

## Lecture 8 - Fracture Toughness

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## schedule

- 10 Feb - Fracture Toughness, HW3 Due, HW 2 Self-grade due
- 15 Feb - Residual Strength
- 17 Feb - Residual Strength, HW4 Due, HW 3 Self-grade due
- 22 Feb - Multiple Site Damage

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- fracture toughness
- R-curve
- thickness effects
- fracture toughness review
- residual strength

## fracture toughness

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## fracture toughness

- The critical load at which a cracked specimen fails produces a critical stress intensity factor
- The “critical stress intensity factor” is known as  $K_C$
- For Mode I, this is called  $K_{Ic}$
- The critical stress intensity factor is also known as fracture toughness

$$K_{Ic} = \sigma_c \sqrt{\pi a} \beta$$

- Note: “Fracture Toughness” can also refer to  $G_{Ic}$  which is analogous to  $K_{Ic}$  but not the same

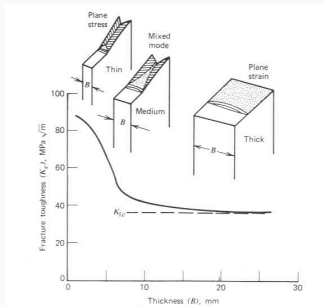
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## fracture toughness

- Fracture toughness is a material property, but it is only well-defined in certain conditions
- Brittle materials
- Plane strain (smaller plastic zone)
- In these cases ASTM E399-12 is used.

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# fracture toughness



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## unstable cracks

- Stable crack growth means the crack extends only with increased load
- Unstable crack growth means the crack will continue to extend indefinitely under the same load
- For a perfectly brittle material, there is no stable crack growth, as soon as a critical load is reached, the crack will extend indefinitely

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## stable cracks

- For an elastic-plastic material, once the load is large enough to extend the crack, it will extend slightly
- The load must be continually increased until a critical value causes unstable crack growth

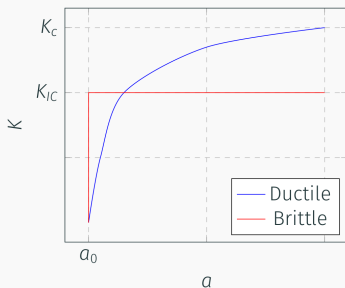
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## fracture toughness

- During an experiment, we will record the crack length and applied load ( $P_i$ ,  $a_i$ ) each time we increase the load
- We can calculate a unique stress intensity factor  $K_{Ii}$  at each of these points
- These are then used to create a “K-curve”, plotting  $K_I$  vs.  $a$

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## K-curve



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## K-curve

- Materials will generally not be as flat as the perfectly brittle example
- Plane strain conditions and brittle materials will tend towards a “flat” K-curve
- $K_{IC}$  for brittle/plane strain is very well defined
- $K_C$  for plane stress can refer to two things
- Either the maximum  $K_C$  during a test, or tangent point on  $K_R$ -curve (R-curve)

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## example

- In composites, and adhesives, some work is needed to ensure stable crack growth
- The Double-Cantilever Beam (DCB) experiment to find  $G_{Ic}$  illustrates this

$$C = \frac{\delta}{P}$$

$$C = \frac{2a^3}{3EI}$$

$$G = \frac{P^2}{2b} \frac{dC}{da}$$

$$G = \frac{P^2 a^2}{bEI}$$

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## example

- For crack growth to be stable we need

$$\frac{dG}{da} \leq 0$$

- Under fixed-load conditions, we find

$$\frac{dG}{da} = \frac{2P^2 a}{bEI}$$

- This is always positive, and thus results in unstable crack growth

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- Under fixed-displacement conditions, we substitute for  $P$
- We find

$$\frac{dG}{da} = -\frac{9\delta^2 EI}{ba^3}$$

- Which is always stable, so for DCB tests, displacement control is generally used

## R-curve

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## R-curve

- For materials with some plasticity, the  $K_R$  Curve, or R Curve, is very important
- Sometimes called a “resistance curve” it is generally dependent on
  - Thickness
  - Temperature
  - Strain rate

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## R-curve

- When done correctly,  $K_R$  curves are not dependent on initial crack size or the specimen type used
- ASTM E561 describes a general procedure

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- While we can look up plane stress  $K_c$  for various materials, it is best if we have a  $K_R$  curve
- We may not know if the table uses  $K_c$  using the tangent intersection method, or maximum stress intensity
- Even if tangent intersection method is used,  $K_c$  will differ somewhat based on initial crack length

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## R-curve

- There are two main methods for plotting the R-curve
- Crack size is measured directly (possibly with a drawn-on scale and camera)
- Effective crack size is calculated from the load-displacement data

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- When the physical crack size is measured, we need to calculate the effective crack length (and effective stress intensity factor) at each data point
- The effective crack length calculated from the load-displacement data already has the plastic zone effect built in

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## plane stress fracture toughness

- For a plane stress (or any thickness that is not plane strain) we can find  $K_c$  two ways
- One way is simply the maximum value of the  $K_R$  curve, but this does not account for unstable crack growth
- The more reliable way is to use the tangent intersection method

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## tangent intersection method

- Construct curves for  $K_I$  based on our specimen geometry with constant applied load and varying crack length
- Plot these curves on the same graph as  $K_R$
- NOTE:  $K_R$  curve should be plotted vs.  $a_{eff}$ , not  $\Delta a$  or  $\Delta a_{eff}$
- $K_c$  is the point at which one of the  $K_I$  curves is the tangent intersection with the  $K_R$  curve

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## R-Curve examples

- example<sup>1</sup>
- Excel Solver

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<sup>1</sup><https://colab.research.google.com/drive/1TIGuadrMRM5xSGic8soVFglPDyWuDaeP?usp=sharing>

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## thickness effects

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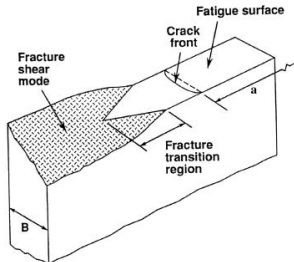
### thickness effects

- We already know there is a difference between plane strain and plane stress fracture toughness
- As a material gets thicker and thicker, it converges to the plane strain solution
- Thinner specimens tend towards the plane stress solution
- When a specimen is thinner than some critical thickness, the material behavior is somewhat unknown

- There is also a difference in the fracture surface between thin and thick specimens
- Thin specimens (in plane stress region) fail due to slant fracture
- This actually indicates some mixed-mode conditions at failure
- Thick specimens fail due to square fracture (with a small shear tip near the edges)
- This is more consistent with pure Mode I

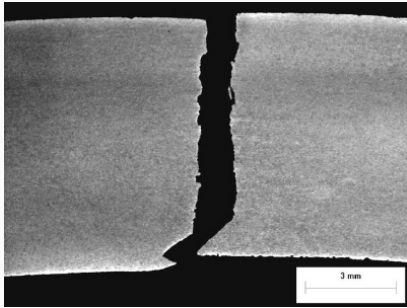
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## slant fracture



**Figure 1:** A slant fracture, where the failure plane rotates 45 degrees from the crack plane, considered a shear mode

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**Figure 2:** In this shear lip, there is a long crack that near the end rotates away by 45 degrees creating a shear lip near the surface

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## fracture toughness review

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- Group 1 - Sketch  $K_R$ -curve (for ductile material), explain what it means, how to find  $K_c$
- Group 2 - Sketch  $K_c$  vs. crack length, explain what's happening
- Group 3 - How can we determine whether a panel is in plane strain or plane stress?
- Group 4 - Sketch  $K_R$ -curves for ductile and brittle materials, what is the difference?

## residual strength

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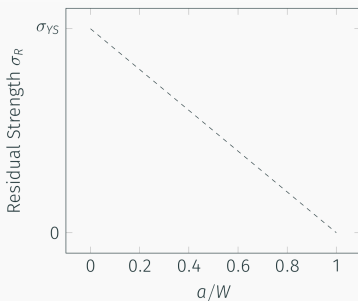
## residual strength

- As the crack grows, the area of the sample decreases, increasing the net section stress
- The residual strength,  $\sigma_R$  is given in terms of the gross area, so as the crack grows the residual strength due to yield decreases
- We can relate the net-section stress to  $\sigma_R$  by

$$\sigma_R = \sigma_{YS} \frac{A_{net}}{A_{gross}}$$

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## residual strength

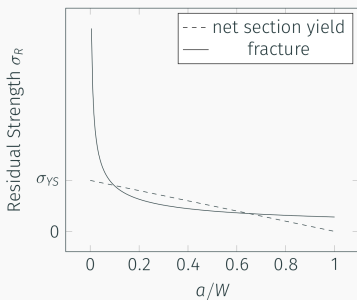


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- For brittle fracture to occur, we need to satisfy the condition

$$\sigma_R = \sigma_C = \frac{K_C}{\sqrt{\pi a \beta}}$$

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## residual strength

- Within the same family of materials (i.e. Aluminum), there is generally a trade-off between yield stress and fracture toughness
- As we increase the yield strength, we decrease the fracture toughness (and vice versa)
- Consider a comparison of the following aluminum alloys
  1. 7178-T6,  $K_C = 43 \text{ ksi}\sqrt{\text{in.}}$ ,  $\sigma_{YS} = 74 \text{ ksi}$
  2. 7075-T6,  $K_C = 68 \text{ ksi}\sqrt{\text{in.}}$ ,  $\sigma_{YS} = 63 \text{ ksi}$
  3. 2024-T3,  $K_C = 144 \text{ ksi}\sqrt{\text{in.}}$ ,  $\sigma_{YS} = 42 \text{ ksi}$

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## residual strength

- As an example let us consider an edge-cracked panel with  $W = 6$  and  $t = 0.1$  inches
- The net section yield condition will be given by

$$\sigma_C = \sigma_{YS} \frac{W - a}{W} = \sigma_{YS} \frac{6 - a}{6}$$

- And the fracture condition by

$$\sigma_C = \frac{K_C}{\sqrt{\pi a \beta}}$$

With

$$\{\beta = 1.12 - 0.231 \left(\frac{a}{W}\right) + 10.55 \left(\frac{a}{W}\right)^2 - 21.72 \left(\frac{a}{W}\right)^3 + 30.39 \left(\frac{a}{W}\right)^4\}$$

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- Uses a different grain nomenclature

| $K_C$ | $\sigma_{YS}$ |
|-------|---------------|
| L-T   | L             |
| T-L   | L-T           |

- A-Basis vs. B-Basis values are reported (A = 99% of population will meet/exceed value, B = 90% of population)
- S-Basis - no statistical information available, standard value to be used

- $F_{tu}$  - ultimate tensile strength
- $F_{ty}$  - tensile yield strength
- $F_{cy}$  - compressive yield strength
- $F_{su}$  - ultimate shear strength
- $F_{bru}$  - ultimate bearing strength
- $F_{bry}$  - bearing yield strength
- $E$  - tensile Young's Modulus
- $E_c$  - compressive Young's Modulus
- $G$  - shear modulus
- $\mu$  - Poisson's ratio

- Fracture data is on pp. 111-121
- Tensile data is on pp. 138-143
- $K_c$  charts are also available in interactive versions here<sup>2</sup>

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<sup>2</sup><http://ndaman.github.io/damagetolerance/examples/Fracture%20Toughness%20Figures.html>