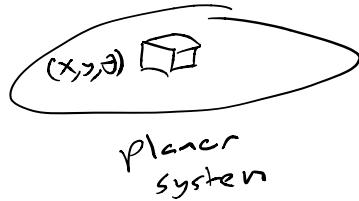
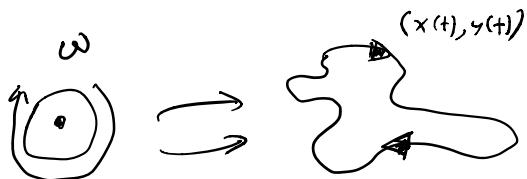


Linkage systems

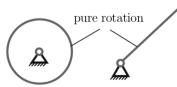
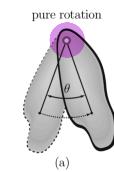
- Mobility



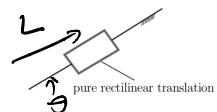
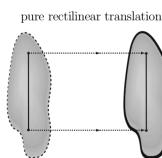
6-DOF
Spatial system

Connecting rigid bodies together through joints reserves DOF.

Mobility of a linkage system is the DOF

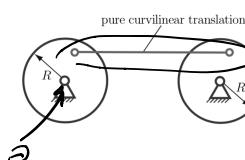
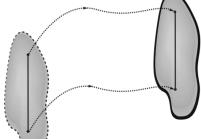


Revolute joints



Prismatic joint

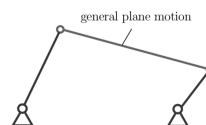
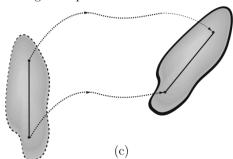
pure curvilinear translation



Single DOF

(b)

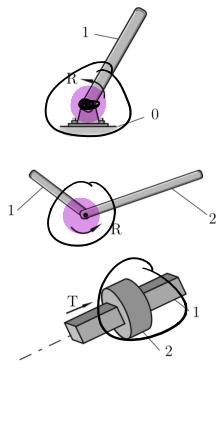
general plane motion



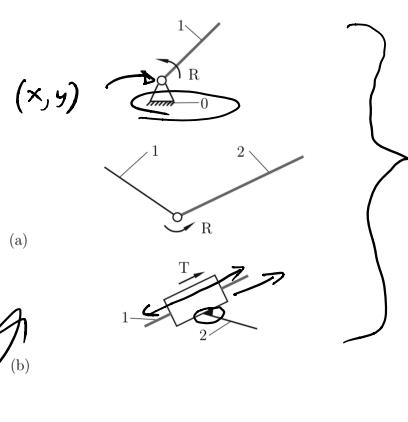
(c)

Planar systems

One degree of freedom joint

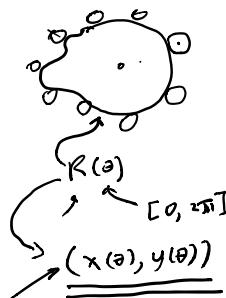
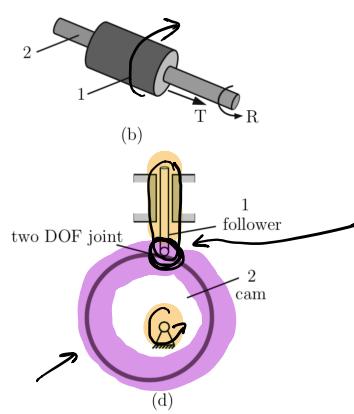
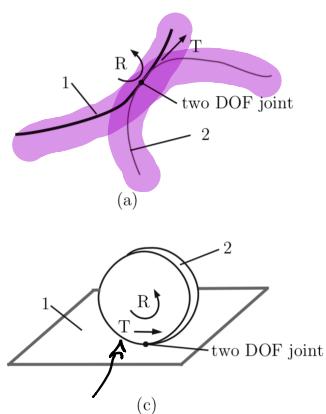


Schematic representation

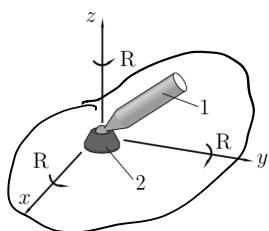


1-DOF joints

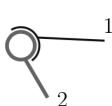
2 DOF joint



3 - DOF joint \rightarrow Spatial joint



Schematic representation



Planar \rightarrow motion plane

Spatial \rightarrow motion in space

Mobility equation? Gruebler equation
 Chebyshev condition

$$M = l(j - 1) + \sum_i f_i$$

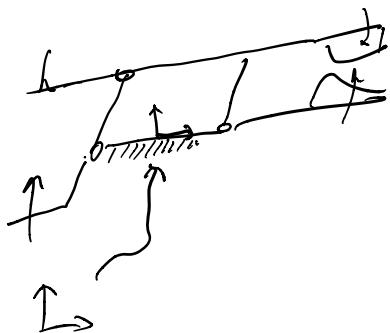
$\#$ links in mechanism $\#$ joints in mechanism

DOF of each joint

3: for planar systems

3: for spherical systems

6: Generic spatial linkages

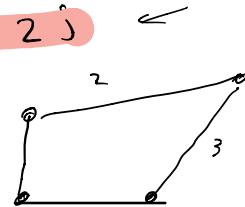


Planar systems: $f_i = 1$ $\lambda = 3$

$$M = 3 \cdot (l-1) - 3j + j$$

$$M = 3 \cdot (l-1) - 2j$$

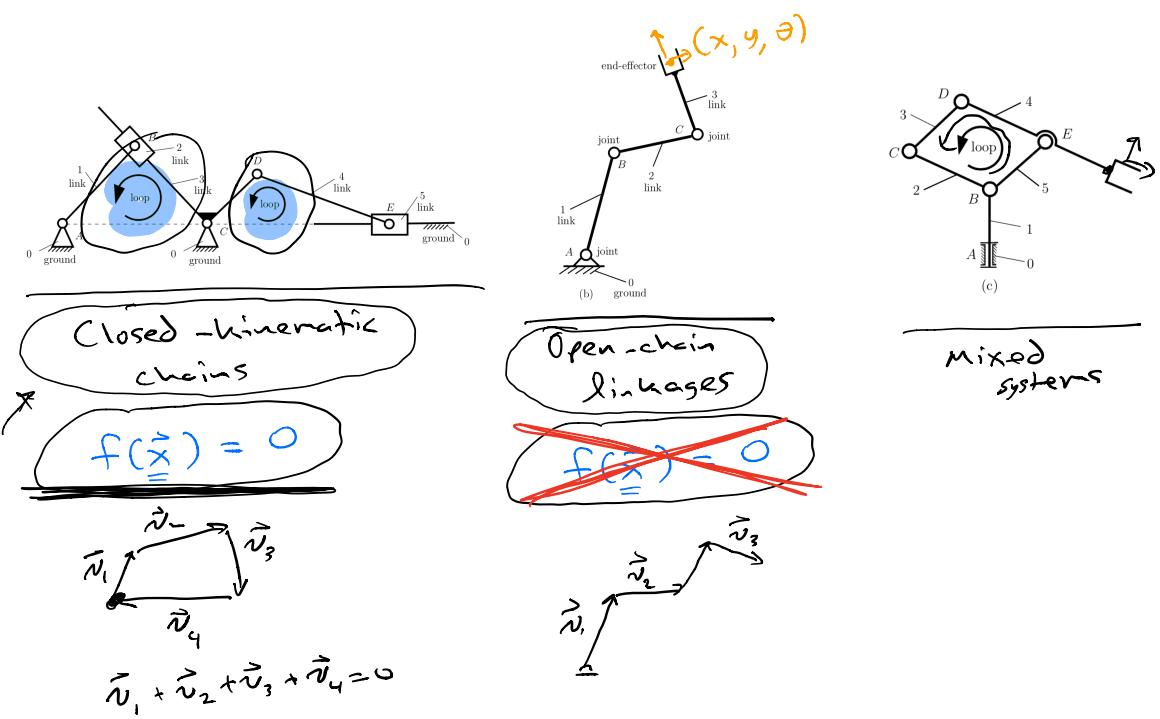
Total # of links



$$M = 3 \cdot n - 2 \cdot j$$

mobile links

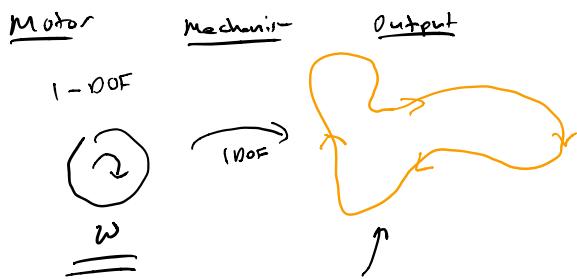
$$l-1 = n$$



planar mobility

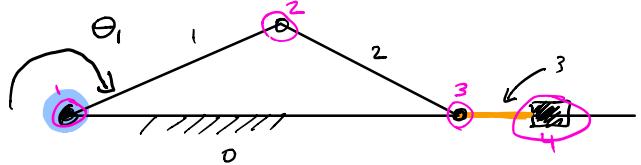
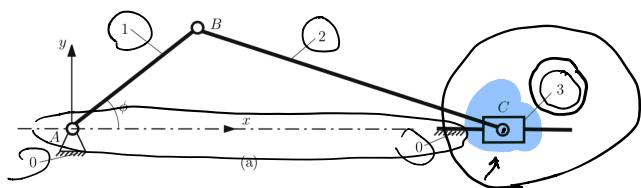
$$M = 3 \cdot (l - 1) - 2 \cdot j$$

$$= 3 \cdot n - 2j$$



$RRRP$

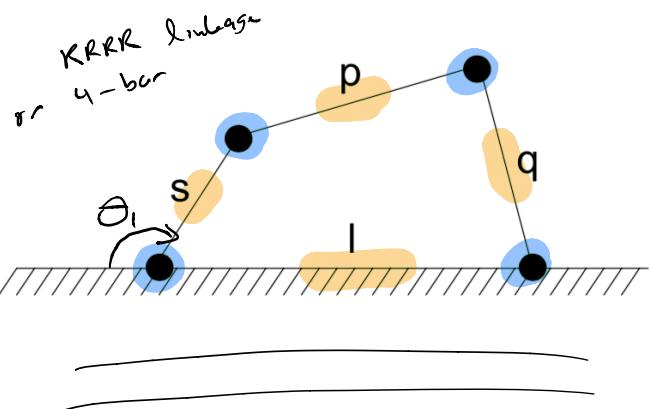
$$M = 3 \cdot (l-1) - 2 \cdot j$$



$$l = 4$$

$$j = 4$$

$$\begin{aligned} M &= 3 \cdot 3 - 2 \cdot 4 \\ &= \underline{\underline{1}} \end{aligned}$$

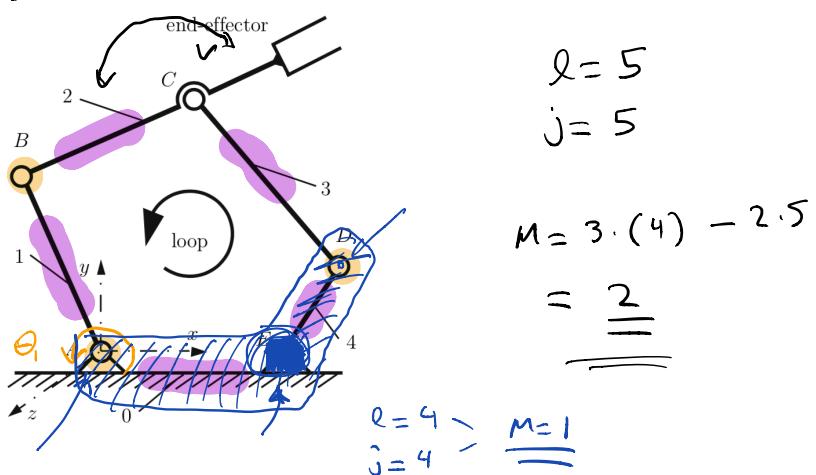


$$l = 4$$

$$j = 4$$

$$\begin{aligned} M &= 3 \cdot 3 - 2 \cdot 4 \\ &= \underline{\underline{1}} \end{aligned}$$

5-bar linkage



$$l = 5$$

$$j = 5$$

$$\begin{aligned} M &= 3 \cdot (4) - 2 \cdot 5 \\ &= \underline{\underline{2}} \end{aligned}$$

$$\begin{aligned} l &= 4 \\ j &= 4 > M = 1 \end{aligned}$$

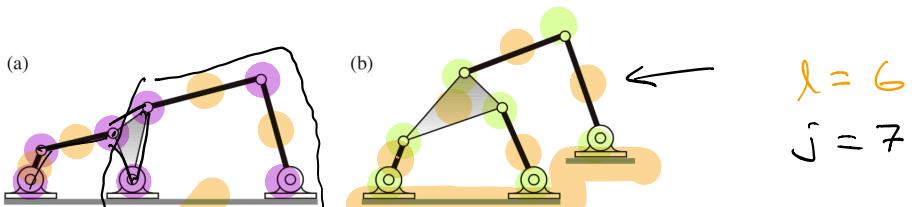
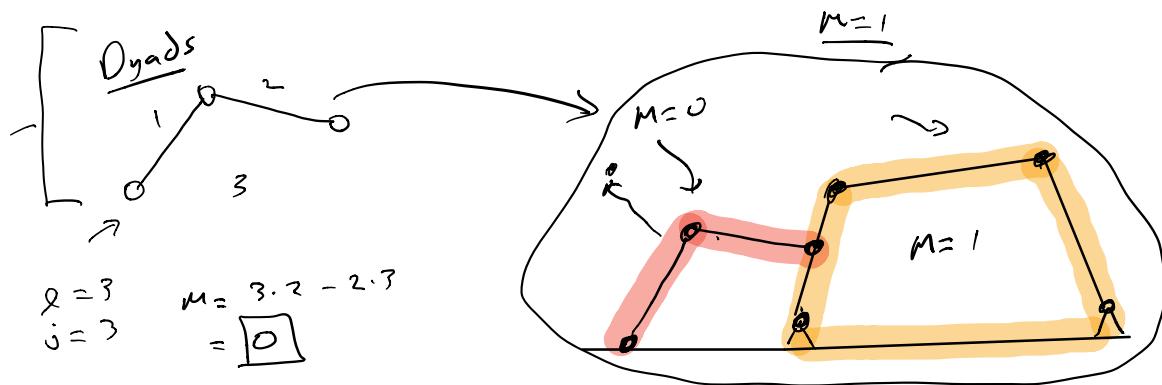


Fig. 1.2 Examples of the two classes of six bar linkages: (a) the Watt six-bar linkage; and (b) the Stephenson six-bar linkage.

$$\begin{aligned} l &= 6 \\ j &= 7 \\ m &= 3.5 - 2 \cdot 7 \\ &= 15 - 14 \\ &= 1 \end{aligned}$$



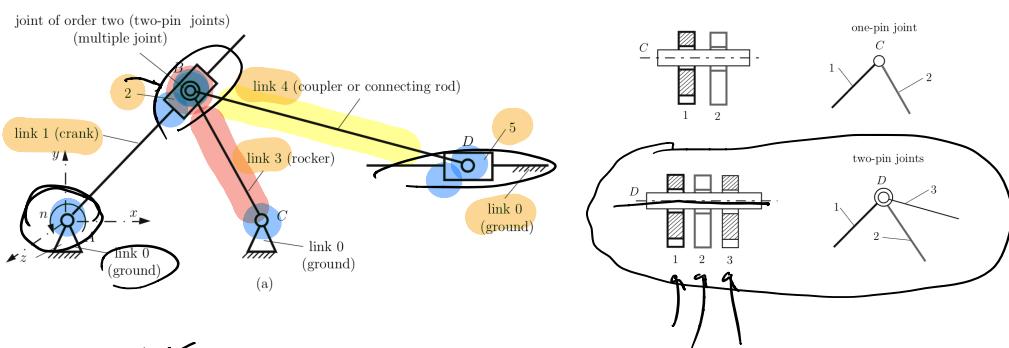
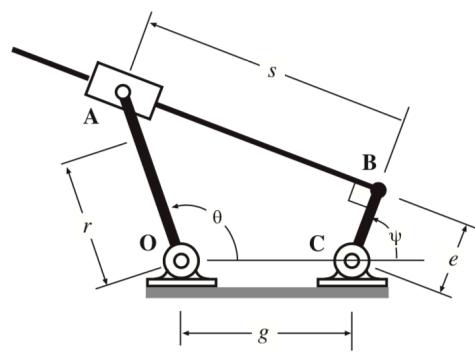
Dyads can be added to mechanism and don't change the net mobility.

1-DOF planar systems

$$m = 1 = 3 \cdot (l-1) - 2j \quad \leftarrow \quad \# l \text{ even for } m = 1$$

$$l = 3l - 3 - 2j$$

$$4 + 2j = 3l \rightarrow \quad l = \frac{4+2j}{3}$$



$$\begin{aligned}
 l &= 6 \\
 j &= 7 \\
 M &= 3(6 - 1) - 2 \cdot 7 \\
 &= 3 \cdot 5 - 2 \cdot 7 \\
 &= 1
 \end{aligned}$$

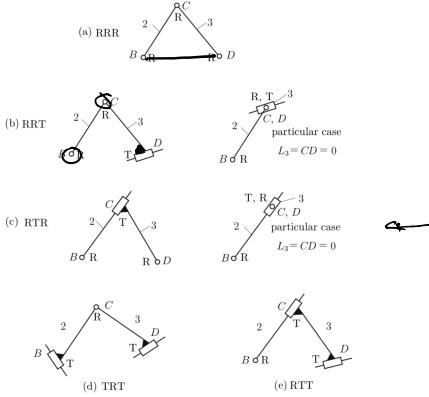
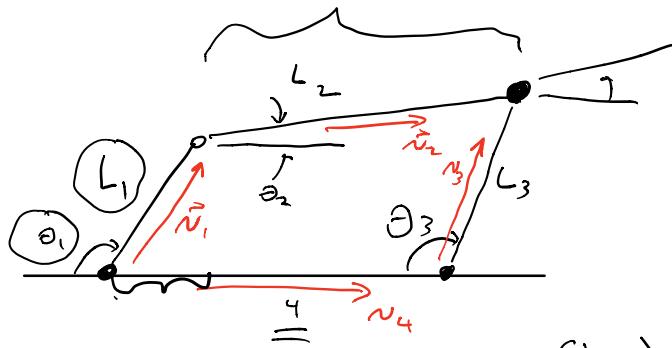


Fig. 1.9 Types of dyads: (a) RRR, (b) RRT, (c) RTR, (d) TRT, and (e) RTT

4-bar linkage



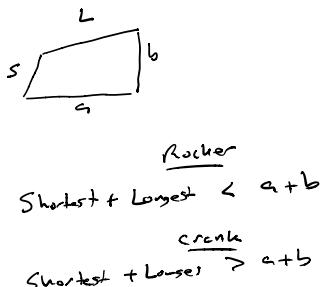
$$\text{Closed chain} \rightarrow \underline{\underline{f(\vec{x})}} = 0$$

Any link that can fully rotate \rightarrow crank

$$\vec{n}_1 + \vec{n}_2 = \vec{n}_3 + \vec{n}_4$$

Any link that oscillates \rightarrow rocker

$$\vec{n}_1 + \vec{n}_2 - \vec{n}_3 - \vec{n}_4 = 0$$



$$\begin{cases} x: L_1 \cos \theta_1 + L_2 \cos \theta_2 - L_4 - L_3 \cos \theta_3 = 0 \\ y: L_1 \sin \theta_1 + L_2 \sin \theta_2 - 0 - L_3 \sin \theta_3 = 0 \end{cases}$$

$$\theta_1 + \theta_2 + \theta_3 + \theta_4 = 360$$


```

%% Start anew
clear
clc
close all

%% Define geometry
theta_2 = pi/2;
l1 = 2;
l2 = 1;
l3 = 2;
l4 = 1;

%% Set up the problem symbolically

% define variables
syms theta_3_sym theta_4_sym

assume(theta_3_sym, 'real');
assume(theta_4_sym, 'real');

assume(theta_3_sym >= 0 & theta_3_sym < 2*pi)
assume(theta_4_sym >= 0 & theta_4_sym < 2*pi)

% define constraint equations
A = l2*cos(theta_2) + l3*cos(theta_3_sym) - l4*cos(theta_4_sym) - l1;
B = l2*sin(theta_2) + l3*sin(theta_3_sym) - l4*sin(theta_4_sym);

%% Solve symbolically

sol1 = solve([A==0, B==0], [theta_3_sym, theta_4_sym]);

theta_3 = eval(sol1.theta_3_sym)
theta_4 = eval(sol1.theta_4_sym)

% two solutions

%% Let's look at an animation!!
% Original geometry
% l1 = 2;
% l2 = 1;
% l3 = 2;
% l4 = 1;

% test something else
l1 = 2;
l2 = 1;
l3 = 2;
l4 = 1.5;

for theta_2 = 0:0.1:100000
    a = mod(theta_2, 2*pi);

    % define constraint equations
    A = l2*cos(theta_2) + l3*cos(theta_3_sym) - l4*cos(theta_4_sym) - l1;
    B = l2*sin(theta_2) + l3*sin(theta_3_sym) - l4*sin(theta_4_sym);

    %% Solve symbolically
    sol1 = solve([A==0, B==0], [theta_3_sym, theta_4_sym]);
    theta_3 = eval(sol1.theta_3_sym);
    theta_4 = eval(sol1.theta_4_sym);

    %% plot
    iis1;
    l1_vec = [l1, 0];
    l2_vec = [l2*cos(theta_2), l2*sin(theta_2)];
    l3_vec = [l2_vec + [l3*cos(theta_3(iis1)), l3*sin(theta_3(iis1))]];
    l4_vec = l1_vec + [l4*cos(theta_4(iis1)), l4*sin(theta_4(iis1))]; % -x because epsilon wrt interior angle

    clf;
    plot(0, l1_vec(1)), [0, l1_vec(2)], 'o-', 'LineWidth', 3); % link1
    hold on;
    plot(0, l2_vec(1)), [0, l2_vec(2)], 'o-', 'LineWidth', 3); % link2
    plot(l2_vec(1), l3_vec(1)), [l2_vec(2), l3_vec(2)], 'o-', 'LineWidth', 3); % link3
    plot(l1_vec(1), l4_vec(1)), [l1_vec(2), l4_vec(2)], 'o-', 'LineWidth', 3); % link4

    axis equal;
    axis([-3.5:-1, 1, -1, 1]);
    drawnow;
end

```

fsolve

Solve system of nonlinear equations

Syntax

```
x = fsolve(fun,x0)
x = fsolve(fun,x0,options)
x = fsolve(problem)
[x,fval] = fsolve(__)
[x,fval,exitflag,output] = fsolve(__)
[x,fval,exitflag,output,jacobian] = fsolve(__)
```

Description

Nonlinear system solver

Solves a problem specified by

$$F(x) = 0$$

for x , where $F(x)$ is a function that returns a vector value.

x is a vector or a matrix; see [Matrix Arguments](#).

`x = fsolve(fun,x0)` starts at $x0$ and tries to solve the equations $fun(x) = 0$, an array of zeros.

```
%% Let's look at an animation!!
%
% Original
l1 = 2;
l2 = 1;
l3 = 2;
l4 = 1.2;

%
% l1 = 1;
% l2 = 2;
% l3 = .5;
% l4 = 1;

x_guess = [0, 0];

input_angle = 0;
output_angle = 0;
cnt = 1;

omega = 1;

for t = 0:0.1:100000
    theta_2 = mod(omega*t, 2*pi);

    %% Solve numerically
    [x,fval] = fsolve(@(x) four_bar_constraint(x, theta_2, l1, l2, l3, l4), [0, output_angle(end)]);

    theta_3 = x(1);
    theta_4 = x(2);

    input_angle(cnt) = theta_2;
    output_angle(cnt) = theta_4;
    cnt = cnt + 1;

    % Only plot solutions that satisfy a certain final tolerance
    if norm(fval) < 0.000001
        %% plot
        l1_vec = [l1, 0];
        l2_vec = [l2*cos(theta_2), l2*sin(theta_2)];
        l3_vec = l2_vec + [l3*cos(theta_3), l3*sin(theta_3)];
        l4_vec = l3_vec + [l4*cos(theta_4), l4*sin(theta_4)]; % -x because epsilon wrt interior angle

        clf;
        plot([0, l1_vec(1)], [0, l1_vec(2)], 'o-', 'LineWidth', 3); % link1
        hold on;
        plot([0, l2_vec(1)], [0, l2_vec(2)], 'o-', 'LineWidth', 3); % link2
        plot([l2_vec(1), l3_vec(1)], [l2_vec(2), l3_vec(2)], 'o-', 'LineWidth', 3); % link3
        plot([l3_vec(1), l4_vec(1)], [l3_vec(2), l4_vec(2)], 'o-', 'LineWidth', 3); % link4

        axis equal;
        axis(3.5*[-1, 1, -1, 1]);
        drawnow;
    end
    pause;
end
```