AE 737 - MECHANICS OF DAMAGE TOLERANCE

LECTURE 13

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SCHEDULE

- · 3 Mar Section 1 Review, Homework 5 return
- 8 Mar Exam 1
- 10 Mar Exam return, Final Project discussion
- · 22 Mar Stress based fatigue, Homework 6 assigned
- · 24 Mar Stress based fatigue

OUTLINE

- 1. exam notes
- 2. stress intensity
- 3. fracture toughness
- 4. residual strength
- 5. stiffeners
- 6. multiple site damage
- 7. mixed mode fracture
- 8. extra credit

EXAM NOTES

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- · Equation sheet is posted on Blackboard



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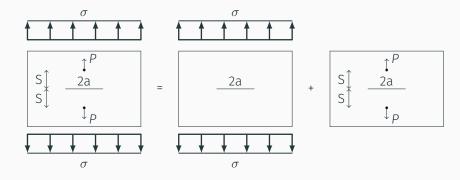
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- · Experimental

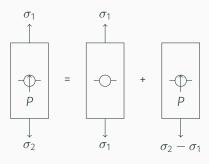
- Since the stress intensity factor is derived using Linear Elasticity, the principle of superposition applies
- Multiple applied loads can be superposed to find the effective stress intensity factor of the combined loading



$$K_{l} = K_{l(\sigma)} + K_{l(P)}$$

$$K_{l} = \sigma \sqrt{\pi a} + \frac{P}{t\sqrt{\pi a}} \frac{1 - 0.5\left(\frac{a}{W}\right) + 0.975\left(\frac{a}{W}\right)^{2} - 0.16\left(\frac{a}{W}\right)^{3}}{\sqrt{1 - \left(\frac{a}{W}\right)}}$$

- Sometimes, the superposition needed to solve a problem is not obvious
- It can be helpful to subtract a known solution from the problem





- The critical load at which a cracked specimen fails produces a critical stress intensity factor
- The "critical stress intensity factor" is known as K_c
- For Mode I, this is called K_{IC}
- The critical stress intensity factor is also known as fracture toughness

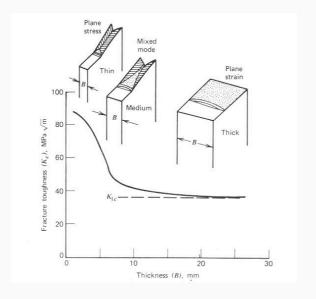
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• NOTE: "Fracture Toughness" can also refer to G_{lc} , which is analogous to K_{lc} , but not the same

- Fracture toughness is a material property, but it is only well-defined in certain conditions
- · Brittle materials
- Plane strain (smaller plastic zone)
- In these cases ASTM E399-12 is used.



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- The load must be continually increased until a critical value causes unstable crack growth

FRACTURE TOUGHNESS

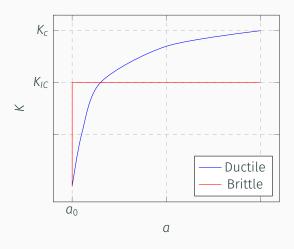
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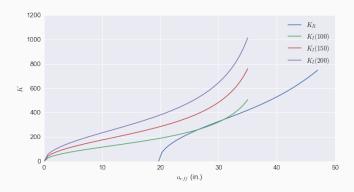
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- These are then used to create a "K-curve", plotting K_l vs. α



k_r CURVE





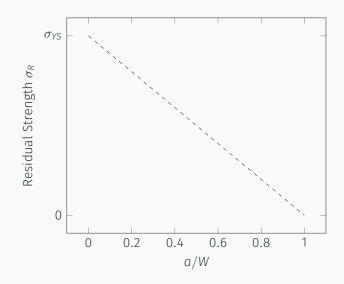
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- The residual strength, σ_R is given in terms of the gross area, so as the crack grows the residual strength due to yield decreases
- We can relate the net-section stress to σ_R by

$$\sigma_R = \sigma_{YS} \frac{A_{net}}{A_{gross}} \tag{13.2}$$

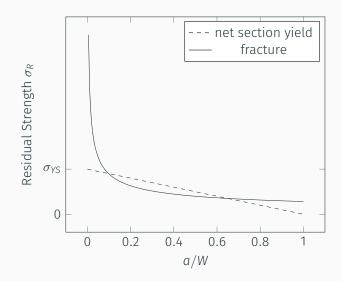


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$$\sigma_R = \sigma_C = \frac{K_C}{\sqrt{\pi a}\beta} \tag{13.3}$$



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 - 3. 2024-T3, $K_C = 144 \text{ ksi} \sqrt{\text{in.}}, \sigma_{YS} = 42 \text{ksi}$

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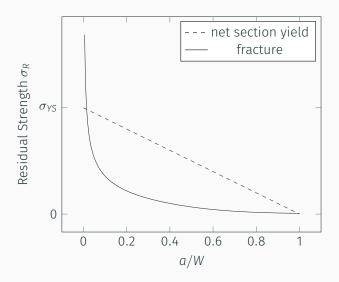
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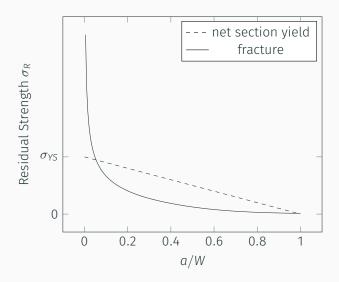
And the fracture condition by

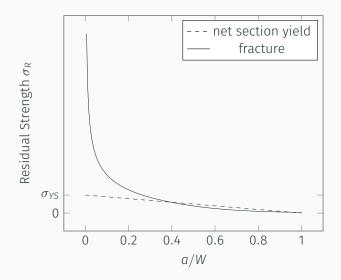
$$\sigma_{\rm C} = \frac{K_{\rm C}}{\sqrt{\pi a}\beta}$$

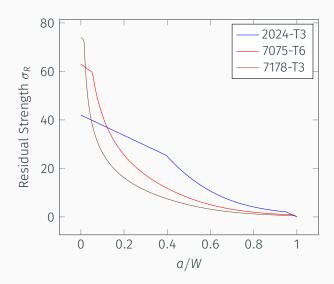
With

$$\beta = 1.12 - 0.231 \left(\frac{a}{W}\right) + 10.55 \left(\frac{a}{W}\right)^2 - 21.72 \left(\frac{a}{W}\right)^3 + 30.39 \left(\frac{a}{W}\right)^4$$











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- When σ_R is exceeded, the panel fails due to unstable crack growth
- Stiffeners reverse this trend to some extent, but causing some sections of residual strength curve to have positive slope
- When the slope of the residual strength curve is positive, crack growth is stable
- Thus in some cases, we can predict some amount of crack growth

CRITICAL CRACK LENGTH

sketch

sketch



MULTIPLE SITE DAMAGE

 $\boldsymbol{\cdot}$ Often damage can accumulate among multiple sources

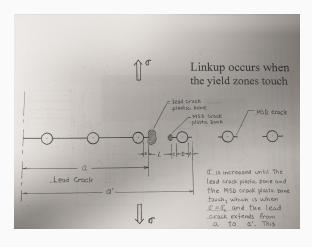
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- · Often damage can accumulate among multiple sources
- This is very common when there are a series of holes, each can develop cracks with a potential to link up

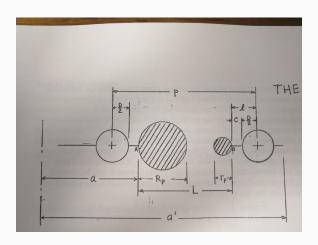
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- "link up" occurs when the plastic zones between two adjacent cracks touch

LINKUP



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LINKUP EQUATION

· We know that

$$R_p = \frac{1}{2\pi} \left(\frac{K_{la}}{\sigma_{YS}}\right)^2 \tag{13.4}$$

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LINKUP EQUATION

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Where we define the stress intensity factors at a and L as

$$K_{Ia} = \sigma \sqrt{\pi a} \beta_a \tag{13.6}$$

$$K_{ll} = \sigma \sqrt{\pi l} \beta_l \tag{13.7}$$

LINKUP EQUATION

• Since fast cracking occurs when $R_p + r_p = L$, we solve for the condition where $R_p + r_p < L$

$$\frac{1}{2\pi} \left(\frac{K_{la}}{\sigma_{YS}} \right)^2 + \frac{1}{2\pi} \left(\frac{K_{ll}}{\sigma_{YS}} \right)^2 < L \tag{13.8a}$$

$$\frac{1}{2\pi\sigma_{YS}^2} \left[K_{la}^2 + K_{ll}^2 \right] < L \tag{13.8b}$$

$$\frac{1}{2\pi\sigma_{YS}^2} \left[\sigma^2 \pi a \beta_a^2 + \sigma^2 \pi l \beta_l^2 \right] < L \tag{13.8c}$$

$$\frac{\sigma^2}{2\sigma_{YS}^2} \left[a\beta_a^2 + l\beta_l^2 \right] < L \tag{13.8d}$$

$$\frac{\sigma_c^2}{2\sigma_{VS}^2} \left[a\beta_a^2 + l\beta_l^2 \right] = L \tag{13.8e}$$

$$\sigma_{\rm c} = \sigma_{\rm YS} \sqrt{\frac{2L}{a\beta_a^2 + l\beta_l^2}} \tag{13.8f}$$

CAVEATS

- The link-up equation is not a good predictor for materials with a small plastic zone size
- Even for ductile materials, some fine tuning of the equation is needed
- In practice, MSD predictions are based on experiments

MIXED MODE FRACTURE

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- · Also assumes crack propagates in Mode I direction



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- Use Google Doc to write the page of a figure you are working on (so we don't repeat)

LINKS

- Google Doc: https://docs.google.com/spreadsheets/ d/lay4HfJQG2mF-nyr3fgtDr0lHDQoWP30TIMynKGxiwp0/ edit?usp=sharing
- Chart tracer: http://arohatgi.info/WebPlotDigitizer/app/?



REVIEW PROBLEMS

- p. 415 problem 6
- p. 418 problem 9
- p. 419 problem 10-11
- p. 421 problem 13
- · p. 423 problem 17
- p. 424 problem 3
- p. 425 problem 5

- p. 426 problem 1
- p. 427 problem 3
- p. 429 problem 6
- · p. 432 problem 9
- · p. 433 problem 14
- p. 434 problem 3
- p. 437 problem 8