# Surge Current Ruggedness in Vertical GaN-on-GaN PiN Diode: Role of Conductivity Modulation

Jiahong Du<sup>1</sup>, Shu Yang<sup>1,2\*</sup>, Guangwei Xu<sup>1</sup>, Shibing Long<sup>1</sup>

<sup>1</sup>School of Microelectronics, University of Science and Technology of China, Hefei, China <sup>2</sup>College of Electrical Engineering, Zhejiang University, Hangzhou, China

\*Email: eesyang@ustc.edu.cn

Abstract—In this work, we investigate the surge current ruggedness and role of the conductivity modulation in the vertical GaN-on-GaN PiN diode. With varying t<sub>surge</sub> (5 μs~10 ms) and I<sub>peak</sub> up to 10 kA/cm², the evolvement of surge current capability of vertical GaN-on-GaN PiN diode has been systematically investigated. Owing to the desirable photon- and thermally-enhanced conductivity modulation in the direct-bandgap GaN, a high surge energy density of 282 J/cm² has been realized in the vertical GaN-on-GaN PiN diode, showing great potential of vertical GaN-on-GaN PiN diodes for high power electronic applications.

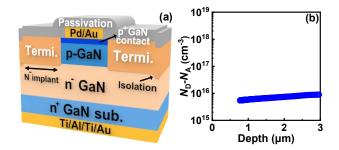
Keywords—Conductivity modulation, GaN-on-GaN, PiN diode, surge current ruggedness.

# I. INTRODUCTION

Compared with the conventional lateral GaN HEMTs grown on foreign substrate, vertical GaN-on-GaN power devices are promising to extend the voltage/power ratings with superior dynamic performance [1-4], benefiting from thick homo-epitaxial GaN drift layer with reduced dislocation density, and the vertical configuration that is more suitable for high current capability and less sensitive to surface trapping.

Power diodes would undergo a high surge current from circumstances of current overshoot/oscillation in switching converters, circuit failure or electrostatic discharge [5]. For indirect-bandgap bipolar devices with relatively long minority carrier lifetime ( $\sim 10^{-6}$ – $10^{-3}$  s for Si [6] and  $\sim 10^{-6}$  s for SiC [7]), minority carrier injection and conductivity modulation play an important role in their surge current capability [8]. In recent years, there are also reports demonstrating surge current capability of vertical GaN-on-GaN and quasi-vertical GaN-on-sapphire diodes, which mainly focus on the evaluation of the peak current  $(I_{peak})$  at a certain surge pulse width  $(t_{\text{surge}})$  [9-12]. However, the evolvement of surge current capability with varying  $I_{\text{peak}}$  and  $t_{\text{surge}}$ , as well as the underlying mechanism, has been seldom investigated to date. On the other hand, whether the minority carrier injection in directbandgap GaN with an ultrashort intrinsic lifetime of  $\sim 10^{-8}$  s [13] and the conductivity modulation [3] can play a role in the surge current capability remain unclear.

In this work, we systematically investigate the evolvement of surge current capability of vertical GaN-on-GaN PiN diode with varying  $t_{\rm surge}$  (5  $\mu$ s $\sim$ 10 ms) and  $I_{\rm peak}$  up to 10 kA/cm², in which the role of photon- and thermally-enhanced conductivity modulation in direct-bandgap GaN has also been analyzed. Vertical GaN-on-GaN PiN diode exhibits enhanced conduction capability with hole injection and consequently anti-clockwise hysteresis in the double-sweep dynamic I-IV curves which are extracted from surge current



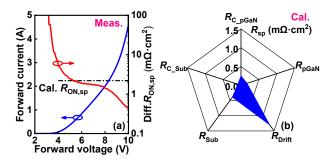
**Fig. 1:** (a) Schematic cross section of the vertical GaN-on-GaN PiN diode. (b) Net doping concentration  $(N_D-N_A)$  extracted from C-V measurements at 100 kHz in the  $n^-$  GaN drift layer.

characterizations. The  $I_{\rm peak}/t_{\rm surge}$ -dependent surge current capability of vertical GaN-on-GaN PiN diode is attributed to photon- and thermally-enhanced conductivity modulation.

# II. DEVICE STRUCTURE AND QUASI-STATIC PERFORMANCE

Fig. 1(a) shows the schematic cross section of the vertical GaN-on-GaN PiN diode, which primarily consists of Pd/Au anode, p<sup>+</sup>-GaN contact layer, 500-nm p-GaN layer, 15- $\mu$ m n<sup>-</sup>GaN drift layer, n<sup>+</sup>-GaN substrate, Ti/Al/Ti/Au cathode and nitrogen-implanted termination at the junction edge. The epitaxial structure was grown by metal-organic chemical vapor deposition. The net doping concentration ( $N_D$ – $N_A$ ) of the n<sup>-</sup>-GaN drift layer is  $\sim$ 6×10<sup>15</sup> cm<sup>-3</sup> (Fig. 1(b)), which is extracted from the C-V measurements at 100 kHz. The nitrogen-implanted termination can effectively suppress the electric field crowding at the junction edge and enhance the breakdown voltage up to  $\sim$ 2000 V in vertical GaN-on-GaN PiN diode.

Fig. 2(a) shows the forward I-V characteristics with the extracted specific differential  $R_{\rm ON}$  ( $R_{\rm ON,sp}$ ) of the vertical GaN-on-GaN PiN diode. The calculated  $R_{\rm ON,sp}$  (Fig. 2(b)), consisting of contact resistance to p-GaN ( $R_{\rm C\_P-GaN}$ ), p-GaN



**Fig. 2:** (a) Measured I-V characteristics and corresponding differential  $R_{\rm ON,sp}$  of the vertical GaN-on-GaN PiN diode. (b) Calculated  $R_{\rm ON,sp}$  components.



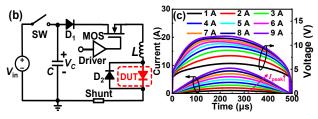
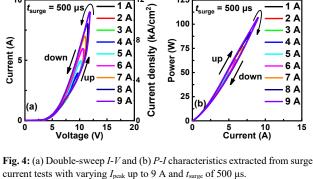


Fig. 3: (a) Characterization platform for surge current ruggedness evaluation. (b) Schematic of the PCB test board. (c) Surge current and voltage waveforms of the vertical GaN-on-GaN PiN diode.

resistance ( $R_{p-GaN}$ ), drift layer resistance ( $R_{Drift}$ ), substrate resistance ( $R_{Sub}$ ) and contact resistance to substrate ( $R_{C Sub}$ ), is 2.2 m $\Omega$ ·cm<sup>2</sup>, in which the calculated  $R_{\text{Drift}}$  of ~1.3 m $\Omega$ ·cm<sup>2</sup> occupies a relatively large portion. It is noteworthy that the measured  $R_{\rm ON,sp}$  (~0.45 m $\Omega$ ·cm<sup>2</sup> at 4 A) is significantly lower than the calculated value, and continuously decreases with higher current, suggesting the desirable conductivity modulation in direct-bandgap GaN vertical PiN diode.

# III. SURGE CURRENT RUGGEDNESS

Fig. 3(a) and Fig. 3(b) show the platform and schematic circuit diagram for the surge current characterizations, respectively. The test board is based on LC resonance, mainly including a DC power supply, switch (SW), charge capacitor (C), MOSFET, driver circuit, load inductor (L), device under test (DUT) and coaxial current shunt. Firstly, the switch is on and MOSFET is off, whereby C is charged to the power supply voltage  $(V_{in})$ . When the MOSFET is turned on while the switch is off, the resonance can generate a half-sinusoidal surge current that flows into the DUT. The current and voltage waveforms of the DUT can be captured by current shunt and voltage probe, respectively. In order to investigate the evolvement and mechanisms of surge current capability in the vertical GaN PiN diode,  $t_{\text{surge}}$  is varying within 5 µs~10 ms whereas  $I_{\text{peak}}$  is increased up to 10 kA/cm<sup>2</sup>, by adjusting C, Land capacitor voltage ( $V_{\rm C}$ ) according to Eqs. (1) and (2)

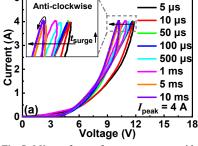


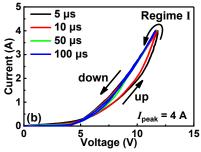
$$t_{\text{surge}} = \pi \times \sqrt{C \times L} \tag{1}$$

$$I_{\text{peak}} = V_{\text{C}} \times \sqrt{\frac{C}{L}}$$
 (2)

Fig. 3(c) shows the representative surge current and voltage waveforms, from which the corresponding forward I-V characteristics (Fig. 4(a)) with varying  $I_{peak}$  from 1 A up to 9 A (or  $10 \text{ kA/cm}^2$ ) at a certain  $t_{\text{surge}}$  can be extracted. With  $t_{\text{surge}}$ of 500  $\mu$ s, all the double-sweep I-V curves with  $I_{peak}$  varying from 1 A up to 9 A exhibit anti-clockwise hysteresis, which is a unique feature of the vertical GaN-on-GaN PiN diode and is distinct from that of Si and SiC devices [8]. Moreover, the down-sweep I-V continuously shifts toward the negative direction with higher  $I_{\text{peak}}$ , suggesting enhanced forward conduction with increased  $I_{\text{peak}}$ . Such enhanced forward conduction, yielding reduced forward voltage drop at a certain current in the down sweep than that in the up sweep, also leads to clockwise hysteresis in the double-sweep P-I characteristics (Fig. 4(b)). Such enhanced forward conduction capability with increased  $I_{\text{peak}}$  is correlated with the conductivity modulation in Fig. 2(a), which is desirable for enhanced surge current capability in vertical GaN power devices.

Fig. 5 shows the double-sweep *I-V* curves extracted from surge current tests with  $t_{\text{surge}}$  varying from 5 µs to 10 ms at a certain  $I_{\text{peak}}$  of 4 A, which can be primarily classified into two regimes according to the  $t_{\text{surge}}$ -dependent hysteresis evolvement: (I) With  $t_{\text{surge}}$  increasing from 5 µs to 100 µs, the initial anti-clockwise hysteresis gradually decreases and diminishes as the up-sweep I-V curves continuously shift towards the negative direction, possibly resulting from accumulated hole injection at longer  $t_{\text{surge}}$ , photon reabsorption/recycling and photon-enhanced conductivity





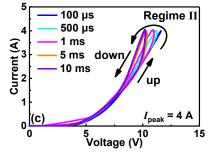


Fig. 5. I-V waveforms of surge current test with I<sub>peak</sub> of 4 A and t<sub>surge</sub> varying (a) from 5 μs to 10 ms, which is primarily classified into 2 regimes according to t<sub>surge</sub>. dependent hysteresis evolvement: (b)  $t_{\text{surge}}$  from 5  $\mu$ s to 100  $\mu$ s, (c)  $t_{\text{surge}}$  from 100  $\mu$ s to 10 ms.

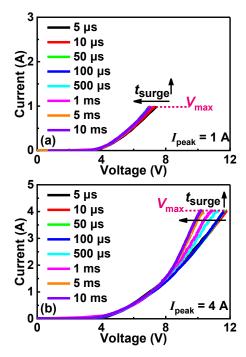


Fig. 6. Corresponding down-sweep I-V curves of surge current test with  $t_{\rm surge}$  varying from 5  $\mu s$  to 10 ms and  $I_{\rm peak}$  of (a) 1 A and (b) 4 A.

modulation [3, 14]. (II) With  $t_{\rm surge}$  increasing from 100  $\mu$ s to 10 ms, the anti-clockwise hysteresis re-occurs as there is significant negative shift particularly in the down-sweep I-V curves, possibly stemming from modest self-heating at higher surge current and thermally-enhanced conductivity modulation thanks to the higher p-GaN activation that will be discussed in Section IV. In addition, the enhanced forward conduction capability with  $t_{\rm surge}$  leads to a decrease in the required maximum voltage ( $V_{\rm max}$ ) at a certain  $I_{\rm peak}$ , as the down-sweep I-V curves continuously shifting towards the negative direction particularly at longer  $t_{\rm surge}$  in regime (II) (Fig. 5(c)) and higher current level (Fig. 6).

The surge current and voltage waveforms with a typical  $t_{\rm surge}$  of 10 ms are shown in Fig. 7. Owing to the desirable conductivity modulation, a surge energy density of  $282 \, J/\text{cm}^2$  can be realized in the vertical GaN-on-GaN PiN diode with  $t_{\rm surge}$  of 10 ms. The device failure possibly results from severe thermal accumulation at high current level [9, 10].

# IV. CONDUCTIVITY MODULATION

Two possible mechanisms of photon-enhanced conductivity modulation in the vertical GaN-on-GaN PiN diode are illustrated in Fig. 8, which feature reabsorption of photons generated by the radiative recombination in the direct-bandgap GaN [14]. In agreement with the  $I_{\rm peak}/t_{\rm surge}$ -dependent surge current capability abovementioned, the higher intensity of hole injection at increased  $I_{\rm peak}$  or hole accumulation with longer  $t_{\rm surge}$ , leads to the photon-enhanced conductivity modulation.

On the other hand, self-heating during surge current characterizations and the impact of elevated junction temperature on the forward conduction of vertical GaN PiN diode, should also be considered. In general, the forward conduction capability of the unipolar diode would deteriorate at higher temperature due to phonon scattering and the reduced carrier mobility [10, 11, 15, 16]. By contrast, the vertical GaN-on-GaN PiN diode exhibits enhanced forward

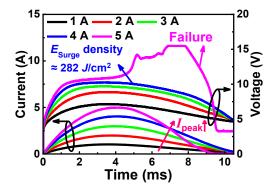
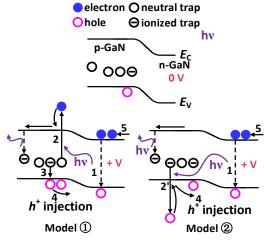


Fig. 7: Surge current and voltage waveforms of the vertical GaN-on-GaN PiN diode with  $t_{\text{surge}}$  of 10 ms and  $I_{\text{peak}}$  varying from 1 A and 5 A.



1: Radiative recombination,

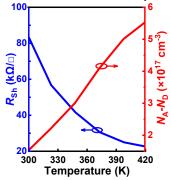
2/2': Reabsorption & trap emission (w/ phonon)

3: Ionization, 4:  $h^+$  injection from p-GaN,

5: e<sup>-</sup> injection from n<sup>+</sup>-GaN

**Fig. 8:** Energy-band diagrams illustrating two possible photon-enhanced conduction mechanisms (reabsorption of the radiative recombination by the initially neutral or ionized traps in p-GaN) in GaN PiN diode.

conduction performance with higher  $I_{\rm peak}$  and  $t_{\rm surge}$  prior to device failure in this work, suggesting thermally-enhanced conductivity modulation. In fact, the sheet resistance ( $R_{\rm Sh}$ ) of p-GaN is reduced and the effective acceptor doping concentration ( $N_{\rm A}$ – $N_{\rm D}$ ) is increased with temperature rising from 25 °C to 150 °C (Fig. 9), verifying thermally-enhanced p-GaN activation that would facilitate hole injection and conductivity modulation. The thermally-enhanced p-GaN



**Fig. 9:** Extracted sheet resistance  $(R_{\rm Sh})$  and effective acceptor concentration  $(N_{\rm A}-N_{\rm D})$  in p-GaN as a function of temperature.

activation and hole injection is particularly correlated with the enhanced forward conduction performance at higher  $I_{\rm peak}$  (Fig. 6(b)) or with longer  $t_{\rm surge}$  (Fig. 5(c)). Owing to the desirable photon- and thermally-enhanced conductivity modulation, vertical GaN-on-GaN PiN diode can deliver superior surge current capability.

# V. CONCLUSION

In this work, the evolvement of surge current capability in vertical GaN-on-GaN PiN diode with varying  $t_{\rm surge}$  (5 µs~10 ms) and  $I_{\rm peak}$  up to 10 kA/cm² has been systematically investigated, in which the role of conductivity modulation in direct-bandgap GaN is also analyzed and discussed. With longer  $t_{\rm surge}$  and higher  $I_{\rm peak}$ , vertical GaN-on-GaN PiN diode features anti-clockwise hysteresis in the double-sweep dynamic I-V characteristics extracted from surge current measurements. Thanks to the desirable photon- and thermally- enhanced conductivity modulation, the superior surge current ruggedness in direct-bandgap GaN vertical PiN diode show great potential in high power electronic applications.

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