AE 737: Mechanics of Damage Tolerance

Lecture 3 - Superposition, Compounding

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schedule

- 28 Jan Superposition, Compounding
- 30 Jan Curved Boundaries, Homework 1 Due
- 4 Feb Plastic Zone
- 6 Feb Plastic Zone

office hours

- Office hours will be TBD
- As a back-up, AE 333 Office Hours are TBD
- Take advantage of office hours, this is time that I have already set aside for you
- If the regular office hours do not work for your schedule, send me an e-mail and we can work out a time to meet

homework notes

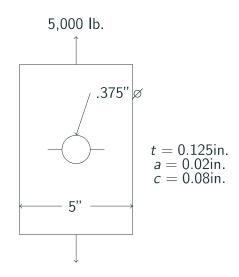
- Watch units (beam problem, foot-lbs vs. in-lbs)
- Significant figures
- My grading philosophy
- Individual work

outline

- Review
- Superposition
- Compounding

review

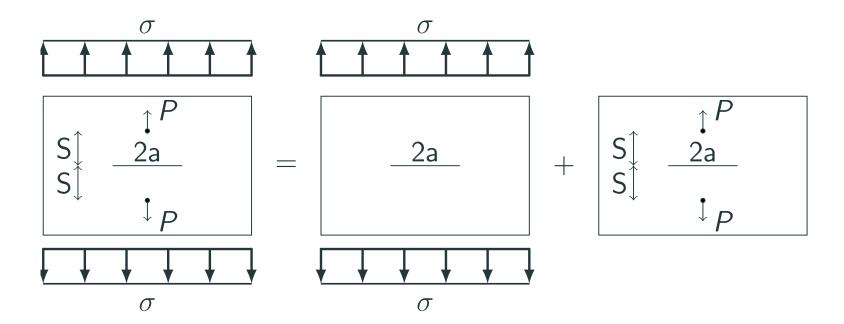
example



example

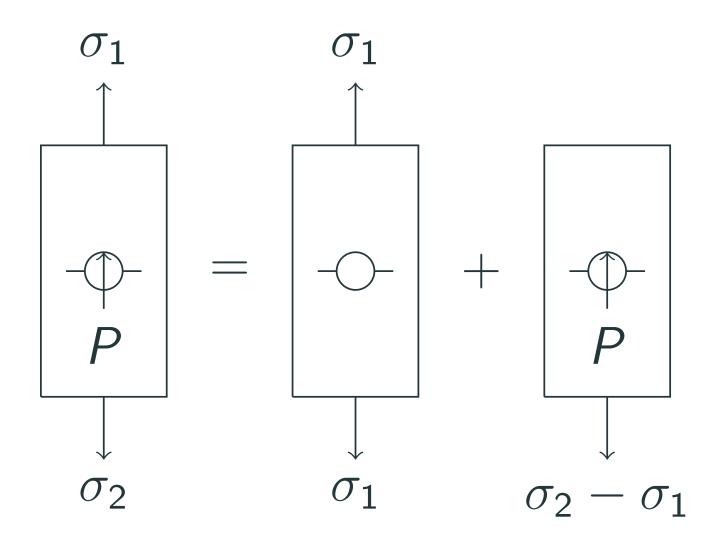
- Case 1 symmetric through cracks
- Case 2 single through crack
- Case 3 symmetric corner cracks
- Case 4 single corner crack
- Case 5 symmetric surface cracks
- Case 6 single surface crack
- Viewable here

- Since the stress intensity factor is derived using Linear Elasticity, the principle of superposition applies
- Multiple applied loads can be superposed to find the effective stress intensity factor of the combined loading

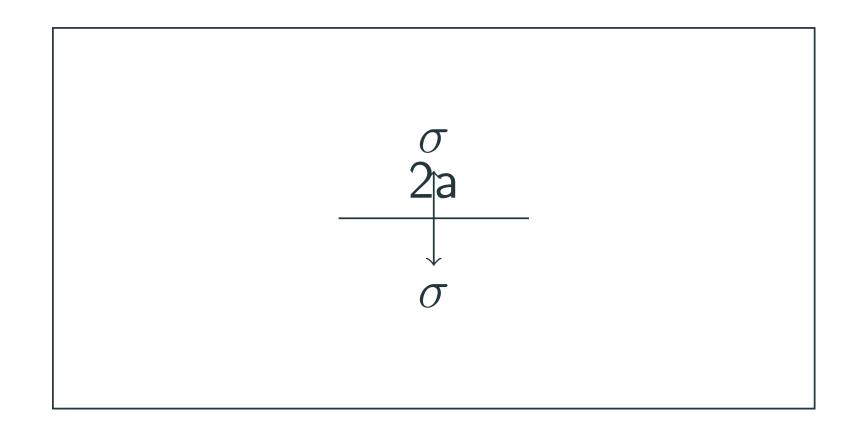


$$K_I = K_{I(\sigma)} + K_{I(P)}
onumber \ K_I = \sigma \sqrt{\pi a} + rac{P}{t\sqrt{\pi a}} rac{1 - 0.5\left(rac{a}{W}
ight) + 0.975\left(rac{a}{W}
ight)^2 - 0.16\left(rac{a}{W}
ight)^3}{\sqrt{1 - \left(rac{a}{W}
ight)}}$$

- Sometimes, the superposition needed to solve a problem is not obvious
- It can be helpful to subtract a known solution from the problem
- Note: Every super-posed solution must satisfy equilibrium.



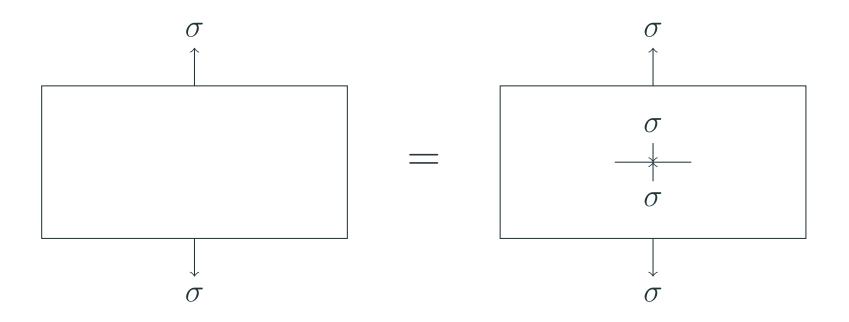
example - pressurized crack



example - pressurized crack

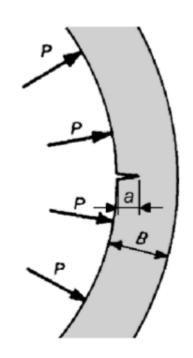
- We can find the stress intensity for a pressurized crack using a non-obvious superposition
- An un-cracked panel with remote stress would be equal to a cracked panel under remote stress with a negative pressure applied to the crack

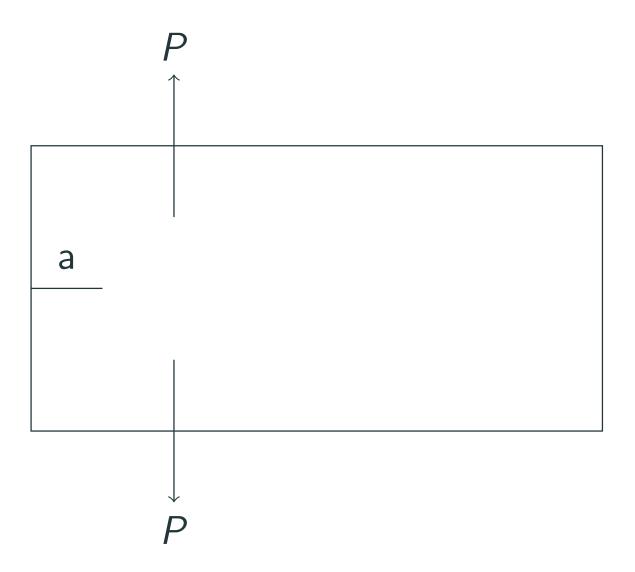
example - pressurized crack

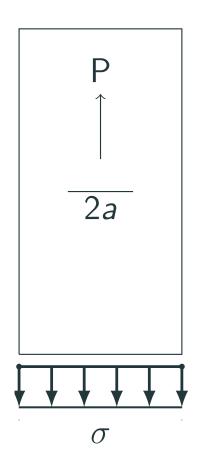


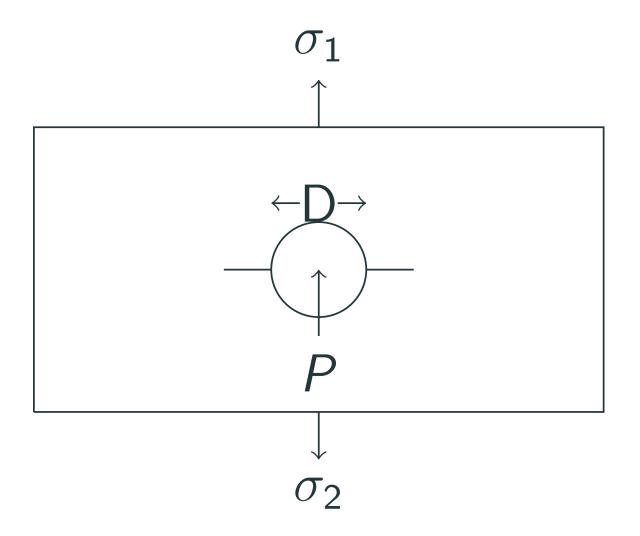
group problems

- Purpose of group problems is not just to solve a problem
- By teaching or explaining concepts to other members of your group, you also reinforce the concept yourself
- When problems are discussed as a group, you will find questions and problems you might not have otherwise found









compounding

superposition vs. compounding

- In this course, we use *superposition* to combine loading conditions
- We use *compounding* to combine edge effects
- Both are very powerful tools and important concepts

compounding

- Different types of boundaries create different correction factors to the usual stress intensity factor
- We often use β to indicate the total correction factor
- When multiple boundaries are present, we can combine them into one effective correction factor
- There are two general methods we use to create a compound correction factor

- The first method uses linear superposition, and thus is restricted to cases where the effect of each boundary can be assumed to add linearly
- While in most cases this is not strictly true, it provides a reasonable approximation

$$K_r = ar{K} + \sum_{i=1}^N (K_i - ar{K})$$

• Where N is the number of boundaries, \bar{K} is the stress intensity factor with no boundaries present and K_i is the stress intensity factor associated with the i^{th} boundary.

• We can rewrite this equation as

$$K_r = \sigma \sqrt{\pi a} eta_r = \sigma \sqrt{\pi a} + \sum_{i=1}^N (\sigma \sqrt{\pi a} eta_i - \sigma \sqrt{\pi a})$$

• Which leads to an expression for β_r as

$$eta_r = 1 + \sum_{i=1}^N (eta_i - 1)$$

• An alternative empirical method approximates the boundary effect as

$$\beta_r = \beta_1 \beta_2 \dots \beta_N$$

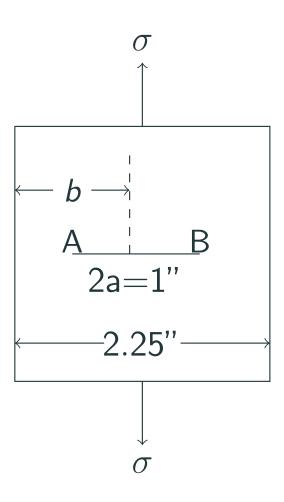
• If there is no interaction between the boundaries, method 1 and method 2 will give the same result

p. 68 - example 1

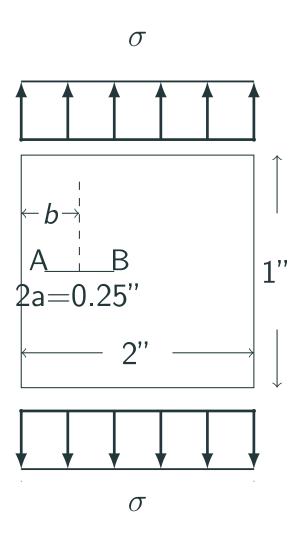
- A crack in a finite-width panel is centered between two stiffeners
- Assume the β correction factor for this stiffener configuration is $\beta_s = 0.9$
- Assume the β correction factor for this finite-width panel is β_w = 1.075
- Use both compounding methods to estimate the stress intensity
- How accurate do you expect this to be?

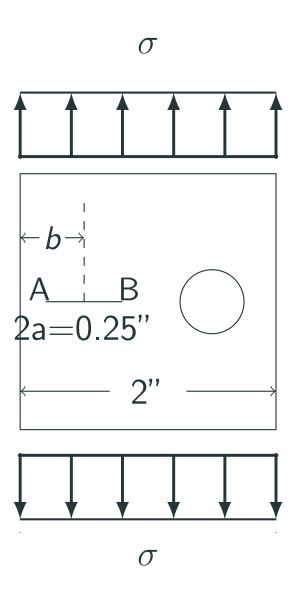
p. 69 - example 3

b = 1 inch



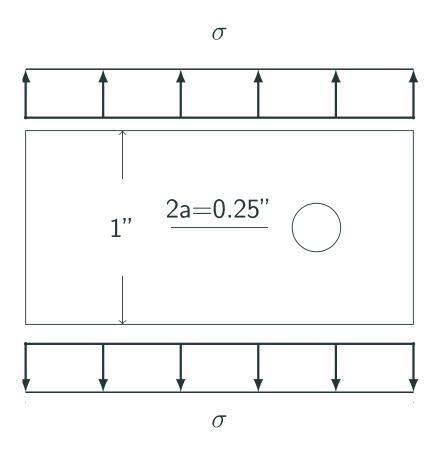
b = 0.4 inches



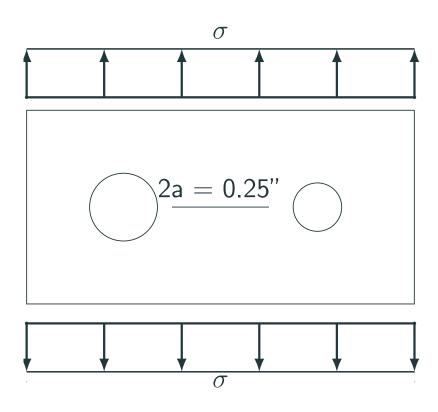


b = 0.4 inches

Hole diameter is 0.5 inches and spaced 0.5 inches away from the crack tip



Hole diameter is 0.5 inches and spaced 0.5 inches away from the crack tip



The right crack tip is 0.5 inches away from a 0.5 inch diameter hole and the left crack tip is 0.25 inches away from a 1 inch diameter hole.

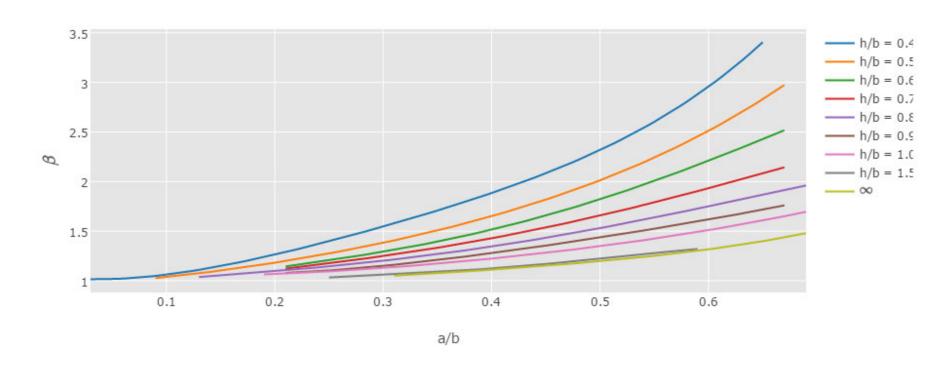
errata and supplemental charts

textbook notes

- on p. 64 there is a + missing between two terms, see Lecture 2 for the fix
- Also on p. 64, in equation 29 it is not clear, but use the f_w from a previous equation, on p. 56
- Some of the black and white figures can be difficult to use, we have scanned and recreated the plots online
- Interactive versions of compounding figures from p. 50, 71-73 can be found at here

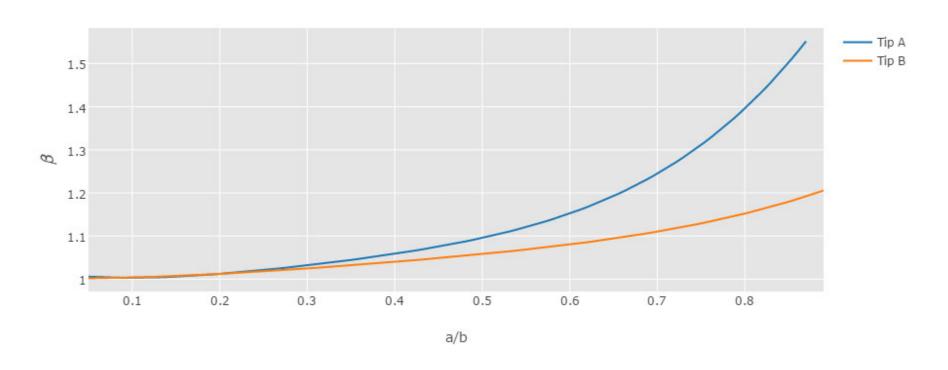
finite height - p. 50

Finite height in finite width center-cracked panel



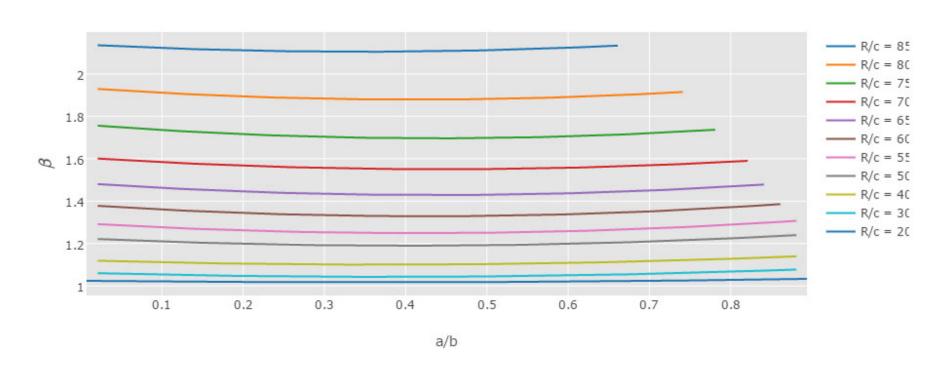
offset crack - p. 71

Internal crack near one edge (p. 71)



crack near hole - p. 72

Crack Near Hole, Tip A (p. 72)



crack near hole - p. 73

Crack Near Hole, Tip B (p. 73)

