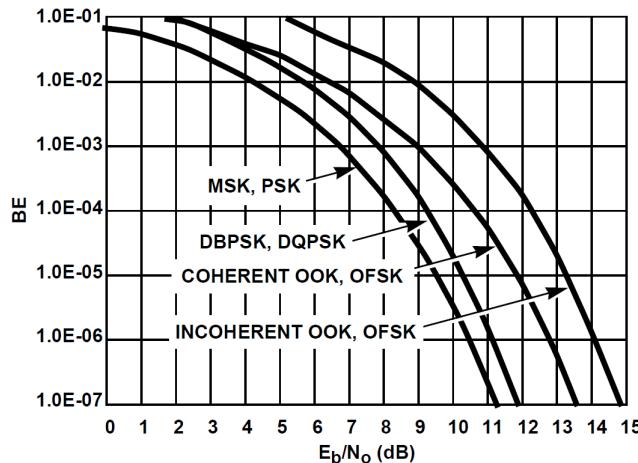


Figure 10.7.5: Probability of bit error for common modulation methods [6]

A graph of E_b/N_o vs BER is shown in Figure 10.7.5. E_b/N_o is a measure of the required energy per bit relative to the noise power. Note that E_b/N_o is independent of the system data rate. In order to convert from E_b/N_o to SNR , the data rate and system bandwidth must be taken into account as shown below:

$$SNR = (E_b/N_o)(R/B_T) \quad (10.7.4)$$

where:

E_b = Energy required per bit of information

N_o = thermal noise in 1Hz of bandwidth

R = system data rate

B_T = system bandwidth

AstreaSAT is equipped with Software Defined Radios, it has the ability to change the modulation methods when its flying, for calculus MSK and PSK modulations will be considered, because of their more restrictive conditions.

System Noise

The system noise temperature (T_S) is the sum of the antenna noise temperature (T_A) and the composite temperature of other components (T_{comp}), according to: [5]

$$T_S = T_A + T_{comp} \quad (10.7.5)$$

T_A may be known if the total attenuation due to rain and gas absorption (A), the temperature of the rain medium (T_m) and the temperature of the cold sky (T_C) are also

known. Then, the following expression may be applied:

$$T_A = T_m (1 - 10^{-A/10}) + T_C 10^{-A/10} \quad (10.7.6)$$

Usually, for clouds it is considered $T_m = 280K$ and for the rain $T_m = 260K$. The sky noise tends to be $T_C = 10K$. Taking into account the values from Fig.10.7.3 and Fig.10.7.2 the following estimation can be made:

$$T_A = 280 \cdot (1 - 10^{-(5 \times 10^{-3})/10}) + 22 \cdot 10^{-(5 \times 10^{-3})/10} = \mathbf{22.29K} \quad \text{S band}$$

$$T_A = 280 \cdot (1 - 10^{-2 \cdot (4 \times 10^{-3})/10}) + 20 \cdot 10^{-2 \cdot (4 \times 10^{-3})/10} = \mathbf{20.48K} \quad \text{X band}$$

According to [5] a good components temperature approximation for a typical ground station is $T_{comp} = 65.5K$.

AstreaSAT system temperature will be considered as $T_S = 22.29 + 65.5 = \mathbf{87.79K}$ for S band and $T_S = 20.48 + 65.5 = \mathbf{85.98K}$ for X band. Since both frequencies are part of the microwave spectrum, we see that system temperatures are pretty much the same.

Channel Noise All objects which have heat emit RF energy in the form of random (Gaussian) noise. The amount of radiation emitted can be calculated by [6]:

$$N = kTB \quad (10.7.7)$$

where:

N = noise power (watts)

k = Boltzman's constant ($1.38 \times 10^{-23} J/K$)

T = system temperature, usually assumed to be 290K

B = channel bandwidth (Hz)

This is the lowest possible noise level for a system with a given physical temperature. For most applications, temperature is typically assumed to be room temperature (290K). Equations 10.7.1 and 10.7.7 demonstrate that RF power and bandwidth can be traded off to achieve a given performance level (as defined by BER). [6]

Link Budget Calculation

Methodology From the expected requirements fixed on the Project Charter, general radio systems parameters will be computed, in order to have a reference to look for the best communications system on board the Astrea satellites. As background, general losses parameters had been calculated on previous sections.

Budget

The most important concern on AstreaSAT link Budget is how far every satellite can emit on the desired frequencies. This is a key factor to know the utility of the modules selected. At least, Project Charter communication requirements must be accomplish.

$$EIRP = P_T - L_T - G_T$$

FRIIS EQUATION + GRAPH RANGE

SENSITIVITY CALCULUS A PARTIR DE LA DE CAPACITAT + NOISE
ADJUDICANT BANDWITH

Budget

System	Cost/unit (€)	Total cost (€)	N. of units
STRUCTURE AND MECHANICS			
Structure	3900	3900	1
Thermal protection	1000	1000	1
Total		4900	
ELECTRIC POWER SYSTEM			
Solar arrays	17000	68000	4
Batteries	6300	12600	2
Power management	16000	16000	1
Total		96600	
PAYLOAD			
Patch antenna	18000 1st unit 7000 others	67000	8
Transceiver inter-satellite	8545	25635	3
Transceiver space to ground	5500	5500	1
Data handling system	5000	5000	1
Antenna Deployable	3000	3000	1
Variable expenses	4000	4000	1
Total		110135	
AOCDS			
Thruster	1350	50000	1
ADACS	280	15000	1
Total		65000	
TOTAL		276635	
TOTAL ESTIMATION		297000	
+Fixed cost	(includes all CubeSats)	150000	

The difference between the total cost and the total estimation is due to the fact that every satellite has to go through a process to be ready for operation. This is, the CubeSat has to be assembled and has to be tested as well to ensure that all the systems are working properly. Thus, an estimation of the costs related with this operation has to be made.

The fixed cost for assembling the satellites will be 150000€(cost of renting the building, the electricity, ...) and an additional cost 20000€/*unit*, which will include the wages of the people assembling and testing the satellite and also other variable costs that may appear in the process, is added to every satellite. Furthermore, this extra 20000€ includes the costs of transport to launch site.

Several options have been studied for assembling and testing the satellite, and the option chosen is *OpenCosmos*. Astrea is committed to encourage the growth of the local economy and we are sure that *OpenCosmos* would be a perfect partner for the mission. They provide companies and individuals with simple and affordable access to space offering integration and testing services.

Astrea satellite Final Configuration

System	Weight/unit (g)	Sizes (mm)	N. of units
STRUCTURE AND MECHANICS			
Structure	304.3	100 x 100 x 300	1
Thermal protection	38	Covers all	1
Total	342.3		
ELECTRIC POWER SYSTEM			
Solar arrays	175	98 x 83 x 8.50	4
Batteries	155	90 x 63 x 12.02	2
Power management	126	92.0 x 88.9 x 20.5	1
Total	1136		
PAYLOAD			
Patch antenna	30	90 x 90 x 4.35	8
Transceiver inter-satellite	16.4	65 x 40 x 6.5	3
Transceiver space to ground	101.5	86 x 86 x 45	1
Data handling system	28.3	65 x 40 x 6.5	1
Antenna Deployable	83	100 x 83 x 6.5	1
Variable	150	-	1
Total	652		

AOCDS			
Thruster	1350	90 x 90 x 95	1
ADACS	506	90 x 90 x 58	1
Total	1856		
TOTAL ESTIMATION	3986.3		

Part V

ANNEX V: Financial and Other Considerations

*"The first rule is to never lose money.
The second rule is to never forget the
first one."*

Warren Buffett

Over this chapter, the **financial study** is going to be performed. The costs and the profits will be analyzed, and some important figures will be acquired.

Moreover, some other important considerations, such as social and security issues or environmental impact will be studied too.

Chapter 11

Financial Study

The different departments have estimated the main costs of the project. It is high time to start performing a deep analysis on the economical solvency of the project. The analysis carried on will be of 12 years. The decision of this amount of years has been done taking into account that every 5 years there is a re-launching of the whole constellation, which means that in year 5, 10, 15... a considerable increase in the costs is to be done. In order to have a good view of the whole project, it has been decided that at least two full cycles had to appear complete (years 0 to 4 and 5 to 9) and also to see the tendency it was recommended to add some more time. This is the reason why the studied is carried on for 12 years.

Up to this point, it is important to determine how this product will be sold, so as to quantify the benefits of the project and be able to determine some figures such as the Pay Back Time or the Net Present value, and be able to make some conclusions.

Selling the product

The aim of the project is to be able to sell to the customers the chance of both sending and receiving data from satellites. Therefore, it seems logic that the price of the product has to be somehow related to the amount of data passed on. Then, there will be a price for every Mbit, either sent or received.

From the Communications Department, there is a limitation of 3 Ground Stations operating, and each one can carry up to 25 Mbits/second. Accepting that those Ground Stations will fully operating the whole year, and calculating the amount of seconds that

there are in a normal year:

$$365 \cdot 24 \cdot 60 \cdot 60 = 31536000s \quad (11.1.1)$$

It can be easily calculated the amount of Mbits that Astrea Constellation is able to either send or receive:

$$31536000 \cdot 75 = 2365200000 Mbits \quad (11.1.2)$$

This means that no more than 2365200000 Mbits can be sold. This is the maximum supply.

But how can the demand be estimated? There is a need to make assumptions.

Estimation of demand

Universities

Firstly, it has been thought that the service offered has great academic interests. In fact, any student could build a satellite with a certain payload, send it to space and then receive data from the satellite at any time thanks to Astrea constellation.

In order to study the possible demand of Mbits, an estimation of the possible universities that would want to use the services has been done. Fortunately, the list of universities that offer studies in the aerospace field goes back a total of 400 schools approximately. Nevertheless, it is highly improbable that all those colleges become clients because not all universities have the same sources or interests. Therefore, the following list presents the number of existing colleges having an aerospace degree in each continent.

Continent	Number of Universities
Europe	124
Asia	138
North America	97
South America	18
Australia	8
Africa	12

Table 11.1.1: Table. List of Universities with Aerospace Degrees

By analyzing this information, it can be determined that the continents with countries with higher PIB have more colleges interested in the space field. It is noticed that Asia is the continent with more colleges because, even if it is mostly poor, it is so big that it has rich countries such as Japan, Korea or China and the United Arab Emirates. Moreover,

Selling the product

Europe and North America are not so extensive but have a higher aerospace culture and interest.

On the basis the service is affordable for many prestigious colleges and it permits to provide their students with the chance to improve their knowledge by doing their own experiments, it has been estimated that about 25 universities will end up contracting Astrea's service in the next years. If we assume that each university would be interested in sending or receiving a total of 985500 Mbits annually, therefore the number of Mbits for universities, annually, will be of 49275000 Mbits.

Particular customers

Another extremely important sector of clients are the private ones. It is harder to make an assumption on the number of Mbits consumed by this sector. Nevertheless, some figures are needed in order to perform a good feasibility study.

According to the Union of Concerned Scientists of the United States of America, right now there are about 1500 satellites orbiting around the Earth. But every day space technology is more affordable and feasible, which leads to think that in the next years a good figure of satellites would be of roughly 2000. Therefore, there are two big groups of potential clients, the ones already orbiting and the ones who will be doing it soon enough.

Of the 1500 already existing satellites, it must be taken into account that they already have their own communication system. Astrea provides them a way of communicating with the satellites almost in real time, which is a great improvement, but as they already have their own method of communicating, they might not find so attractive this new company. Therefore, the demand is that of those 1500 satellites, about 50 would really be interested in using Astrea to send and receive data in real time, because they would really take good profit of it.

Of the 500 which are forecasted to be, it is easier that they are interested in Astrea, because they still have not determined the communication system of their satellite, and therefore they would really find interesting Astrea's service. As Astrea provides a very competitive price, it seems reasonable to think that a good percentage of those satellites would be interested. In order to be conservative, a 50% of those would be potential clients. This means that 250 full operating satellites would use Astrea, and assuming also than the average amount of data that those satellites would either send or receive annually is of 946080 Mbits, the number of Mbits for particular clients, annually, will be of 246375000 Mbits.

It can be checked that the sum of the amounts of Mbits for universities and for particular

clients, which is of 295650000 Mbits, is lower than the maximum amount of Mbits due to the 3 Ground Stations, which is of 2365200000 Mbits. There will not be problem of demand over capacity.

Demand

Taking into account both the universities and the particular clients, and making a conservative assumption, the estimation of the demand, in Mbits, is of a eighth of the maximum capacity of Astrea, this is, 295650000 Mbits annually. Also, in order to simulate the uncertainty of the company during the first years (as years pass, the company gets reputation and therefore its amount of clients also enlarges), a percentage is applied during the first years. This means that first year only a 75% of the potential customers exposed before will be achieved, the second year a 80%, and so on, until the sixth year, in which a 100% is achieved.

Pricing the service

The determination of the price is made upon the feasibility study, in order to get a reasonable Pay Back Time and benefit. Nevertheless, it is a fact that the fare of Astrea service must fulfill a condition: it has to be competitive.

Comparing with some others similar services, in order to provide a competitive fare, it seems reasonable a price per Mbit of no more than 0.5 € per Mbit, as an upper tape.

Economic Feasibility Report

In order to perform the analysis on the economical solvency of the project, next there is a table which contains the main costs of the project, as well as the numerical operations that allow to calculate some important financial parameters, such as the Net Present Value (NPV), the Internal Rate of Return (IRR), the Simple Pay Back Time (PBT), the Updated Pay Back Time (UPBT) and the Break Even Point (BEP). From this data, some conclusions will be drawn.

Firstly, though, there is need to take into account some costs that are not included in the other departments, and which are key to analyzing the costs and benefits.

Previous costs

Engineering hours

The engineering hours, which were specified in the Project Charter, are again synthesized in the following table:

Engineering hours budget	Hours	Labor cost (€)
MANAGEMENT		
Meetings documentation		
Meetings	340	6800
Meetings preparation		
Agendas	10	200
Minutes	10	200
Task Tracking and scheduling		
Project Charter	170	3400
Team tasks monitoring	20	400
WBS and Gantt update	10	200
SATELLITE DEVELOPMENT		
Spacecraft subsystems	180	3600
Payload		
Antenna	40	800
PHDS	50	1000
ORBITAL DESIGN		
Constellation geometry	220	4400
Orbit parameters		
General parameters	120	2400
Drift	100	2000
Legislation	50	1000
LAUNCH SYSTEMS		
Vehicle	60	1200
Satellite deployer	10	200
Replacement strategy	100	2000
OPERATION		
Communication protocol	100	2000
Ground station	80	1600
End of life strategy	80	1600
FINANCIAL PLAN		
Costs		

Engineering hours budget	Hours	Labor cost (€)
Fix		
Maintenance and cost analysis	10	200
Insurance cost analysis	15	300
Administration cost analysis	15	300
Taxes cost analysis	25	500
Variable		
Manufacturing cost report	10	200
Launching cost report	10	200
Income		
Price analysis	25	500
Revenue forecast	25	500
Economic feasibility report	40	800
Marketing Plan	20	400
PROJECT EXHIBITION		
Constellation simulation	30	600
TOTAL	1975	39500

Administrarion costs

It has to be taken in account that administrating the company will require resources and manpower. To budged this costs there have been considered the following factors:

- **Manpower.** It is estimate that it will be needed 6 people working at full time. 3 for the administration of the stations, 2 more for the clients, and an other one for the purchases of new satellites and contracting launchings. The annual salary of each worker would be of 24000 €, which make a total of 144000€
- **Financial costs.** The treasury of the company will require a bank, with its associated costs. This is estimated in 100000€ per year.
- **Local** The place where the administrators will work would cost annually around 10000€.
- **Supplies** The water, electricity, internet and telephone would cost 5000€.

This result in 259000€/year

Taxes

The headquarters of effective management is located in Spanish territory, so it is crucial to take into consideration the corresponding taxes. It is known that any entity that directs and controls all of its activities of effective management in Spanish territory is considered as resident. Consequently by having the residence there they are subjected to the Spanish Corporation Tax. It has to be known that this tax is an annual and proportional tribute belonging to the Spanish tax system that taxes the income of the companies.

Moreover, by following the Article 29 of the Law 27/2014 on the CT it is possible to determine the tax rate that is going to be paid. As a result, for any company located in Catalonia the annual fee to be paid is 25% of annual profits. However, for being a company of new creation, the first two years the tax will be 15% of profits only. It is important to notice that this kind of tax will be paid when the taxpayer begins to obtain benefit, in other words since the enterprise starts to be profitable.

Nevertheless, the study of the taxes is beyond the aim of this project, which is studying the EBITA (Earnings Before Interest, Taxes and Amortization).

Insurance

The responsibility for possible damages or errors is an important aspect to consider. In a satellite, there are different stages that need an insurance because they have possibilities to fail and cause high damages.

From an international point of view, from 1972 there is a treaty, *The Space Liability Convention*, which says that the states must assume their responsibility of their space objects launched in their territories. This liability was created to provide compensation to parties injured by space activities. This treaty was ratified in January 2013 by 89 states and signed but not ratified by 22 states. [?]

As a private company, Astrea should provide a compensation to third people if they are injured by one of the CubeSats. Furthermore, as has been explained in *Social and security considerations*, there are some little risks in different stages of a Cubesat (launch and in-orbit) and it might be advantageous to have economic security contracting a insurance.

Currently, there are a lot of insurance companies that provide their services to space companies and specifically to satellites companies. After a market study, there are two companies to consider, *SpaceCo*, a subsidiary of *Allianz* company and *Marsh*. Both provide the main services that we need: satellite launch and in-orbit insurance and satellite third

party liability insurance.

Finally, *SpaceCo* has been chosen as Astrea insurer company, due to it is considered one of the best insurer for space companies and it has more experiences than others.

This insurer provide a great coverage, in which highlights:

- Launch and commissioning – cover for the launch systems and commissioning equipment.
- In-orbit – operational life insurance for the space satellite.
- In-orbit incentives – cover for the manufacturer's obligation to the client in the event of malfunction or non-performance.
- Liability – cover for third party liability during a launch or in-orbit activities.
- Captive services – assisting cover for companies that self-insure space risks. [?]

The cost of the insurance is around a 20% of cubesat value, which is 297000 €, to pay in the 5 life-years of each. Then, the total cost of the constellation insurance would be:

N. of CubeSats	189
Cost per Cubesat	59400 €
Total cost in 5 years	11226600 €
Cost per year	2245320 €

Economic feasibility study

Finally, the mentioned financial table can be made. The costs are the ones taken from every department, as well as the costs just explained.

As it has been said, upon this financial table, in order to get a good feasibility situation, the pricing of the service is decided to be of 0.1 € per Mbit.

Economic Feasibility Report

TIME	Year 0	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9	Year 10	Year 11	Year 12
INVESTMENT	-4,07												
INCOME													
Percentage (learning curve)	0,75	0,80	0,85	0,90	0,95	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00
Number of Mbits hired	221,737,500,00	236,520,000,00	251,302,500,00	266,085,000,00	280,867,500,00	295,650,000,00	295,650,000,00	295,650,000,00	295,650,000,00	295,650,000,00	295,650,000,00	295,650,000,00	295,650,000,00
Gain (M euros)	22,17	23,65	25,13	26,61	28,09	29,57	29,57	29,57	29,57	29,57	29,57	29,57	29,57
Total	0,00	22,17	23,65	25,13	26,61	28,09	29,57	29,57	29,57	29,57	29,57	29,57	29,57
COSTS													
n planes/year	9	189	0	0	0	9	0	0	0	9	0	0	0
Satellites/year	-0,0395	-0,259	-0,259	-0,259	-0,24532	-0,24532	-0,24532	-0,24532	-0,24532	-0,24532	-0,24532	-0,24532	-0,24532
Engineering hours													
Administration	-2,24532	-2,24532	-2,24532	-2,24532	-2,24532	-2,24532	-2,24532	-2,24532	-2,24532	-2,24532	-2,24532	-2,24532	-2,24532
Insurance													
Web hosting, maint. and promotion	-0,005	-0,005	-0,005	-0,005	-0,005	-0,005	-0,005	-0,005	-0,005	-0,005	-0,005	-0,005	-0,005
Launching													
Planes	-48,256	0,000	0,000	0,000	0,000	-48,256	0,000	0,000	0,000	-48,256	0,000	0,000	0,000
Satellites	-3,024	0,000	0,000	0,000	0,000	-3,024	0,000	0,000	0,000	-3,024	0,000	0,000	0,000
System													
Assembly (individual)	-3,78	0,00	0,00	0,00	0,00	-3,78	0,00	0,00	0,00	-3,78	0,00	0,00	0,00
Structure	-0,15	0,00	0,00	0,00	0,00	-0,15	0,00	0,00	0,00	-0,15	0,00	0,00	-0,15
Thermal protection	-0,737	0,000	0,000	0,000	0,000	-0,74	0,000	0,000	0,000	-0,74	0,000	0,000	0,000
Electric power system	-0,189	0,000	0,000	0,000	0,000	-0,19	0,000	0,000	0,000	-0,19	0,000	0,000	0,000
Solar arrays	-12,852	0,000	0,000	0,000	0,000	-12,85	0,000	0,000	0,000	-12,85	0,000	0,000	0,000
Batteries	-2,381	0,000	0,000	0,000	0,000	-2,38	0,000	0,000	0,000	-2,38	0,000	0,000	0,000
Power management	-3,024	0,000	0,000	0,000	0,000	-3,02	0,000	0,000	0,000	-3,02	0,000	0,000	0,000
Payload													
Patch antenna	-10,595	-0,011	-0,011	-0,011	-0,011	-10,60	0,000	-0,011	-0,011	-10,60	0,000	-0,011	-0,011
Antenna deployment	-0,567	0,000	0,000	0,000	0,000	-0,57	0,000	0,000	0,000	-0,57	0,000	0,000	0,000
Transceiver inter-satellite	-4,845	0,000	0,000	0,000	0,000	-4,85	0,000	0,000	0,000	-4,85	0,000	0,000	0,000
Transceiver space to ground	-1,040	0,000	0,000	0,000	0,000	-1,04	0,000	0,000	0,000	-1,04	0,000	0,000	0,000
Data handling system	-0,945	0,000	0,000	0,000	0,000	-0,95	0,000	0,000	0,000	-0,95	0,000	0,000	0,000
Variable expenses	-0,756	0,000	0,000	0,000	0,000	-0,76	0,000	0,000	0,000	-0,76	0,000	0,000	0,000
AO/DS													
Thruster	-9,450	0,000	0,000	0,000	0,000	-9,45	0,000	0,000	0,000	-9,45	0,000	0,000	0,000
CubeSpace ACDS	-2,835	0,000	0,000	0,000	0,000	-2,84	0,000	0,000	0,000	-2,84	0,000	0,000	0,000
Communications													
Maintenance GS Canada	-0,011	-0,011	-0,011	-0,011	-0,011	-0,011	-0,011	-0,011	-0,011	-0,011	-0,011	-0,011	-0,011
Maintenance GS Scotland (UK)	-0,015	-0,015	-0,015	-0,015	-0,015	-0,015	-0,015	-0,015	-0,015	-0,015	-0,015	-0,015	-0,015
Maintenance GS Malvinas	-0,015	-0,015	-0,015	-0,015	-0,015	-0,015	-0,015	-0,015	-0,015	-0,015	-0,015	-0,015	-0,015
Salaries GS Canada	-0,382	-0,382	-0,382	-0,382	-0,382	-0,382	-0,382	-0,382	-0,382	-0,382	-0,382	-0,382	-0,382
Salaries GS Scotland (UK)	-0,226	-0,226	-0,226	-0,226	-0,226	-0,226	-0,226	-0,226	-0,226	-0,226	-0,226	-0,226	-0,226
Salaries GS Malvinas	-0,082	-0,082	-0,082	-0,082	-0,082	-0,082	-0,082	-0,082	-0,082	-0,082	-0,082	-0,082	-0,082
Salaries MCC	-0,430	-0,430	-0,430	-0,430	-0,430	-0,430	-0,430	-0,430	-0,430	-0,430	-0,430	-0,430	-0,430
Licenses													
TOTAL	-109,54	18,48	19,96	21,44	-31,22	-39,16	25,87	25,87	-0,010	-0,010	-0,010	-0,010	-0,010
CASH FLOW	-113,61	40,66	43,61	46,57	-4,61	-11,07	55,44	55,44	1,30	4,17	55,29	55,29	55,29
DISC CF	-113,61	38,36	38,82	39,10	-3,65	-8,27	38,08	38,08	0,77	2,33	29,13	27,48	27,48
CUM CF	-113,61	-72,95	-29,34	17,23	12,62	1,55	56,99	112,43	167,87	169,18	173,35	228,63	285,92
DIS CUM CF	-113,61	-75,25	-36,44	2,67	-0,99	-9,26	29,82	66,89	101,48	102,25	104,58	133,70	161,18

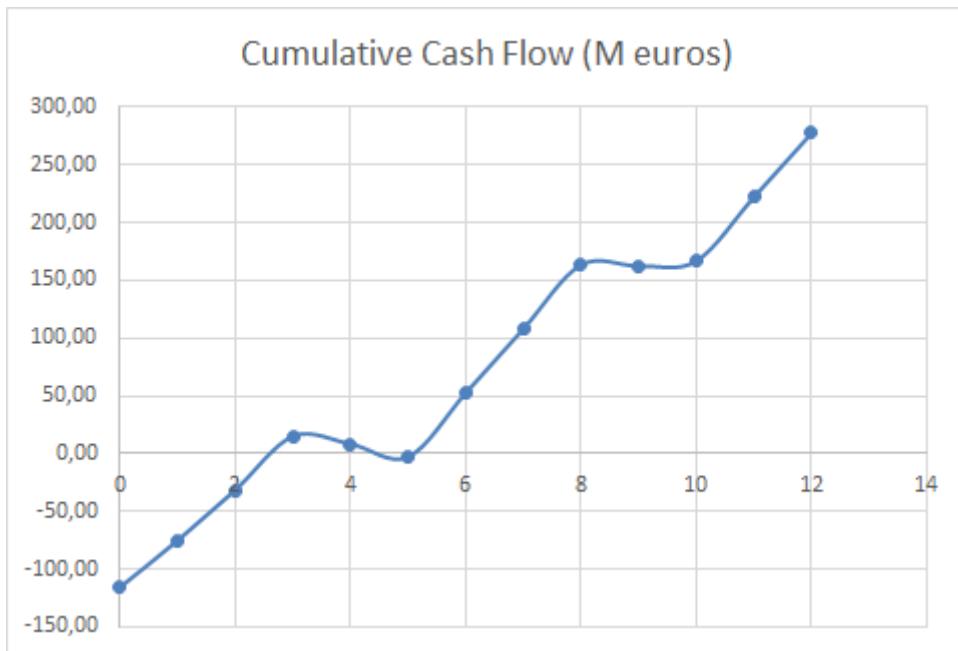
Table 11.2.3: Feasibility Study

Conclusions of the financial study

Some conclusions might be extracted from the previous table, by determining the five key economical parameters: the Pay Back Time, the Updated Pay Back Time, the Break Even Point, the Net Present Value and the Internal Rate of Return.

Pay Back Time (PBT)

The Cumulative Cash Flow can be plotted as follows:



From the shown graphic and also from the table, it can be seen that between years 2 and 3, the Cumulative Cash Flow goes from a negative value to a positive one. Therefore, the Pay Back Time is between those two years. This gives a rough approximation of when will the investment be recouped. To be more precise about it, it can be linearly interpolated:

$$\frac{15.08 - (-31.46)}{3 - 2} = \frac{15.08 - 0}{3 - x} \quad (11.3.1)$$

Solving for x, the result is of a PBT of 2.68 years.

In year 4, the satellites that are going to be launched in year 5 are made. This means an increase in the cost, due to the fabrication and assembly. Moreover, in year 5, there is also a increase, even more significant, because of the re-launching itself of those satellites. This is what causes that interval of time in which the Cumulative Cash Flow does not increase,

but even decreases a bit: that year, the income is slightly smaller than the re-launching costs. This is why the Cumulative Cash Flows decreases a bit. A second Pay Back Time can be found doing an analog calculation:

$$\frac{52.68 - (-2.73)}{6 - 5} = \frac{52.68 - 0}{6 - x} \quad (11.3.2)$$

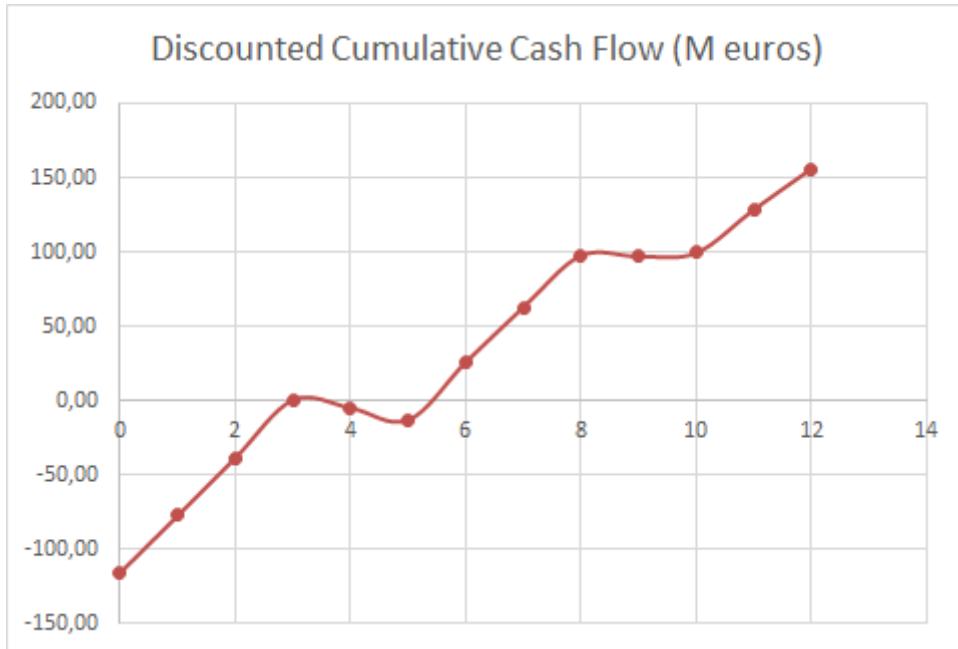
It turns out to be the second Pay Back Time of 5.05 years. Since the investment was done on year 4, this means an actual Pay Back Time of 1.05 years.

In years 9 and 10, the same process takes place again: the fabrication and re-launching of the new satellites. Nevertheless, profit is high enough at this point so that the Cumulative Cash Flow does not get to negative values again.

The value of the first PBT (2.63 years) found seems reasonably acceptable, taking into account that this project requires a great budget, as all space projects do, due to its own nature.

Updated Pay Back Time (UPBT)

Again, the Discounted Cumulative Cash Flow can be plotted as follows:



The discount rate that has been considered is of a 6% annual. It can be seen that between years 2 and 3, this value goes from a negative value to a positive one. Thus, the Updated

Pay Back Time is between those two years. It can be linearly interpolated to gain some precision:

$$\frac{0.52 - (-38.56)}{3 - 2} = \frac{0.52 - 0}{3 - x} \quad (11.3.3)$$

Solving for x, the result is of a UPBT of 2.99 years.

This time, because of the significant costs during year 4 (building and assembling of satellites) and especially year 5 (re-launching of satellites), added to the fact that the discount rate is now being taken into account, it makes the Discounted Cumulative Cash Flow negative again, as can be seen in the graphic. Therefore, there will be another Updated Pay Back Time for the inversion done during years 4 and 5. It might be interesting to find it. It can be seen that it will be between years 5 and 6. Interpolating again:

$$\frac{25.98 - (-13.09)}{6 - 5} = \frac{25.98 - 0}{6 - x} \quad (11.3.4)$$

Solving last time for x, the result if a second UPBT of the year 5.33. Taking into account that this inversion was made during the year 4, it turns out to be an actual UPBT of 1.76 years.

There won't be a third UPBT. In years 9 and 10 there is a big investment again, but by then, the profit is high enough so as to make it possible for the Discounted Cumulative Cash Flow to not become negative any more.

Again, that first value of UPBT (2.93 years) seems reasonably acceptable, because of the nature of the project, within the space sector, a very demanding and expensive one. The second investment required will also have a Updated Pay Back time, in this case of 1.76 years. It is smaller because the investment is not as high as the initial one, and there is already being great benefit.

Break Even Point (BEP)

The Break Even Point is the point at which total cost and total revenue are equal, there is no net loss or gain. This figure represents the sales amount (quantity) required to cover total costs, consisting of both fixed and variable costs to the company. At this point, the total profit is zero.

In Astrea's case, the Break Even Point is the number of Mbits sold the first year so that the Cash Flow of that year is just 0 (or approximately).

By changing manually the parameter "Number of Mbits hired" of first year, it is found that the Break Even Point is of 18375000 Mbits (with this value of Mbits hired the first year, the Cash Flow is approximately 0). This means that under no account there can be less Mbits hired, otherwise, the Cash Flow would be negative and the Cumulative Cash Flow, negative at beginning since first year is fully just invest, would never reach a positive value, generating losses.

From the assumptions of demand already explained, it can be seen that having a greater demand than the BEP is very likely to happen. Thus, the cash flow will be positive and consequently there will be a time in which there is benefit.

Net Present Value (NPV)

From the table, it can be immediately seen that the Net Present Value (for the period of time studied, of 12 years) is of +156.01M€. The Net Present Value is the difference between the present value of cash inflows and the present value of cash outflows over a period of time. It is clearly positive, which indicates that the project earnings generated by the investment exceeds the costs. In other words, it will be profitable. The Net Present Value coincides with the value of the Discounted Cumulative Cash Flow of the twelfth year.

Internal Rate of Return (IRR)

The internal rate of return is the interest rate at which the Net Present Value of all the cashflows is equal to zero. This is used to evaluate the attractiveness of a project. If the Internal Rate of Return of a project exceeds a company's required rate of return, the project is desirable, and if on the other hand the IRR falls below the required rate of return, the project should be rejected.

The studied carried on uses a 6% as the discount rate, and this value gives a positive Net Present Value, as has been already explained. By manually changing the discount rate, it can be achieved that the Net Present Value gets to 0, or very closely. This value of the discount rate is the Internal Rate of Return, and is used to evaluate the attractiveness of a project. In this case, it has been found that the IRR is of 26.80%. The higher the IRR is, the more desirable is to undertake the project. In any case, it must be greater than the actual discount ratio. In this case, not only the IRR is greater, but it is actually a very high rate. Therefore, the project is very attractive, feasibly speaking.

Conclusions of the feasibility study

It has already been seen that the Pay Back Time and the Updated Pay Back Time are both between 2 and 3 years. Taking into account that the space sector is a very exclusive one, in which the investment required is massive, those two parameters seem to be quite reasonable, indicating that the time required to recoup the funds expended in the investment is of less than 3 years. Moreover, since in years 4 and 5 there is again another investment because of the fabrication and re-launching of the satellites, there is a second Updated Pay Back time, in this case of roughly 2 years from the time the investment is done.

Regarding the Break Even Point, it has been determined that the amount of Mbits needed to make cost equal to total revenues is much smaller than the actual demand of data expected. Therefore, the cash flow will be positive and thus there will eventually profit.

Finally, analysing the Net Present Value and the Internal Rate of Return, the first one is positive and considerably big, and the secon one is greater than the actual discount ratio. This means that the investment is very likely to provide a good financial result.

As a final conclusion for this study, it has been clearly seen that the project is economically feasible. Nevertheless, it must not be forgotten than this study is done upon some important assumptions, which provide a certain degree of uncertainty. Nonetheless, the results of the study have been so positive that a slight variation of the hypothesis done could not lead to a unfeasible situation.

Chapter 12

Marketing Plan

Executive Summary

Astrea is the result of an enormous amount work and effort from its 17 co-founders and its name needs to be spread all over the world in order to start selling its services. In order to do that it is important to define the target customers to whom the service offered is going to be sold. Being the latter clear, it's essential to point out what does Astrea offer that makes it stand out from the rest of companies in the sector, that is, making an assessment of the strong points of the company. Moreover, it is necessary to establish the price at which the service is going to be sold to the customers and defining the position of the company among its competitors in the sector.

Of course none of the above would make sense without defining a distribution plan in which the way customers buy from us is defined. In addition to that, the marketing materials used also have to be defined along with the online marketing strategy.

A conversion strategy has to be defined too, that is, defining a way to turn prospective customers into paying ones. Finally, possible partnerships or future partnership plans will be assessed.

Target Customers

One of the most important items when it comes to selling a product or service is to whom it may be of interest. Since the service sold is essentially a communication bridge between satellite-to-satellite, Earth-to-satellite or Earth-to-Earth, it is well obvious that

Unique Selling Proposition

the average customer is not going to be an average consumer.

Instead the service offered is projected towards public or private institutions such as aerospace universities who would like to execute experiments which require a reliable communication between their own spacecraft and their ground stations. Also towards start-up enterprises who would like to enter into the aerospace industry and need Astrea's infrastructure to accomplish their own projects.

In addition to all of the above, the service is also targeted towards space agencies who plan on doing pilot missions with which Astrea could help with. Also aerospace enterprises who nonetheless would like to test their technologies and need real time feedback from them. Finally another targeted sector would be the communications enterprises who would like to acquire real time information from Earth's surface or outer space.

Unique Selling Proposition

The USP is, as the title appoints, what Astrea has to offer that sets it apart from other companies in its sector. Everyone in Astrea knows what the company is capable of and what it can offer and this is no more and no less than:

- Global signal coverage: Astrea's constellation covers every single spot on Earth's surface. This means that every ground station will have full-time signal coverage.
- Ground station support: Astrea offers ground stations to its customers. For advanced users, custom ground stations are also available.
- High reliability: Astrea's constellation is robust. Therefore, reliability is guaranteed.
- Cheapest price on sector: Astrea brings global communication to customers at the lowest and most affordable price.

Pricing & Positioning Strategy

The communication service Astrea offers is set to a price of 0.1€/Mb. Since there are no other companies offering the same kind of service it is not possible to make a comparison as of now.

Distribution Plan

Since what Astrea offers is not a conventional service, people will not be able to purchase it directly. Instead, we use our website to get people to know what Astrea does as well as a way for our customers to get in touch with us. When a customer contacts us we provide them with all the necessary information on how to properly use our systems. Once the contract is made they can start using our communication systems right away. The payment is done monthly much like a regular mobile carrier. Customers will get their invoices with their total data consumption and price.

Marketing Materials

The marketing materials we count on are:

- A website: <http://astrea.upcprogram.space/>
- An informative and encouraging video.
- Brochures.
- A poster.

Online Marketing Strategy

Given the fact that our distribution plan is executed in an essentially online manner, it makes sense to elaborate an Online Marketing Strategy. The key components to our online marketing strategy are:

1. Keyword Strategy: it is important to identify the keywords to optimize our website for. In our case the keywords would be: "Astrea", "constellation", "reliability", "CubeSat" and "communication".
2. Search Engine Optimization: document updates will be made to the website in order to appear more prominently in online search engines.
3. Social Media Strategy: nowadays it is crucial to be in the social media. The world is permanently connected through the social media and it can be one of most powerful ways to show off what we've produced. Therefore, Astrea will have its own Twitter, Instagram and Facebook accounts.

Conversion Strategy

The technique we use to turn prospective customers into actual paying customers will be showing testimonials from actual customers who were satisfied with our service in our website. In addition to that, we will post in our website every successful project we provide service to. This will show the reliability of the service to the insecure customers and hopefully turn them into actual customers

Joint Ventures & Partnerships

Right at its beginning Astrea does not count on any Joint Ventures nor Partnerships with other enterprises. Nevertheless, Astrea is open to future partnerships with businesses who would like to work in collaboration with us.

Chapter 13

Environmental Impact Study

Introduction

This chapter pretends to assess the environmental consequences (positive and negative) of developing the project. The target of this study is to identify, predict, evaluate and mitigate the biophysical and social negative effects that the project could generate during the execution of it.

Ground Stations

At first sight the Ground Stations do not represent any environmental problem. The main factor that has to be taken into account is the placement of the stations. They have to be located in a place where they do not interfere with the ecosystem. The placement of the stations has to be adequate with the environmental legislation of the countries.

Satellites

For analysing the impact of the satellites it has to be studied the possible environmental impact during the fabrication and during the orbital life. The fabrication of the satellite components is externalized, and they are bought as products of these companies. All these products have been tested and checked, complying all regulations. The fabrication of these products does not involve an environmental damage. During the orbital performance of the satellites, it has to be taken into account whether or not they would become orbital waste. The satellites are designed to burn out in the atmosphere at the end of their useful

life. This burnt should not leave any solid residue that could precipice over the surface. The deorbit would be forced and controlled by the propulsion system of the satellite. In the case that this system fails, given that they will orbit in a LEO, they will be deorbited and burnt out naturally in a period around 5 years.

Launch system

The most critical part of the entire process, in environmental terms, is the launch of the satellites. For this reason the main relevance in this report is given to the spacecraft that will put the satellites in orbit, the Electron rocket of Rocket-Lab. The company operate in New Zealand, and for doing it, the Ministry for the Environment make an accurate study of the environmental impact of the Electron launching. The entire document can be seen at [?]. In this document are analysed the critical components of the spacecraft:

- **Structure.** The primary structural material is carbon fibre reinforced polymer. The carbon filaments are chemically inert and do not react to seawater.
- **Propellants.** Liquid oxygen and kerosene (RP-1 analogue) propellants are used on both the first and second stages of the launch vehicle. Liquid oxygen, if released to the atmosphere, rapidly boils and returns to the atmosphere as gaseous oxygen. RP-1 kerosene is a highly refined grade of hydrocarbon with low density, a thin surface film and rapid evaporation.
- **Pneumatics.** All inflight pneumatic systems use stored pressurised cold gases to provide tank pressurisation, cold-gas manoeuvring thrust in space, and for stage separation mechanisms. All gases are non-toxic.
- **Engines.** The launch vehicle uses nine engines for stage 1 and a single engine for stage 2. The engines are constructed of inconel, an inert high performance, corrosion resistant nickel alloy. At stage 1 separation, the thrust section is likely to separate from the stage, return to Earth's surface and land in the Exclusive Economical Zone.
- **Batteries.** The first stage batteries are highly likely to burn-up before returning to Earth's surface. The stage 2 batteries will entirely burn-up downrange, with only the first battery potentially landing in the EEZ. The batteries are lithium-based, and contain no lead, acid, mercury, cadmium, or other toxic heavy metals.

The document also evaluates the following possible risks:

- **Risk of toxic effects.** The toxic effects of the materials comprising stage 1, the fairings and the two stage 2 LithiumIon batteries were assessed as low at all levels of launch activity.

- **Risk of ingestion of materials and provision of floating shelter.** Floating jettisoned materials as shelter for pelagic organisms and the ingestion of jettisoned materials were both evaluated as having low ecological risk at all levels of launch activity.
- **Environmental effect of the displacement of fishing activities.** For the demersal fish and mobile invertebrate community, marine mammals and seabirds, the effects of fishing displacement would be low because these populations could also be impacted in the areas to which fishing is displaced. In the eastern jettison zone there is less fishing activity so the consequences of fishing displacement on the seabed community, demersal fish and mobile invertebrates, marine mammals and seabirds are negligible, reaching minor impacts after 1000 or more launches.
- **Effect of the provision of hard substrates.** Another potential positive outcome for seafloor biota requiring hard substrates is that the jettisoned materials would provide further attachment sites. However, even after 10,000 launches this would provide only about 50 ha of additional attachment surface, leading to a moderate benefit at most.
- **Disturbance to marine fauna.** Noise and disturbance to marine fauna above and below water is a potential consequence of the jettisoned materials falling into the jettison zone. The chance of repeated disturbance to the same individuals or groups of marine mammals or seabirds increases with the number of launches. This was assessed as a low risk for up to 100 launches over two years, a moderate risk for up to 1000 launches over almost 20 years, and a high risk for up to 10,000 launches over almost 200 years.
- **Risk of direct strikes causing mortality to components of the ecosystem.** Direct strikes causing mortality are a low risk for all components of the ecosystem up to 1000 launches over an almost 20 year period. Direct strikes reach moderate levels of risk for the benthic invertebrate community, sensitive benthic environments, and a rare threatened species, the magenta petrel, after 10,000 launches over a period of almost 200 years.
- **Risk of smothering of sea floor organisms.** Smothering the feeding or respiratory structures of sea floor organisms by jettisoned materials was assessed as a low risk for all levels of launches up to 1000 launches and a moderate risk by 10,000 launches. This is likely to be a factor principally in areas of hard substrate where the jettisoned materials are unlikely to become buried in sediment so will be important principally on the Bounty Platform.

New Zealand legislation does not yet regulate these activities, since Rocket Lab is the first company that pretends to operate rocket launchings in the territory. The study concludes

Launch system

that the environmental effects of the activity may become significant after 10,000 launches, this would take 200 years to reach at one launch per week. The regulatory regime would have been reviewed well before this number of launches. During this review the Ministry allows the activity of the company.

Chapter 14

Social and Security Considerations

Social and security considerations

The potential of the CubeSats is very high and they might be the future of satellites. Their low cost and the easiness to construct them, compared to large satellites, make them accessible to countries with fewer resources, universities and people in general, making them able to explore the space and to pursue different missions. The assembly of a CubeSat is not very complicated but requires a minimum knowledge about the subject; in other words, now "you've got a user manual, a datasheet and a 3D model that you can download, and you've got an online shop where people can buy their power systems, etc with their credit card" [?].

This project is based on the design of a satellite constellation dedicated to communications relay between LEO satellites and between LEO satellites and the ground. This project is helping to develop the CubeSat industry and its use and it will demonstrate that these small satellites can carry out different missions that were previously done only by large satellites, as for example the communication.

Currently, the constellations of CubeSats dedicated to the communication are in development and the market is not very extensive, this is why this project, and the global coverage that it provides, could have a privileged place in this industry. The main commitment that this project has with the customers is to ensure that they will be able to communicate with any part of the world without problems.

Another important aspect to consider is that the constellation will provide total privacy to the customers, ensuring that they make a correct use of it and avoiding that third people interfering in the communication.

In relation to security, it must ensure the proper functioning of the constellation. To do this, it must be considered three main factors, where CubeSats could be in danger: the launch of the payload, the permanence of the CubeSats in space and the ground stations.

The launch stage is one of the most important, because it is where the mission has more probability to fail. In the next figure can be observed the success rate of orbital launches in the last 57 years. In 2014, there were a total of 92 unmanned launches and only 4 of them were failed. This indicates that the fail rate is only a 4,34 %, which is very low.

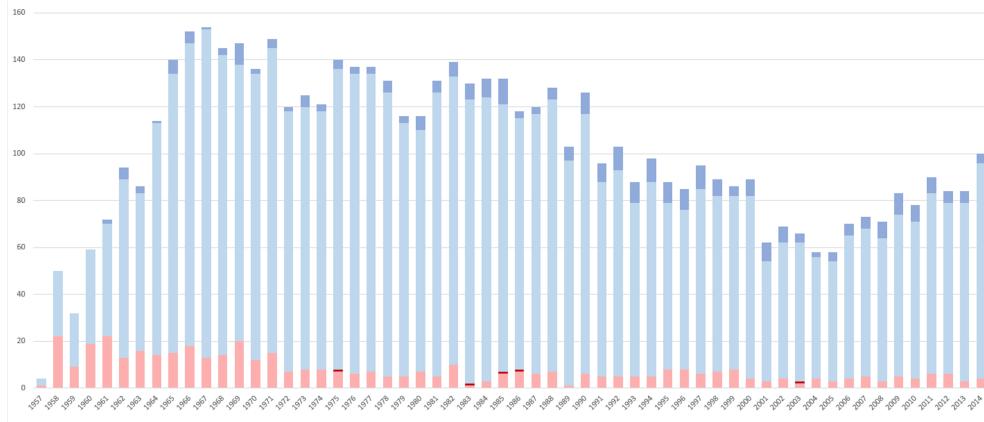


Figure 14.1.1: Orbital Launch Summary by Year

Once the constellation is in orbit, CubeSats can find dangers how colliding with other satellites or with space debris. The distances between most satellites is around hundreds of miles and there is not danger of collision, but the movement of space debris is unpredictable. In order to avoid this space debris, a CubeSat can perform a Debris Avoidance Manoeuvre (DAM). The responsible to control these fragmentation debris is *The United States Space Surveillance Network*. It consists of ground-based radars and optical sensors at 25 sites worldwide and Currently tracks more than 8000 orbiting objects.

Finally, the ground stations are a key element for the correct operation of the constellation and they must prevented from stop working. To do this, each ground station will have its operator, to control the operation of the installation, and a security system, to avoid intrusions.

Legislation

The legislation concerning activities related to space is the Space Law. Space Law is an international law comprised of international treaties and agreements. Its most important rules are the five international treaties, which have been developed under the supervision of the United Nations. The body that promotes these regulations is the United Nations Office for Outer Space Affairs (UNOOSA).

The international law is only applicable to the states that are parties to the treaties. According to the Outer Space Treaty, states are responsible for their national space activities, public or private. For this reason, each state usually adopts its national space regulations.

In the case of the Astrea constellation, since the company is based in Spain (a

Legislation

party of the Space Law), the current legislation is the *Real Decreto 278/1995* of 24 February 1995. According to this Royal Decree, the objects launched from Spain or whose launch has been promoted by Spain, should be registered in the *Registro Español de Objetos Espaciales Lanzados al Espacio Ultraterrestre* (Spanish Registry of Objects Launched into Outer Space). The necessary data to register the satellite must be provided to the *Dirección General de Tecnología Industrial del Ministerio de Industria y Energía* (Department of Industrial Technology of the Ministry of Industry and Energy). This department will notify the registry to the Secretary-General of the United Nations.

The registration has to contain the following data:

- a) Name of launching State or States;
- b) An appropriate designator of the space object or its registration number;
- c) Date and territory or location of launch;
- d) Basic orbital parameters, including:
 - I) Nodal period;
 - II) Inclination;
 - III) Apogee;
 - IV) Perigee;
- e) General function of the space object.

and any other useful information. For example, in the case of one of the Astrea satellites, the registration will be:

- a) Spain
- b) AstreaSAT 1
- c) 22 February 2018,
- d) Basic orbital parameters: Low Earth Orbit
 - I) 95,4815 minutes
 - II) 72 degrees
 - III) 6.913,0 km
 - IV) 6.913,0 km
- e) CubeSat 3U, part of the communications constellation Astrea

Part VI

ANNEX VI: Matlab Codes

Satellite Footprint

```

1 %----ASTREA CONSTELLATION----
2 %PROJECTS - 220028
3 %Aerospace Engineering Bachelor's Degree
4 %ESEIAAT - UPC
5 %Autumn 2016-2017
6
7 % ORBIT DESIGN TEAM
8 % COMPUTATION OF A SATELLITE FOOTPRINT
9
10 clc
11 clear all
12 close all
13
14 %% PHYSICAL CONSTANTS AND PARAMETERS
15
16 Re = 6378;           %Earth's Radius [Km]
17 Se = 4*pi*Re^2;      %Earth's Surface [Km^2]
18 h = 500:100:1000;    %Satellte height [Km]
19 eo = 0:5:40;         %Elevation angle [deg]
20
21 %% SOLVER
22
23 for i = 1:length(h)
24     for j = 1:length(eo)
25
26         d(i,j)= Re*(sqrt(((h(i)+Re)/Re)^2-(cosd(eo(j)))^2 )-sind(eo(j)));
27         Bo(i,j) = asind( d(i,j)*cosd(eo(j)) / (h(i)+Re) );
28
29         S(i,j) = 2 * pi * Re^2 * ( 1-cosd(Bo(i,j)) );
30
31         R(i,j) = sqrt( d(i,j)^2 - h(i)^2 );
32
33         %Satellite coverage expressed as a fraction of Earth's Area (%)
34 Cov(i,j) = ( S(i,j) / Se )*100;
35
36         %Number of satellites needed
37         nsat(i,j) = ( Se / S(i,j) );
38
39     end
40 end
41
42 %% PLOTS
43
44 figure
45 for k = 1:length(h)
46     plot ( eo , Cov(k,:) )

```

Minimum Plane Inclination

```

47      hold on
48 end
49
50 title('Coverage vs Elevation')
51 xlabel('Elevation [deg]') % x-axis label
52 ylabel('Coverage [%]') % y-axis label
53 legend(num2str(h(1)),num2str(h(2)),num2str(h(3)),...
54     num2str(h(4)),num2str(h(5)),num2str(h(6)))
55
56 figure
57 for k = 1:length(h)
58     plot ( eo , nsat(k,:) )
59     legend ('h(j)')
60     hold on
61 end
62
63 title('Num.Satellites vs Elevation')
64 xlabel('Elevation [deg]') % x-axis label
65 ylabel('Num.Satellites') % y-axis label
66 legend(num2str(h(1)),num2str(h(2)),num2str(h(3)),...
67     num2str(h(4)),num2str(h(5)),num2str(h(6)))
68
69 figure
70 for k = 1:length(h)
71     plot ( eo , 2*Bo(k,:) )
72     hold on
73 end
74
75 title('Angle vs Elevation')
76 xlabel('Elevation [deg]') % x-axis label
77 ylabel('Angle between satellites[deg]') % y-axis label
78 legend(num2str(h(1)),num2str(h(2)),num2str(h(3)),...
79     num2str(h(4)),num2str(h(5)),num2str(h(6)))

```

Minimum Plane Inclination

```

1 %----ASTREA CONSTELLATION----
2 %PROJECTS - 220028
3 %Aerospace Engineering Bachelor's Degree
4 %ESEIAAT - UPC
5 %Autumn 2016-2017
6
7 % ORBIT DESIGN TEAM
8 %%%%%% %%%%%% %%%%%% %%%%%% %%%%%% %%%%%% %%%%%% %%%%%%
9 % MINIMUM INCLINATION - To provide Full coverage %
10 %%%%%% %%%%%% %%%%%% %%%%%% %%%%%% %%%%%% %%%%%% %%%%%%

```

Minimum Plane Inclination

```

11
12 %PROBLEM:
13 % Given: - Minimum Elevation over the horizon to contact the satellite
14 %           - Height of the orbit
15 % Compute the minimum elevation to ensure visual contact
16 clear; clc;
17
18 %% Key variable
19 min_elevation_pole=5; %Initially set by @lfore as 32;
20
21 %% Previous Calculation: Visibility(latitude)
22
23 R = 6371;
24 N = 180;
25 deg = 180;
26 x = linspace(0,90,N);
27
28 %%% Minimum angle of elevation due to atmospheric conditions at given
29 %%% latitudes. 0 km represents the poles whereas 6371 km represents the
30 %%% Earth's equator taking as reference point the south pole.
31
32 elvlat = zeros (1,deg);
33 for i = 1:deg/5
34     elvlat(i) = min_elevation_pole-(min_elevation_pole-15)/(2*(90-75))*i;
35 end
36 for i = deg/5+1:4*deg/10
37     elvlat(i) = elvlat(deg/5);
38 end
39 for i = 4*deg/10+1:6*deg/10
40     elvlat(i) = elvlat(2*deg/5)+3/15*(i-4*deg/10);
41 end
42 for i = 6*deg/10+1:8*deg/10
43     elvlat(i) = elvlat(6*deg/10)-3/15*(i-6*deg/10);
44 end
45 for i = 8*deg/10+1:10*deg/10
46     elvlat(i) = elvlat(8*deg/10)-1/15*(i-8*deg/10);
47 end
48 elvlat=flipr(elvlat); %Sets the first value to the value in the equator
49                         %The first value matches 0 latitude
50
51 %% Minimum i computation
52
53 h = 400:100:1000;    %Satelllte height [Km]
54 L = 0:5:90;           %Latitude angle [deg]
55 e = (interp1q(x',elvlat',L'))'; %Minimum elevations interpolation [deg]
56
57 figure(1)
58 subplot(1,2,1)
59 plot(x,elvlat)
60 subplot(1,2,2)

```

Minimum Plane Inclination

```

61 title('Interpolation Verification')
62 plot(L,e)
63
64 inc=zeros(length(h),length(L)); %Inclinations preallocation
65
66 for i = 1:length(h)
67     for j = 1:length(L)
68
69         A=cosd(e(j))/(1+h(i)/R);
70         theta=acosd(A)-e(j); %Earth Central Angle
71         inc(i,j)=L(j)-theta;
72         if inc(i,j)<0
73             inc(i,j)=0;
74         end
75     end
76 end
77
78 %% 3. Results Plotting
79
80 figure(2)
81 colors=['r','b','y','g','m','k','c'];
82 for k = 1:length(h)
83     hold on
84     plot ( L , inc(k,:),colors(k))
85 end
86
87 grid on
88 title('Minimum inclination required to fulfill global coverage')
89 xlabel('Latitude [deg]')
90 ylabel('Inclination [deg]')
91 legend(num2str(h(1)),num2str(h(2)),num2str(h(3)),...
92 num2str(h(4)),num2str(h(5)),num2str(h(6)),num2str(h(7)))
93
94 %% Bonus!!!
95
96 L=90;
97 e=5.33;
98 h=500:1:600;
99 inc=zeros(1,length(h));
100 for i = 1:length(h)
101     A=cosd(e)/(1+h(i)/R);
102     theta=acosd(A)-e; %Earth Central Angle
103     inc(i)=L-theta;
104     if inc(i)<0
105         inc(i)=0;
106     end
107 end
108
109 figure(3)
110 plot(h,inc)

```

```

111 xlabel('Heights')
112 ylabel('Inclination')
113 grid on
114 axis([min(h) max(h) 45 90])

```

Satellite Number Computation for Polar Orbits

```

1 %----ASTREA CONSTELLATION----
2 %PROJECTS - 220028
3 %Aerospace Engineering Bachelor's Degree
4 %ESEIAAT - UPC
5 %Autumn 2016-2017
6
7 % ORBIT DESIGN TEAM
8 % POLAR ORBITS Number of satellites computation
9
10 %PROBLEM:
11 % Given: - Elevation over the horizon to contact the satellite
12 %           - Height of the orbit
13 % Compute the final number of satellites
14 % Through the "Streets of coverage" method.
15
16 clear; clc;
17
18 %% 1. Input data
19 % PHYSICAL CONSTANTS AND PARAMETERS
20
21 Re = 6378;           %Earth's Radius [Km]
22 Se = 4*pi*Re^2;     %Earth's Surface [Km^2]
23 h = 500:20:600;     %Satellte height [Km]
24 eo = 20;            %Elevation angle [deg]
25
26 %% 2. Number of satellites computation
27
28 d=zeros(length(h),length(eo));
29 nsats_opt=d;
30
31 for i = 1:length(h)
32     for j = 1:length(eo)
33
34         d(i,j)= Re*(sqrt(((h(i)+Re)/Re)^2-(cosd(eo(j)))^2)-sind(eo(j)));
35         Bo = asind( d(i,j)*cosd(eo(j)) / (h(i)+Re) );
36         Sup = 2 * pi * Re^2 * ( 1-cosd(Bo) );
37
38         Nspp_min=ceil(360/(2*Bo));      %Number of satellites per plain
39         Nsat spp=Nspp_min:1:Nspp_min+50; %Array of sats/plain to optimize

```

```

40
41         S=360./Nsatspp;
42
43         Lstreet=acosd(cosd(Bo)./cosd(S/2));
44
45         DmaxS=Lstreet+Bo;
46         DmaxO=2*Lstreet;
47
48         Nplains=ceil(1+((180-DmaxO)./DmaxS));
49         Nsats=Nplains.*Nsatspp;
50         [row,col]=find(min(Nplains));
51         Nplains_opt(i,j)=Nplains(row,col);
52         nsats_opt(i,j)=Nsats(row,col);
53
54         %Number of satellites needed
55         nsat(i,j) = ( Se / Sup );
56
57     end
58 end
59
60 %% 3. Results Plotting
61
62 figure(2)
63 colors=['r','b','y','g','m','k','c'];
64 for k = 1:length(eo)
65     subplot(1,2,1)
66     hold on
67     semilogy ( h , nsats_opt(:,k),colors(k))
68     subplot(1,2,2)
69     hold on
70     semilogy ( h , Nplains_opt(:,k),colors(k))
71 end
72
73 subplot(1,2,1)
74 title('Num.Sats vs Height')
75 xlabel('Height [km]') % x-axis label
76 ylabel('Num.Satellites') % y-axis label
77 %legend(num2str(eo(1)),num2str(eo(2)),num2str(eo(3)),...
78 %      num2str(eo(4)),num2str(eo(5)),num2str(eo(6)),num2str(eo(7)))
79 axis([400 900 0 1000])
80 grid on
81
82 subplot(1,2,2)
83 title('Num.Planes vs Height')
84 xlabel('Height [km]') % x-axis label
85 ylabel('Num of Orbital Planes') % y-axis label
86 % legend(num2str(eo(1)),num2str(eo(2)),num2str(eo(3)),...
87 %      num2str(eo(4)),num2str(eo(5)),num2str(eo(6)),num2str(eo(7)))
88 axis([400 900 0 30])
89 grid on

```

Orbit Parameters

```

90
91 %% Single detailed analysis
92
93 figure(1)
94 plot(h,nsats_opt)
95 title('Num.Sats vs Height - Streets of coverage Method')
96 xlabel('Height [km]') % x-axis label
97 ylabel('Num.Satellites') % y-axis label
98 grid on
99
100 %% Multianalysis variation with height
101
102 figure(3)
103 colors=['r','b','y','g','m','k'];
104 for k = 1:length(h)
105     subplot(1,2,1)
106     hold on
107     plot ( eo , nsats_opt(k,:),colors(k))
108     subplot(1,2,2)
109     hold on
110     plot ( eo , Nplains_opt(k,:),colors(k))
111 end
112
113 subplot(1,2,1)
114 title('Num.Sats vs Elevation - Streets of coverage Method')
115 xlabel('Elevation [deg]') % x-axis label
116 ylabel('Num.Satellites') % y-axis label
117 legend(num2str(h(1)),num2str(h(2)),num2str(h(3)),...
118     num2str(h(4)),num2str(h(5)),num2str(h(6)))
119 axis([0 40 0 700])
120 grid on
121
122 subplot(1,2,2)
123 title('Num.Planes vs Elevation - Surfaces Method')
124 xlabel('Elevation [deg]') % x-axis label
125 ylabel('Num.Orbital Planes') % y-axis label
126 legend(num2str(h(1)),num2str(h(2)),num2str(h(3)),...
127     num2str(h(4)),num2str(h(5)),num2str(h(6)))
128 axis([0 40 0 30])
129 grid on

```

Orbit Parameters

```

1 %----ASTREA CONSTELLATION----
2 %PROJECTS - 220028
3 %Aerospace Engineering Bachelor's Degree

```

Orbit Parameters

```

4 %ESEIAAT - UPC
5 %Autumn 2016-2017
6
7 % ORBIT DESIGN TEAM
8 % ORBIT PARAMETERS
9
10 % This routine calculates the minimum number of planes and satellites
11 % to guarantee global coverage.
12 %
13 % _v2 --> Computes angles with arccosine
14 % _v3 --> Also iterates in f
15
16 clc
17 clear all
18 close all
19
20 tic
21
22 %% DATA INPUT
23
24 Re = 6371; %Earth's Radius [Km]
25 Se = 4*pi*Re^2; %Earth's Surface [Km^2]
26 h = 500:5:600; %Height vector [km]
27 in = 75:3:90; %Inclination vector [deg]
28 pmin = 5; p=12; %Minimum number of planes
29 pmax = 20; %Maximum number of planes
30 sppmin = 10; spp=10; %Minimum number of satellites each plane
31 sppmax = 24; %Maximum number of satellites each plane
32 typeWD = 2; %Defines:
33 % 1- Semi-Walker-Delta
34 % 2- 3/4 of Walker-Delta
35 % 3- Full Walker-Delta
36 plaunch = 5.76e6; %Launch price
37 psat = 250e3; %Price per satellite
38 eo = 20; %Vison angle
39 q=0; %Variable used as counter
40 nplanes_win=0;
41 %Boolean, Indicates a succesful combination with that number of planes
42
43 %% COMPUTATIONS
44 %result=zeros(6,100);
45
46 for j=1:length(h)
47     fprintf('\n\nH = %g km',h(j))
48     Bo = visibleangle(h(j),eo); %Footprint angle
49
50     for k=1:length(in)
51         fprintf('\ni=%g: ',in(k))
52
53         for p=pmin:pmax

```

Orbit Parameters

```

54         F=0:1:p-1; nF=length(F); anglesp_f=zeros(1,nF);
55
56     for spp=sppmin:sppmax
57         angles = 360/spp; %Angle between satellites of same plane
58
59         for kf=1:nF
60             % We look for the optimum f for this spp,npp,inc,h
61             anglesp_f(kf)=distance_opt_f(in(k),h(j),p,spp,typeWD,F(kf));
62             %Angle between satellites of different planes
63         end
64
65         [anglesp,kf_min]=min(anglesp_f);
66
67         if (angles <= 2*Bo) && (anglesp <= Bo)
68
69             q=q+1;
70             result(:,q)=[h(j) in(k) spp p spp*p F(kf_min)];
71             fprintf(['Solution %g: h=%gkm - i=%g - ...
72                     %gspp - %gpplanes - %g sats - f=%g'],q,result(:,q))
73             nplanes_win=1;
74             break %Stop iteration in satellites per plain
75
76         end
77
78     end
79     if nplanes_win      %If a combination with that num of planes
80         nplanes_win=0; %works, then jump to the next inclination
81         break
82     end
83     end
84 end
85 end
86
87 %% Optimum Results
88 % Minimum number of cubesats
89 numsat = result (5,1:q);
90 [minsat,index] = min(numsat);
91
92 disp(sprintf('\nMINIMUM SATELLITES\nheight: %d', result(1,index)))
93 disp(sprintf('inclination: %d',result(2,index)))
94 disp(sprintf('number of satellites in each plane: %d',result(3,index)))
95 disp(sprintf('number of planes: %d',result(4,index)))
96 disp(sprintf('minimum number of satellites: %d',result(5,index)))
97
98 % Minimum number of planes
99 numplane = result(4,1:q);
100 [minplane,index]= min(numplane);
101
102 disp(sprintf('\nMINIMUM PLANES\nheight: %d', result(1,index)))
103 disp(sprintf('inclination: %d',result(2,index)))

```

Orbit Parameters

```

104 disp(sprintf('number of satellites in each plane: %d',result(3,index)))
105 disp(sprintf('number of planes: %d',result(4,index)))
106 disp(sprintf('minimum number of satellites: %d',result(5,index)))
107
108 % Price Optimization
109 TCost = plaunch*result(4,:)+psat*result(5,:); TCost = TCost/(1e6);
110 [CostOpt,index] = min(TCost);
111 height = result(1,:);
112
113 disp(sprintf('\nMINIMUM PRICE\nprice[M]: %d', TCost(index)))
114 disp(sprintf('height: %d', result(1,index)))
115 disp(sprintf('inclination: %d',result(2,index)))
116 disp(sprintf('number of satellites in each plane: %d',result(3,index)))
117 disp(sprintf('number of planes: %d',result(4,index)))
118 disp(sprintf('minimum number of satellites: %d',result(5,index)))
119
120 fprintf('\n\n MORE THAN ONE SOLUTION COULD HAVE THE SAME MIN NUMBER\n')
121
122 %% Plots
123
124 x=0:q-1;
125 plot(x,numplane,x,numsat,x,TCost,x,height)
126 strValues = strtrim(cellstr(num2str([x(:) numplane(:)],'(%d, %d)')));
127 text(x,numplane,strValues,'VerticalAlignment','bottom');
128 strValues = strtrim(cellstr(num2str([x(:) numsat(:)],'(%d, %d)')));
129 text(x,numsat,strValues,'VerticalAlignment','bottom');
130 strValues = strtrim(cellstr(num2str([x(:) TCost(:)],'(%d, %.1f)')));
131 text(x,TCost,strValues,'VerticalAlignment','bottom');
132 strValues = strtrim(cellstr(num2str([x(:) height(:)],'(%d, %d)')));
133 text(x,height,strValues,'VerticalAlignment','bottom');
134 legend('number of planes','number of satellites','Total Cost (M)')
135
136
137
138 toc

```

```

1 function [Bo] = visibleangle (h,eo)
2
3 d=zeros(length(h),length(eo));
4 nsats_opt=d;
5 Re = 6371;
6
7 for i = 1:length(h)
8     for j = 1:length(eo)
9
10         d(i,j)= Re * ( sqrt( ( (h(i)+Re)/Re )^2 - ( cosd(eo(j)) )^2 ) - sind(eo(j)) );
11         Bo = asind( d(i,j)*cosd(eo(j)) / (h(i)+Re) );
12
13     end

```

Orbit Parameters

```

14 end
15
16 end

```

```

1 function [anglesp] = distance_opt_f (i,a,p,s,typeWD,F)
2 %% Data input
3
4 % i: Inclination angle [deg]
5 % a: Height of the orbit [km]
6 % p: Number of planes
7 % s: Number of satellites per plane
8
9 %% Walker Delta type of geometry
10 WD=[180 225 360];
11 degreegenerate = WD(typeWD);
12 % Walker Delta 360 deg, SemiWalker Delta 180 deg,
13 % other constellations range between 180 and 360
14
15 m = degreegenerate/180;
16 % generates Walker Delta Constellation
17 % (m=2 -> 2*180 generated constellation),
18 % Semi Walker (m=1 -> 1*180) or other 1<m<2.
19
20 % Phasing between adjacent planes
21 %f = F*p*cosd(i); % parameter defined graphically
22 f = F; % Whereas F is a number 0 < f < (p-1)
23 % According to Astrodynamics notes
24
25 REarth = 6371; % [km]
26 h = (REarth+a)/REarth; %radius of the orbit
27 %(in terms of the sphere radius) R=h*r;
28
29 %% Distribution of Coordinates of the satellites
30 Omega = zeros(1,p);
31 nu = zeros(s,p);
32 angle = zeros(1,p);
33 X = zeros(3,s,p);
34
35 for j = 1:p
36     Omega(j) = m*pi*(j-1)/p;
37     angle(j) = f*2*pi*(j-1)/(s*p); %Phasing due to f between planes
38     for k = 1:s
39         % True anomalies of the s satellites
40         nu(k,j) = 2*pi*(k-1)/s+angle(j);
41         X(:,k,j) = cartesian(h,0,i,Omega(j),0,nu(k,j));
42         % h[adim] --> X[adim]
43     end
44 end
45

```

```

46 %% Fast comprobation
47 % Does the adjacent phasing exceed pi
48 % THIS MEANS
49 % The minimum might be between
50
51
52 %% Angle between different satellites
53
54 c=zeros(s,p); %General aproach. Where is the minimum angle?
55
56 for j=2:p
57   for i=1:s-1
58
59     % We need to assess the angles between the last and first plane
60     % Specially in Semi-Walker configurations. That's why we add this
61     % auxiliar variables.
62
63     p1=j;
64     if j==1
65       p2=p;
66     else
67       p2=j-1;
68     end
69
70     % Angles a2 and a3 could be used to increase de reliability of the
71     % constellation, allowing greater possibilities of communication
72     % between planes. (not only between (i,p1) and (i,p2)
73
74     % Angle between satellite (i,p1) and satellite (i,p2)
75     a1=acosd((X(:,i,p1)'*X(:,i,p2))/(norm(X(:,i,p1))*norm(X(:,i,p2)))); 
76
77     % Angle between satellite (i,j) and satellite (i+1,j-1)
78     a2=acosd((X(:,i,p1)'*X(:,i+1,p2))/(norm(X(:,i,p1))*norm(X(:,i+1,p2)))); 
79
80     % Angle between satellite (i,j) and satellite (i-1,j-1)
81     a3=acosd((X(:,i,p1)'*X(:,i-1,p2))/(norm(X(:,i,p1))*norm(X(:,i-1,p2)))); 
82
83     % Among the computed angles, choose the minimum
84     [angle(i,j),c(i,j)]=min([a1 a2]);
85
86     % Why minimum? Then we know that at least it will be able to
87     % cover the angle with one of the two adjacent close nodes.
88
89   end
90 end
91
92 anglesp = max(max(angle));
93 %Maximum angle between satellites of different planes

```

```

1 %----ASTREA CONSTELLATION----
2 %PROJECTS - 220028
3 %Aerospace Engineering Bachelor's Degree
4 %ESEIAAT - UPC
5 %Autumn 2016-2017
6
7 % ORBIT DESIGN TEAM
8 % ORBIT SMART WALKER-DELTA
9
10 % This routine compute the WD possible configurations that give global
11 % coverage by having the distance between planes matches the planes
12 % rotation
13
14 p=[12 15 18];
15 S=360./p; S=S*pi/180;
16
17 re=6378.01e3;
18 u=3.986012e14;
19 J2=1.0826e-3;
20
21 we=2*pi/(24*3600);
22
23 syms a;
24 inc=75; inc=inc*pi/180;
25 a_sol=zeros(1,length(inc));
26
27 for i=1:length(inc)
28     dOmega=-1.5*J2*(re/a)^2*sqrt(u/a^3)*cos(inc(i));
29     P0=2*pi*sqrt(a^3/u);
30     Pn=P0*(1-1.5*J2*(re/a)^2-0.75*J2*(4-5*sin(inc(i))^2)*(re/a)^2);
31     eq=S(2)-Pn*(we-dOmega);
32     sol=vpasolve(eq,re*1.15);
33     if imag(sol)==0
34         a_sol(i)=sol;
35     end
36 end
37
38 plot(inc*180/pi,(a_sol-re)/1000)
39 h=(a_sol-re)/1000
40
41 %% Satellites computation
42
43 emin=20*pi/180;
44 Lstreet=5*pi/180;
45
46 rho=re/(re+h*1000);

```

```

47 etha=asin(sin(rho)*cos(emin));
48 Lmax=pi/2-emin-etha;
49 S=2*acos(cos(Lmax)/cos(Lstreet));
50 N=ceil(2*pi/S)

```

Orbit Plotter

```

1 %----ASTREA CONSTELLATION----
2 %PROJECTS - 220028
3 %Aerospace Engineering Bachelor's Degree
4 %ESEIAAT - UPC
5 %Autumn 2016-2017
6
7 % ORBIT DESIGN TEAM
8 % ORBIT PLOTTER - Influential phenomena computation
9
10 % This matlab routine plots the position of the satellites of a Walker
11 % Delta / SemiWalker Delta or other generated configurations.
12
13 clc, clear, close all;
14 %-----
15 %% 0. Data Input
16 %add the subfolder programs to the current path
17 addpath(genpath('./auxiliar'));
18
19 %____Physical input_____
20
21 global h, h = 542; % [km]
22 degreegen = 225; % Walker Delta 360 deg, SemiWalker Delta 180 deg,
23 % other constellations range between 180 and 360 deg
24 in = degtorad(72); % inclination of the planes
25 s = 21; % satellites per plane
26 p = 9; % number of planes
27 f=8; % f = 1.25*p*cos(i); % parameter defined graphically
28 eo=degtorad(20); % elevation angle [rad]
29
30 %____Numerical Input_____
31 r = 1; %radius of the sphere
32 n = 50; %number of cells of the sphere generated
33 N = 50; %number of points used to print the orbit
34 nn = 100; %number of points used to compute the footprint
35
36 %____Physical Constants_____
37 global Re, Re = 6371; %Earth's Radius [Km]
38 %% 1. Preprocessing
39

```

```

40 global m, m = degreegen/180;
41 % generates Walker Delta Constellation (m=2 -> 2*180)
42 % generated constellation), Semi Walker (m=1 -> 1*180)
43 % or other 1<m<2.
44
45 global a, a = (Re+h)/Re;
46 %radius of the orbit (in terms of the sphere radius) R=h*r;
47
48 %% 2. Main Process
49
50 %compute the sat RAAN and some sat. parameters (Laura)
51 Omega = zeros(1,p);
52 nu = zeros(s,p); %true anomaly of the satellites
53 angle = zeros(1,p); %angle between satellites
54 for i = 1:p
55     Omega(i) = m*pi*(i-1)/p; %orbits
56
57     angle(i) = f*2*pi*(i-1)/(s*p); %sats
58     for k = 1:s
59         nu(k,i) = 2*pi*(k-1)/s+angle(i);
60     end
61 end
62
63 % Compute the satellite coordinates (Laura)
64 X = zeros(3,s,p);
65 for i = 1:p
66     for k = 1:s
67         X(:,k,i) = cartesian(a,0,in,Omega(i),0,nu(k,i));
68     end
69 end
70 sCOOR=reshape(X,3,p*s)'; %put the data in a more friendly structure
71
72 %compute the radius of the footprint
73 %SATELLITE_FOOTPRINT_COMPUTATION.m
74 d=Re*((h+Re)/Re)^2-cos(eo)^2^.5-sin(eo));
75 Bo=asin(d*cos(eo)/(h+Re));
76 S=2*pi*Re^2*(1-cos(Bo));
77 R=(S/pi)^.5;
78
79 %create the footprint of each satellite
80 SATfp=[];
81 for i=1:s*p
82     %unitary vector pointing to the sat from the earth's center
83     u=-sCOOR(i,:)/norm(sCOOR(i,:));
84     %Generate the circle coordinates (2D)
85     [satfp(:,1),satfp(:,2),satfp(:,3)]=circle3D(sCOOR(i,:),u, R/Re, nn);
86     satfp=satfp+repmat(u*h/Re,nn,1); %move the circle to be tg to Earth
87
88     for j=1:size(satfp,1)
89         v=sCOOR(i,:)-satfp(j,:); v=v/norm(v);

```

Orbit Plotter

```

90         %unitary vector sat->footprint
91
92         %verify if the footprint intersect with the earth's surface
93         tol=satfp(j,1)^2+satfp(j,2)^2+satfp(j,3)^2-r^2;
94         while tol>1e-2
95             satfp(j,:)=satfp(j,:)-0.01*v;
96             tol=satfp(j,1)^2+satfp(j,2)^2+satfp(j,3)^2-r^2;
97         end
98     end
99     %store the footprint
100    SATfp=[SATfp; satfp];
101 end
102
103
104 %% 3. Plots
105
106 %3D plot
107 [COOR]=Orbitplot3D( in,r, X,n, SATfp, nn );
108 %Ground track
109 x=zeros(size(COOR,1),size(COOR,2)/3); y=x; z=x;
110 for i=1:size(COOR,2)/3
111     x(:,i)=COOR(:,3*(i-1)+1);
112     y(:,i)=COOR(:,3*(i-1)+2);
113     z(:,i)=COOR(:,3*(i-1)+3);
114 end
115 GroundTrackPlot( x, y, z, sCOOR, SATfp, nn);

```

```

1 function [x,y,z]=circle3D(center,normal, radius,n)
2 %This matlab function generates the points of a circle normal to a 3D
3 %vector
4 %In:
5 %   center: center of the circle (x, y, z)
6 %   normal: vector normal to the circle
7 %   radius: radius of the circle
8 %   n: number of points (small number can make the circle not smooth)
9 %Out:
10 %   x, y z: vectors containing the coord.
11 %
12
13 theta=linspace(0,2*pi,n);
14 v=null(normal);
15 points=repmat(center',1,size(theta,2))+...
16     radius*(v(:,1)*cos(theta)+v(:,2)*sin(theta));
17 x=points(1,:); y=points(2,:); z=points(3,:);
18 end

```

```

1 function [COOR] = Orbitplot3D( in,r, X,n, sCOOR, N )

```

```

2 %Orbitplot3D is a function that creates a 3D representation of a
3 %constellation and plots the satellites. It can be also configured to plot
4 %their footprint
5 %In:
6 %    in: inclination angle [rad]
7 %    r: sphere radius [-]
8 %    X: Coordinates of the sats (3,spp,p)
9 %    n: number of points used to draw the sphere
10 %
11 %    COOR: coordinates of the footprints
12 %    N: number of points used to compute the footprint
13 %
14 p=size(X,3);
15 s=size(X,2);
16 global a m;
17
18 % Earth
19 %Create the earth instance as an sphere
20 [x,y,z]=sphere(n); %Generate the sphere
21 surf(r*x,r*y,r*z,'FaceColor','interp','EdgeColor','none'); %plot the sphere
22 colormap(linspace(0,1,n)'*[0 0.6 1]); %custom colormap (blue tones);
23 axis equal;
24 box off;
25 hold on;
26 rotate3d on;
27
28 % Orbits
29 %Generate the circle coordinates (2D)
30 coor=zeros(N+1,3);
31 for i=1:N
32     coor(i,:)=[a*r*cos(2*i*pi/N), a*r*sin(2*i*pi/N), 0];
33 end
34 coor(N+1,:)=coor(1,:);
35
36 %Rotation Matrices
37 Ry=[ cos(in) 0 sin(in)
38         0      1      0
39     -sin(in) 0 cos(in)];
40
41 Rz=@(Omega) [-sin(Omega) cos(Omega) 0
42                  cos(Omega) sin(Omega) 0
43                  0          0          1]; % he modificant aquesta matriu
44
45 coor=coor*Ry; %Rotate the circle in the y axis (inclination)
46
47 %rotate the plane to get the other planes
48 COOR=zeros(N+1,3*p);
49 for i=1:p
50     COOR(:,(1+(i-1)*3):(3+(i-1)*3))=coor*Rz(m*(i-1)*pi/p);
51 end

```

```

52 for i=1:p
53 plot3(COOR(:,1+(i-1)*3),COOR(:,2+(i-1)*3),COOR(:,3+(i-1)*3),...
54     'linewidth',1.5);
55 end
56
57 % Satellites (Laura)
58 for i = 1:p
59     for k = 1:s
60         scatter3(X(1,k,i),X(2,k,i),X(3,k,i),25,'square','k','filled');
61         hold on;
62     end
63 end
64
65 %Plot also the footprint if the number of input variables is bigger than 4
66 if nargin > 4
67     for i=1:p*s
68         b=1+N*(i-1); c=N+N*(i-1);
69         fill3(sCOOR(b:c,1),sCOOR(b:c,2),sCOOR(b:c,3),[1 0 0],...
70             'FaceAlpha','.', 'LineStyle','none');
71     end
72 end
73 end

```

```

1 function [] = GroundTrackPlot( x, y, z, coor, fp_coor, N)
2
3 %GroundTrackPlot is used to plot the ground
4 %track of the constellation orbits
5 %given their coordinates (cartesian). It has two variants, only introducing
6 %the first 3 inputs will plot the orbits and if you introduce all the
7 %inputs it plots the satellites and their footprint.
8 %In:
9 %    x: matrix containing the x coordinate of the orbits to plot
10 %    y: matrix containing the y coordinate of the orbits to plot
11 %    z: matrix containing the z coordinate of the orbits to plot
12 %
13 %    coor: satellite coordinates (nx3)
14 %    fp_coor: satellite footprint coordinates ((n*nn)x3)
15 %    N: number of points used to compute the footprint
16 %
17 p=size(x,2); %n of planes
18 s=size(coor,1)/size(x,2); %n of spp
19
20 %% Set the background image for the ground track plot
21 figure('name','Constellation Ground Track');
22 tit=['Num. of planes: ' num2str(p) ' Num. of spp: ' num2str(s)];
23 ground='World-satellite-map.png';
24 im=imread(ground);
25 imagesc([-180,180],[-90,90],im);
26 grid on;

```

Orbit Plotter

```

27 axis([-180 180 -90 90]);
28 title(tit);
29 hold on;
30 %set the plot lines color
31 c = ['r','y','m','g','w']; C=[];
32 for i=1:ceil(size(x,2)/5)
33     C=[C c];
34 end
35
36 %% Main process
37 for i=1:size(x,2)
38     %convert the cartesian coordinates to spherical
39     [lon,lat]=cart2sph(x(:,i),y(:,i),z(:,i));
40     %get the coordinates of the orbit in spherical coord.
41     lon=radtodeg(lon); %pass to degrees
42     lat=radtodeg(lat);
43     Lon=[lon(end); lon(1:end-1)];
44
45     %Plot the sat ground track
46     [~,j]=max(abs(lon-Lon));
47     plot(lon(1:j-1),lat(1:j-1),C(i),'linewidth',1.2);
48     plot(lon(j:end),lat(j:end),C(i),'linewidth',1.2);
49 end
50
51 if nargin > 3
52     [slon,slat]=cart2sph(coor(:,1),coor(:,2),coor(:,3));
53     %get the coordinates of the sats in spherical coord.
54     slon=radtodeg(slon); %pass to degrees
55     slat=radtodeg(slat);
56
57     %plot the sats
58     scatter(slon,slat,30,'square','w','filled');
59
60     %get the coordinates of the sats footprint in spherical coord.
61     [fpLon,fplat]=cart2sph(fp_coor(:,1),fp_coor(:,2),fp_coor(:,3));
62     fpLon=radtodeg(fpLon); %pass to degrees
63     fplat=radtodeg(fplat);
64
65     %Plot their footprint
66     for i=1:p*s
67         b=1+N*(i-1); c=N+N*(i-1);
68         fpLon=[fpLon(c); fpLon(b:c-1)];
69
70         %get the maximum values (plotting purposes)
71         [sorted, I]=sort(abs(fpLon(b:c)-fpLon));
72         M=sorted(end-1:end);
73         j=I(end-1:end); j(2)=j(2)-1;
74
75         if M(1) > 300
76             if j(1) < j(2)

```

```

77         auxlon=fplon(b+j(1):b+j(2)-1); %negative lon. part
78         auxlat=fplat(b+j(1):b+j(2)-1);
79
80         auxlon2=[fplon(b+j(2):c); fplon(b:b+j(1)-2)]; %+ lon. part
81         auxlat2=[fplat(b+j(2):c); fplat(b:b+j(1)-2)];
82     else
83         auxlon2=fplon(b+j(2):b+j(1)-2); %negative lon. part
84         auxlat2=fplat(b+j(2):b+j(1)-2);
85
86         auxlon=[fplon(b+j(1):c); fplon(b:b+j(2)-1)];
87         %positive lon. part
88         auxlat=[fplat(b+j(1):c); fplat(b:b+j(2)-1)];
89     end
90
91     fill(auxlon,auxlat,[1 0 0],'FaceAlpha','.', 'LineStyle','none');
92     fill(auxlon2,auxlat2,[1 0 0],'FaceAlpha','.', 'LineStyle','none');
93 else
94     fill(fplon(b:c),fplat(b:c),[1 0 0],...
95          'FaceAlpha','.', 'LineStyle','none');
96
97     %%%%%%%%%%%%%%
98     pause(.05); %
99     %%%%%%%%%%%%%%
100 end
101
102
103 end
104 end
105 end

```

```

1 % This function converts kepler orbit elements to cartesian coordinates
2
3 % a: semimajor axis
4 % e: eccentricity
5 % i: inclination [rad]
6 % Omega: longitude of the ascending node [rad]
7 % w: Argument of periaxis [rad]
8 % nu: True anomaly [rad]
9
10 function [X] = cartesian(a,e,i,Omega,w,nu)
11
12 % Position in cylindrical coordinates
13 r = a*(1-e^2)/(1+e*cos(nu));
14
15 % Position components
16 X = [r*(cos(Omega)*cos(w+nu)-sin(Omega)*sin(w+nu)*cos(i));
17       r*(sin(Omega)*cos(w+nu)+cos(Omega)*sin(w+nu)*cos(i));
18       r*sin(i)*sin(w+nu)];
19

```

```
20 end
```

Perturbations

```

1 %----ASTREA CONSTELLATION----
2 %PROJECTS - 220028
3 %Aerospace Engineering Bachelor's Degree
4 %ESEIAAT - UPC
5 %Autumn 2016-2017
6
7 % ORBIT DESIGN TEAM
8 % ORBIT PERTURBATIONS - Influential phenomena computation
9
10 %PROBLEM:
11 % Given: - Initial orbital parameters
12 % Compute the final orbital parameters after each orbit
13 %clear; clc;
14
15 %% 1.A Input data physical constants
16 % PHYSICAL CONSTANTS AND PARAMETERS
17 %Physical data
18 RE=6.378e6; %Earth Radius [m]
19 u=3.986e14; %GM Earth
20 J2=1082.6e-5; %J2 coefficient;
21
22 %% 1. Input data Orbit parameters
23 % SPACECRAFT DATA
24 m=4; % Satellite mass [kg]
25 Cd=2.2; % Drag Coefficient
26 A=0.1; % Satellite surface [m^2] --> 3U pointing to Earth
27 Bc=m/(Cd*A); % Ballistic coefficient of the satellite;
28
29 % ORBIT DATA
30 H0=542e3; % Altura inicial [m]
31 e0=0.0001; % Excentricity
32 i0=72*pi/180; % Inclination [deg]
33 a0=RE+H0;
34
35 % INITIAL PARAMETERS
36 P=2*pi*(a0^3/u)^.5; % Orbit Period [s]
37 v=sqrt(u/a0); %satellite velocity [m/s]
38 n=(2*pi/P)*86400; %number of revolutions/day
39
40
41 % SIMULATION PARAMETERS
42 N=10000000;
```

Perturbations

```

43
44 %% 2. Perturbations propagation
45 %Outputs de la funcio Perturbation:
46 % Pert: matrix (4x5) with the perturbations causes at the rows (J2,Drag,
47 % Moon,Sun) and the orbital elements in the columns (a,e,i,omega,Omega)
48 %     a e i w Omega
49 %     [ ]J2
50 %     [ ]Drag
51 %     [ ]Moon
52 %     [ ]Sun as 3rd Body
53
54
55
56 t=zeros(1,N); t(1)=0;
57 a=t; a(1)=a0;
58 e=t; e(1)=e0;
59 i=t; i(1)=i0;
60
61 w_sun=zeros(1,N-1); w_moon=w_sun; w_J2=w_sun;
62 Om_sun=w_sun; Om_moon=w_sun; Om_J2=w_sun;
63
64 w0=0; Omega0=0;
65 w=t; w(1)=w0;
66 Omega=t; Omega(1)=Omega0;
67
68 tic
69 for n=2:N
70
71     a0=a(n-1);
72     e0=e(n-1);
73     i0=i(n-1);
74     w0=w(n-1);
75     Omega0=Omega(n-1);
76
77     P=2*pi*(a0^3/u)^.5; % Orbit Period [s]
78
79     [Perti rho]=Perturbation(a0,e0,i0,Bc);
80
81     a(n)=a0+sum(Perti(:,1));
82     e(n)=e0+sum(Perti(:,2));
83     i(n)=i0+sum(Perti(:,3));
84     w(n)=w0+sum(Perti(:,4));
85     Omega(n)=Omega0+sum(Perti(:,5));
86
87     w_sun(n-1)=Perti(4,4);
88     w_moon(n-1)=Perti(3,4);
89     w_J2(n-1)=Perti(1,4);
90
91     Om_sun(n-1)=Perti(4,5);
92     Om_moon(n-1)=Perti(3,5);

```

Perturbations

```

93      Om_J2(n-1)=Perti(1,5);
94
95      % We don't want angles bigger than 360!
96      w(n)=w(n)-360*floor(w(n)/360);
97      Omega(n)=Omega(n)-360*floor(Omega(n)/360);
98
99      if Omega(n)>2*pi
100         Omega(n)=Omega(n)-2*pi;
101     end
102
103     t(n)=t(n-1)+P;
104
105     if a(n)<(RE+180e3)
106         fprintf('Your satellite successfully burned in the atmosphere.\n\n')
107         break
108     end
109
110 end
111
112 %% Post processing and results plotting
113
114 time=toc;
115 fprintf('Time to do %g iterations = %g s.\n',n,time)
116
117 figure(1)
118 plot(t(1:n)/(3600*24),(a(1:n)-RE)/1000)
119 ylim([100 500])
120 grid on
121 ylabel('Orbit height [km]')
122 xlabel('Time [days]')
123 tfin=floor(t(n)/(3600*24));
124 days = num2str(floor(tfin/365));
125 titulaso=['Orbit decay in ' num2str(tfin) ' days = ' days 'years'];
126 title(titulaso)
127
128
129 figure(2)
130 subplot(1,2,1)
131 plot(t(1:n)/(3600*24),w(1:n))
132 grid on
133 ylabel('Perigee Argument [deg]')
134 xlabel('Time [days]')
135 title('Perigee Argument deviation in 100 days')
136 axis([0 100 0 360])
137
138 subplot(1,2,2)
139 plot(t(1:n)/(3600*24),Omega(1:n))
140 grid on
141 ylabel('Ascenent Node Argument [deg]')
142 xlabel('Time [days]')

```

Perturbations

```

143 tfin=t(n)/(3600*24);
144 title('Ascendent Node deviation in 100 days')
145 axis([0 100 0 360])
146
147 %% Modulus Analysis
148
149 figure(3)
150
151 subplot(1,2,1)
152 semilogy(t(2:n+1)/(3600*24),abs(w_sun(1:n)), 'b','LineWidth',2);
153 hold on
154 semilogy(t(2:n+1)/(3600*24),abs(w_moon(1:n)), 'r','LineWidth',2)
155 semilogy(t(2:n+1)/(3600*24),abs(w_J2(1:n)), 'k','LineWidth',2)
156 legend('Sun','Moon','J2')
157 xlabel('Time (days)');
158 ylabel('Modulus of Perturbation []');
159 title('Effects on Argument of the Perigee');
160 grid on
161 axis([0 t(n)/(3600*24) 1e-8 1])
162
163 subplot(1,2,2)
164 semilogy(t(2:n+1)/(3600*24),abs(Om_sun(1:n)), 'b','LineWidth',2);
165 hold on
166 semilogy(t(2:n+1)/(3600*24),abs(Om_moon(1:n)), 'r','LineWidth',2)
167 semilogy(t(2:n+1)/(3600*24),abs(Om_J2(1:n)), 'k','LineWidth',2)
168 legend('Sun','Moon','J2')
169 xlabel('Time (days)');
170 ylabel('Modulus of Perturbation []');
171 title('Effects on Argument of Ascendent Node');
172 axis([0 t(n)/(3600*24) 1e-8 1])
173 grid on
174
175 print -depsc ModulusAngulars

```

```

1 function [pert rho] = Perturbation( a,e,i,Bc)
2 %% Perturbations
3 % This matlab is used to compute the perturbations in the classical orbital
4 % elements due to:
5 % J2 (non spherical earth)
6 % Atmospheric drag
7 % Third body (Moon and Sun)
8 %Inputs:
9 % a: semi-major axis [m]
10 % e: eccentricity [-]
11 % i: inclination [rad]
12 % m: mass of the satellite [kg]
13 % Cd: drag coefficient [-]
14 % A: Area of the satellite [m^2]
15 %Outputs:

```

Perturbations

```

16 % Pert: matrix (4x5) with the perturbations causes at the rows (J2,Drag,
17 % Moon,Sun) and the orbital elements in the columns (a,e,i,omega,Omega)
18 % incP/revolution
19 % incv/revolution
20 %TO DO:
21 %Les perturbacions degudes a J2 i 3rd body no se si son en pert/dia o no,
22 %cal mirar-ho per tal de tenir totes les pertrubacions escalades igual
23 %
24 %% Previous calculations and PreAllocation
25 %Physical data
26 RE=6.378e6; %Earth Radius [m]
27 u=3.986e14; %GM Earth
28 J2=1082.6e-5; %J2 coefficient;
29
30 P=2*pi*(a^3/u)^.5; % Orbit Period [s]
31 v=sqrt(u/a); %satellite velocity [m/s]
32 n=(2*pi/P)*86400; %number of revolutions/day
33
34
35 % ATMOSPHERIC MODEL
36 %get the density from MSISE model (extracted as a list from
37 %http://omniweb.gsfc.nasa.gov/vitmo/msis\_vitmo.html
38 % h[km] rho[kg/m^3]
39 % filename1='msis_26371.lst'; filename2='msis_2226.lst';
40 % formatSpec='%f %f';
41 % size=[2 Inf];
42 % fileID=fopen(filename1,'r');
43 % rho_h=fscanf(fileID,formatSpec,size);
44 % fclose(fileID);
45 % fileID=fopen(filename2,'r');
46 % rho_h=[rho_h fscanf(fileID,formatSpec,size)];
47 % fclose(fileID);
48 % rho=interp1(rho_h(1,:),rho_h(2,:)',(a-RE)/1000);
49
50 H = (a - RE)*1e-3;
51 % Compute exospheric temperature [K]
52 T = 900 + 2.5*(120-70);
53 % Compute effective atmospheric molecular mass [km/K], valid 180<H<500
54 M = 27 - 0.012 * (H - 200);
55 % Compute atmospheric scale height [km]
56 SH = T / M;
57 % Compute atmospheric density [kg/m3]
58 rho = 6E-10 * exp(-(H - 175) / SH);
59
60
61 pert=zeros(4,5);
62
63 %% Computation
64
65 %J2 perturbation_____ PER REVOLUCIO

```

Orbit Decay

```

66 j=1;
67 pert(j,5)=-1.5*n*J2*(RE/a)^2*cos(i)*(1-e^2)^-2;
68 pert(j,4)=0.75*n*J2*(RE/a)^2*(4-5*(sin(i))^2)*(1-e^2)^-2;
69
70 %Atmospheric Drag_____ PER REVOLUCIO
71 %Perturbations/revolution
72 j=2;
73 pert(j,1)=-2*pi*rho*a^2/Bc;
74
75 % incP=-6*pi^2*a^2*rho/(v*Bc);
76 % incv=pi*a*rho*v/Bc;
77
78 %Moon Perturbation_____ /DIA --> /REV
79 j=3;
80 pert(j,5)=-0.00338*cos(i)/n;
81 pert(j,4)=0.00169*(4-5*(sin(i))^2)/n;
82
83 % Fins aqui son /dia,
84 % Canviem unitats + apliquem periode actual
85 pert(j,5)=pert(j,5)*P/(24*3600);
86 pert(j,4)=pert(j,4)*P/(24*3600);
87
88 %Sun Perturbation_____ /DIA --> /REV
89 j=4;
90 pert(j,5)=-0.00154*cos(i)/n;
91 pert(j,4)=0.00077*(4-5*(sin(i))^2)/n;
92
93 % Fins aqui son /dia,
94 % Canviem unitats + apliquem periode actual
95 pert(j,5)=pert(j,5)*P/(24*3600);
96 pert(j,4)=pert(j,4)*P/(24*3600);
97
98
99 end

```

Orbit Decay

```

1 %----ASTREA CONSTELLATION----
2 %PROJECTS - 220028
3 %Aerospace Engineering Bachelor's Degree
4 %ESEIAAT - UPC
5 %Autumn 2016-2017
6
7 % ORBIT DESIGN TEAM
8 % ORBIT DECAY
9

```

```

10 % This routine computes the orbital decay of an spacecraft with time
11 % using the cowell's method.
12 % The differential equations are integrated using "ode45" (Runge-Kutta 4th,
13 % 5th order)
14
15
16 %-----%
17 %%
18 clear all;
19 clc;
20 close all;
21
22 %% Initialization %%%%%%%%%%%%%%%%
23 global mu mmu smu re rs rm omega J2;
24
25 %_____Physical Variables_____
26 mu=3.986004418e14; % earth gravitational constant [m^3/s^2]
27 mmu=4902.800076e9; %moon gravitational constant [m^3/s^2]
28 smu=132712440040.944e9; %sun gravitational constant [m^3/s^2]
29
30 re=6378136.3; %earth radius [m]
31 rs=696e6; %sun radius [m]
32 rm=1730e3; %moon radius [m]
33
34 omega=7.292115e-5; %earth angular velocity [rad/s]
35 J2=0.001081874; %earth oblateness gravity coeff []
36
37 au=149597870691; %astronomical unit [m]
38 c=2.99792458e8; %[m/s] speed of light
39
40 %_____Numerical variables_____
41 hlim=180; %minimum height for considering the decay [km]
42 dt=15*60; %timestep of the simulation [s]
43 t0=0; %initial time of the sim
44 tf=dt;
45
46 %% User Input %%%%%%%%%%%%%%%%
47 %__Orbital elements_____
48 a=re+542e3; %[m] semimajor axis
49 e=0.0001; % eccentricity
50 i=degtorad(72); %[rad] inclination
51 w=0; %[rad] argumetn f periapsis
52 Omega=0; %[rad] RAAN
53 nu=0; %true anomaly
54
55 date=datetime(2017,2,4); %datetime array [Y, M, D]
56
57 %__Oblateness parameters_____
58 znlsls=0; %zonals [0-18]
59 tssrls=0; %tesserals [0-18]

```

```

60
61 %__Drag perturbation inputs_____
62 Cd=2.2; %Drag coefficient (Typical for sats, various ref.)
63 Adrag=.09; %[m^2] Wet area for the drag
64 m=4.1; %[kg] Cubesat mass
65
66 Bc=Adrag*Cd/m; %Ballistic coeff.
67
68 %__SRP perturbation inputs_____
69 Cr=2; %reflectivity ct.
70 Asrp=.5; %[m^2] Area for the SRP
71
72 % Ws (@Dap) = 1361/(1+0.0334*cos(2*pi*Dap/365));
73 Ws=1361; %W/m^2 approximation for the solar irradiance
74
75 srp=Ws/c*Cr*Asrp/m*au^2; %Solar radiation pressure ct.
76
77 %% Main Process %%%%%%%%%%%%%%%%
78 display('Computing...');

79 f=@(q) q*((3+3*q+q^2)/(1+(1+q)^3/2)); %richard Battin's function
80
81 aobl=zeros(3,1);
82 adrag=aobl; asun=aobl; amoon=aobl; asrp=aobl;
83
84
85 y=cartesian2(a,e,i,Omega,w,nu); %obtain the state vector (r,v)
86 jdate0=juliandate(date); %compute the julian date
87
88 tic
89 iter=0; tt=[]; xx=[];
90
91 h=(norm(y(1:3))-re)*1e-3;
92 while h>hlim
93     jdate=jdate0+t0/86400;
94     %     GMST=JD2GMST(jdate);
95     %
96     %     Acceleration due to oblateness
97     %     aobl=Oblat((t0+tf)/2,y,znls,tssrls,GMST);
98     %
99     %     Acceleration due to the 3rd body pert.
100    %     rsun=planetEphemeris(jdate,'Earth','Sun');
101    %     geocentric pos of the Sun
102    %     rmoon=planetEphemeris(jdate,'Earth','Moon');
103    %     geocentric pos of the Moon
104    %     rsun=rsun'; rmoon=rmoon';
105    %
106    %     rs2s=y(1:3)-rsun; %vector sun-sat
107    %     rm2s=y(1:3)-rmoon; %vector moon-sat
108    %
109    %     qs=dot(y(1:3),(y(1:3)-2*rsun))/dot(rsun,rsun);

```

Orbit Decay

```

110 %      qm=dot (y(1:3), (y(1:3)-2*rmoon))/dot (rmoon,rmoon);
111 %
112 %      asun=-smu/norm(rs2s)^3*(y(1:3)+f(qs)*rsun);
113 %      amoon=-mmu/norm(rm2s)^3*(y(1:3)+f(qm)*rmoon);
114 %
115 %      %Acceleration due to the solar radiation pressure.
116 %      usun=rsun/norm(rsun); %unit vector of the pos of the sun
117 %      us=y(1:3)/norm(y(1:3)); %unit vector of the pos of the sat
118 %
119 %      shadow=random('Normal',0.5,.1); %shadow factor
120 %
121 %      asrp=srp*rs2s/norm(rs2s)^3;
122
123 %Acceleration due to the drag force
124 % Compute exospheric temperature [K]
125 T = 900 + 2.5*(100-70);
126 % Compute effective atmospheric molecular mass [km/K], valid 180<H<500
127 M = 27 - 0.012 * (h - 200);
128 % Compute atmospheric scale height [km]
129 SH = T / M;
130 % Compute atmospheric density [kg/m3]
131 rho = 6E-10 * exp(-(h - 175) / SH);
132
133 atmosV=y(4:6)+omega*[y(2); -y(1); 0];
134 %relative vel between sat and atmos
135
136 adrag=-.5*rho*Bc*atmosV*norm(atmosV);
137
138 %%%%%%%%
139 acc=aoбл+asun+amoon+asrp+adrag;
140
141 ode=@(t,y)[y(4);
142             y(5);
143             y(6);
144             acc(1)-mu/norm(y(1:3))^3*y(1);
145             acc(2)-mu/norm(y(1:3))^3*y(2);
146             acc(3)-mu/norm(y(1:3))^3*y(3)
147 ]; %function to integrate (6eqn)
148
149 [t,x]=ode45(ode,[t0 tf], y);
150
151 y=x(size(x,1),:);
152 %save one value each 12 hours
153 if mod(t(length(t)),12*3600)==0
154     tt=[tt; t(length(t))]; xx=[xx; y];
155 end
156 y=y';
157
158 %%%%%%%%
159 %End of the timestep

```

Orbit Decay

```

160      t0=tf;
161      tf=tf+dt;
162
163      h=(norm(y(1:3))-re)*1e-3;
164
165      iter=iter+1;
166      if mod(iter,300)==0
167          fprintf('Days elapsed: %0.1f \nH=%0.3f km\n',(jdate-jdate0),h);
168      end
169  end
170 toc
171 %% Post Process %%%%%%%%%%%%%%
172 fprintf('The satellite decays in %0.0f days',tf/86400);
173
174 h=zeros(size(xx,1),1);
175 for i=1:size(xx,1)
176     h(i)=(norm(xx(i,1:3))-re)*1e-3;
177 end
178
179 plot(tt/86400,h);

```

```

1 % This function converts kepler orbit elements to cartesian coordinates
2
3 % a: semimajor axis
4 % e: eccentricity
5 % i: inclination [rad]
6 % Omega: longitude of the ascending node [rad]
7 % w: Argument of periaxis [rad]
8 % nu: True anomaly [rad]
9
10 function [y] = cartesian2(a,e,i,Omega,w,nu)
11 global mu;
12 % Position in cylindrical coordinates
13 r = a*(1-e^2)/(1+e*cos(nu));
14
15 % Position components
16 X = [r*(cos(Omega)*cos(w+nu)-sin(Omega)*sin(w+nu)*cos(i));
17       r*(sin(Omega)*cos(w+nu)+cos(Omega)*sin(w+nu)*cos(i));
18       r*sin(i)*sin(w+nu)];
19
20 A = sin(Omega)*cos(i)*(e*cos(w)+cos(w+nu));
21 v(1)=-sqrt(mu/( a*(1-e^2)))*(cos(Omega)*(e*sin(w)+sin(w+nu))+A);
22
23 B = cos(Omega)*cos(i)*(e*cos(w)+cos(w+nu));
24 v(2)=-sqrt(mu/( a*(1-e^2)))*(sin(Omega)*(e*sin(w)+sin(w+nu))-B);
25
26 v(3)=sqrt(mu/( a*(1-e^2)))*(e*cos(w)+cos(w+nu))*sin(i);
27
28 y=[X;v'];

```

```
29 end
```

Performance Evaluator

```

1 %----ASTREA CONSTELLATION----
2 %PROJECTS - 220028
3 %Aerospace Engineering Bachelor's Degree
4 %ESEIAAT - UPC
5 %Autumn 2016-2017
6
7 % ORBIT DESIGN TEAM
8 % PERFORMANCE EVALUATOR
9
10 clear all;
11
12 %% Input Data
13
14 a=6378.01e3;
15 u=3.986012e14;
16 h=(a+546.5101e3)/a;
17 ap=h*a;
18 J2=1.0826e-3;% J2=0;
19
20 ws=sqrt(u/ap^3); % Satellite mean motion
21 we=2*pi/(24*3600); % Earth mean motion
22 dOmega=-1.5*J2*(a/ap)^2*sqrt(u/ap^3)*cosd(75);
23
24 At=1/6; % [min]           % Every 10 seconds
25 t=0:At:60*24; t=t*60; % Time array in seconds
26
27 i=72*pi/180;
28
29 p=9;
30 spp=21;
31 N=p*spp;
32 %f=floor(0.25*spp);
33 f=0;
34 fprintf('\ni=%gdeg, p=%g, spp=%g, N=%g\n',i*180/pi,p,spp,N);
35
36 latGS=57.5*pi/180;
37 longGS=(17.73-60)*pi/180; longGS=0;
38
39 fprintf('GS Coordinates: Lat=%g, Long=%g \n',latGS*180/pi, longGS*180/pi)
40
41 f1=pi/2-latGS; f2=longGS;
42 R1=[cos(f1) 0 -sin(f1);0 1 0;sin(f1) 0 cos(f1)];
```

```

43 R2=[cos(f2) sin(f2) 0; -sin(f2) cos(f2) 0; 0 0 1];
44 RotGS=R1*R2;
45
46 % Rotation Matrix:
47 % From ECEF - To SEZ
48 % Where:
49 % ECEF = Earth Centered Earth Fix - Coordinate System
50 % SEZ = Topocentric Horizon - Coordinate System
51
52 emin=20*pi/180;
53
54 %% Le simulasion
55 %Omega = 0:30:240; Omega=Omega*pi/180;
56 Omega = 0:225/(p-1):225; Omega=Omega*pi/180;
57 %Omega=0:360/p:360-360/p; Omega=Omega*pi/180;
58
59 nu = zeros(spp,p);
60 angle = zeros(1,p);
61 X = zeros(3,spp*p);
62
63 flight_time=zeros(1,1000); % Length of the flyby of a satellite
64 links_at_time=zeros(1,1000); % Number of links when one sat has finished
65 time_end_flyby=zeros(1,1000); % When did this flyby end?
66
67 contact=zeros(1,length(t)); % Number of links
68
69 quality_time=zeros(1,length(t));
70 %If a flyby lasts longer than 3 minutes,
71 % then the previous 3 minutes were successfully covered.
72
73 time_record=zeros(1,N); % Accumulates Timesteps being on the GS
74 before_tracking=zeros(1,N);
75 % Boolean to know which ones are already passing by
76 now_tracking=zeros(1,N); % Boolean to know which ones are now passing by
77 Nflyby=0; % Number of flight paths computed
78
79 for n=1:length(t)
80
81 % J2 deviation
82 Omegat=Omega+dOmega*t(n);
83
84 % Ground Station Coordinates
85 f1=we*t(n)+longGS;
86 f2=latGS;
87 RGS=cos(f2);
88 XGS=[RGS*cos(f1);RGS*sin(f1);sin(f2)];
89
90 R2=[cos(f1) sin(f1) 0; -sin(f1) cos(f1) 0; 0 0 1];
91 RotGS=R1*R2;
92

```

```

93      % Constellation Coordinates
94      nu_t=ws*t(n);    % True anomaly due to time passing by
95      for j = 1:p
96          angle(j) = f*2*pi*(j-1)/(spp*p); %Phasing due to f between planes
97          for k = 1:spp
98              % True anomalies of the s satellites
99              A = spp*(j-1)+k; % Number of the satellite
100             nu(k,j) = 2*pi*(k-1)/spp+angle(j);
101             X(:,A) = cartesian(h,0,i,Omegat(j),0,nu(k,j)+nu_t);
102         end
103     end
104
105     % Contact Evaluation
106     win=0; % Counter to know number of links
107     now_tracking=zeros(1,N);
108     for sat=1:N
109         X_hor=RotGS*(X(:,sat)-XGS);
110 % fprintf('%g,%g,%g --> |r|=%g\n',X_hor(1),X_hor(2),X_hor(3),norm(X_hor));
111         ang=asin(X_hor(3)/norm(X_hor));
112         if ang >= emin
113             win=win+1;
114             time_record(sat)=time_record(sat)+1;
115             now_tracking(sat)=1;
116         end
117
118         % Flight time computation and reset of this satellite flyby
119         if before_tracking(sat)==1 && now_tracking(sat)==0
120             Nflyby=Nflyby+1;
121             flight_time(Nflyby)=At*time_record(sat);
122
123             links_at_time(Nflyby)=contact(n-1);
124             time_end_flyby(Nflyby)=t(n);
125
126             % THE KEY QUESTION
127             % Was this flyby useful?
128             if flight_time(Nflyby)>3
129                 start=n-time_record(sat);
130                 finish=n;
131                 quality_time(start:finish)=quality_time(start:finish)+1;
132             end
133             time_record(sat)=0;
134         end
135     end
136     before_tracking=now_tracking;
137     contact(n)=win;
138 end
139
140 %% Post-Processing
141 % PLOT 1: NUMER OF LINKS
142 figure(1)

```

```

143 title('Links vs Time')
144 plot(t/(3600),contact)
145 axis([min(t)/(3600) max(t)/(3600) 0 max(contact)+1]);
146 fails=length(find(contact==0));
147 ratio=fails/length(contact);
148 fprintf('Links on GS           : %g percent of the time\n',(1-ratio)*100)
149
150 % PLOT 2: LENGTH OF THE LINKS
151 figure(2)
152 plot(flight_time(1:Nflyby));
153 titola=['Length of the ' num2str(Nflyby) ' flyby s. Mean time = '...
154     num2str(mean(flight_time(1:Nflyby))) 'min'];
155 title(titola)
156 ylabel('Length (minutes)')
157 xlabel('Contact')
158 %xlim([1 Nflyby])
159
160 % PLOT 3: ANALYSIS OF THE FLYBYS
161 figure(3)
162 index=1:Nflyby; % X variable to the following plots
163 plot(time_end_flyby(index)/3600,flight_time(index),...
164     time_end_flyby(index)/3600,links_at_time(index),...
165     t/3600,quality_time);
166
167 titola='Flybys Analysis';
168 title(titola)
169
170 legend('Length of flybys','Links by end of flyby',...
171     'Num of sats @flybys longer than 3 min')
172 xlabel('Time (h)')
173
174 epic_wins=length(find(quality_time≥1));
175 ratio_covered=epic_wins/length(t);
176 fprintf('Quality flybys on GS: %g percent of the time\n',ratio_covered*100)
177 fprintf('Mean flyby time = %g minutes\n',mean(flight_time(1:Nflyby)))
178
179 %% MAXIMUM GAP SEARCH
180 gap=0;
181 at_gap=0;
182 gap_record=zeros(1,100);
183 ngap=0;
184
185 for n=1:length(t)
186     if quality_time(n)==0
187         at_gap=1;
188         gap=gap+1;
189     end
190
191     if quality_time(n)>0 && at_gap==1

```

Thrust

```

193         at_gap=0;
194         ngap=ngap+1;
195         gap_record(ngap)=gap*At;
196         gap=0;
197     end
198 end
199
200 max_gap=max(gap_record);
201 fprintf('Maximum gap = %g minutes\n',max_gap)
202 fprintf('Number of gaps = %g\n\n',ngap)

```

Thrust

```

1 %----ASTREA CONSTELLATION----
2 %PROJECTS - 220028
3 %Aerospace Engineering Bachelor's Degree
4 %ESEIAAT - UPC
5 %Autumn 2016-2017
6
7 % ORBIT DESIGN TEAM
8 % THRUST
9
10 % This function computes the ΔV and propellant mass necessary to
11 % maintain an orbit between two heights
12
13 %function [mp,ΔV,tHoh] = thrust(hmax,hmin,ms,Isp,Thr)
14
15 % This function computes the ΔV and propellant mass necessary to
16 % maintain an orbit between two heights
17
18 % Input variables:
19 % - hmax: maximum height [m]
20 % - hmin: minimum height [m]
21 % - ms: dry mass of the spacecraft [kg]
22 % - Isp: specific impulse of the spacecraft [s]
23 % - Thr: thrust of the spacecraft [N]
24
25 % Output variables:
26 % - mp: array of propellant mass necessary for every Hohmann transfer [kg]
27 % - ΔV: array of ΔVs necessary for every Hohmann transfer [m/s]
28 % - tHoh: array of time necessary to do a Hohmann transfer [s]
29
30 % Proposed values:
31 hmax = 550e3;
32 hmin = hmax-8;
33 ms = 3.95;           % Dry mass [kg]

```

```

34 Isp = 2150;
35 Thr = 100e-6;
36
37 %% Data
38
39 % PHYSICAL CONSTANTS AND PARAMETERS
40 RE = 6.378e6; %Earth Radius [m]
41 mu = 3.986e14; %GM Earth
42 g0 = 9.81;
43
44 % SPACECRAFT DATA
45 m = 4; % Satellite mass [kg]
46 Cd = 2.2; % Drag Coefficient
47 A = 0.1*0.3; % Satellite surface [m^2] --> 3U pointing to Earth
48
49 % ORBIT DATA
50 H0 = hmax; % Altura inicial [m]
51 E0 = 0.01; % Excentricity
52 I0 = 80*pi/180; % Inclination [deg]
53 A0 = RE+H0;
54
55 % SIMULATION PARAMETERS
56 N=100000;
57 M = 10000;
58
59 %% 2. Perturbations propagation
60
61 % Creation of the matrices
62 temp=zeros(M,N);
63 temp(1,1)=0;
64 H = zeros(M,N);
65 H(1,1) = H0;
66 % ΔV = zeros(2,N);
67
68 % Asign initial values
69 W0=0; OMEGA0=0;
70 a=zeros(1,N); a(1)=A0;
71 e=a; e(1)=E0;
72 i=a; i(1)=I0;
73 t=a; t(1)=0;
74 w=a; w(1)=W0;
75 Omega=a; Omega(1)=OMEGA0;
76
77 for j = 1:M
78
79     n = 1;
80     while a(n)≥(RE+hmin)
81
82         n = n+1;
83

```

```

84         a0=a(n-1);
85         e0=e(n-1);
86         i0=i(n-1);
87         w0=w(n-1);
88         Omega0=Omega(n-1);
89
90         P=2*pi*(a0^3/mu)^.5; % Orbit Period [s]
91
92         Bc = m/(Cd*A);% Ballistic coefficient of the satellite
93         Perti=Perturbation(a0,e0,i0,Bc);
94
95         a(n)=a0+sum(Perti(:,1));
96         e(n)=e0+sum(Perti(:,2));
97         i(n)=i0+sum(Perti(:,3));
98         w(n)=w0+sum(Perti(:,4));
99         Omega(n)=Omega0+sum(Perti(:,5));
100
101        % We don't want angles bigger than 360!
102        w(n)=w(n)-360*floor(w(n)/360);
103        Omega(n)=Omega(n)-360*floor(Omega(n)/360);
104
105        if Omega(n)>2*pi
106            Omega(n)=Omega(n)-2*pi;
107        end
108
109        t(n)=t(n-1)+P;
110
111    end
112
113    % Hohmann
114    [ΔV1,ΔV2,mpit,tHohit] = Hohmann(a(n)-RE,hmax,m,Isp);
115    m = m-mpit;
116
117    if m≤ms
118        break
119    end
120
121    ΔV(1,j) = ΔV1; % first row of the column -> ΔV1
122    ΔV(2,j) = ΔV2; % second row of the column -> ΔV2
123    mp(j) = mpit;
124    tHoh(j) = tHohit;
125
126    a(1)=A0;
127    e(1)=E0;
128    i(1)=I0;
129    w(1)=W0;
130    Omega(1)=OMEGA0;
131    altura = a-RE;
132
133    H(j,:)=altura;

```

```

134      temp(j,:) = t;
135
136 end
137
138 %% Post process
139
140 mfr = Thr/(g0*Isp);
141
142 for i = 1:N
143     if H(1,i)≤0
144         break
145     end
146 end
147 for j = 1:M
148     if H(j,1)≤0
149         break
150     end
151 end
152 H = H(1:(j-1),1:(i-1));
153
154 for i = 2:N
155     if temp(1,i)≤0
156         break
157     end
158 end
159 for j = 2:M
160     if temp(j,2)≤0
161         break
162     end
163 end
164 temp = temp(1:(j-1),1:(i-1));
165 for j = 2:size(temp,1)
166     temp(j,:) = temp(j,:)+tHoh(j-1)+temp(j-1,size(temp,2));
167 end
168
169 % Convert matrix to vector
170 H = reshape(H.',1,size(H,1)*size(H,2));
171 temp = reshape(temp.',1,size(temp,1)*size(temp,2));
172
173 figure(1)
174 plot(temp/(3600*24),H/1000)
175 grid on
176 ylabel('Orbit height [km]')
177 xlabel('Time [days]')
178 tfin=floor(temp(length(temp))/(3600*24));
179 days=num2str(floor(tfin/365));
180 titulaso=['Orbit decay in ' num2str(tfin) ' days = ' days ' years'];
181 title(titulaso)
182
183 %% Final calculations

```

Thrust

```

184
185 % % Perimeter of the ellipse
186 % r1 = RE+hmax; % semimajor axis
187 % r2 = RE+hmin; % semiminor axis
188 % h = (r1-r2)^2/(r1+r2)^2;
189 % % Ramanujan approximation
190 % C = pi*(r1+r2)*(1+3*h/(10+sqrt(4-3*h)));
191 %
192 % % Check if ΔV is possible for the given thruster
193 % OK = true;
194 % for j = 1:length(mp)
195 %     for i = 1:2
196 %         mfrnecessary = ΔV(i, j)*mp(j)/(C/2);
197 %         if mfrnecessary>mfr
198 %             OK = false;
199 %         end
200 %     end
201 % end
202 %
203 % if OK ==true
204 %     fprintf('The trajectory is possible\n\n');
205 % else
206 %     fprintf('Trajectory not possible\n\n');
207 % end
208 if length(mp)<M
209     fprintf('There is still propellant left ._.\n\n')
210 end

```

```

1 function [ΔV1,ΔV2,mp,t] = Hohmann(hinitial,hfinal,m,Isp)
2
3 % Hohmann transfer orbit between two circular orbits
4 % - hinitial: height of the first orbit [m]
5 % - hfinal: height of the second orbit [m]
6 % - m: mass of the satellite (total) [kg]
7 % - Isp: Specific impulse [s]
8 % - mp: fuel mass [kg]
9 % - t: time needed to do the maneuver [s]
10
11 mu = 3.986004418e14; % Standard gravitational parameter (Earth)
12 REarth = 6.371e6; % [m]
13 g0 = 9.81; % Earth's gravity [m/s^2]
14
15 % First orbit
16 r1 = REarth+hinitial; % [m]
17 v1 = sqrt(mu/r1); % [m/s]
18
19 % Second orbit
20 r2 = REarth+hfinal; % [m]
21 v2 = sqrt(mu/r2); % [m/s]

```

```

22
23 % Transfer orbit (ellipse)
24 vp = sqrt(2*mu*r2/(r1*(r1+r2))); % [m/s]
25 va = sqrt(2*mu*r1/(r2*(r1+r2))); % [m/s]
26 a = (r1+r2)/2;
27 T = sqrt(2*pi^2*a^3/mu);
28
29 % ΔV 1 -> p(transfer orbit)
30 ΔV1 = vp-v1;
31 % ΔV a(transfer orbit) -> 2
32 ΔV2 = v2-va;
33 % Total
34 ΔV = ΔV1+ΔV2;
35
36 % Fuel mass
37 mp = m*(1-exp(-ΔV/(g0*Isp)));
38
39 % Time
40 t = T/2;
41
42 end

```

Satellites Datasheet

```

1 %----ASTREA CONSTELLATION----
2 %PROJECTS - 220028
3 %Aerospace Engineering Bachelor's Degree
4 %ESEIAAT - UPC
5 %Autumn 2016-2017
6
7 % ORBIT DESIGN TEAM
8 % SATELLITES DATASHET
9
10 % Writing the constellation characteristics
11
12 a=6378.01e3;
13 u=3.986012e14;
14 h=(a+542e3)/a;
15 ap=h*a;
16 J2=1.0826e-3;% J2=0;
17
18 ws=sqrt(u/ap^3); % Satellite mean motion
19 i=72*pi/180;
20
21 p=9;
22 spp=21;

```

```

23 N=p*spp;
24 %f=floor(0.25*spp);
25 f=0;
26 fprintf ('\ni=%gdeg, p=%g, spp=%g, N=%g\n',i*180/pi,p,spp,N);
27
28
29 %Omega = 0:30:240; Omega=Omega*pi/180;
30 Omega = 0:225/(p-1):225; %Omega=Omega*pi/180;
31 %Omega=0:360/p:360-360/p; Omega=Omega*pi/180;
32
33 P=2*pi/ws/60;
34
35 %% Excel IMPORT
36
37 D=zeros(N, 9);
38 for sat=1:N
39
40     Om=ceil(sat/spp); ID_p=sat-(Om-1)*spp;
41     ph=(ID_p-1)*360/spp;
42     %[ID Plane h P i e Omega phase per]
43     D(sat,1:9)=[sat Om (ap-a)/1000 P i*180/pi 0 Omega(Om) ph 0];
44
45 end
46 NameCells=['B2:I' num2str(N)];
47 xlswrite('SatsDatasheet.xls',D,NameCells)
48
49 %% Latex IMPORT
50
51 for sat=1:N
52
53     Om=ceil(sat/spp); ID_p=sat-(Om-1)*spp;
54     ph=(ID_p-1)*360/spp;
55     %[ID Plane h P i e Omega phase per]
56     D(sat,1:9)=[sat Om (ap-a)/1000 P i*180/pi 0 Omega(Om) ph 0];
57
58 end
59
60 [rows,cols]=size(D);
61 file=fopen('Autotable.txt','w');
62
63 for i=1:rows
64     Text=['AstreaSAT ' num2str(i) ' $ '];
65     for j=2:cols
66         if j!=cols
67             Text=[Text num2str(D(i,j-1)) ' $ '];
68         else
69             Text=[Text num2str(D(i,j-1)) ' \\ '];
70         end
71     end
72     fprintf(file,[Text '\n']);

```

```

73 end
74
75 fclose(file);

```

Ground Station Localization

```

1 %----ASTREA CONSTELLATION----
2 %PROJECTS - 220028
3 %Aerospace Engineering Bachelor's Degree
4 %ESEIAAT - UPC
5 %Autumn 2016-2017
6
7 % COMMUNICATION TEAM
8 % GROUND STATIONS LOCALIZATION
9
10 clc; clear;
11
12 %% Input Data
13 N_sat=21; %number of sats in a plane
14 N_planes=9; %number of orbital planes
15 h=542; %high of the sats in km
16 I=72; %inclination of the orbits in degrees
17 phase=210/(N_planes-1); %Angle between planes in the equator
18 At=0.1; %time step in minutes
19 T=48; %time to simulate in hours
20 t=0:At:T*60; %array of time in minutes
21 e_min=7.5; %minimum elevation in degrees
22 lambda=57.5; %latitudes to simulate in degrees
23 lat=length(lambda);
24 mu=0; %longitudes to simulate in degrees
25 long=length(mu);
26 l=length(t);
27
28 %% Solver
29
30 Xs=Orbitalposition(N_sat,N_planes,h,I,phase,t);
31 L=zeros(lat,l);
32
33 for i=1:lat
34     Xg=Groundposition(lambda(i),mu,t);
35     [L(i,:)] = Links(Xs,Xg,e_min);
36 end
37
38 %% Plots
39
40 figure;plot(t/60,L);legend 0 30 60 90;xlabel('time (h)');ylabel('links');

```

```

1 function [X] = Orbital_position(N_sat,N_planes,h,I,mu,t)
2 %N_sat: number of sats per plane
3 %N_planes: number of planes
4 %h: Orbit high in km
5 %I: inclination of the orbital plane in degrees
6 %mu: Angle between two adjacent orbital planes at the equatorial plane in
7 %degrees
8 %t: array of time in minutes
9
10 I=I*pi/180;    %I in rad
11 mu=mu*pi/180;  %mu in rad
12 Omega=0:mu:(N_planes-1)*mu;
13 %longitude of the ascending node respect the inertial X axe [rad]
14
15 %for defining the orbits are defined a system of
16 %local axes X_o in which the y_o is the rotation axe and x_o is
17 %contained in the equatorial plane. The transformation for the inertial
18 %system X_I to the local system 2 rotations are defined.
19 %FIRST ROTATION: it defines a intermediate system X_1. The inertial system
20 %rotates around z_I an Omega angle.
21 %SECOND ROTATION: The X_1 system is rotated (90deg-I) around x_1
22
23 L_lo=[1 0 0; 0 sin(I) cos(I); 0 -cos(I) sin(I)]; %1st rotation matrix.
24 %It transform a vector from local coordinates X_o to intermediate
25 %coordinates X_1. This matrix is the same for every orbital plane
26 %since all orbits have the same inclination
27
28 Re=6371;    %Earth radius km.
29 %The distances are going to be referred to the earth radius
30 h=h/Re;      %high in earth radius
31 GM=6.474e-11*5.972e24*3600/Re^3;
32 %Gravitational constant*earth mass [(Re^3)/min^2]
33 Ro=1+h;      %orbital radius in earth radius
34
35 w=sqrt(GM/(Ro^3));  %sat's angular speed [rad/min]
36 phi=0:2*pi/N_sat:(N_sat-1)*2*pi/N_sat;
37 %relative angle between every sat of a plane respect the first one
38 f=8;
39 %factor to module the relative desfase of the first sat of one plane
40 %to the first sat of the next plane
41 l=length(t);
42
43 for p=1:N_planes    %going through each plane
44
45     phi_0(p)=f*2*pi*(p-1)/(N_planes*N_sat);
46     %relative desfase of the first sat of one plane to the
47     %first sat of the next plane
48
49     One = cos(Omega(p));
50     Two = sin(Omega(p));

```

Ground Station Localization

```

51      L_I1=[One -Two 0; Two One 0; 0 0 1];
52      %2nd rotation matrix. It transforms a vector from
53      %intermediate coordinates X_1
54      %to inertial coordinates X_I. This matrix is characteristic of every
55      %plane since every plane has a different longitude of the ascending node
56      %(Omega)
57
58      L_eo=L_I1*L_lo;
59      %Global rotation matrix from local coordinates to inertial coordinates
60
61      for s=1:N_sat    %going through every sat of the plane
62
63          for k=1:l    %going through every time step
64
65              First = Ro*cos(w*t(k)+phi(s)+phi_0(p));
66              Second = -Ro*sin(w*t(k)+phi(s)+phi_0(p));
67              X_loc=[First;0;Second];
68              %Coordinates of the sat at the given time in
69              %local coordinates X_o.
70              %It defines a circumference at the plane x_o-z_o with a angular
71              %velocity w, a initial phase respect the first sat and a
72              %initial phase respect the first sat of the previous orbit
73              %first sat.
74
75              X(:,(p-1)*N_sat+s,k)=L_eo*X_loc;
76              %Coordinates of the sat in inertial system
77              %(Coordinate [x y z], Sat number, instant(time))
78          end
79      end
80  end
81 end

```

```

1 function [X] = Ground_position(lambda,long,t)
2 %Ground_position calculates the position of a place of the earth, with a
3 %given longitude and latitude, in an inertial system of coordinates X_I in
4 %a given period of time
5
6 %lambda: is the latitude of the place in degrees[-90,90]
7 %long: is the longitude of the place in degrees [0,360)
8 %t: is an array of time in minutes
9
10 long=long*pi/180;    %long in radians
11 lambda=lambda*pi/180;  %lambda in radians
12
13 Rg=cos(lambda);
14 %distance between the Earth point to the rotation axis of the Earth [0,1]
15 hg=sin(lambda);
16 %distance between the Earth point to the equatorial plane [0,1]
17 %these 2 distances are measured in earth radius.

```

```
18
19 w=2*pi/(24*60); %angular velocity of the Earth [rad/min]
20
21 X=[Rg*cos(w*t+long);Rg*sin(w*t+long);hg*ones(1,length(t))];
22 %position of the point in X_I
23 %for the given time. The point describes a circumference
24 %with a Rg radius in the horizontal
25 %plane x_I-y_I with an angular velocity w and a initial phase long. The
26 %coordinate z_I is allways hg. It is expresed in earth radius.
27 %X(cooridinates, instant (time)
28
29 end
```

Chapter 15

Bibliography

- [1] Howard D. Curtis. *Orbital Mechanics for Engineering Students*, volume 3rd editio. Elsevier, 2014.
- [2] J.G. Walker. Some Circular Orbit Pattern Providing Continuous Whole Earth Coverage. *Journal of the British Interplanetary Society*, 24:369–384, 1971.
- [3] J.G. Walker. Continuous whole-Earth coverage by circular-orbit satellite patterns. *Royal Aircraft Establishment. Technical report 77044*, 1977.
- [4] Vladimir A Chobotov. *Orbital Mechanics*. 2002.
- [5] Carlos Jorge and Rodrigues Capela. Protocol of Communications for VORSAT Satellite - Link Budget. (April), 2012.
- [6] Application Note. Tutorial on Basic Link Budget Analysis. *Intersil*, (June 1998):1–8, 1998.
- [7] D.A. Vallado. *Fundamentals of Astrodynamics and Applications*. Springer-Verlag New York, 3 edition, 2007.
- [8] R.R. Bate, D.D. Mueller, and J.E. White. *Fundamentals of Astrodynamics*. 1971.
- [9] Behrouz a. Forouzan. *Data Communications and Networking - Global Edition*. 2012.
- [10] CCSDS Secretariat. Overview of Space Communications Protocols. (CCSDS 130.0-G-3):43, 2014.
- [11] CCSDS. TC Space Data Link Protocol. (September), 2010.
- [12] CCSDS. TM Synchronization and Channel Coding—Summary of Concept and Rationale. *CCSDS Green Book*, (November 2012), 2012.

-
- [13] CCSDS. *Report Concerning Space Data System Standards - Overview of Space Communications Protocols*. Number CCSDS 130.0-G-3. 2014.
 - [14] CCSDS. *Recommendation for Space Data System Standards - Space Packet Protocol*. Number CCSDS 133.0-B-1. 2003.
 - [15] CCSDS. *Recommendation for Space Data System Standards - Encapsulation Service*. Number 133.1-B-2. 2009.
 - [16] Space Assigned Number Authority (SANA) Registry. <http://sanaregistry.org/>.
 - [17] CCSDS. *Recommendation for Space Data System Standards - IP over CCSDS Space Links*. Number CCSDS 702.1-B-1. 2012.
 - [18] Information Sciences Institute University of Southern California 4676 Admiralty Way and California 90291 Marina del Rey. *Internet Protocol Specification*. 1981.
 - [19] S Deering and R Hinden. *Internet Protocol, Version 6 (IPv6) Specification*. 1998.
 - [20] Space Assigned Number Authority (SANA) Registry: Packet Version Number. http://sanaregistry.org/r/packet_version_number/packet_version_number.html.
 - [21] Space Assigned Number Authority (SANA) Registry: Application Identifier. http://sanaregistry.org/r/space_packet_protocol_application_process_id/space_packet_protocol_application_process_id.html.
 - [22] Space Assigned Number Authority (SANA) Registry: Protocol Identifier. http://sanaregistry.org/r/protocol_id/protocol_id.html.
 - [23] Space Assigned Number Authority (SANA) Registry: IP Extension header. http://sanaregistry.org/r/ipe_header/ipe_header.html.
 - [24] J Postel. Internet Control Message Protocol. pages 1–21, 1981.
 - [25] A Conta, S Deering, and M Gupta. Internet Control Message Protocol (ICMPv6) for the Internet Protocol Version 6 (IPv6) Specification. 6:1–24, 2006.
 - [26] H Holbrook, B Cain, and B Haberman. *Using Internet Group Management Protocol Version 3 (IGMPv3) and Multicast Listener Discovery Protocol Version 2 (MLDv2) for Source-Specific Multicast*. 2006.
 - [27] S Kent and K Seo. Security Architecture for the Internet Protocol. pages 1–101, 2005.
 - [28] B Fenner, M Handley, H Holbrook, I Kouvelas, R Parekh, Z Zhang, and L Zheng. *Protocol Independent Multicast - Sparse Mode (PIM-SM): Protocol Specification (Revised)*. 2016.

-
- [29] A Adams, J Nicholas, and W Siadak. *Protocol Independent Multicast - Dense Mode (PIM-DM): Protocol Specification (Revised)*. 2005.
 - [30] D Savage, J Ng, S Moore, D Slice, P Paluch, and R White. *Cisco's Enhanced Interior Gateway Routing Protocol (EIGRP)*. 2016.
 - [31] J Moy. *OSPF Version 2 Status*. 1998.
 - [32] R Coltun, D Ferguson, J Moy, and A Lindem. *OSPF for IPv6*. 2008.
 - [33] G Malkin. RIP Version 2. pages 1–39, 1998.
 - [34] G Malkin and R Minnear. RIPng for IPv6. pages 1–19, 1997.
 - [35] Internet Assigned Number Authority (IANA) Registry: Protocol Numbers. <http://www.iana.org/assignments/protocol-numbers/protocol-numbers.xhtml>.
 - [36] Energy Star. US Energy Use Intensity by Property Type, 2016.
 - [37] Endesa. Precios de Tarifas Reguladas Luz y Gas.
 - [38] Precios de contratos de mantenimiento en Madrid | Fojenet.
 - [39] LimpiezasSIL. Como Calcular un Presupuesto de Limpieza.
 - [40] OVO Energy. Average electricity prices around the world.
 - [41] CalPoly. Cubesat design specification (CDS). page 42, 2014.
 - [42] Robert Burt. Distributed Electrical Power System in Cubesat Applications. pages 2–3, 2011.
 - [43] IADC Space Debris Mitigation Guidelines. 2007.
 - [44] Secretaría de Estado de telecomunicaciones y para la sociedad de la información. Cuadro Nacional de Atribución de Frecuencias (CNAF) revisado 2015. pages 3–110, 2015.
 - [45] España. Ministerio de la Presidencia. Real Decreto 278/1995, de 24 de febrero, por el que se crea en España el Registro previsto en el Convenio de 12 de noviembre de 1974 de la Asamblea General de las Naciones Unidas. Ministerio. *Boletín Oficial del Estado*, (58, 9 de marzo), 1995.