# Homework 2

## **Problem 1**

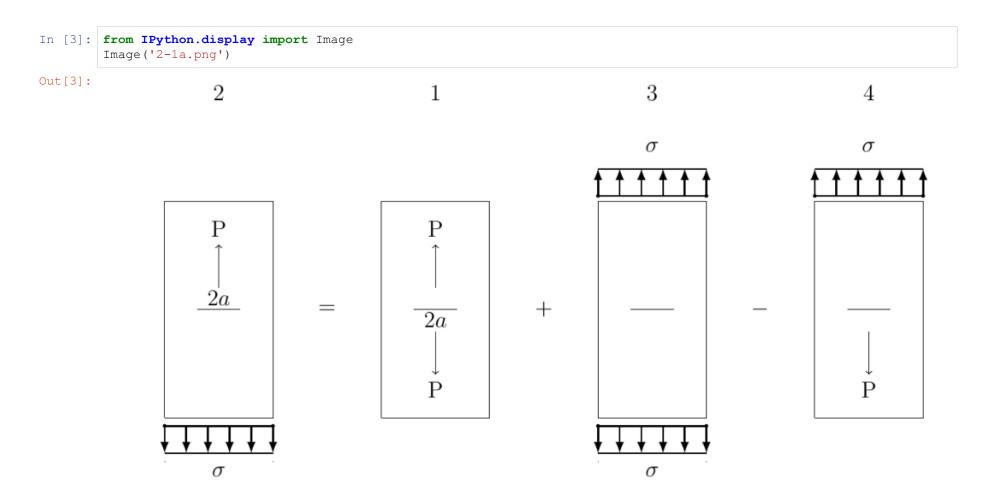
For Panel 1, we use equations (2.6) and (2.7) from the notes, or p. 52 from the text

$$K_I = \frac{P}{t\sqrt{\pi a}}\beta\tag{2.6}$$

$$K_{I} = \frac{P}{t\sqrt{\pi a}}\beta \tag{2.6}$$

$$\beta = \frac{1 - 0.5\left(\frac{a}{W}\right) + 0.975\left(\frac{a}{W}\right)^{2} - 0.16\left(\frac{a}{W}\right)^{3}}{\sqrt{1 - \left(\frac{a}{W}\right)}}$$

In Panel 2 we construct the following superposition



Since Panels 2 and 4 will give equivalent stress intensity factors, we can add Panel 4 to both sides to get

$$K_{I2} + K_{I4} = K_{I1} + K_{I3} \ 2K_{I2} = K_{I1} + K_{I3} \ K_{I2} = rac{1}{2}(K_{I1} + K_{I3})$$

We can now substutite the known equations for  $K_{I1}$  and  $K_{I3}$  to find

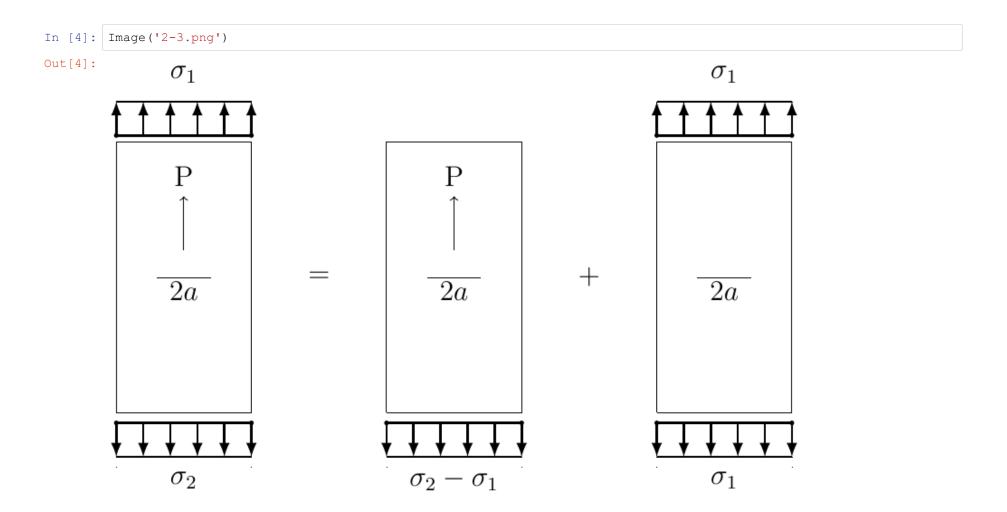
$$K_{I2} = rac{1}{2}igg(rac{P}{t\sqrt{\pi a}}eta_1 + \sigma\sqrt{\pi a}\sqrt{\sec(\pi a/W)}igg) \ eta_1 = rac{1-0.5\left(rac{a}{W}
ight) + 0.975\left(rac{a}{W}
ight)^2 - 0.16\left(rac{a}{W}
ight)^3}{\sqrt{1-\left(rac{a}{W}
ight)}}$$

#### **Problem 2**

For a corner crack as indicated in Problem 2, one possible method is to superpose the lug corner-crack and bending corner-crack solutions (p. 63 and p. 64).

#### **Problem 3**

This problem is very similar to Panel 2 from Problem 1. If we superpose the solution from Problem 1 with a center crack under remote stress we will have the same conditions as here.



#### **Problem 4**

In this case we will have two crack tips, one at A and one at B, with different stress intensity factors. We need to consider the effects of both edges, and the hole, but since no height dimension is given, we assume a negligible finite height effect.

From the left edge, we have a=1.25 and b=2.45, looking at the chart gives  $\beta_A=1.10$  and  $\beta_B=1.06$ . From the right edge, we have a=1.25 and b=6-2.45=3.55, notice that we switch the A and B lines from the chart to match our labeling, and we find  $\beta_A=1.03$  and  $\beta_B=1.05$ .

For the circular hole we have R=0.5, c=2.55, and b=2.05. This gives  $\beta_A=1.02$  and  $\beta_B=1.07$ . In summary we have

$$\begin{array}{c|cccc}
\beta_A & \beta_B \\
\hline
1.10 & 1.06 \\
1.03 & 1.05 \\
1.02 & 1.07
\end{array}$$

```
In [5]: #method one
beta_a_1 = 1+ (1.10-1+1.03-1+1.02-1)
beta_b_1 = 1+ (1.06-1+1.05-1+1.07-1)

#method two
beta_a_2 = 1.10*1.03*1.02
beta_b_2 = 1.06*1.05*1.07

print beta_a_1
print beta_a_2

print beta_b_1
print beta_b_2

1.15
1.15566
1.18
1.19091
```

We have about 1% difference between methods 1 and 2 for both crack tip A and B, which means we have very little interaction of edge effects and we would expect both values to be fairly accurate.

We use  $K_I = \sigma \sqrt{\pi a} eta$  to find the stress intensity factor

```
In [6]: import numpy as np
        s = 15 \# ksi
        a = 1.25 \#in
        #method one
        k_a_1 = s*np.sqrt(np.pi*a)*beta_a_1
        k b 1 = s*np.sqrt(np.pi*a)*beta b 1
        #method 2
        k_a_2 = s*np.sqrt(np.pi*a)*beta_a_2
        k b 2 = s*np.sqrt(np.pi*a)*beta b 2
        print k_a_1
        print k a 2
        print k b 1
        print k b 2
        34.18369794185185
        34.351941185635226
        35.0754465838132
        35.39974583993982
```

### **Problem 5**

Since we are dealing with cracks along a curved boundary, both "short" and "long," we will use the combined method to interpolate between the two solutions.

For a short crack, we start by finding the stress concentration factor from p. 84. For that chart,  $r/d=\frac{0.25}{4-(0.1+0.25)}$ , we also have  $D/d=\frac{4}{4-(0.1+0.25)}$ 

```
In [7]: r = 0.25
d = 4-(.1+.25)
D = 4
print r/d
print D/d

0.0684931506849
1.09589041096
```

We find on the chart that  $K_{tn}=2.5$ . Next we relate the given panel to one with a hole in the center and a very short crack on one side of the hole. For this case we find  $K_{tq}=3.05$ .

Our next task is to convert the net stress equation into global stress. We do this by making a free-body cut through the crack plane. (See Example 6 on p. 86 of text). Since the force on the cut face acts slightly off-center, we need to also include a bending moment for the body to be in equilibrium.

```
In [8]: s = 6 #ksi, applied stress t = 0.375 P = s*D*t #equivalent force from applied stress M = P*(2-d/2) #moment equal to force times eccentricity of load at mid-plane SP = P/(d*t) + M*(d/2)/(t*3.65**3/12) #net stress is force/area + My/I
```

 $K_{tq}\sigma=K_{tn}\sigma_n$  (equate net-stress concentration factor to global stress concentration factor)

$$K_{tg}=K_{tn}\sigma_n/\sigma$$

```
In [9]: K_tn = 2.5
K_tg = K_tn*sn/s
print K_tg
3.52786639144
```

We can now find what  $\sigma_A$  needs to be by equation  $\sigma_{max,A}$  with  $\sigma_{max,A}$ 

$$egin{aligned} \sigma_{max,B} &= \sigma_{max,A} \ K_{tgB}\sigma &= K_{tgA}\sigma_A \ rac{K_{tgB}}{K_{tgA}}\sigma &= \sigma_A \end{aligned}$$

```
In [10]: sa = K_tg/3.05*s
    print sa
6.94006503235
```

Since  $K_{IA}=K_{IB}$  for short cracks, we can now find  $K_I$  using a crack on one side of a hole (eq 2.12)

```
In [11]: import numpy as np
    rc = 1 #for short cracks c = 0
    B_3 = .7071+.7548+.3415+.6420+.9196
    Fw = 1/np.cos(np.pi*.25/4)
    Fww = 1 #because c=0
    B_s = B_3*Fw*Fww*K_tg/3.05
    B_s
Out[11]: 3.9684728996351324
```

So the  $\beta_S$  for short cracks is 3.97. For long cracks we use the formula for edge cracks in a finite panel, where the extra geometry, e is 0.35

D:\Anaconda\lib\site-packages\ipykernel\_launcher.py:6: RuntimeWarning: divide by zero encountered in divide

We now find the tangent curve to generate a cohesive plot

```
In [13]: from scipy import interpolate
    #interpolate our discrete points
    spl = interpolate.splrep(c[1:],B_l[1:])
    x1 = 0.0743 #guess, adjust until they match
    fa = interpolate.splev(x1,spl,der=0)
    fprime = interpolate.splev(x1,spl,der=1)
    print fa-fprime*x1
    print B_s #(to find x1)

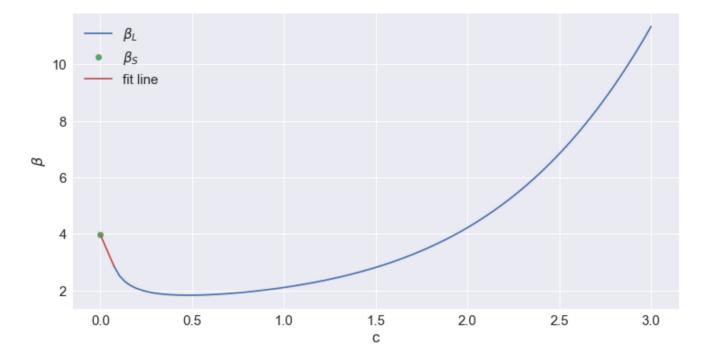
3.96788123325723
3.9684728996351324
```

And we plot the full result

```
In [14]: import matplotlib.pyplot as plt
         import seaborn as sb
         sb.set(font scale=1.5)
         %matplotlib inline
         plt.figure(figsize=(12,6))
         c = np.linspace(x1,3,100) # only plot B_1 from end of tangent
         shortc = np.linspace(0,x1)
         aw = (c+e)/W
         B = 1.122 - 0.231*aw + 10.55*aw**2 - 21.71*aw**3 + 30.82*aw**4
         B l = np.sqrt((c+e)/c)*B
         plt.figure(figsize=(12,6))
         plt.plot(c,B l,label=r'$\beta L$')
         plt.plot(0,B s,'o',label=r'$\beta S$')
         plt.plot(shortc,fa+fprime*(shortc-x1),label='fit line')
         plt.xlabel('c')
         plt.ylabel(r'$\beta$')
         plt.legend(loc='best')
```

Out[14]: <matplotlib.legend.Legend at 0xb48b898>

<Figure size 864x432 with 0 Axes>



Visually, we can see that for part a we are using only the long crack formula, calculating  $K_I$ :

```
In [15]: c = 0.4
a = c + e
aw = a/W
B = 1.122 - 0.231*aw + 10.55*aw**2 - 21.71*aw**3 + 30.82*aw**4
K_I = s*np.sqrt(np.pi*a)*B
print K_I
12.383412965569004
```

So  $K_I=12.38 ext{ksi}\ \sqrt{ ext{in.}}$ 

For part b we need to use our linear interpolation, we find that

```
In [16]: c = 0.05
B = fa+fprime*(c-x1)
print B
3.218144130597965
```

## Substituting this $\beta$ in gives

```
In [17]: K_I = s*np.sqrt(np.pi*c)*B
    print K_I
    7.652735088257687
```

So  $K_I=7.65 ext{ksi}\ \sqrt{ ext{in.}}$ 

If we used only the short-crack assumption, we would find  $K_I=3.97(6000)\sqrt{.05\pi}$ 

```
In [18]: 3.97*6*np.sqrt(np.pi*.05)
Out[18]: 9.440645622897518
```

Which gives a stress intensity factor of  $K_I = 9.44 \text{ ksi}$ .

Even though we might assume a 0.05" crack is very short, using the short crack assumptions leads to an error of about 20%.

#### **Problem 6**

1.3493

We formulate this problem much like Problem 4. For the left crack tip, we have a/b=0.33, which gives  $\beta_A=1.04$  and  $\beta_B=1.03$ . For the right crack tip (with A and B switched from the chart) we have a/b=.05, which gives  $\beta_A\approx\beta_B\approx1$ . For the circular hole we have R=0.3, c=0.6, and b=0.3. This gives  $\beta_A=1.19$  and  $\beta_B=1.31$ . In summary we have

$$\beta_A$$
  $\beta_B$ 

1.04 1.03

1.00 1.00

1.19 1.31

```
In [19]: #method one
    beta_a_1 = 1+ (1.04-1+1.00-1+1.19-1)
    beta_b_1 = 1+ (1.03-1+1.00-1+1.31-1)

#method two
    beta_a_2 = 1.04*1.*1.19
    beta_b_2 = 1.03*1.0*1.31

print beta_a_1
    print beta_a_2

print beta_b_1
    print beta_b_2

1.23
    1.2376
    1.34
```

Once again Methods 1 and 2 agree well, indicating little interaction. However we see in this problem that  $\beta$  is dominated by the hole, the edge effects are minimal. The stress intensities are:

```
In [20]: a = 0.1 #in

#method one
k_a_1 = np.sqrt(np.pi*a)*beta_a_1
k_b_1 = np.sqrt(np.pi*a)*beta_b_1

#method 2
k_a_2 = np.sqrt(np.pi*a)*beta_a_2
k_b_2 = np.sqrt(np.pi*a)*beta_b_2

print k_a_1
print k_a_2
print k_b_1
print k_b_2

0.6894139196169452
0.6936737129414077
```

0.7510688229973225

0.7562814648285726

#### (multiplied by the applied stress)

```
In [ ]:
```