

AE 737 - MECHANICS OF DAMAGE TOLERANCE

LECTURE 13

Dr. Nicholas Smith

Last Updated: March 7, 2016 at 4:42pm

Wichita State University, Department of Aerospace Engineering

SCHEDULE

- 3 Mar - Section 1 Review, Homework 5 return
- 8 Mar - Exam 1
- 10 Mar - Exam return, Final Project discussion
- 22 Mar - Stress based fatigue, Homework 6 assigned
- 24 Mar - Stress based fatigue

OUTLINE

1. exam notes
2. stress intensity
3. fracture toughness
4. residual strength
5. stiffeners
6. multiple site damage
7. mixed mode fracture
8. extra credit

EXAM NOTES

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- Equation sheet is posted on Blackboard

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METHODS FOR FINDING STRESS INTENSITY

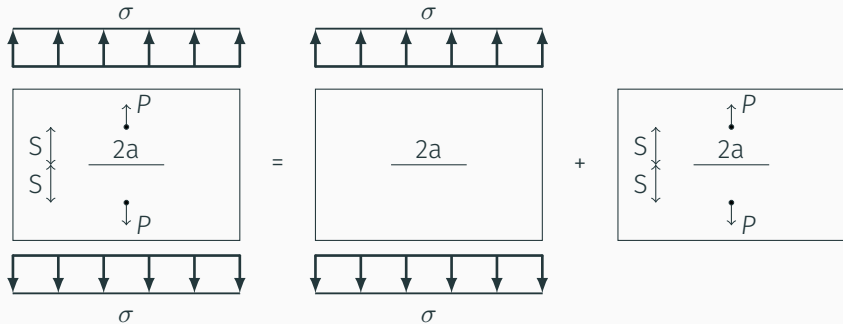
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- Experimental

- Since the stress intensity factor is derived using Linear Elasticity, the principle of superposition applies
- Multiple applied loads can be superposed to find the effective stress intensity factor of the combined loading

SUPERPOSITION

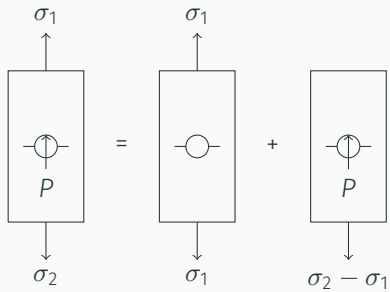


$$K_I = K_{I(\sigma)} + K_{I(P)}$$

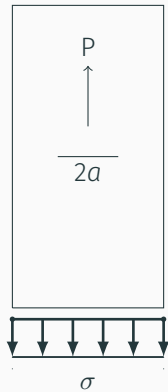
$$K_I = \sigma\sqrt{\pi a} + \frac{P}{t\sqrt{\pi a}} \frac{1 - 0.5\left(\frac{a}{W}\right) + 0.975\left(\frac{a}{W}\right)^2 - 0.16\left(\frac{a}{W}\right)^3}{\sqrt{1 - \left(\frac{a}{W}\right)}}$$

- Sometimes, the superposition needed to solve a problem is not obvious
- It can be helpful to subtract a known solution from the problem

SUPERPOSITION



SUPERPOSITION



FRACTURE TOUGHNESS

- The critical load at which a cracked specimen fails produces a critical stress intensity factor
- The "critical stress intensity factor" is known as K_c
- For Mode I, this is called K_{Ic}
- The critical stress intensity factor is also known as fracture toughness

$$K_{Ic} = \sigma_c \sqrt{\pi a} \beta \quad (13.1)$$

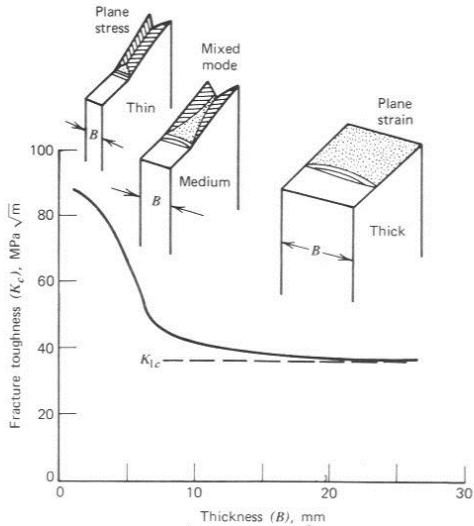
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- NOTE: "Fracture Toughness" can also refer to G_{Ic} , which is analogous to K_{Ic} , but not the same

- Fracture toughness is a material property, but it is only well-defined in certain conditions
- Brittle materials
- Plane strain (smaller plastic zone)
- In these cases ASTM E399-12 is used.

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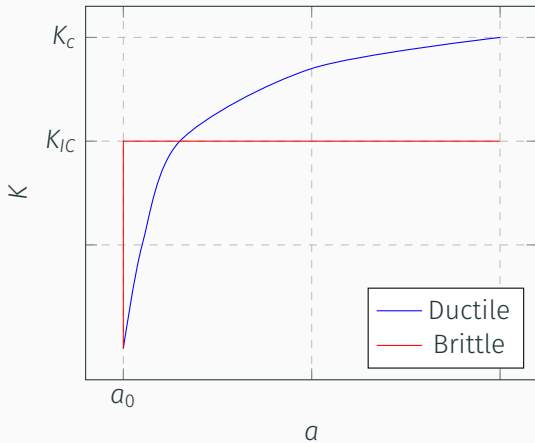
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- For an elastic-plastic material, once the load is large enough to extend the crack, it will extend slightly
- The load must be continually increased until a critical value causes unstable crack growth

- During an experiment, we will record the crack length and applied load (P_i, a_i) each time we increase the load

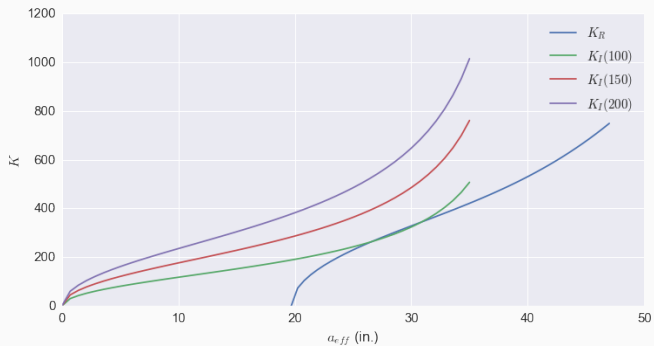
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- These are then used to create a "K-curve", plotting K_I vs. a

K-CURVE



k_r CURVE



RESIDUAL STRENGTH

- In the last chapter we performed some basic residual strength analysis by checking for net section yield

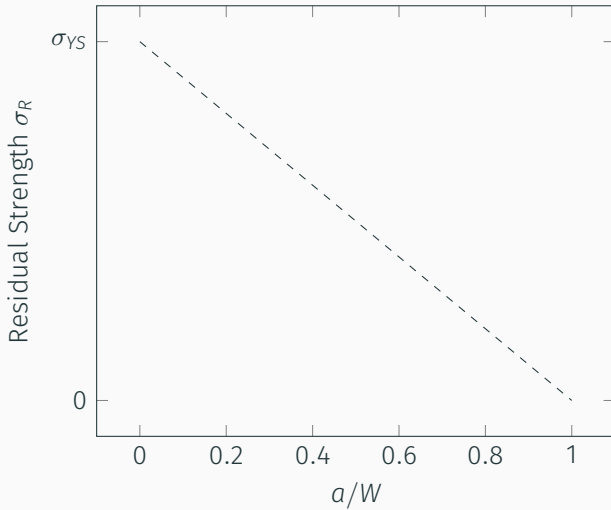
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- We can relate the net-section stress to σ_R by

$$\sigma_R = \sigma_{YS} \frac{A_{net}}{A_{gross}} \quad (13.2)$$

RESIDUAL STRENGTH



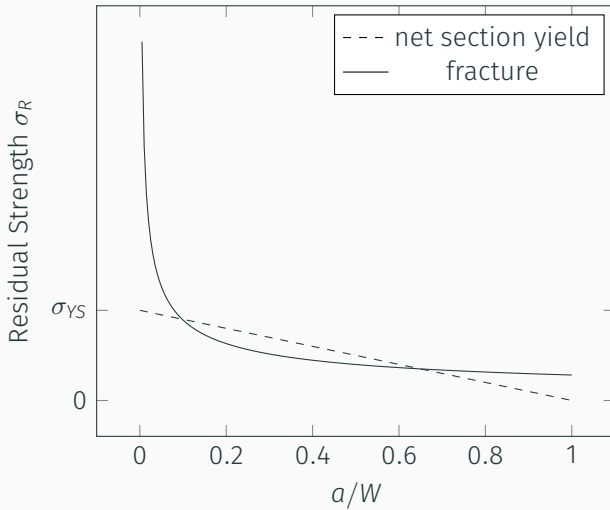
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$$\sigma_R = \sigma_C = \frac{K_C}{\sqrt{\pi a} \beta} \quad (13.3)$$

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 3. 2024-T3, $K_C = 144 \text{ ksi}\sqrt{\text{in.}}$, $\sigma_{YS} = 42\text{ksi}$

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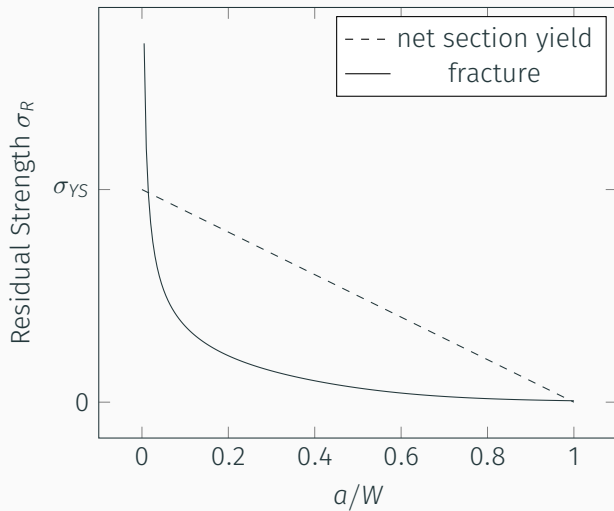
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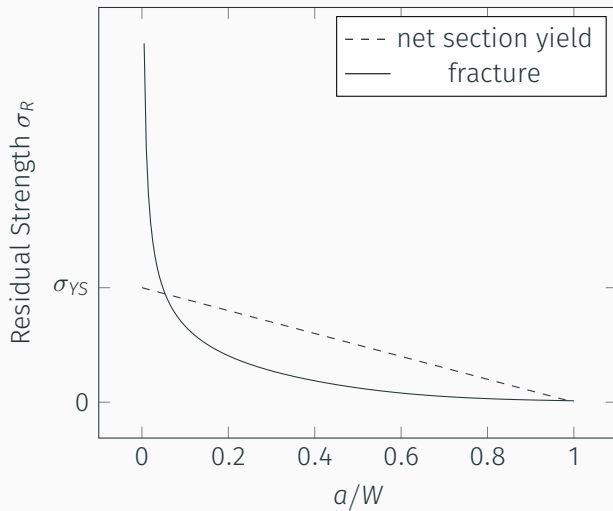
- And the fracture condition by

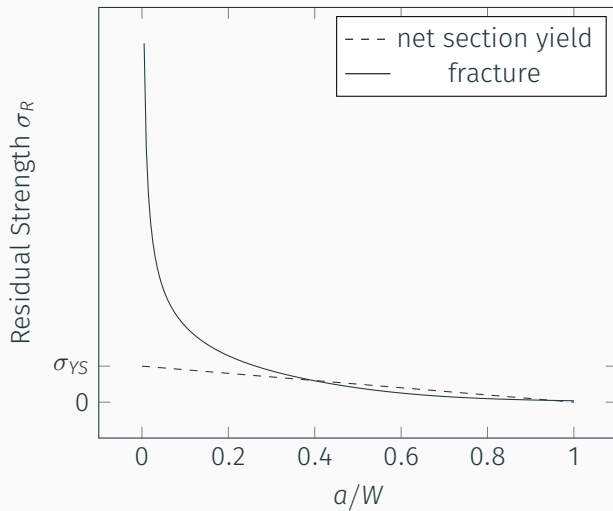
$$\sigma_C = \frac{K_C}{\sqrt{\pi a} \beta}$$

With

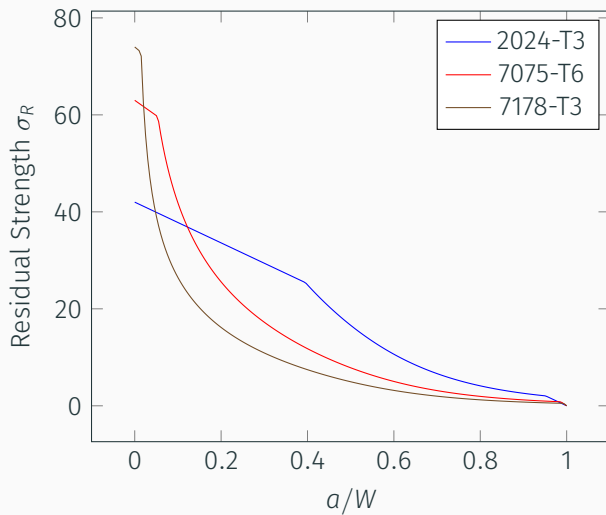
$$\beta = 1.12 - 0.231 \left(\frac{a}{W} \right) + 10.55 \left(\frac{a}{W} \right)^2 - 21.72 \left(\frac{a}{W} \right)^3 + 30.39 \left(\frac{a}{W} \right)^4$$







COMPARISON



STIFFENERS

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- Stiffeners reverse this trend to some extent, but causing some sections of residual strength curve to have positive slope
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- Thus in some cases, we can predict some amount of crack growth

sketch

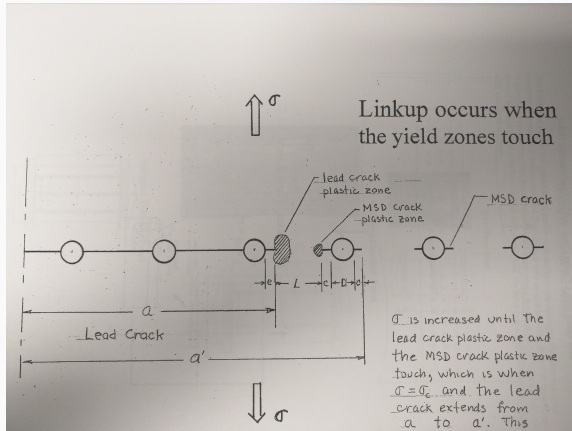
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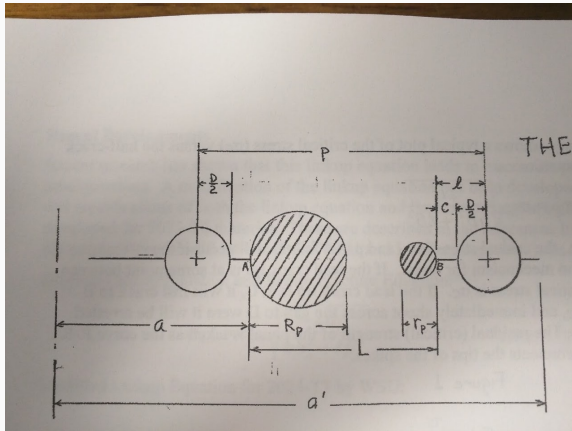
MULTIPLE SITE DAMAGE

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- "link up" occurs when the plastic zones between two adjacent cracks touch





- We know that

$$R_p = \frac{1}{2\pi} \left(\frac{K_{Ia}}{\sigma_{YS}} \right)^2 \quad (13.4)$$

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- Where we define the stress intensity factors at a and L as

$$K_{Ia} = \sigma \sqrt{\pi a} \beta_a \quad (13.6)$$

$$K_{Il} = \sigma \sqrt{\pi l} \beta_l \quad (13.7)$$

LINKUP EQUATION

- Since fast cracking occurs when $R_p + r_p = L$, we solve for the condition where $R_p + r_p < L$

$$\frac{1}{2\pi} \left(\frac{K_{Ia}}{\sigma_{YS}} \right)^2 + \frac{1}{2\pi} \left(\frac{K_{II}}{\sigma_{YS}} \right)^2 < L \quad (13.8a)$$

$$\frac{1}{2\pi\sigma_{YS}^2} [K_{Ia}^2 + K_{II}^2] < L \quad (13.8b)$$

$$\frac{1}{2\pi\sigma_{YS}^2} [\sigma^2\pi a\beta_a^2 + \sigma^2\pi l\beta_l^2] < L \quad (13.8c)$$

$$\frac{\sigma^2}{2\sigma_{YS}^2} [a\beta_a^2 + l\beta_l^2] < L \quad (13.8d)$$

$$\frac{\sigma_c^2}{2\sigma_{YS}^2} [a\beta_a^2 + l\beta_l^2] = L \quad (13.8e)$$

$$\sigma_c = \sigma_{YS} \sqrt{\frac{2L}{a\beta_a^2 + l\beta_l^2}} \quad (13.8f)$$

- The link-up equation is not a good predictor for materials with a small plastic zone size
- Even for ductile materials, some fine tuning of the equation is needed
- In practice, MSD predictions are based on experiments

MIXED MODE FRACTURE

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- Maximum circumferential stress finds the principal stress direction near the crack tip
- Assumes crack will propagate due to maximum opening stress
- Maximum principal stress theory finds the maximum principal stress, neglecting crack tip stress field
- Also assumes crack propagates in Mode I direction

EXTRA CREDIT

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- Use Google Doc to write the page of a figure you are working on (so we don't repeat)

- Google Doc: <https://docs.google.com/spreadsheets/d/1ay4HfJQG2mF-nyr3fgtDr0lHDQoWP30TIMynKGxiwp0/edit?usp=sharing>
- Chart tracer:
<http://arohatgi.info/WebPlotDigitizer/app/>

REVIEW PROBLEMS

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- p. 415 problem 6
- p. 418 problem 9
- p. 419 problem 10-11
- p. 421 problem 13
- p. 423 problem 17
- p. 424 problem 3
- p. 425 problem 5
- p. 426 problem 1
- p. 427 problem 3
- p. 429 problem 6
- p. 432 problem 9
- p. 433 problem 14
- p. 434 problem 3
- p. 437 problem 8