

# AE837

## Advanced Mechanics of Damage Tolerance

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## upcoming schedule

- Aug 29 - Griffith Fracture
- Sep 3 - Elastic Stress Field, Homework 1 Due
- Sep 5 - Elastic Stress Field
- Sep 10 - Elastic Stress Field

# outline

- relation among energies

# relation among energies

## energy balance

- Griffith's theory is founded on the principle of energy balance
- During crack extension, the external work done,  $dW_e$  must equal the increment of surface energy,  $dW_s$ , and the increment of elastic strain energy,  $dU$

$$dW_s + dU = dW_e$$

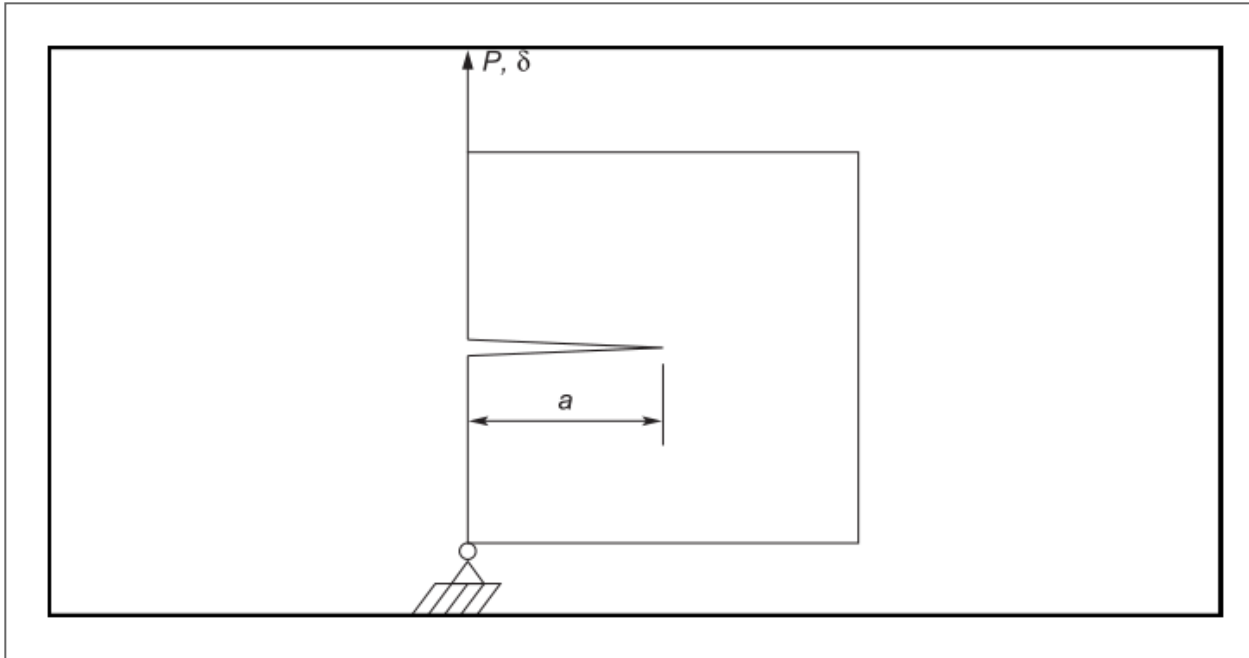
## energy balance

- For a conservative field we can write this as

$$\frac{\partial}{\partial a}(W_s + U + V) = 0$$

- Where a negative potential,  $V$ , implies positive external work done  $dW_e$

# example



## example

- The displacement at the top edge will be proportional to the applied load by some elastic compliance of the specimen

$$\delta = SP$$

- Note that this compliance,  $S$ , will be a function of the crack length,  $a$
- The strain energy can be expressed as

$$U = \int_{\delta=0}^{\delta=SP} P d\delta = \int_{\delta=0}^{\delta=SP} \frac{\delta}{S} d\delta$$



## example

- After integrating

$$U = \frac{1}{2S} (\delta^2) \Big|_0^{SP} = \frac{1}{2} SP^2$$

## example

- To find the incremental strain energy increase (where both  $P$  and  $S$  should be treated as variable), we find

$$dU = \frac{1}{2}P^2 dS + SPdP$$

- We will now consider two loading cases, one with fixed displacement and the other with fixed loading force

## fixed displacement

- Under constant displacement we have  
 $\delta = SP = \text{constant}$
- This means that the derivative of displacement will be zero, hence  
 $d\delta = SdP + PdS = 0$
- and  
 $SdP = -PdS$

## fixed displacement

- Substituting into the previous equation gives

$$dU = -\frac{1}{2}P^2 dS$$

- Since  $d\delta = 0$ , the external work,  $dW_e = 0$  and we find

$$dW_s = -dU = \frac{1}{2}P^2 dS$$

## fixed load

- If instead of fixing displacement we fix the applied load we have  
 $dP = 0$
- Which gives  
$$dU = \frac{1}{2} P^2 dS$$
- The strain energy increases (while under fixed displacement it decreased)

## fixed load

- Further, we can find the external work done as

$$dW_e = Pd\delta = P^2dS$$

- And thus, from energy balance, we find the surface energy

$$dW_s = \frac{1}{2}P^2dS$$

- In this case the external work is equally split between strain energy and surface energy

## comparison

- In both cases, the energy released is  $dW = dW_e - dU$

$$dW = 0 - \left(-\frac{1}{2}P^2 dS\right) \quad \text{fixed displacement}$$

$$dW = P^2 dS - \frac{1}{2}P^2 dS \quad \text{fixed load}$$

- And we see that the energy released is independent of the load type

## example - stable crack

- During experimental characterization, it is often desirable to measure crack growth
- To do this accurately, the crack growth must be stable
- For crack growth to be stable, the strain energy should decrease as crack length increases ( $\partial G / \partial a \leq 0$ )
- If we recall  $G$  for the Double-Cantilever Beam (DCB) specimen

$$G = \frac{P^2 a^2}{bEI}$$



## example - stable crack

- Under fixed-load conditions, we find

$$\frac{dG}{da} = \frac{2P^2 a}{bEI}$$

- This is always positive, and thus results in unstable crack growth
- Under fixed-displacement conditions, we substitute for  $P$  in terms of displacement using  $P = \delta/S$

## example - stable crack

- From beam theory we can express  $S$  more precisely as

$$S = \frac{2a^3}{3EI}$$
$$\frac{dG}{da} = -\frac{9\delta^2 EI}{ba^5}$$

- Which is always stable, so for DCB tests, displacement control is generally used

## example - peel of thin film

