

**REPORT**

**PROJECT - PREFINAL STUDY**  
**Programming Assignment II**  
**Performance Calculations**  
**HOVER CASE**

Helicopter Theory

Uck459E - 22532

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## - Introduction

In the first assignment, the AH-1W Cobra helicopter was selected and information was given about this helicopter. In line with this information, the required input values for the matlab code were taken as discussed below. The required power and power coefficient of the main rotor of the helicopter, the thrust force developed by the tail rotor, the required power and power coefficient of the tail rotor, excess power, merit and rate of climb shall be calculated for different altitude values.

Operating density altitudes as  $h_Q = 1 \text{ km}, 3 \text{ km and } 5 \text{ km}$

|  |   |   |                         |
|--|---|---|-------------------------|
| Contractor                             | Bell Helicopter, Textron, Inc. (Prime), General Electric, Kollsman Inc.     |   |                         |
| Power Plant                            | Two General Electric T700-GE-401 Turboshift engines (1,690 horsepower each) |   |                         |
| Main rotor diameter                    | 14.63 m   | Weight empty  | 4,634 kg                |
| Main rotor blade chord                 | 0.84 m  | Mission fuel load (usable)                          | 946 kg                  |
| Tail rotor diameter                    | 2.97 m  | Maximum useful load (fuel and disposable ordinance) | 2,065 kg                |
| Tail rotor blade chord                 | 0.305 m   | Maximum Takeoff and landing weight                  | 6,690 kg                |
| Distance between rotor centers         | 8.89 m  | Maximum disc loading                                | 39.80 kg/m <sup>2</sup> |
| Wing span                              | 3.28 m  | Maximum power loading                               | 4.42 kg/kW              |
| Wing aspect ratio                      | 3.74  | Main rotor blades (each)                            | 6.13 m <sup>2</sup>     |
| Length (overall, rotors turning)       | 17.68 m   | Tail rotor blades (each)                            | 0.45 m <sup>2</sup>     |
| Length (fuselage)                      | 13.87 m   | Main rotor disc                                     | 168.11 m <sup>2</sup>   |
| Width overall                          | 3.28 m  | Tail rotor disc                                     | 6.94 m <sup>2</sup>     |
| Height (to top of rotor head)          | 4.11 m  | Vertical fin  | 2.01 m <sup>2</sup>     |
| Overall height                         | 4.44 m  | Horizontal tail surfaces                            | 1.41 m <sup>2</sup>     |
| Ground clearance (main rotor, turning) | 2.74 m  | Climb rate  | 1,925 feet              |
| Elevator span                          | 2.11 m  | Maximum altitude                                    | 14,750 feet             |
| Width over skids                       | 2.24 m  | Maximum attainable speed                            | 170 knots               |
|  |   | Maximum cruising speed                              | 152 knots               |

**AH1W - COBRA**

## - 1) Equation Theory

- a) First, the air temperature at different altitudes and the pressure accordingly were calculated. As a result, density ratios were calculated for these heights. Troposphere equations in Figure 1.1 are used.

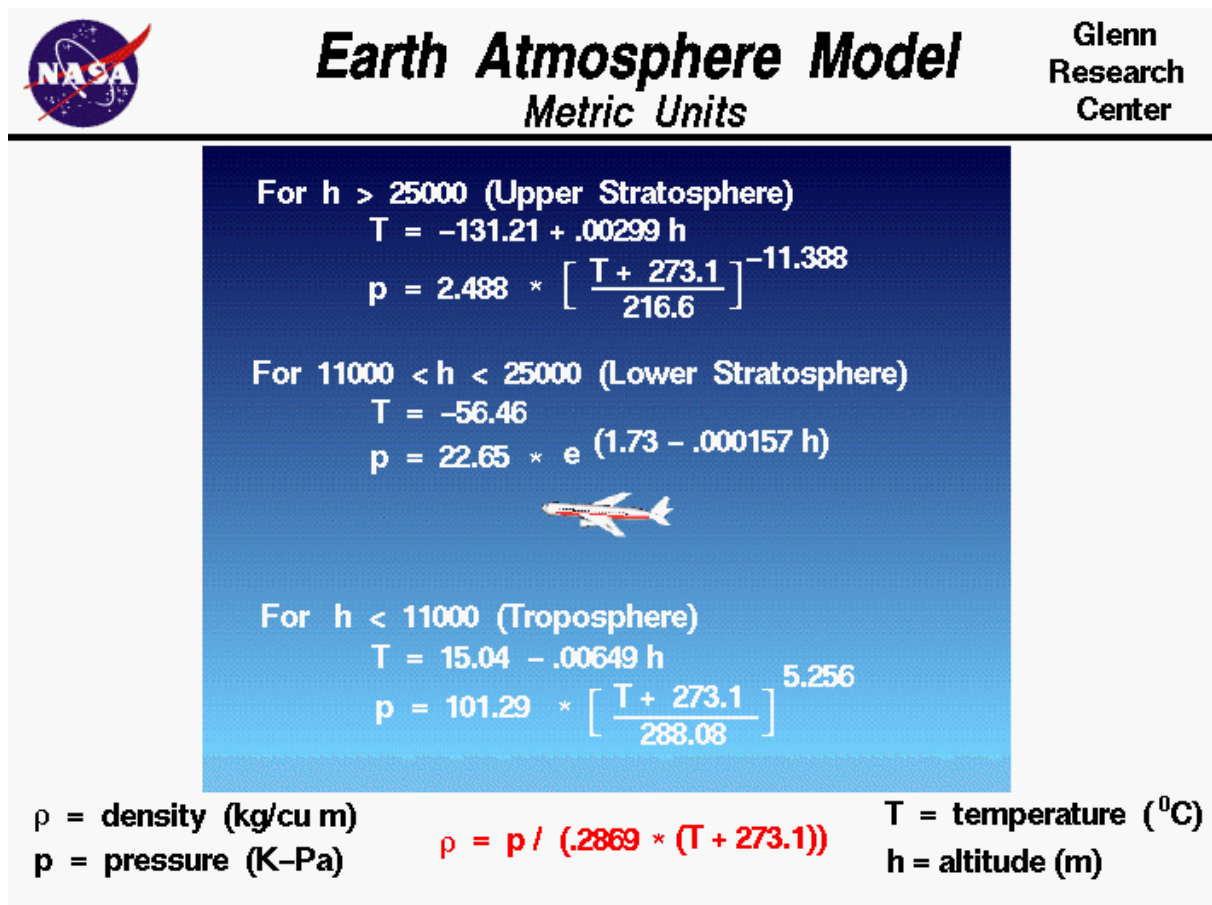


Figure 1.1

- b) The AH1W- Cobra has two General Electric T700-GE-401 engines, both have 1300kW power, for variable altitude using the equation below.

$$P = P_0 \frac{\rho}{\rho_0}$$

- c) The required power and power coefficient of the main rotor were calculated using the following equations.

$$(P_{main})_h = P_i + P_0 = \frac{\kappa T^{3/2}}{\sqrt{2\rho A}} + \rho A (\Omega R)^3 \frac{\sigma C_{d0}}{8}$$

$$C_p = \frac{P_i + P_0}{\rho \times A \times (\Omega \times R)^3}$$

- d) To calculate the thrust produced by the tail rotor, the distance between the main rotor and the tail rotor and the main engine torque were needed.

$$(Q_{main})_h = (P_{main})_h / \Omega$$

$$T_{tail} = \frac{Q_{main}}{Dstncem_t}$$

- e) The following equations were used to calculate the required power and power coefficient of the tail rotor.

$$(P_{tail})_h = P_{i_{tr}} + P_{0tr} = \left( \frac{\kappa T^{3/2}}{\sqrt{2\rho A}} \right)_{tr} + \left[ \rho A (\Omega R)^3 \frac{\sigma C_{d0}}{8} \right]_{tr}$$

$$(C_p)_{tail} = \frac{(P_i)_{tail} + (P_0)_{tail}}{\rho \times A_t \times (\Omega_t \times R_t)^3}$$

- f) Following equations were used to calculation of the excess power at each altitude

$$\Delta P = P_{available} - [(P_{main})_h + (P_{tail})_h]$$

- g) The Figure of Merit (FM) equation, which measures the aerodynamic performance of a rotor while suspended in air at variable altitude, is as follows.

$$C_t = \frac{T}{\rho \times (\Omega \times R)^2 \times A}$$

$$P_{ideal} = \frac{C_t^{3/2}}{\sqrt{2}}$$

$$P_h = k \times P_{ideal} + \frac{\sigma C_{d0}}{8}$$

$$FM = \frac{P_{ideal}}{P_h}$$

## - 2) Table

| Altitude (km)                           | 1 km                | 3 km                | 5 km                |
|---|---------------------|---------------------|---------------------|
| Air density (kg/m <sup>3</sup> )        | 1.1141              | 0.9115              | 0.7383              |
| Available power (W)                     | 2.3646<br>1.0e+06 * | 1.9345<br>1.0e+06 * | 1.5670<br>1.0e+06 * |
| Required induced power (main rotor) (W) | 6.3640<br>1.0e+05 * | 7.0360<br>1.0e+05 * | 7.8177<br>1.0e+05 * |
| Required profile power (main rotor) (W) | 2.8597<br>1.0e+05 * | 2.3395<br>1.0e+05 * | 1.8950<br>1.0e+05 * |
| Required induced power (tail rotor) (W) | 4.2223<br>1.0e+04 * | 4.7838<br>1.0e+04 * | 5.6047<br>1.0e+04 * |
| Required profile power (tail rotor) (W) | 6.5698<br>1.0e+03 * | 5.3747<br>1.0e+03 * | 4.3536<br>1.0e+03 * |
| Excess power (m/s)                      | 1.3935<br>1.0e+06 * | 0.9438<br>1.0e+06 * | 0.5353<br>1.0e+06 * |
| Figure of Merit                         | 0.6000              | 0.6526              | 0.6999              |

## - 3) Comments

- As the altitude rises above sea level, the air density decreases as the temperature and pressure decrease. The AH1W-Cobra has a turboshaft engine. These engines are a type of gas turbine engine designed to generate shaft power instead of jet thrust, that is, to generate power by pushing air. As the density of this air decreases, the total thrust also decreases. As the helicopter weight remains the same, the higher the helicopter is, the more power is used to keep the helicopter in the air. As the density decreases, the thrust produced by the main rotor decreases. When the density decreases, the required profile force decreases as the rotor system can move more easily due to the density. Therefore, as the height of the

helicopter increases, the required profile power decreases. The explanations for the tail rotor are the same, the higher the helicopter's height, the higher the overall power consumption. As the altitude increases, the total power produced by the motor decreases and the total power consumption increases.

## - Codes

```
clc
clear all

Ro = 1.225; % Sea level air density at - kg/m^3
To = 288.15; % Sea level air temperature - K
altitude = [1000,3000,5000]; % Given density altitudes - m
k = 1.15; % In hover case k value is 1.10-1.15
Gtow = 4953*9.81; % Weight of helicopter - N
T = Gtow; % Thrust in hover case - N

% Main Rotor
Po = 2*1300*1000; % 2x General Electric T700 engine - W
N = 2; % Number of blades
r = 14.6/2 ; % Rotor radius (Rotor diameter 14.6m) - m
Da = 168.11; % Disc area - m^2
omega = 2*pi*(360/60); % Velocity, RPM = 360 - 1/s
Cdo = 0.008; % Drag coefficient
c = 0.84; % Chord - m
solidity = N*c/(pi*r); % Solidity

% Tail Rotor
Nt = 2; % Number of blades
rt = 2.97/2 ; % Rotor radius (Rotor diameter 2.97m) - m
Dat = 6.94; % Disc area - m^2
omega_t = 2*pi*(1200/60); % Velocity, RPM = 1200 - 1/s
Cdot = 0.008; % Drag coefficient
ct = 0.305; % Chord - m
solidityt = Nt*ct/(pi*rt); % Solidity
Dstncem_t = 8.89; % Distance between rotor centers - m

% a) Calculation of the air density at 3 different altitudes, ρ
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Talt = 15.04 - 0.00649 * altitude
Pres = (101.29) * ((Talt + 273.15)/288.08).^(5.256)
Roalt = Pres./(0.2869*(Talt + 273.15))

% b) Calculation of the available engine power at different altitudes.
Poav = Po.*(Roalt/Ro)

% c) Power and power coefficient of the main rotor at each altitude
Pim = (k.*T.^1.5)./(sqrt(2.*Roalt*Da))
Pom = Da.*Roalt.*((omega*r)^3)*solidity*Cdo/8
Phm = Pim + Pom
Cpm = Phm./(Roalt.*Da.*((omega*r)^3))

% d) Calculation of the thrust developed by the tail rotor
Q_main_h = Phm./omega
T_t = Q_main_h./Dstncem_t

% e) Power and power coefficient of the tail rotor at each altitude
Pit = (k.*T_t.^1.5)./(sqrt(2.*Roalt*Dat))
Pot = Dat.*Roalt.*((omega_t*rt)^3)*solidityt*Cdot/8
Pht = Pit + Pot
Cpt = Pht./(Roalt.*Dat.*((omega_t*rt)^3))

% f) Calculation of the excess power at each altitude
Deltap = Poav - (Phm+Pht)

% Calculation of available maximum climb velocity
V_c = Deltap./Gtow

% g) Calculation of the Figure of Merit (FM) at each altitude
ct =T./(Roalt.*(omega.*r).^2.*Da)
Pideal = ct.^(3/2)./sqrt(2)
FM = Pideal ./(k.*Pideal + (solidity.*Cdo./8))

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