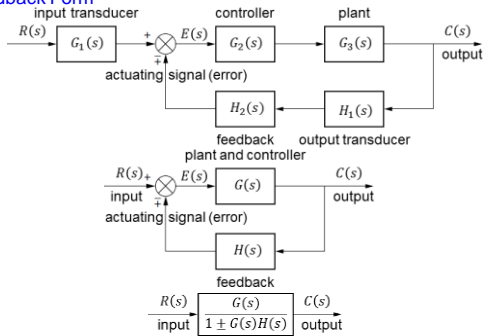




## §2. Block Diagrams

## Feedback Form

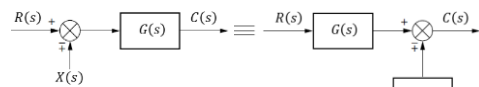


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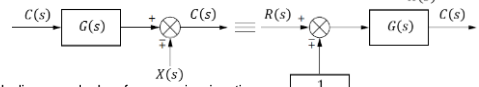
Nguyen Tan Tien

## §2. Block Diagrams

## Moving Blocks to Create Familiar Forms



Block diagram algebra for summing junctions - equivalent forms for moving a block to the left past a summing junction

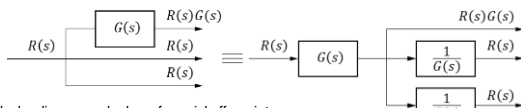


Block diagram algebra for summing junctions - equivalent forms for moving a block to the right past a summing junction

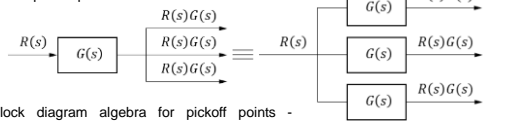
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## §2. Block Diagrams



Block diagram algebra for pickoff points - equivalent forms for moving a block to the left past a pickoff point



Block diagram algebra for pickoff points - equivalent forms for moving a block to the right past a pickoff point

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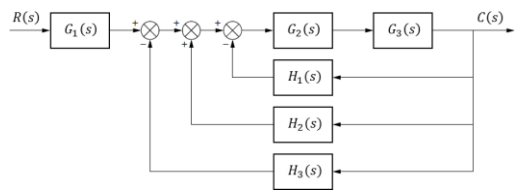
Nguyen Tan Tien

## §2. Block Diagrams

## - Ex.5.1

## Block Diagram Reduction via Familiar Forms

Reduce the block diagram to a single transfer function



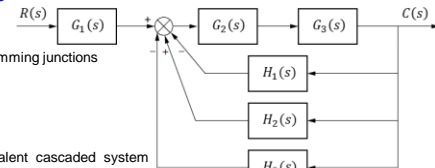
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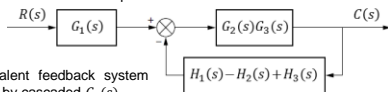
## §2. Block Diagrams

## Solution

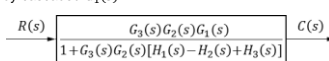
1. Collapse summing junctions



2. Form equivalent cascaded system in the forward path and equivalent parallel system in the feedback path



3. Form equivalent feedback system and multiply by cascaded G1(s)



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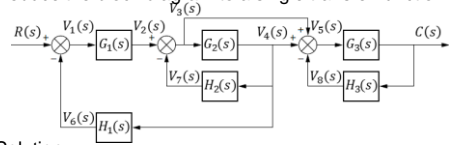
Nguyen Tan Tien

## §2. Block Diagrams

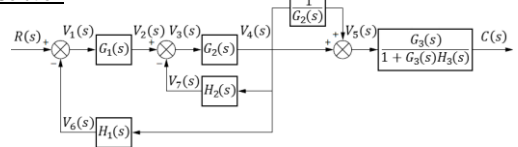
## - Ex.5.2

## Block Diagram Reduction via Familiar Forms

Reduce the block diagram to a single transfer function



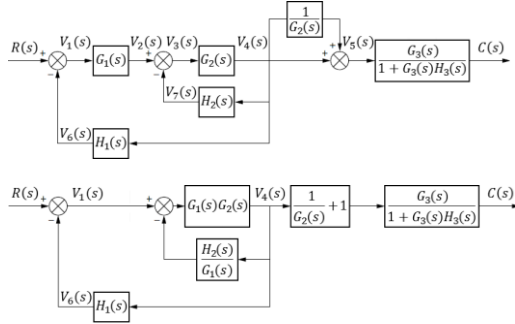
## Solution



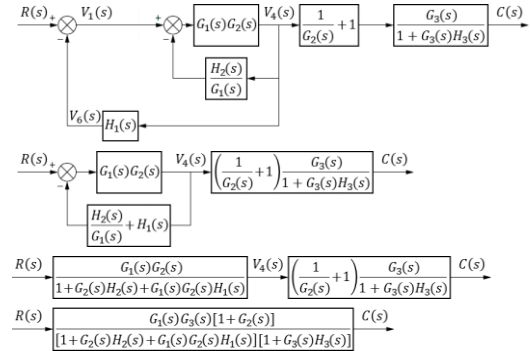
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Nguyen Tan Tien

## §2. Block Diagrams



## §2. Block Diagrams



## §2. Block Diagrams



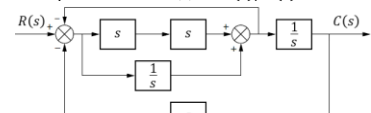
Run ch5p1 in Appendix B

Learn how to use MATLAB to

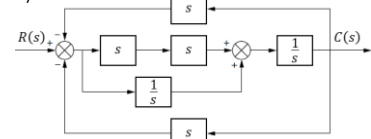
- perform block diagram reduction

## §2. Block Diagrams

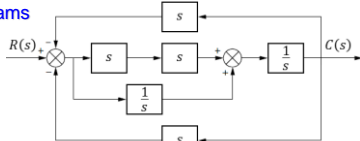
## Skill-Assessment Ex.5.1

**Problem** Find the equivalent TF,  $T(s) = C(s)/R(s)$ , for the system**Solution**

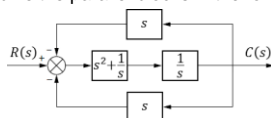
Push 1/s to the left



## §2. Block Diagrams



Combine the parallel blocks in the forward path



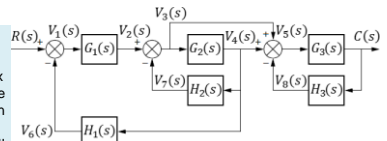
Apply the feedback formula, simplify, and get

$$T(s) = \frac{s^3 + 1}{2s^4 + s^2 + 2s}$$

## §2. Block Diagrams

## TryIt 5.1

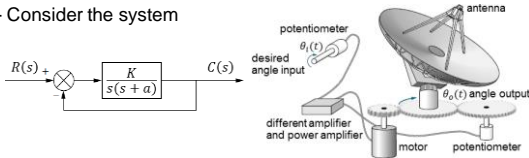
Use the following MATLAB and Control System Toolbox statements to find the closed loop transfer function of the system in Ex.5.2 if all  $G_i(s) = 1/(s+1)$  and all  $H_i(s) = 1/s$



```
G1=tf(1,[1 1]); G2=G1; G3=G1;
H1=tf(1,[1 0]); H2=H1; H3=H1;
System=append(G1,G2,G3,H1,H2,H3);
input=1; output=3;
Q=[1 -4 0 0 0; 2 1 -5 0 0; 3 2 1 -5 -6;
4 2 0 0 0; 5 2 0 0 0; 6 3 0 0 0];
T=connect(System,Q,input,output);
T=tf(T); T=minreal(T)
```

## §3. Analysis and Design of Feedback Systems

- Consider the system



which can model a control system such as the antenna azimuth position control system. For example, the transfer function,  $K/s(s+a)$ , can model the amplifiers, motor, load, and gears.

The closed-loop transfer function,  $T(s)$ , for this system

$$T(s) = \frac{K}{s^2 + as + K}$$

$K$  : models the amplifier gain, that is, the ratio of the output voltage to the input voltage

## §3. Analysis and Design of Feedback Systems

$$T(s) = \frac{K}{s^2 + as + K}$$

- As  $K$  varies, the poles move through the three ranges of operation of a second-order system

$$\bullet \text{ overdamped: } 0 < K < a^2/4 \quad s_{1,2} = -\frac{a}{2} \pm \frac{\sqrt{a^2 - 4K}}{2}$$

As  $K$  increases, the poles move along the real axis

$$\bullet \text{ critically damped: } K = a^2/4 \quad s_{1,2} = -\frac{a}{2}$$

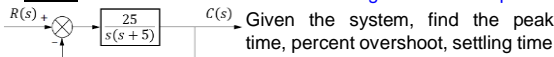
$$\bullet \text{ underdamped: } K > a^2/4 \quad s_{1,2} = -\frac{a}{2} \pm j \frac{\sqrt{4K - a^2}}{2}$$

As  $K$  increases, the real part remains constant and the imaginary part increases. Thus, the peak time decreases and the percent overshoot increases, while the settling time remains constant

## §3. Analysis and Design of Feedback Systems

- Ex.5.3

Finding Transient Response



Given the system, find the peak time, percent overshoot, settling time

Solution

The closed-loop transfer function

$$T(s) = \frac{25}{s^2 + 5s + 25} = \frac{5^2}{s^2 + 2 \times 0.5 \times 5s + 5^2}$$

and  $\omega_n = \sqrt{25} = 5$ ,  $\zeta = 0.5$ . From these values of  $\zeta$  and  $\omega_n$

$$T_p = \frac{\pi}{\omega_n \sqrt{1 - \zeta^2}} = \frac{\pi}{5 \sqrt{1 - 0.5^2}} = 0.726s$$

$$\%OS = e^{-\zeta \pi / \sqrt{1 - \zeta^2}} \times 100 = e^{-0.5 \pi / \sqrt{1 - 0.5^2}} \times 100 = 16.303$$

$$T_s = \frac{4}{\zeta \omega_n} = \frac{4}{0.5 \times 5} = 1.6s$$

## §3. Analysis and Design of Feedback Systems

MATLAB

ML

Run ch5p2 in Appendix B

Learn how to use MATLAB to

- perform block diagram reduction followed by an evaluation of the closed-loop system's transient response by finding,  $T_p$ ,  $\%OS$ , and  $T_s$
- generate a closed-loop step response
- solve Ex.5.3

## §3. Analysis and Design of Feedback Systems

Simulink

SL

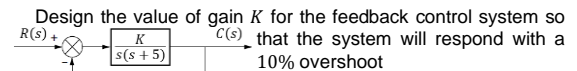
Learn how to use MATLAB's Simulink to

- explore the added capability of MATLAB's Simulink using Appendix C
- simulate feedback systems with nonlinearities through Ex.C.3 (p.842 Textbook)

## §3. Analysis and Design of Feedback Systems

- Ex.5.4

Gain Design for Transient Response



Design the value of gain  $K$  for the feedback control system so that the system will respond with a 10% overshoot

Solution

The closed-loop transfer function

$$\begin{aligned} T(s) &= \frac{K}{s(s+5)} \cdot \frac{K}{s^2 + 5s + K} \\ &= \frac{(\sqrt{K})^2}{s^2 + 2 \times \frac{5}{2\sqrt{K}} \times \sqrt{K}s + (\sqrt{K})^2} \end{aligned}$$

$$\text{and } \omega_n = \sqrt{K}, \zeta = 5/2\sqrt{K}$$

### §3. Analysis and Design of Feedback Systems

Percent overshoot is a function only of  $\zeta$

$$\%OS = e^{-\zeta\pi/\sqrt{1-\zeta^2}} \times 100 = 10\%$$

$$\Rightarrow \zeta = 0.591$$

From this damping ratio

$$\zeta = \frac{5}{2\sqrt{K}}$$

$$\Rightarrow K = \left(\frac{5}{2\zeta}\right)^2 = \left(\frac{5}{2 \times 0.591}\right)^2 = 17.9$$

Although we are able to design for percent overshoot in this problem, we could not have selected settling time as a design criterion because, regardless of the value of  $K$ , the real parts,  $-2.5$ , of the poles of  $K/(s^2 + 5s + K)$  remain the same

### §3. Analysis and Design of Feedback Systems

#### Skill-Assessment Ex.5.2

**Problem** For a unity feedback control system with a forward-path TF  $G(s) = 16/s(s+a)$ , design the value of  $a$  to yield a closed-loop step response that has 5% overshoot

**Control Solutions**

**Solution** The closed-loop transfer function

$$T(s) = \frac{G(s)}{1 + G(s)H(s)} = \frac{16}{s^2 + as + 16} = \frac{4^2}{s^2 + 2 \times \frac{a}{8} \times 4s + 4^2}$$

$$\text{and } \omega_n = 4, \zeta = a/8$$

Percent overshoot

$$\%OS = e^{-\zeta\pi/\sqrt{1-\zeta^2}} \times 100$$

$$\Rightarrow \zeta = \frac{-\ln(\%OS)}{\sqrt{\pi^2 + \ln^2(\%OS)}} = \frac{-\ln(0.05)}{\sqrt{\pi^2 + \ln^2(0.05)}} = 0.69$$

$$\Rightarrow a = 8\zeta = 8 \times 0.69 = 5.52$$

### §3. Analysis and Design of Feedback Systems

#### TryIt 5.2

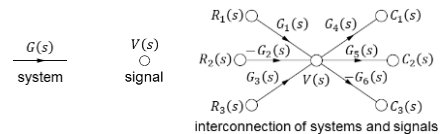
Use the following MATLAB and Control System Toolbox statements to find  $\zeta$ ,  $\omega_n$ ,  $\%OS$ ,  $T_s$ ,  $T_p$ , and  $T_r$  for the closed-loop unity feedback system described in Skill-Assessment Ex.5.2. Start with  $a = 2$  and try some other values. A step response for the closed loop system will also be produced

```
G(s) = 16/(s(s+a))
a=2; numg=16; deng=poly([0 -a]);
G=tf(numg,deng);
T=feedback(G,1);
[numt,dent]=tfdata(T,'v');
wn=sqrt(dent(3));
z=dent(2)/(2*wn);
Ts=4/(z*wn);
Tp=pi/(wn*sqrt(1-z^2));
pos=exp(-z*pi/sqrt(1-z^2))*100;
Tr=(1.76*z^3-0.417*z^2+1.039*z+1)/wn;
step(T)
```

### §4. Signal-Flow Graphs

- A signal-flow graph consists only of

- branches: represent systems
- nodes: represent signals



- A system is represented by a line with an arrow showing the direction of signal flow through the system. Adjacent to the line we write the transfer function. A signal is a node with the signal's name written adjacent to the node

### §4. Signal-Flow Graphs

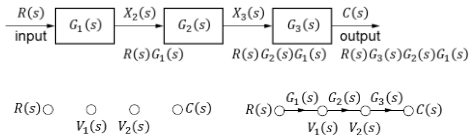
#### - Ex.5.5 Converting Common Block Diagrams to Signal-Flow Graphs

Convert the cascaded, parallel, and feedback forms of the following block diagrams into signal-flow graphs

#### Solution

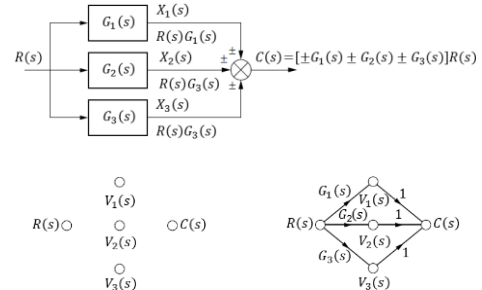
- Start by drawing the signal nodes for that system
- Next interconnect the signal nodes with system branches

#### a. Cascaded form



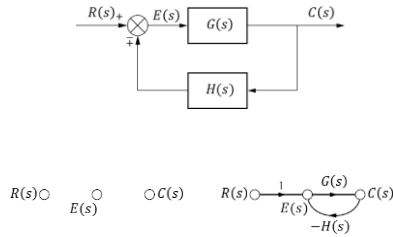
### §4. Signal-Flow Graphs

#### b. Parallel form



## §4. Signal-Flow Graphs

## c. Feedback form

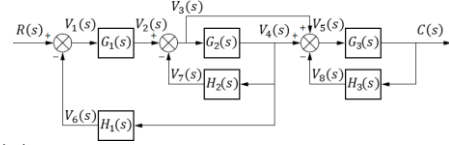


## §4. Signal-Flow Graphs

## - Ex.5.6

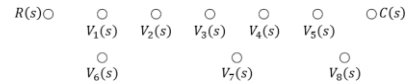
## Converting a Block Diagram to a Signal-Flow Graph

Convert the block diagram to a signal-flow graph

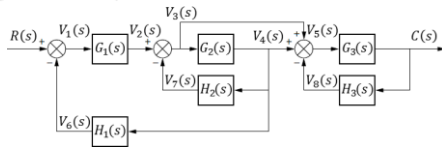


## Solution

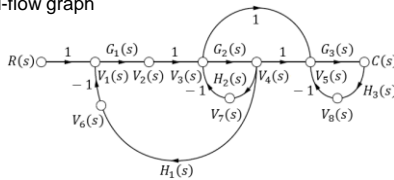
## Signal nodes



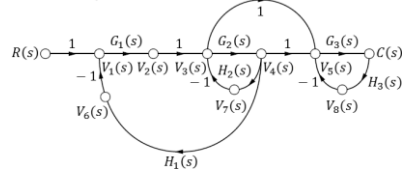
## §4. Signal-Flow Graphs



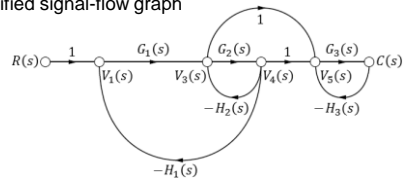
## Signal-flow graph



## §4. Signal-Flow Graphs



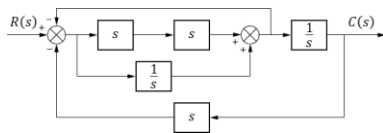
## Simplified signal-flow graph



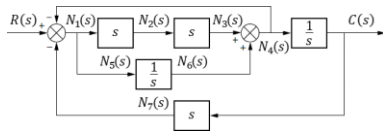
## §4. Signal-Flow Graphs

## Skill-Assessment Ex.5.3

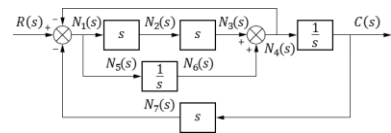
Problem Convert the block diagram to a signal-flow graph



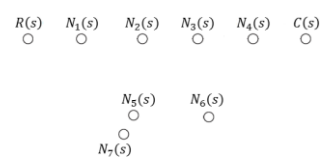
## Solution Label nodes



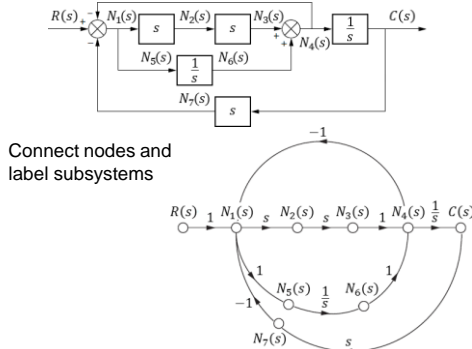
## §4. Signal-Flow Graphs



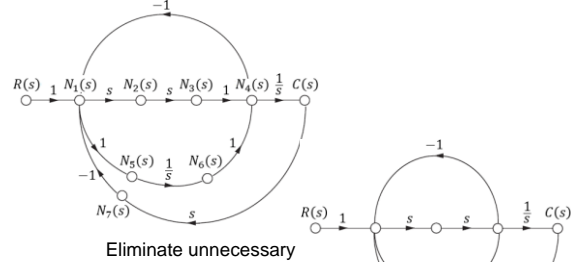
## Draw nodes



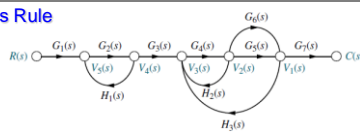
## §4. Signal-Flow Graphs



## §4. Signal-Flow Graphs



## §5. Mason's Rule

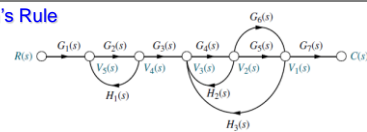


- **Loop gain:** the product of branch gains found by traversing a path that starts at a node and ends at the same node, following the direction of the signal flow, without passing through any other node more than once

Ex.

$$\begin{aligned} G_2(s)H_1(s) \\ G_4(s)H_2(s) \\ G_4(s)G_5(s)H_3(s) \\ G_4(s)G_6(s)H_3(s) \end{aligned}$$

## §5. Mason's Rule

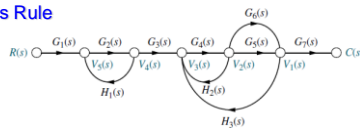


- **Forward-path gain:** the product of gains found by traversing a path from the input node to the output node of the signal-flow graph in the direction of signal flow

Ex.

$$\begin{aligned} G_1(s)G_2(s)G_3(s)G_4(s)G_5(s)G_7(s) \\ G_1(s)G_2(s)G_3(s)G_4(s)G_6(s)G_7(s) \end{aligned}$$

## §5. Mason's Rule

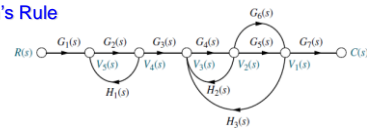


- **Nontouching loops:** loops that do not have any nodes in common

Ex.

Loop  $G_2(s)H_1(s)$  does not touch loops  $G_4(s)H_2(s)$ ,  $G_4(s)G_5(s)H_3(s)$ , and  $G_4(s)G_6(s)H_3(s)$

## §5. Mason's Rule



- **Nontouching-loop gain:** the product of loop gains from nontouching loops taken two, three, four, or more at a time

Ex.

The product of loop gain  $G_2(s)H_1(s)$  and loop gain  $G_4(s)H_2(s)$  is a nontouching-loop gain **taken two at a time**

In summary, all three of the nontouching-loop gains **taken two at a time**

$$\begin{aligned} [G_2(s)H_1(s)][G_4(s)H_2(s)] \\ [G_2(s)H_1(s)][G_4(s)G_5(s)H_3(s)] \\ [G_2(s)H_1(s)][G_4(s)G_6(s)H_3(s)] \end{aligned}$$

## §5. Mason's Rule

## - Mason's Rule

The transfer function,  $C(s)/R(s)$ , of a system represented by a signal-flow graph is

$$G(s) = \frac{C(s)}{R(s)} = \frac{\sum_k T_k \Delta_k}{\Delta}$$

$k$  : number of forward paths

$T_k$  : the  $k^{th}$  forward-path gain

$\Delta$  :  $1 - \sum$  loop gains +  $\sum$  nontouching-loop gains taken two at a time  $- \sum$  nontouching-loop gains taken three at a time +  $\sum$  nontouching-loop gains taken four at a time  $- \dots$

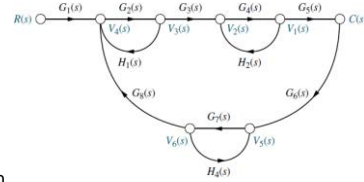
$\Delta_k$  :  $\Delta - \sum$  loop gain terms in  $\Delta$  that touch the  $k^{th}$  forward path. In other words,  $\Delta_k$  is formed by eliminating from  $\Delta$  those loop gains that touch the  $k^{th}$  forward path

## §5. Mason's Rule

## - Ex.5.7

## Transfer Function via Mason's Rule

Find the transfer function,  $C(s)/R(s)$ , for the signal-flow graph

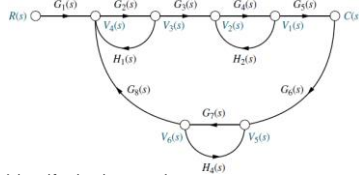


## Solution

First, identify the forward-path gains

$$G_1(s)G_2(s)G_3(s)G_4(s)G_5(s)$$

## §5. Mason's Rule



Second, identify the loop gains

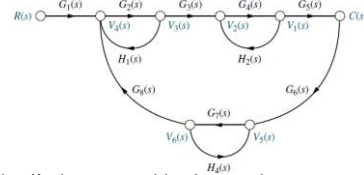
$$G_2(s)H_1(s)$$

$$G_4(s)H_2(s)$$

$$G_7(s)H_4(s)$$

$$G_2(s)G_3(s)G_4(s)G_5(s)G_6(s)G_7(s)G_8(s)$$

## §5. Mason's Rule



Third, identify the nontouching loops taken two at a time

- loop 1 does not touch loop 2:  $G_2(s)H_1(s)G_4(s)H_2(s)$

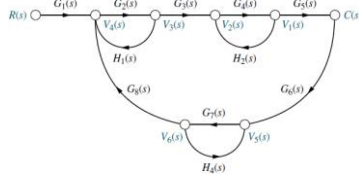
- loop 1 does not touch loop 3:  $G_2(s)H_1(s)G_7(s)H_4(s)$

- loop 2 does not touch loop 3:  $G_4(s)H_2(s)G_7(s)H_4(s)$

Finally, the nontouching loops taken three at a time

- loops 1, 2 and 3:  $G_2(s)H_1(s)G_4(s)H_2(s)G_7(s)H_4(s)$

## §5. Mason's Rule

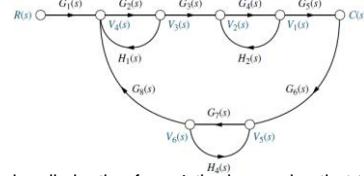


Form  $\Delta$

$$\begin{aligned} \Delta = 1 &- [G_2(s)H_1(s) + G_4(s)H_2(s) + G_7(s)H_4(s) \\ &+ G_2(s)G_3(s)G_4(s)G_5(s)G_6(s)G_7(s)G_8(s)] \\ &+ [G_2(s)H_1(s)G_4(s)H_2(s) + G_2(s)H_1(s)G_7(s)H_4(s) \\ &+ G_4(s)H_2(s)G_7(s)H_4(s)] \\ &- [G_2(s)H_1(s)G_4(s)H_2(s)G_7(s)H_4(s)] \end{aligned}$$

$\Delta$  :  $1 - \sum$  loop gains +  $\sum$  nontouching-loop gains taken two at a time  $- \sum$  nontouching-loop gains taken three at a time +  $\sum$  nontouching-loop gains taken four at a time  $- \dots$

## §5. Mason's Rule



Form  $\Delta_k$  by eliminating from  $\Delta$  the loop gains that touch the  $k^{th}$  forward path

$$\Delta_1 = 1 - G_7(s)H_4(s)$$

The transfer function

$$G(s) = \frac{T_1 \Delta_1}{\Delta} = \frac{[G_1(s)G_2(s)G_3(s)G_4(s)G_5(s)][1 - G_7(s)H_4(s)]}{\Delta}$$

$\Delta_k$  :  $\Delta - \sum$  loop gain terms in  $\Delta$  that touch the  $k^{th}$  forward path. In other words,  $\Delta_k$  is formed by eliminating from  $\Delta$  those loop gains that touch the  $k^{th}$  forward path

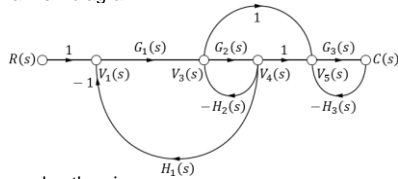


## §5. Mason's Rule

## Skill-Assessment Ex.5.4

**Problem** Use Mason's rule to find the transfer function of the signal-flow diagram

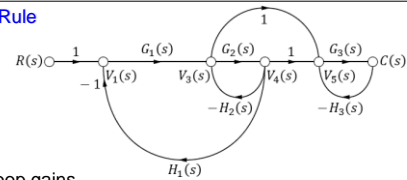
WileyPLUS  
WPCS  
Control Solutions



**Solution** Forward path gains

- $G_1 G_2 G_3$
- $G_1 G_3$

## §5. Mason's Rule



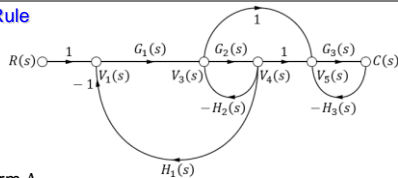
Loop gains

- $-G_1 G_2 H_1$
- $-G_2 H_2$
- $-G_3 H_3$

Nontouching loops

- $[-G_1 G_2 H_1][-G_3 H_3] = G_1 G_2 G_3 H_1 H_3$
- $[-G_2 H_2][-G_3 H_3] = G_2 G_3 H_2 H_3$

## §5. Mason's Rule



Form  $\Delta$

$$\Delta = 1 + G_1 G_2 H_1 + G_2 H_2 + G_3 H_3 + G_1 G_2 G_3 H_1 H_3 + G_2 G_3 H_2 H_3$$

Form  $\Delta_k$

$$\Delta_1 = 1$$

$$\Delta_2 = 1$$

The transfer function

$$T(s) = \frac{C(s)}{R(s)} = \frac{\sum_k T_k \Delta_k}{\Delta} = \frac{G_1 G_3 [1 + G_2]}{[1 + G_2 H_2 + G_1 G_2 H_1][1 + G_3 H_3]}$$

## §6. Signal-Flow Graphs of State Equations

- Consider the following state and output equations

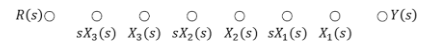
$$\dot{x}_1 = 2x_1 - 5x_2 + 3x_3 + 2r$$

$$\dot{x}_2 = -6x_1 - 2x_2 + 2x_3 + 5r$$

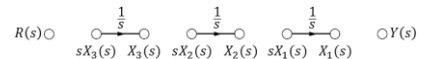
$$\dot{x}_3 = x_1 - 3x_2 - 4x_3 + 7r$$

$$y = -4x_1 + 6x_2 + 9x_3$$

- First, identify state variables,  $x_1$ ,  $x_2$ , and  $x_3$ ; nodes, the input,  $r$ , and the output,  $y$



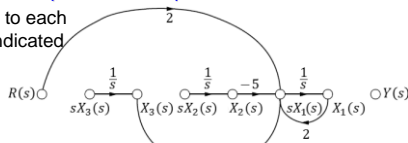
- Next interconnect the state variables and their derivatives with the defining integration,  $1/s$



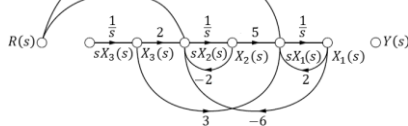
## §6. Signal-Flow Graphs of State Equations

- Then, feed to each node the indicated signals

- $sX_1(s)$



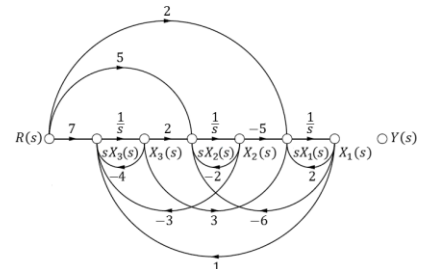
- $sX_2(s)$



$$\dot{x}_1 = 2x_1 - 5x_2 + 3x_3 + 2r, \quad \dot{x}_2 = -6x_1 - 2x_2 + 2x_3 + 5r$$

## §6. Signal-Flow Graphs of State Equations

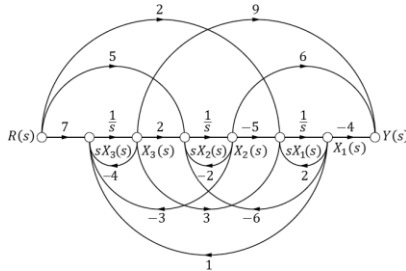
- $sX_3(s)$



$$\dot{x}_3 = x_1 - 3x_2 - 4x_3 + 7r$$

## §6. Signal-Flow Graphs of State Equations

- Finally, the output,  $y$



$$y = -4x_1 + 6x_2 + 9x_3$$

## §6. Signal-Flow Graphs of State Equations

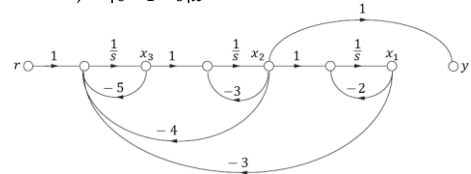
## Skill-Assessment Ex.5.5

**Problem** Draw a signal-flow graph for the following state and output equations

$$\dot{x} = \begin{bmatrix} -2 & 1 & 0 \\ 0 & -3 & 1 \\ -3 & -4 & -5 \end{bmatrix} x + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} r$$

$$y = [0 \quad 1 \quad 0]x$$

**Solution**



$$\dot{x}_1 = -2x_1 + x_2, \quad \dot{x}_2 = -3x_2 + x_3, \quad \dot{x}_3 = -3x_1 - 4x_2 - 5x_3 + r, \quad y = x_2$$

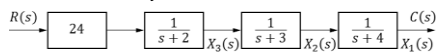
## §7. Alternative Representations in State Space

## Cascade Form

- Consider the system  $\frac{R(s)}{C(s)} = \frac{24}{s^3 + 9s^2 + 26s + 24}$

$$\frac{C(s)}{R(s)} = \frac{24}{s^3 + 9s^2 + 26s + 24} = \frac{24}{(s+2)(s+3)(s+4)} \quad (5.37)$$

- A block diagram representation of this system formed as cascaded first-order systems



Note: these state variables are not the phase variables

- Transforming each block into an equivalent differential equation and cross-multiplying

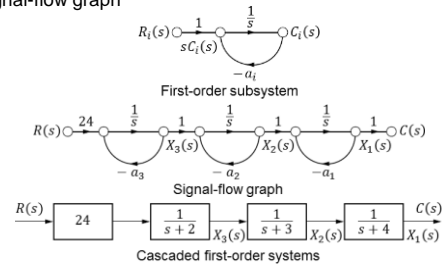
$$\frac{C_i(s)}{R_i(s)} = \frac{1}{s + a_i} \Rightarrow (s + a_i)C_i(s) = R_i(s) \quad (5.39)$$

## §7. Alternative Representations in State Space

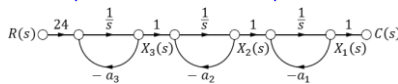
- Solving for  $dc_i(t)/dt$  yields

$$(s + a_i)C_i(s) = R_i(s) \Rightarrow \frac{dc_i(t)}{dt} = -a_i c_i(t) + r_i(t)$$

- Signal-flow graph



## §7. Alternative Representations in State Space



- The state equations for the new representation of the system

$$\begin{aligned} \dot{x}_1 &= -4x_1 + x_2 \\ \dot{x}_2 &= -3x_2 + x_3 \\ \dot{x}_3 &= -2x_3 + 24r \end{aligned}$$

with the system output

$$y = c(t) = x_1$$

- The state equations in vector-matrix form

$$\dot{x} = \begin{bmatrix} -4 & 1 & 0 \\ 0 & -3 & 1 \\ 0 & 0 & -2 \end{bmatrix} x + \begin{bmatrix} 0 \\ 0 \\ 24 \end{bmatrix} r$$

$$y = [1 \quad 0 \quad 0]x$$

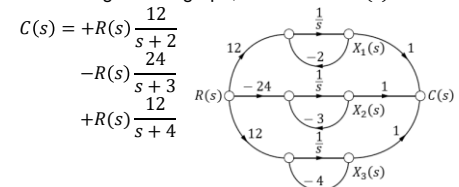
## §7. Alternative Representations in State Space

## Parallel Form

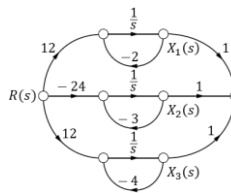
- Consider the system  $\frac{R(s)}{C(s)} = \frac{24}{s^3 + 9s^2 + 26s + 24}$

$$\frac{C(s)}{R(s)} = \frac{24}{s^3 + 9s^2 + 26s + 24} = \frac{12}{s+2} - \frac{24}{s+3} + \frac{12}{s+4} \quad (5.45)$$

- To arrive at a signal-flow graph, first solve for  $C(s)$



## §7. Alternative Representations in State Space



- The state equations for the new representation of the system

$$\begin{aligned}\dot{x}_1 &= -2x_1 + 12r \\ \dot{x}_2 &= -3x_2 - 24r \\ \dot{x}_3 &= -4x_3 + 12r\end{aligned}$$

- The output equation is found by summing the signals that give  $c(t)$

$$y = c(t) = x_1 + x_2 + x_3$$

- The state equations in vector-matrix form

$$\dot{\mathbf{x}} = \begin{bmatrix} -2 & 0 & 0 \\ 0 & -3 & 0 \\ 0 & 0 & -4 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 12 \\ -24 \\ 12 \end{bmatrix} r \quad (5.49)$$

$$y = [1 \quad 1 \quad 1] \mathbf{x}$$

## §7. Alternative Representations in State Space



Run ch5p3 in Appendix B

Learn how to use MATLAB to

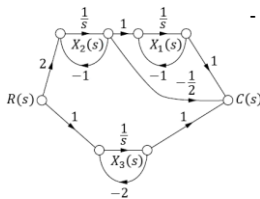
- use MATLAB to convert a transfer function to state space in a specified form
- solve the previous example by representing the transfer function in Eq.(5.45) by the state-space representation in parallel form of Eq.(5.49)

## §7. Alternative Representations in State Space

- If the denominator of the TF has repeated real roots

$$\frac{C(s)}{R(s)} = \frac{s+3}{(s+1)^2(s+2)} = \frac{2}{(s+1)^2} - \frac{1}{s+1} + \frac{1}{s+2}$$

Proceeding as before, the signal-flow graph



- The state equations

$$\begin{aligned}\dot{x}_1 &= -x_1 + x_2 \\ \dot{x}_2 &= -x_2 + 2r \\ \dot{x}_3 &= -2x_3 + r\end{aligned}$$

$$y = c(t) = x_1 - 0.5x_2 + x_3$$

or, in vector-matrix form

$$\dot{\mathbf{x}} = \begin{bmatrix} -1 & 1 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & -2 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 2 \\ 1 \end{bmatrix} r$$

$$y = [1 \quad -0.5 \quad 1] \mathbf{x}$$

- Note: the system matrix will not be diagonal

## §7. Alternative Representations in State Space

## Controller Canonical Form

- Consider the system  $\frac{C(s)}{R(s)} = \frac{s^2 + 7s + 2}{s^3 + 9s^2 + 26s + 24}$  (5.55)

- The phase-variable form

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -24 & -26 & -9 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} r, y = \begin{bmatrix} 2 & 7 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} \quad (5.56)$$

- Renumbering the phase variables in reverse order yields

$$\begin{bmatrix} \dot{x}_3 \\ \dot{x}_2 \\ \dot{x}_1 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -24 & -26 & -9 \end{bmatrix} \begin{bmatrix} x_3 \\ x_2 \\ x_1 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} r, y = \begin{bmatrix} 2 & 7 & 1 \end{bmatrix} \begin{bmatrix} x_3 \\ x_2 \\ x_1 \end{bmatrix} \quad (5.57)$$

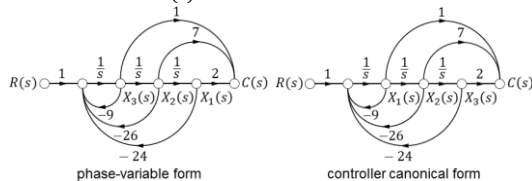
- Finally, rearranging in the controller canonical form

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} -24 & -26 & -9 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} r, y = \begin{bmatrix} 1 & 7 & 2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} \quad (5.58)$$

## §7. Alternative Representations in State Space

- Signal-flow graphs for obtaining forms for

$$\frac{C(s)}{R(s)} = \frac{s^2 + 7s + 2}{s^3 + 9s^2 + 26s + 24}$$



phase-variable form

controller canonical form

## §7. Alternative Representations in State Space

## TryIt 5.3

Use the following MATLAB and Control System Toolbox statements to convert the transfer function of Eq. (5.55) to the controller canonical state-space representation of Eqs. (5.58)

$$\frac{C(s)}{R(s)} = \frac{s^2 + 7s + 2}{s^3 + 9s^2 + 26s + 24} \quad (5.55)$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} -24 & -26 & -9 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} r \quad (5.58)$$

$$y = \begin{bmatrix} 1 & 7 & 2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$$

```
numg=[1 7 2];
```

```
deng=[1 9 26 24];
```

```
[Acc,Bcc,Ccc,Dcc]=tf2ss(numg,deng)
```

## §7. Alternative Representations in State Space

## Observer Canonical Form

- Consider the system

$$\frac{C(s)}{R(s)} = \frac{s^2 + 7s + 2}{s^3 + 9s^2 + 26s + 24} = \frac{\frac{1}{s} + \frac{7}{s^2} + \frac{2}{s^3}}{1 + \frac{9}{s} + \frac{26}{s^2} + \frac{24}{s^3}} \quad (5.59)$$

- Cross-multiplying yields

$$\left(\frac{1}{s} + \frac{7}{s^2} + \frac{2}{s^3}\right)R(s) = \left(1 + \frac{9}{s} + \frac{26}{s^2} + \frac{24}{s^3}\right)C(s) \quad (5.60)$$

- Combining terms of like powers of integration gives

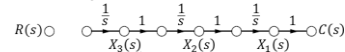
$$C = \frac{1}{s} \left\{ (R - 9C) + \frac{1}{s} \left[ (7R - 26C) + \frac{1}{s} (2R - 24C) \right] \right\} \quad (5.62)$$

This equation can be used to draw the signal-flow graph

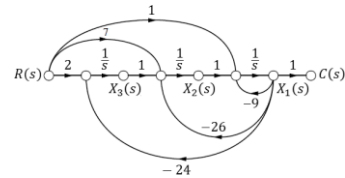
## §7. Alternative Representations in State Space

$$C = \frac{1}{s} \left\{ (R - 9C) + \frac{1}{s} \left[ (7R - 26C) + \frac{1}{s} (2R - 24C) \right] \right\} \quad (5.62)$$

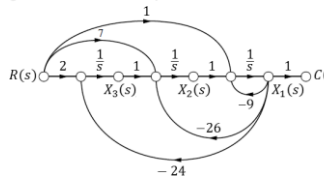
- Start with three integrations



- Signal-flow graph for observer canonical form variables



## §7. Alternative Representations in State Space



- The state equation

$$\begin{aligned} \dot{x}_1 &= -9x_1 + x_2 + r \\ \dot{x}_2 &= -26x_1 + x_3 + 7r \\ \dot{x}_3 &= -24x_1 + 2r \\ y &= c(t) = x_1 \end{aligned}$$

- The state equations in vector-matrix form

$$\dot{x} = \begin{bmatrix} -9 & 1 & 0 \\ -26 & 0 & 1 \\ -24 & 0 & 0 \end{bmatrix} x + \begin{bmatrix} 1 \\ 7 \\ 2 \end{bmatrix} r \quad (5.65)$$

$$y = [1 \ 0 \ 0]x$$

## §7. Alternative Representations in State Space

## TryIt 5.4

Use the following MATLAB and Control System Toolbox statements to convert the transfer function of Eq. (5.55) to the observer canonical state space representation of Eqs. (5.65)

$$\frac{C(s)}{R(s)} = \frac{s^2 + 7s + 2}{s^3 + 9s^2 + 26s + 24} \quad (5.55)$$

$$\dot{x} = \begin{bmatrix} -9 & 1 & 0 \\ -26 & 0 & 1 \\ -24 & 0 & 0 \end{bmatrix} x + \begin{bmatrix} 1 \\ 7 \\ 2 \end{bmatrix} r \quad (5.65)$$

$$y = [1 \ 0 \ 0]x$$

```
numg=[1 7 2];
deng=[1 9 26 24];
[Acc,Bcc,Ccc,Dcc]=tf2ss(numg,deng);
Aoc=transpose(Acc);
Boc=transpose(Bcc);
Coc=transpose(Ccc);
```

## §7. Alternative Representations in State Space

## - Ex.5.8 State-Space Representation of Feedback Systems

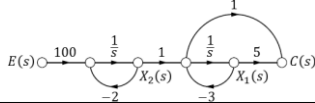
Represent the feedback control system in state space. Model the forward transfer function in cascade form

## Solution

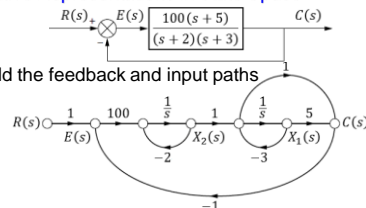
First, model the forward transfer function in cascade form

• The gain of 100, the pole at  $-2, -3 \rightarrow$  in cascaded form

• The zero at  $-5 \rightarrow$  obtained using the method for implementing zeros for a system represented in phase-variable form, as discussed in Section 3.5



## §7. Alternative Representations in State Space



Next add the feedback and input paths

by inspection, write the state equations

$$\begin{aligned} \dot{x}_1 &= -3x_1 + x_2 \\ \dot{x}_2 &= -2x_2 + 100(r - c) \end{aligned}$$

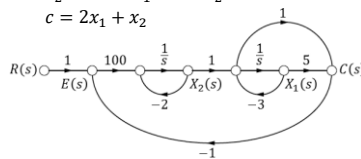
The output  $c = 5x_1 + (x_2 - 3x_1) = 2x_1 + x_2$

$$\begin{aligned} \dot{x}_1 &= -3x_1 + x_2 \\ \dot{x}_2 &= -200x_1 - 102x_2 + 100 \end{aligned}$$

## §7. Alternative Representations in State Space

Then

$$\begin{aligned}\dot{x}_1 &= -3x_1 + x_2 \\ \dot{x}_2 &= -200x_1 - 102x_2 + 100 \\ c &= 2x_1 + x_2\end{aligned}$$



In vector-matrix form

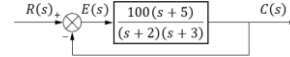
$$\begin{aligned}\dot{\mathbf{x}} &= \begin{bmatrix} -3 & 1 \\ -200 & -102 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 100 \end{bmatrix} r \\ y &= \begin{bmatrix} 2 & 1 \end{bmatrix} \mathbf{x}\end{aligned}$$

## §7. Alternative Representations in State Space

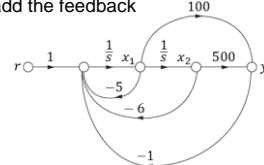
## Skill-Assessment Ex.5.6

**Problem** Represent the feedback control system in state space. Model the forward transfer function in controller canonical form

Control Solutions



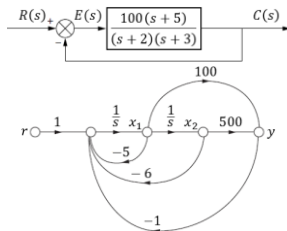
**Solution** Draw the signal-flow graph in controller canonical form and add the feedback



## §7. Alternative Representations in State Space

Writing the state equations from the signal-flow diagram

$$\begin{aligned}\dot{\mathbf{x}} &= \begin{bmatrix} -105 & -506 \\ 1 & 0 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 1 \\ 0 \end{bmatrix} r \\ y &= \begin{bmatrix} 100 & 500 \end{bmatrix} \mathbf{x}\end{aligned}$$



## §7. Alternative Representations in State Space

- Writing the state equations from the signal-flow diagram

$$\frac{C(s)}{R(s)} = \frac{s+3}{(s+4)(s+6)}$$

Form	Transfer function	Signal-flow diagram	State equations
Phase variable	$\frac{1}{(s^2 + 10s + 24)} + (s+3)$		$\begin{aligned}\dot{\mathbf{x}} &= \begin{bmatrix} 0 & 1 \\ -24 & -10 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} r \\ y &= \begin{bmatrix} 3 & 1 \end{bmatrix} \mathbf{x}\end{aligned}$
Parallel	$\frac{-1/2}{(s+4)} + \frac{3/2}{s+6}$		$\begin{aligned}\dot{\mathbf{x}} &= \begin{bmatrix} -4 & 0 \\ 0 & -6 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 1 \\ 3 \end{bmatrix} r \\ y &= \begin{bmatrix} 1 & 1 \end{bmatrix} \mathbf{x}\end{aligned}$

## §7. Alternative Representations in State Space

Form	Transfer function	Signal-flow diagram	State equations
Cascade	$\frac{1}{(s+4)} + \frac{(s+3)}{(s+6)}$		$\begin{aligned}\dot{\mathbf{x}} &= \begin{bmatrix} -6 & 1 \\ 0 & -4 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} r \\ y &= \begin{bmatrix} -3 & 1 \end{bmatrix} \mathbf{x}\end{aligned}$
Controller canonical	$\frac{1}{(s^2 + 10s + 24)} + (s+3)$		$\begin{aligned}\dot{\mathbf{x}} &= \begin{bmatrix} -10 & -24 \\ 1 & 0 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 1 \\ 0 \end{bmatrix} r \\ y &= \begin{bmatrix} 1 & 3 \end{bmatrix} \mathbf{x}\end{aligned}$
Observer canonical	$\frac{1/s + 3/s^2}{1 + 10/s + 24/s^2}$		$\begin{aligned}\dot{\mathbf{x}} &= \begin{bmatrix} -10 & 1 \\ -24 & 0 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 1 \\ 3 \end{bmatrix} r \\ y &= \begin{bmatrix} 1 & 0 \end{bmatrix} \mathbf{x}\end{aligned}$

## §8. Similarity Transformations

- A system represented in state space as

$$\begin{aligned}\dot{\mathbf{x}} &= \mathbf{A}\mathbf{x} + \mathbf{B}u \\ \mathbf{y} &= \mathbf{C}\mathbf{x} + \mathbf{D}u\end{aligned}$$

can be transformed to a similar system

$$\begin{aligned}\dot{\mathbf{z}} &= \mathbf{P}^{-1}\mathbf{A}\mathbf{P}\mathbf{z} + \mathbf{P}^{-1}\mathbf{B}u \\ \mathbf{y} &= \mathbf{C}\mathbf{P}\mathbf{z} + \mathbf{D}u\end{aligned}$$

For example, for 2-space

$$\begin{aligned}\mathbf{P} &= [\mathbf{U}_{z_1} \quad \mathbf{U}_{z_2}] = \begin{bmatrix} p_{11} & p_{12} \\ p_{21} & p_{22} \end{bmatrix} \\ \mathbf{x} &= \begin{bmatrix} p_{11} & p_{12} \\ p_{21} & p_{22} \end{bmatrix} \begin{bmatrix} z_1 \\ z_2 \end{bmatrix} = \mathbf{P}\mathbf{z}\end{aligned}$$

and

$$\mathbf{z} = \mathbf{P}^{-1}\mathbf{x}$$

## §8. Similarity Transformations

## - Ex.5.9

## Similarity Transformations on State Equations

Given the system represented in state space

$$\dot{x} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -2 & -5 & -7 \end{bmatrix} x + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} u$$

$$y = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} x$$

transform the system to a new set of state variables,  $z$ , where the new state variables are related to the original state variables,  $x$ , as follows

$$\begin{aligned} z_1 &= 2x_1 \\ z_2 &= 3x_1 + 2x_2 \\ z_3 &= x_1 + 4x_2 + 5x_3 \end{aligned}$$

## §8. Similarity Transformations

## Solution

$$\begin{aligned} z_1 &= 2x_1 \\ z_2 &= 3x_1 + 2x_2 \\ z_3 &= x_1 + 4x_2 + 5x_3 \end{aligned} \Rightarrow z = \begin{bmatrix} 2 & 0 & 0 \\ 3 & 2 & 0 \\ 1 & 4 & 5 \end{bmatrix} x = P^{-1}x$$

$$P^{-1}AP = \begin{bmatrix} 2 & 0 & 0 \\ 3 & 2 & 0 \\ 1 & 4 & 5 \end{bmatrix} \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -2 & -5 & -7 \end{bmatrix} \begin{bmatrix} 0.5 & 0 & 0 \\ -0.75 & 0.5 & 0 \\ 0.5 & -0.4 & 0.2 \end{bmatrix}$$

$$= \begin{bmatrix} -1.5 & 1 & 0 \\ -1.25 & 0.7 & 0.4 \\ -2.5 & 0.4 & -6.2 \end{bmatrix}$$

$$P^{-1}B = \begin{bmatrix} 2 & 0 & 0 \\ 3 & 2 & 0 \\ 1 & 4 & 5 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 5 \end{bmatrix}$$

$$CP = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} 0.5 & 0 & 0 \\ -0.75 & 0.5 & 0 \\ 0.5 & -0.4 & 0.2 \end{bmatrix} = \begin{bmatrix} 0.5 & 0 & 0 \end{bmatrix}$$

## §8. Similarity Transformations

$$P^{-1}AP = \begin{bmatrix} -1.5 & 1 & 0 \\ -1.25 & 0.7 & 0.4 \\ -2.5 & 0.4 & -6.2 \end{bmatrix}$$

$$P^{-1}B = \begin{bmatrix} 0 \\ 0 \\ 5 \end{bmatrix}$$

$$CP = \begin{bmatrix} 0.5 & 0 & 0 \end{bmatrix}$$

The transformed system is

$$\dot{z} = \begin{bmatrix} -1.5 & 1 & 0 \\ -1.25 & 0.7 & 0.4 \\ -2.5 & 0.4 & -6.2 \end{bmatrix} z + \begin{bmatrix} 0 \\ 0 \\ 5 \end{bmatrix} u$$

$$y = \begin{bmatrix} 0.5 & 0 & 0 \end{bmatrix} z$$

## §8. Similarity Transformations



Run ch5p4 in Appendix B

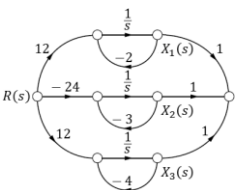
Learn how to use MATLAB to

- perform similarity transformations
- do Ex.5.9

## §8. Similarity Transformations

## Diagonalizing a System Matrix

- The parallel form of a signal-flow graph can yield a diagonal system matrix
- Advantage: each state equation is a function of only one state variable  $\Rightarrow$  each differential equation can be solved independently of the other equations (the equations are decoupled)



Example

$$\dot{x} = \begin{bmatrix} -2 & 0 & 0 \\ 0 & -3 & 0 \\ 0 & 0 & -4 \end{bmatrix} x + \begin{bmatrix} 12 \\ -24 \\ 12 \end{bmatrix} r$$

$$y = \begin{bmatrix} 1 & 1 & 1 \end{bmatrix} x$$

## §8. Similarity Transformations

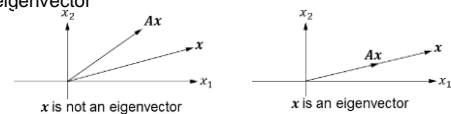
## Diagonalizing a System Matrix

## - Eigenvector

The eigenvectors of the matrix  $A$  are all vectors,  $x_i \neq 0$ , which under the transformation  $A$  become multiples of themselves; that is

$$Ax_i = \lambda_i x_i, \quad \lambda_i : \text{constant} \quad (5.80)$$

- If  $Ax$  is not collinear with  $x$  after the transformation,  $x$  is not an eigenvector
- If  $Ax$  is collinear with  $x$  after the transformation,  $x$  is an eigenvector



## §8. Similarity Transformations

## - Eigenvalue

The eigenvalues of the matrix  $A$  are the values of  $\lambda_i$  that satisfy

$$Ax_i = \lambda_i x_i, \quad \lambda_i : \text{constant} \quad (5.80)$$

for  $x_i \neq 0$

- To find the eigenvectors, rearrange Eq. (5.80). Eigenvectors,  $\lambda_i$ , satisfy

$$0 = (\lambda_i I - A)x_i \quad (5.81)$$

$$x_i = (\lambda_i I - A)^{-1} 0 = \frac{\text{adj}(\lambda_i I - A)}{\det(\lambda_i I - A)} 0$$

Since  $x_i \neq 0$ , a nonzero solution exists if

$$\det(\lambda_i I - A) = 0 \quad (5.83)$$

From which  $\lambda_i$ , the eigenvalues, can be found

## §8. Similarity Transformations

## - Ex.5.10

## Finding Eigenvectors

Find the eigenvectors of the matrix

$$A = \begin{bmatrix} -3 & 1 \\ 1 & -3 \end{bmatrix}$$

Solution

The eigenvectors,  $x_i$ , satisfy Eq. (5.81). First, use  $\det(\lambda_i I - A) = 0$  to find the eigenvalues,  $\lambda_i$ , for Eq. (5.81)

$$\begin{aligned} \det(\lambda_i I - A) &= \begin{vmatrix} \lambda & 0 \\ 0 & \lambda \end{vmatrix} - \begin{vmatrix} -3 & 1 \\ 1 & -3 \end{vmatrix} \\ &= \begin{vmatrix} \lambda + 3 & -1 \\ -1 & \lambda + 3 \end{vmatrix} \\ &= \lambda^2 + 6\lambda + 8 \\ &= (\lambda + 2)(\lambda + 4) \end{aligned}$$

from which the eigenvalues are  $\lambda = -2$ , and  $\lambda = -4$

$$0 = (\lambda_i I - A)x_i \quad (5.81)$$

## §8. Similarity Transformations

Using Eq. (5.80) successively with each eigenvalue, we have

$$Ax_i = \lambda_i x_i$$

Using eigenvalue  $\lambda = -2$

$$\begin{bmatrix} -3 & 1 \\ 1 & -3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = -2 \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

or

$$\begin{aligned} -3x_1 + x_2 &= -2x_1 \\ x_1 - 3x_2 &= -2x_2 \end{aligned}$$

From which  $x_1 = x_2$ . Thus  $x = \begin{bmatrix} c \\ c \end{bmatrix}$

Using eigenvalue  $\lambda = -4$ ,  $x = \begin{bmatrix} c \\ -c \end{bmatrix}$

One choice of eigenvectors is  $x_1 = \begin{bmatrix} 1 \\ 1 \end{bmatrix}$  and  $x_2 = \begin{bmatrix} 1 \\ -1 \end{bmatrix}$

$$Ax_i = \lambda_i x_i, \lambda_i : \text{constant} \quad (5.80)$$

## §8. Similarity Transformations



Run ch5p5 in Appendix B

Learn how to use MATLAB to diagonalize a system, is similar (but not identical) to Ex.5.11

## §8. Similarity Transformations

## Skill-Assessment Ex.5.7

Problem For the system represented in state space as follows

$$\dot{x} = \begin{bmatrix} 1 & 3 \\ -4 & -6 \end{bmatrix} x + \begin{bmatrix} 1 \\ 3 \end{bmatrix} u, \quad y = [1 \quad 4]x$$

convert the system to one where the new state vector

$$z = \begin{bmatrix} 3 & -2 \\ 1 & -4 \end{bmatrix} x$$

Solution

$$P^{-1} = \begin{bmatrix} 3 & -2 \\ 1 & -4 \end{bmatrix} \Rightarrow P = \begin{bmatrix} 0.4 & -0.2 \\ 0.1 & -0.3 \end{bmatrix}$$

$$P^{-1}AP = \begin{bmatrix} 3 & -2 \\ 1 & -4 \end{bmatrix} \begin{bmatrix} 1 & 3 \\ -4 & -6 \end{bmatrix} \begin{bmatrix} 0.4 & -0.2 \\ 0.1 & -0.3 \end{bmatrix} = \begin{bmatrix} 6.5 & -8.5 \\ 9.5 & -11.5 \end{bmatrix}$$

$$P^{-1}B = \begin{bmatrix} 3 & -2 \\ 1 & -4 \end{bmatrix} \begin{bmatrix} 1 \\ 3 \end{bmatrix} = \begin{bmatrix} -3 \\ -11 \end{bmatrix}$$

$$CP = [1 \quad 4] \begin{bmatrix} 0.4 & -0.2 \\ 0.1 & -0.3 \end{bmatrix} = [0.8 \quad -1.4]$$

## §8. Similarity Transformations

$$P^{-1}AP = \begin{bmatrix} 6.5 & -8.5 \\ 9.5 & -11.5 \end{bmatrix}$$

$$P^{-1}B = \begin{bmatrix} -3 \\ -11 \end{bmatrix}$$

$$CP = [0.8 \quad -1.4]$$

The transformed system is

$$\dot{z} = \begin{bmatrix} 6.5 & -8.5 \\ 9.5 & -11.5 \end{bmatrix} z + \begin{bmatrix} -3 \\ -11 \end{bmatrix} u$$

$$y = [0.8 \quad -1.4]z$$

## §8. Similarity Transformations

## Skill-Assessment Ex.5.8

**Problem** For the system represented in state space as follows

$$\dot{x} = \begin{bmatrix} 1 & 3 \\ -4 & -6 \end{bmatrix} x + \begin{bmatrix} 1 \\ 3 \end{bmatrix} u, y = [1 \quad 4]x$$

find the diagonal system that is similar

**Solution** First find the eigenvalues

$$|\lambda_i I - A| = \begin{vmatrix} \lambda & 0 \\ 0 & \lambda \end{vmatrix} - \begin{bmatrix} 1 & 3 \\ -4 & -6 \end{bmatrix} = \begin{bmatrix} \lambda - 1 & -3 \\ 4 & \lambda + 6 \end{bmatrix} \\ = \lambda^2 + 5\lambda + 6 = (\lambda + 2)(\lambda + 3)$$

From which the eigenvalues are  $-2$  and  $-3$

Now use  $Ax_i = \lambda x_i$  for each eigenvalue,  $\lambda$

Thus,

$$\begin{bmatrix} 1 & 3 \\ -4 & -6 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \lambda \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

## §8. Similarity Transformations

$$\begin{bmatrix} 1 & 3 \\ -4 & -6 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \lambda \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

For  $\lambda = -2$

$$3x_1 + 3x_2 = 0$$

$$-4x_1 - 4x_2 = 0$$

$$\Rightarrow x_1 = -x_2$$

For  $\lambda = -3$

$$4x_1 + 3x_2 = 0$$

$$-4x_1 - 3x_2 = 0$$

$$\Rightarrow x_1 = -0.75x_2$$

Let

$$P = \begin{bmatrix} 0.707 & -0.6 \\ -0.707 & 0.8 \end{bmatrix} \Rightarrow P^{-1} = \begin{bmatrix} 5.6577 & 4.2433 \\ 5 & 5 \end{bmatrix}$$

## §8. Similarity Transformations

$$P = \begin{bmatrix} 0.707 & -0.6 \\ -0.707 & 0.8 \end{bmatrix} \Rightarrow P^{-1} = \begin{bmatrix} 5.6577 & 4.2433 \\ 5 & 5 \end{bmatrix}$$

Hence

$$D = P^{-1}AP$$

$$= \begin{bmatrix} 5.6577 & 4.2433 \\ 5 & 5 \end{bmatrix} \begin{bmatrix} 1 & 3 \\ -4 & -6 \end{bmatrix} \begin{bmatrix} 0.707 & -0.6 \\ -0.707 & 0.8 \end{bmatrix}$$

$$= \begin{bmatrix} -2 & 0 \\ 0 & -3 \end{bmatrix}$$

$$P^{-1}B = \begin{bmatrix} 5.6577 & 4.2433 \\ 5 & 5 \end{bmatrix} \begin{bmatrix} 1 \\ 3 \end{bmatrix} = \begin{bmatrix} 18.39 \\ 20 \end{bmatrix}$$

$$CP = [1 \quad 4] \begin{bmatrix} 0.707 & -0.6 \\ -0.707 & 0.8 \end{bmatrix} = [-2.121 \quad 2.6]$$

The transformed system is

$$\dot{z} = \begin{bmatrix} -2 & 0 \\ 0 & -3 \end{bmatrix} z + \begin{bmatrix} 18.39 \\ 20 \end{bmatrix} u$$

$$y = [-2.121 \quad 2.6]z$$

## §7. Alternative Representations in State Space

## TryIt 5.5

Use the following MATLAB and Control System Toolbox statements to do Skill-Assessment Ex.5.8

$$\dot{x} = \begin{bmatrix} 1 & 3 \\ -4 & -6 \end{bmatrix} x + \begin{bmatrix} 1 \\ 3 \end{bmatrix} u, y = [1 \quad 4]x$$

```
A=[1 3;-4 -6];
B=[1;3];
C=[1 4];
D=0;S=ss(A,B,C,D);
Sd=canon(S, 'modal')
```