

# **AE 737 - MECHANICS OF DAMAGE TOLERANCE**

## LECTURE 15

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Last Updated: March 22, 2016 at 2:15pm

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# SCHEDULE

- 22 Mar - Stress based fatigue, Homework 6 assigned
- 24 Mar - Stress based fatigue
- 29 Mar - Influence of notches on fatigue, Homework 7 assigned, Homework 6 due
- 31 Mar - Strain based fatigue, project abstract due



1. fatigue
2. nominal and local stress
3. fatigue tests
4. fatigue life analysis
5. fatigue limit

# FATIGUE

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damage as function of tool speed

- We refer to damage from repeated, or cyclic loads as fatigue damage
- Some of the earliest work on fatigue began in the 1800's
- Chains, railway axles, etc.
- An estimated 80% of failure expenses are due to fatigue

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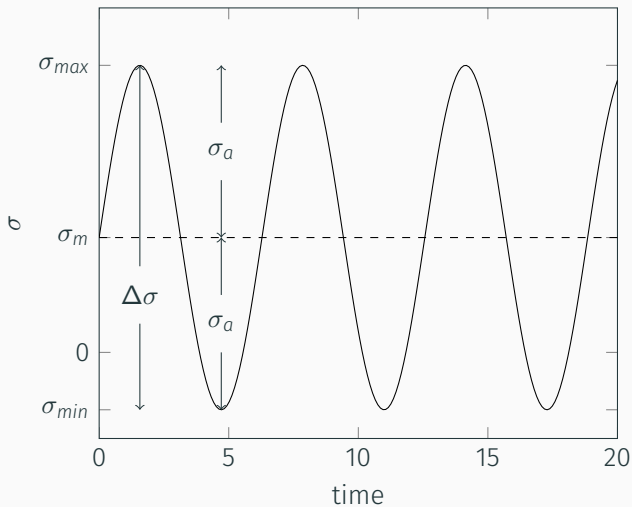
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- Stress based fatigue analysis
- Strain based fatigue analysis
- Fracture mechanics fatigue analysis

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- This is referred to as constant amplitude stressing

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- $\sigma_a$  is the stress amplitude, and is the variation about the mean
- We can express all of these in terms of the maximum and minimum stress

$$\Delta\sigma = \sigma_{max} - \sigma_{min} \quad (15.1)$$

$$\sigma_m = \frac{\sigma_{max} + \sigma_{min}}{2} \quad (15.2)$$

$$\sigma_a = \frac{\sigma_{max} - \sigma_{min}}{2} \quad (15.3)$$

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- And the amplitude ratio,  $A$  is defined as

$$A = \frac{\sigma_a}{\sigma_m} \quad (15.5)$$

- There are some useful relationships between the above equations

$$\Delta\sigma = 2\sigma_a = \sigma_{max}(1 - R) \quad (15.6a)$$

$$\sigma_m = \frac{\sigma_{max}}{2}(1 + R) \quad (15.6b)$$

$$R = \frac{1 - A}{1 + A} \quad (15.6c)$$

$$A = \frac{1 - R}{1 + R} \quad (15.6d)$$

## NOMINAL AND LOCAL STRESS

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- For many cases (bending, notches),  $\sigma \neq S$  in general
- We must also be careful to note  $\sigma_y$ , in some cases  $S < \sigma_y$  but at some locations  $\sigma > \sigma_y$

# SIMPLE TENSION

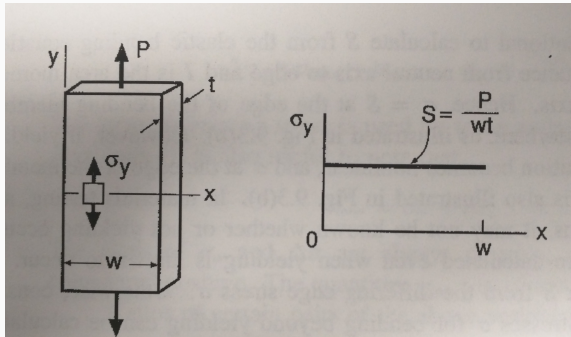
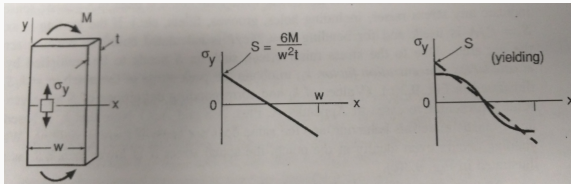


Figure 1: In this case  $S = \sigma$

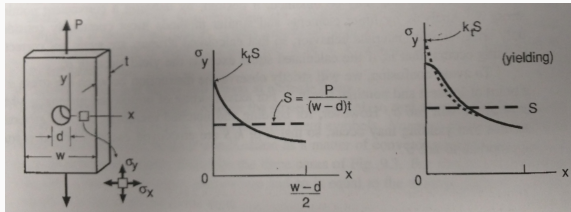
# BENDING



**Figure 2:** As long as  $\sigma < \sigma_y$ ,  $\sigma$  varies linearly. If  $\sigma > \sigma_y$  at any location, however, the relationship is non-linear



# NOTCHES



**Figure 3:** As long as  $\sigma < \sigma_y$ ,  $\sigma$  varies linearly. If  $\sigma > \sigma_y$  at any location, however, the relationship is non-linear

## FATIGUE TESTS

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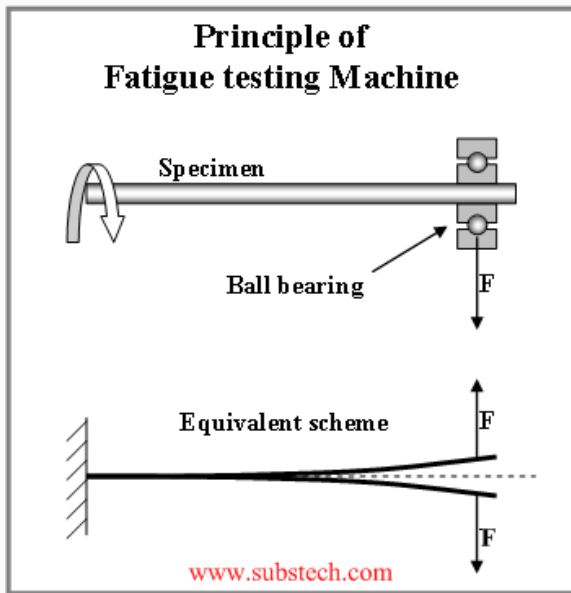
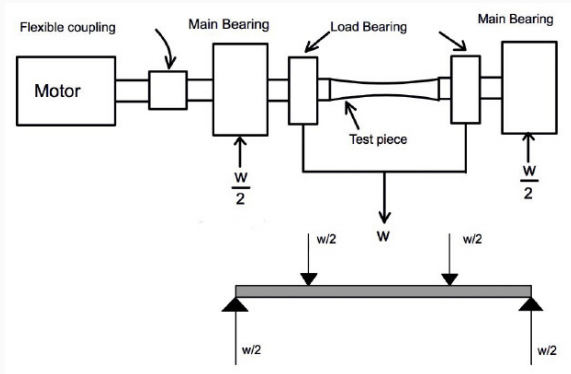


Figure 4. Cantilever beam produces non-uniform stress state

## ROTATING FOUR-POINT BEND



**Figure 5:** Four-point bend gives uniform stress (along top and bottom surfaces)

- The above rotating methods are very common, but in their current configurations can only be used for zero mean stress

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- a reciprocating bend test can be used for non-zero mean stress

# RECIPROCATING BEND TEST

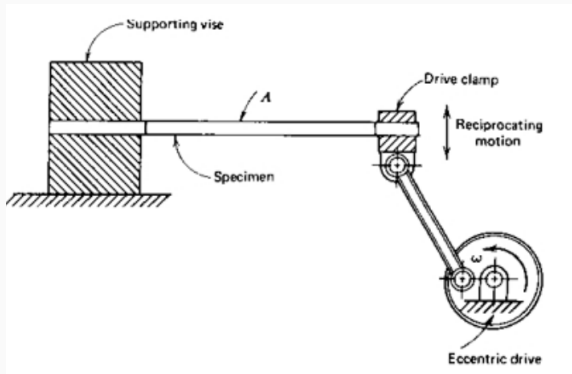


Figure 6: A reciprocating cantilever test allows for non-zero mean stress



SHANGHAI HUALONG TEST INSTRUMENTS CORP

*Enter into a high precision testing world*

## Universal Testing Machine

### WAW Series

 *Dual space*

Standard model



PC Strand model





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- At a speed of 100 Hz, it would take 28 hours for  $10^7$  cycles, 12 days for  $10^8$  cycles, and nearly 4 months for  $10^9$  cycles
- While some machines can test at very high speeds, the inertia of the sample can interfere with results

# FATIGUE LIFE ANALYSIS

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- In general, one set (or family) of S-N curves is generated using the same  $\sigma_m$
- Usually  $S_a$  (the nominal stress equivalent of  $\sigma_a$ ) is plotted versus  $N$  (the number of cycles)

- Each individual point on an S-N curve represents one fatigue experiment

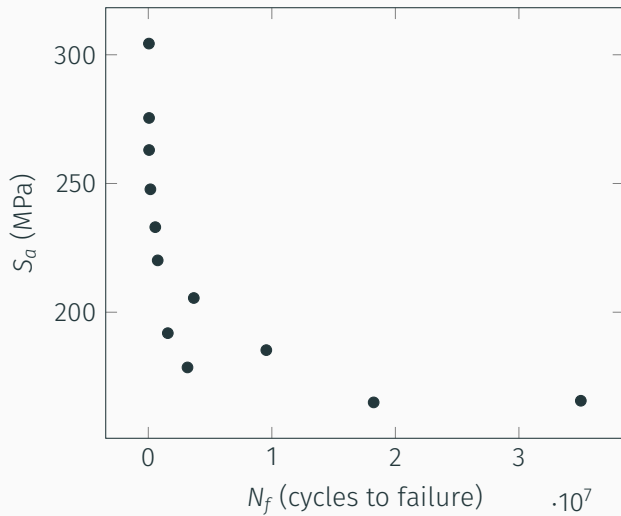
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- In the following plot, if only one test was performed for each point, the total number of cycles tested would be about  $7.3 \times 10^7$
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- Each repetition would further increase the test time required

## STRESS LIFE CURVES



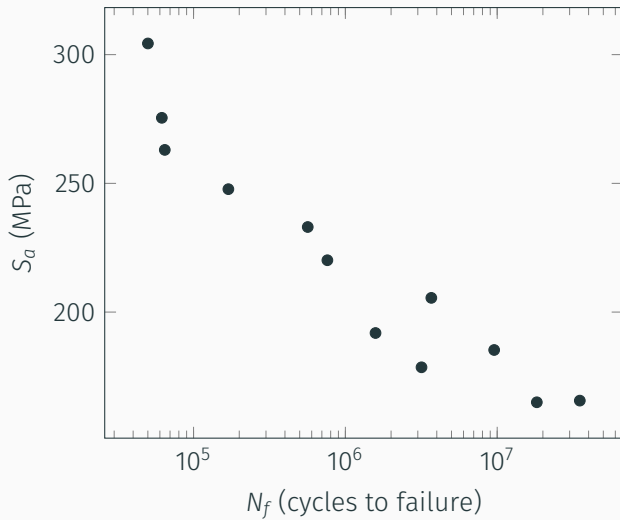


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- It is also very difficult to differentiate between low-cycle fatigue failure stresses
- Instead S-N curves are often plotted on a semi-log or log-log scale, so pay attention to the axes

## STRESS LIFE CURVES



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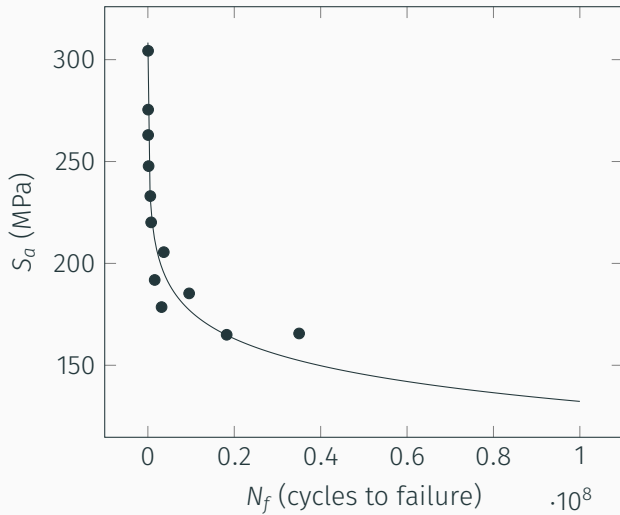
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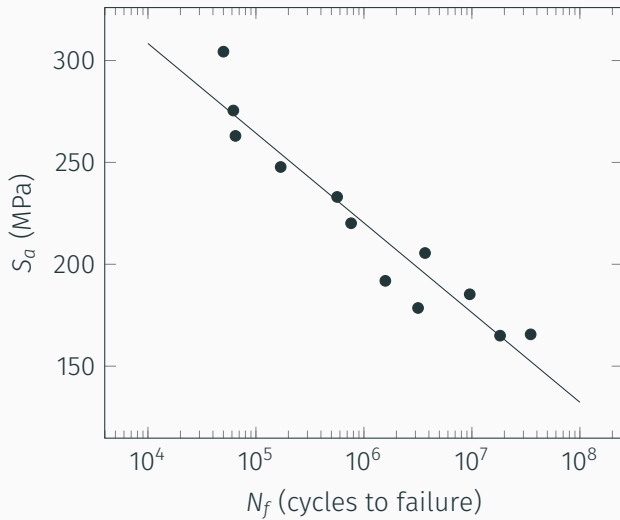
$$\sigma_a = \sigma'_f (2N_f)^b \quad (15.8)$$

- $\sigma'_f$  and  $b$  are often considered material properties and can often be looked up on a table (p. 235)

## CURVE FIT



## STRESS LIFE CURVES



## FATIGUE LIMIT

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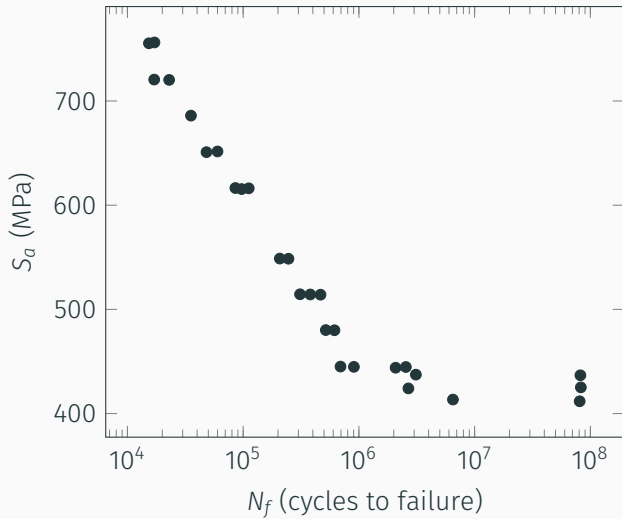
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- In these materials,  $\sigma_e$  is considered to be a material property
- This phenomenon is not typical of aluminum or copper alloys, but is sometimes arbitrarily assigned using whatever the failure stress is at some large number of cycles ( $10^7$  or  $10^8$ )

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- High cycle fatigue occurs when the stress is sufficiently low that yielding effects do not dominate behavior
- When yielding effects do dominate behavior, the strain-based approach is more appropriate