

AE 737 - MECHANICS OF DAMAGE TOLERANCE

LECTURE 9

Dr. Nicholas Smith

Last Updated: February 18, 2016 at 2:57pm

Wichita State University, Department of Aerospace Engineering

OFFICE HOURS

- No Office Hours Friday :(
- Raincheck office hours Monday 3:00 - 5:00
- Homework 4 due Thursday, 25 Feb.

SCHEDULE

- 18 Feb - Residual Strength
- 23 Feb - Residual Strength, Multiple Site Damage
- 25 Feb - Multiple Site Damage, Mixed-mode Fracture, Homework 4 Due, Homework 5 Assigned
- 1 Mar - Section 1 Review, Homework 5 Due
- 3 Mar - Section 1 Review, Homework 5 return
- 8 Mar - Exam 1
- 10 Mar - Exam return, Final Project discussion

OUTLINE

1. thickness effects
2. fracture toughness review
3. residual strength
4. fedderson approach
5. proof testing

THICKNESS EFFECTS

- We already know there is a difference between plane strain and plane stress fracture toughness

THICKNESS EFFECTS

- We already know there is a difference between plane strain and plane stress fracture toughness
- As a material gets thicker and thicker, it converges to the plane strain solution

THICKNESS EFFECTS

- We already know there is a difference between plane strain and plane stress fracture toughness
- As a material gets thicker and thicker, it converges to the plane strain solution
- Thinner specimens tend towards the plane stress solution

THICKNESS EFFECTS

- We already know there is a difference between plane strain and plane stress fracture toughness
- As a material gets thicker and thicker, it converges to the plane strain solution
- Thinner specimens tend towards the plane stress solution
- When a specimen is thinner than some critical thickness, the material behavior is somewhat unknown

THICKNESS EFFECTS

- We already know there is a difference between plane strain and plane stress fracture toughness
- As a material gets thicker and thicker, it converges to the plane strain solution
- Thinner specimens tend towards the plane stress solution
- When a specimen is thinner than some critical thickness, the material behavior is somewhat unknown
- Some materials retain the constant plane stress fracture toughness

THICKNESS EFFECTS

- We already know there is a difference between plane strain and plane stress fracture toughness
- As a material gets thicker and thicker, it converges to the plane strain solution
- Thinner specimens tend towards the plane stress solution
- When a specimen is thinner than some critical thickness, the material behavior is somewhat unknown
- Some materials retain the constant plane stress fracture toughness
- Others exhibit an unpredictable decrease in fracture toughness

THICKNESS EFFECTS

- We already know there is a difference between plane strain and plane stress fracture toughness
- As a material gets thicker and thicker, it converges to the plane strain solution
- Thinner specimens tend towards the plane stress solution
- When a specimen is thinner than some critical thickness, the material behavior is somewhat unknown
- Some materials retain the constant plane stress fracture toughness
- Others exhibit an unpredictable decrease in fracture toughness
- The phenomenon is not well-understood

- There is also a difference in the fracture surface between thin and thick specimens

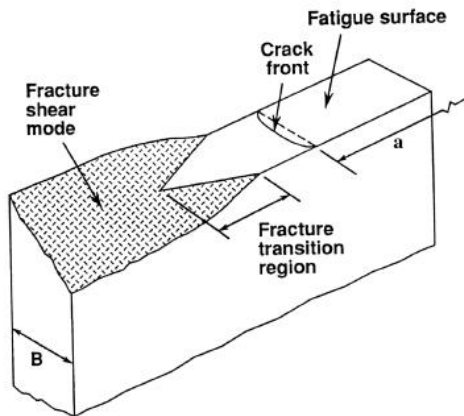
- There is also a difference in the fracture surface between thin and thick specimens
- Thin specimens (in plane stress region) fail due to slant fracture

- There is also a difference in the fracture surface between thin and thick specimens
- Thin specimens (in plane stress region) fail due to slant fracture
- This actually indicates some mixed-mode conditions at failure

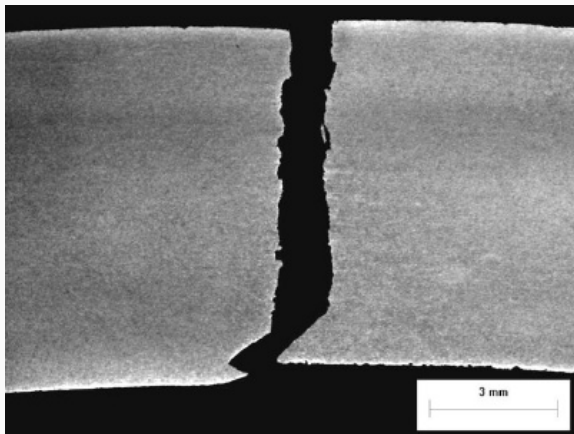
- There is also a difference in the fracture surface between thin and thick specimens
- Thin specimens (in plane stress region) fail due to slant fracture
- This actually indicates some mixed-mode conditions at failure
- Thick specimens fail due to square fracture (with a small shear tip near the edges)

- There is also a difference in the fracture surface between thin and thick specimens
- Thin specimens (in plane stress region) fail due to slant fracture
- This actually indicates some mixed-mode conditions at failure
- Thick specimens fail due to square fracture (with a small shear tip near the edges)
- This is more consistent with pure Mode I

SLANT FRACTURE



SHEAR LIP



FRACTURE TOUGHNESS REVIEW

- Group 1 - Sketch K_R -curve (for ductile material), explain what it means, how to find K_C
- Group 2 - Sketch K_C vs. crack length, explain what's happening
- Group 3 - How can we determine whether a panel is in plane strain or plane stress?
- Group 4 - Sketch K_R -curves for ductile and brittle materials, what is the difference?

RESIDUAL STRENGTH

- In the last chapter we performed some basic residual strength analysis by checking for net section yield

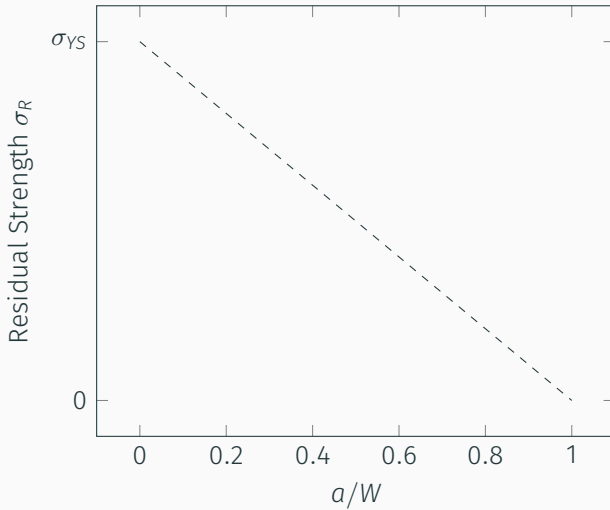
- In the last chapter we performed some basic residual strength analysis by checking for net section yield
- As the crack grows, the area of the sample decreases, increasing the net section stress

- In the last chapter we performed some basic residual strength analysis by checking for net section yield
- As the crack grows, the area of the sample decreases, increasing the net section stress
- The residual strength, σ_R is given in terms of the gross area, so as the crack grows the residual strength due to yield decreases

- In the last chapter we performed some basic residual strength analysis by checking for net section yield
- As the crack grows, the area of the sample decreases, increasing the net section stress
- The residual strength, σ_R is given in terms of the gross area, so as the crack grows the residual strength due to yield decreases
- We can relate the net-section stress to σ_R by

$$\sigma_R = \sigma_{YS} \frac{A_{net}}{A_{gross}} \quad (9.1)$$

RESIDUAL STRENGTH



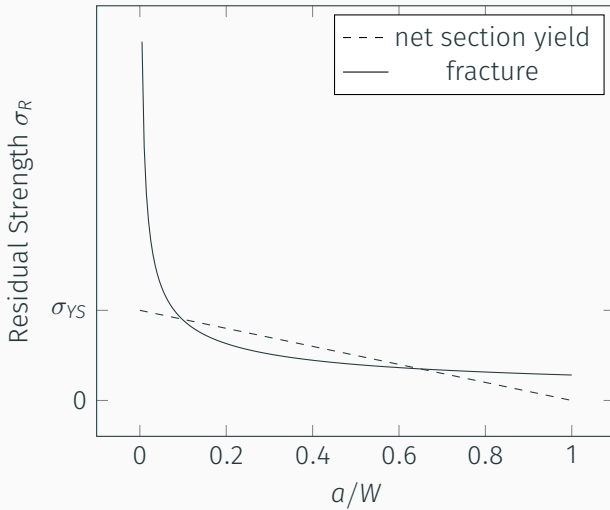
- For brittle fracture to occur, we need to satisfy the condition

- For brittle fracture to occur, we need to satisfy the condition

-

$$\sigma_R = \sigma_C = \frac{K_C}{\sqrt{\pi a} \beta} \quad (9.2)$$

RESIDUAL STRENGTH



- Within the same family of materials (i.e. Aluminum), there is generally a trade-off between yield stress and fracture toughness

- Within the same family of materials (i.e. Aluminum), there is generally a trade-off between yield stress and fracture toughness
- As we increase the yield strength, we decrease the fracture toughness (and vice versa)

- Within the same family of materials (i.e. Aluminum), there is generally a trade-off between yield stress and fracture toughness
- As we increase the yield strength, we decrease the fracture toughness (and vice versa)
- Consider a comparison of the following aluminum alloys

- Within the same family of materials (i.e. Aluminum), there is generally a trade-off between yield stress and fracture toughness
- As we increase the yield strength, we decrease the fracture toughness (and vice versa)
- Consider a comparison of the following aluminum alloys
 1. 7178-T6, $K_C = 43 \text{ ksi}\sqrt{\text{in.}}$, $\sigma_{YS} = 74\text{ksi}$

- Within the same family of materials (i.e. Aluminum), there is generally a trade-off between yield stress and fracture toughness
- As we increase the yield strength, we decrease the fracture toughness (and vice versa)
- Consider a comparison of the following aluminum alloys
 1. 7178-T6, $K_C = 43 \text{ ksi}\sqrt{\text{in.}}$, $\sigma_{YS} = 74\text{ksi}$
 2. 7075-T6, $K_C = 68 \text{ ksi}\sqrt{\text{in.}}$, $\sigma_{YS} = 63\text{ksi}$

- Within the same family of materials (i.e. Aluminum), there is generally a trade-off between yield stress and fracture toughness
- As we increase the yield strength, we decrease the fracture toughness (and vice versa)
- Consider a comparison of the following aluminum alloys
 1. 7178-T6, $K_C = 43 \text{ ksi}\sqrt{\text{in.}}$, $\sigma_{YS} = 74\text{ksi}$
 2. 7075-T6, $K_C = 68 \text{ ksi}\sqrt{\text{in.}}$, $\sigma_{YS} = 63\text{ksi}$
 3. 2024-T3, $K_C = 144 \text{ ksi}\sqrt{\text{in.}}$, $\sigma_{YS} = 42\text{ksi}$

- As an example let us consider an edge-cracked panel with $W = 6''$ and $t = 0.1''$

RESIDUAL STRENGTH

- As an example let us consider an edge-cracked panel with $W = 6''$ and $t = 0.1''$
- The net section yield condition will be given by

RESIDUAL STRENGTH

- As an example let us consider an edge-cracked panel with $W = 6''$ and $t = 0.1''$
- The net section yield condition will be given by

•

$$\sigma_c = \sigma_{ys} \frac{W - a}{W} = \sigma_{ys} \frac{6 - a}{6}$$

RESIDUAL STRENGTH

- As an example let us consider an edge-cracked panel with $W = 6''$ and $t = 0.1''$
- The net section yield condition will be given by

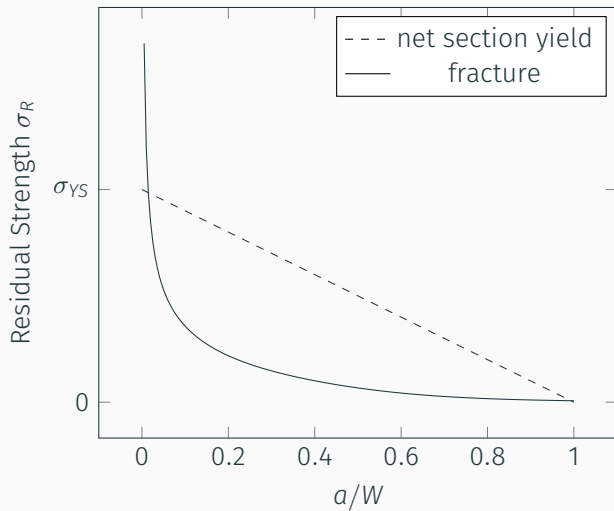
$$\sigma_c = \sigma_{YS} \frac{W - a}{W} = \sigma_{YS} \frac{6 - a}{6}$$

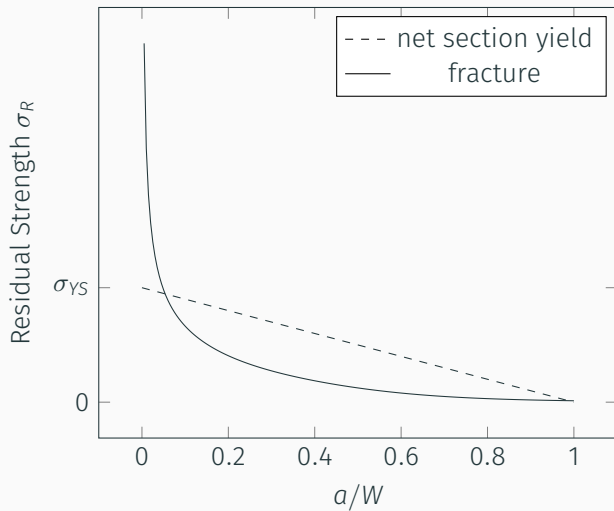
- And the fracture condition by

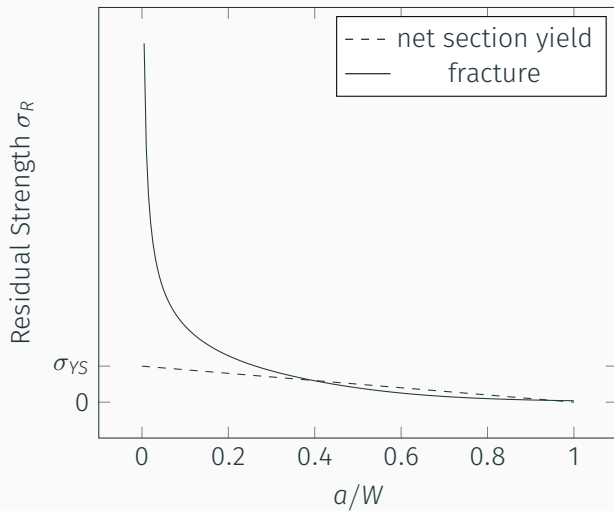
$$\sigma_c = \frac{K_c}{\sqrt{\pi a} \beta}$$

With

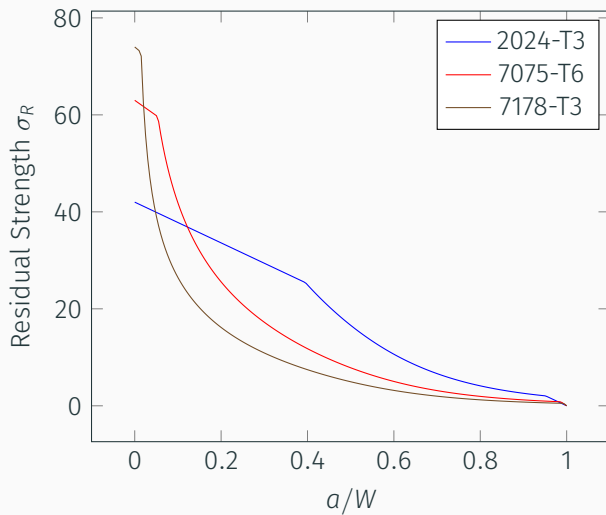
$$\beta = 1.12 - 0.231 \left(\frac{a}{W} \right) + 10.55 \left(\frac{a}{W} \right)^2 - 21.72 \left(\frac{a}{W} \right)^3 + 30.39 \left(\frac{a}{W} \right)^4$$







COMPARISON



- Uses a different grain nomenclature

- Uses a different grain nomenclature

- | | |
|-------|---------------|
| K_C | σ_{YS} |
| L-T | L |
| T-L | L-T |

- Uses a different grain nomenclature

$$\frac{K_C}{L-T} \quad \frac{\sigma_{YS}}{L}$$

$$T-L \quad L-T$$

- A-Basis vs. B-Basis values are reported (A = 99% of population will meet/exceed value, B = 90% of population)

- Uses a different grain nomenclature

$$\frac{K_C}{L-T} \quad \frac{\sigma_{YS}}{L}$$

$$T-L \quad L-T$$

- A-Basis vs. B-Basis values are reported (A = 99% of population will meet/exceed value, B = 90% of population)
- S-Basis - no statistical information available, standard value to be used

- F_{tu} - ultimate tensile strength
- F_{ty} - tensile yield strength
- F_{cy} - compressive yield strength
- F_{su} - ultimate shear strength
- F_{bru} - ultimate bearing strength
- F_{bry} - bearing yield strength
- E - tensile Young's Modulus
- E_c - compressive Young's Modulus
- G - shear modulus
- μ - Poisson's ratio

FEDDERSON APPROACH

- Unfortunately, the method we described above does not quite match experimental results

- Unfortunately, the method we described above does not quite match experimental results
- Fedderson proposed an alternative, where we connect the net-section yield and brittle fracture curves with a tangent line

- Unfortunately, the method we described above does not quite match experimental results
- Fedderson proposed an alternative, where we connect the net-section yield and brittle fracture curves with a tangent line
- This approach agrees very well with experimental data

- Unfortunately, the method we described above does not quite match experimental results
- Fedderson proposed an alternative, where we connect the net-section yield and brittle fracture curves with a tangent line
- This approach agrees very well with experimental data
- Note: We could do something similar when the crack is very long, but we are generally less concerned with this region (failure will have already occurred)

PROOF TESTING

- Proof testing is a way to use the concept of residual strength to check the size of a defect from manufacturing

- Proof testing is a way to use the concept of residual strength to check the size of a defect from manufacturing
- Due to the fatigue life of a certain panel, and/or an inspection cycle that we have prescribed for that part, we determine an "acceptable" initial flaw size, a_0

- Proof testing is a way to use the concept of residual strength to check the size of a defect from manufacturing
- Due to the fatigue life of a certain panel, and/or an inspection cycle that we have prescribed for that part, we determine an "acceptable" initial flaw size, a_0
- We then determine a load which would cause failure at this crack length

- Proof testing is a way to use the concept of residual strength to check the size of a defect from manufacturing
- Due to the fatigue life of a certain panel, and/or an inspection cycle that we have prescribed for that part, we determine an "acceptable" initial flaw size, a_0
- We then determine a load which would cause failure at this crack length
- This is the "proof load"

PROOF TESTING

- Proof testing is a way to use the concept of residual strength to check the size of a defect from manufacturing
- Due to the fatigue life of a certain panel, and/or an inspection cycle that we have prescribed for that part, we determine an "acceptable" initial flaw size, a_0
- We then determine a load which would cause failure at this crack length
- This is the "proof load"
- If the part does not fail in the proof test, we can assume that the largest flaw in the material is a_0

EXAMPLE

- Suppose we are concerned about edge cracks in a panel with $\sigma_{YS} = 65\text{ksi}$, $W = 5''$
- We have determined that the largest allowable crack is $0.4''$
- The fracture toughness of this panel is $K_c = 140 \text{ ksi}\sqrt{\text{in.}}$
- We can find the proof load

$$\begin{aligned}\sigma_c &= \frac{K_c}{\sqrt{\pi a_0} \beta} \\ &= \frac{140}{\sqrt{\pi 0.4} (1.161)} \\ &= 107.6\end{aligned}$$

- So the proof load would need to induce a gross section stress of 107.6 ksi .