

Volatile Organic Compound Detection Using Insect Odorant-Receptor Functionalised Field-Effect Transistors

by

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1. Characteristics of Pristine Carbon Nanotube & Graphene Field Effect Transistors

1.1. Introduction

Several different approaches were followed to fabricate carbon nanotube network and graphene field-effect transistors for biosensor use. The three carbon nanotube film types used for devices were the solvent-deposited, surfactant-deposited and steam-assisted surfactant-deposited (steam-deposited) films discussed in the previous chapter. As minor changes were made to fabrication processes throughout the thesis, the fabrication dates of devices used are stated, alongside a brief description of the process used at the time. This chapter looks to use the characterisation techniques outlined in the previous chapter to compare and contrast the device channel morphologies and electrical characteristics resulting from the various methods used.

Atomic force microscopy and Raman spectroscopy were performed on the carbon nanotube networks to identify the distribution of carbon nanotube diameters and the extent to which defects were present on the carbon nanotube networks. Electrical characterisation was then used to see how the morphology of each film type affected the performance of the completed devices. Both back-gated and liquid-gated transfer characteristics were compared, and figures of merit from the liquid-gated characteristics were examined. Control measurements were also taken to verify the behaviour of the pristine device as a sensor in both liquid-gated and vapour-phase environments. In the liquid-phase, a salt concentration sensing series was performed with a steam-deposited carbon nanotube network device. The device characteristics were taken and device drift was examined and modelled. The sensing series was performed by successively diluting 1× PBS electrolyte in the polydimethylsiloxane ‘well’ (electrolyte container) while passing a current through the device, and measuring the current response to dilutions. Various filters were applied to the collected data to better understand the signal change. Responses of the device to ethyl hexanoate and *trans*-2-hexanal in a vapour phase environment were measured and compared to those from the off-the-shelf reference sensors of the vapour delivery system.

1.2. Carbon Nanotube Network Morphology and Composition

1.2.1. Atomic Force Microscopy

Figure 1.1 shows a side-by-side comparison of the surface morphology of carbon nanotube films fabricated using the methods described in [?@sec-dep-carbon-nanotubes](#). These images were collected using an atomic force microscope and processed in the manner described in [?@sec-afm-characterisation](#). Figure 1.1a shows a film of carbon nanotubes deposited in solvent, Figure 1.1c shows a film of carbon nanotubes dropcast in surfactant, and Figure 1.1e shows carbon nanotubes dropcast in surfactant in the presence of steam. As discussed in previous works using solvent-based deposition techniques for depositing carbon nanotubes, in each network multi-tube bundles form due to strong mutual attraction between nanotubes [1]–[4]. However, when surfactants are present, they adsorb onto the carbon nanotubes and form a highly repulsive structure able to overcome the strong attraction between nanotubes. This repulsion keeps the individual carbon nanotubes more isolated [5]–[9]. The diameter range provided by the supplier for the individual carbon nanotubes used is 1.2–1.7 nm, while the length range is 0.3–5.0 µm (Nanointegrals).

It has previously been demonstrated that the diameter range of deposited single-walled carbon nanotubes can be modelled via a normal or Gaussian distribution [10]–[12]. However, when the height profiles from the 2.5 µm × 2.5 µm AFM images are directly extracted and binned, as plotted in black in Figure 1.1, the histograms obtained do not follow a normal distribution. One reason for this result is that the carbon nanotubes do not lie perfectly flat on the substrate surface, as the silicon dioxide substrate and the carbon nanotubes each possess some surface roughness. To find the contribution of substrate surface roughness to the height profile histogram corresponding to each network deposition method, silicon dioxide substrates were modified using the same processes as in Figure 1.1 but without carbon nanotubes present in the solutions used. 2.5 µm × 2.5 µm AFM images of the modified surfaces are shown in Figure 1.2.

$$f(x) = \frac{2}{\omega} \phi\left(\frac{x - \xi}{\omega}\right) \Phi\left(\alpha\left(\frac{x - \xi}{\omega}\right)\right) \quad (1.1)$$

In Figure 1.2, it appears that each substrate surface has a roughness that follows a normal distribution with some degree of skewness. Figure 1.2b and Figure 1.2d are negatively skewed distributions. The equation for a skew-normal distribution is given in Equation 1.1, where α is the ‘shape parameter’, ξ is the ‘location parameter’, ω is the ‘scale parameter’, $\phi(x)$ is the standard normal distribution and $\Phi(x)$ is the corresponding cumulative distribution function. α indicates the skewness of the distribution. ξ and ω correspond to the mean and standard deviation of the skew-free normal distribution when α is set equal to zero [13]. The fitted skew-normal distribution in Figure 1.2b

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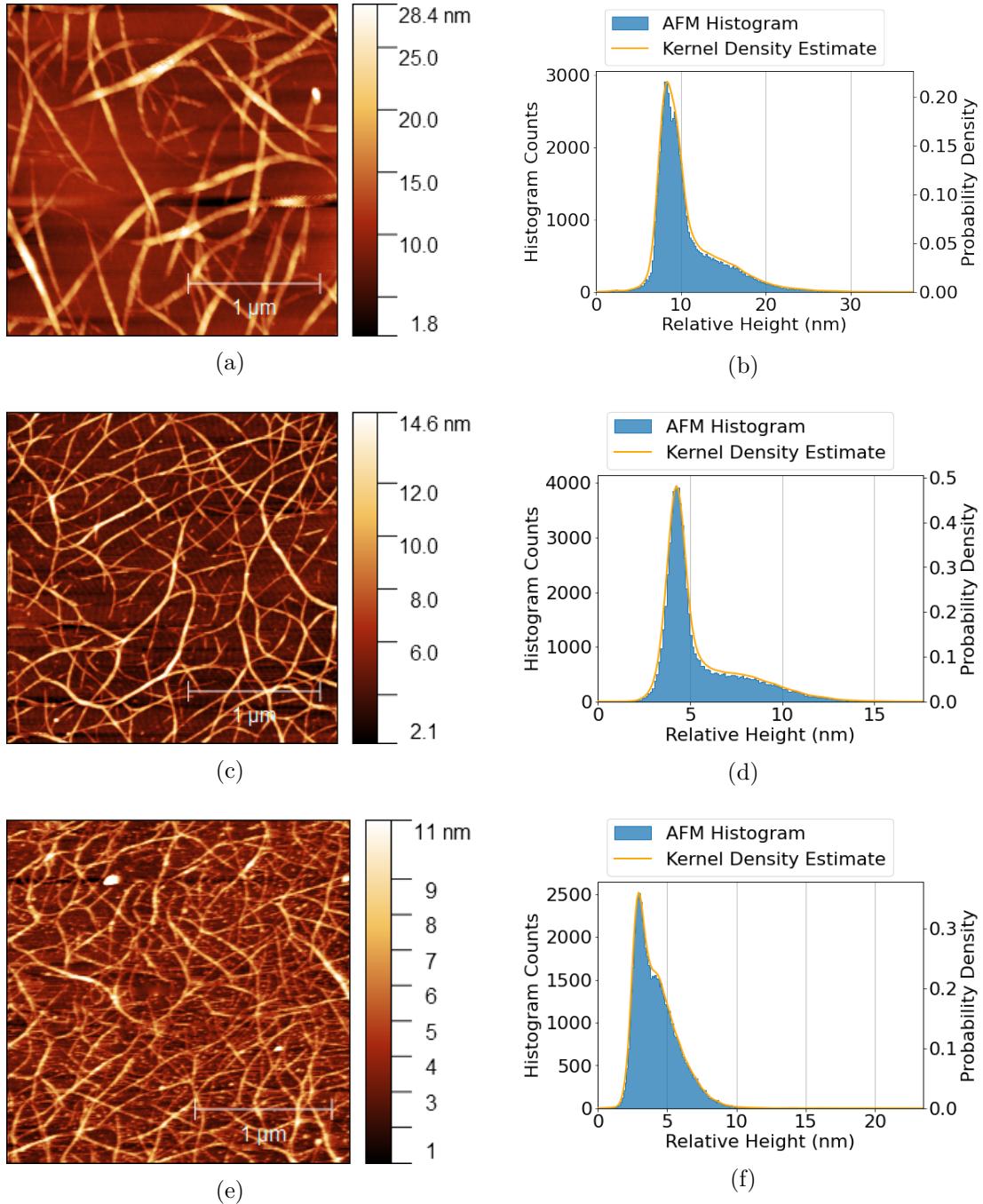


Figure 1.1.: $2.5 \mu\text{m} \times 2.5 \mu\text{m}$ atomic force microscope (AFM) images of carbon nanotube films deposited using various methods, shown side-by-side with histogram height distributions and kernel density estimate (KDE) plots corresponding to each image. The network shown in (a) with height distribution shown in (b) was deposited in solvent, the network shown in (c) with height distribution shown in (d) was dropcast in surfactant, and the network shown in (e) with height distribution shown in (f) was dropcast in surfactant with steam present.

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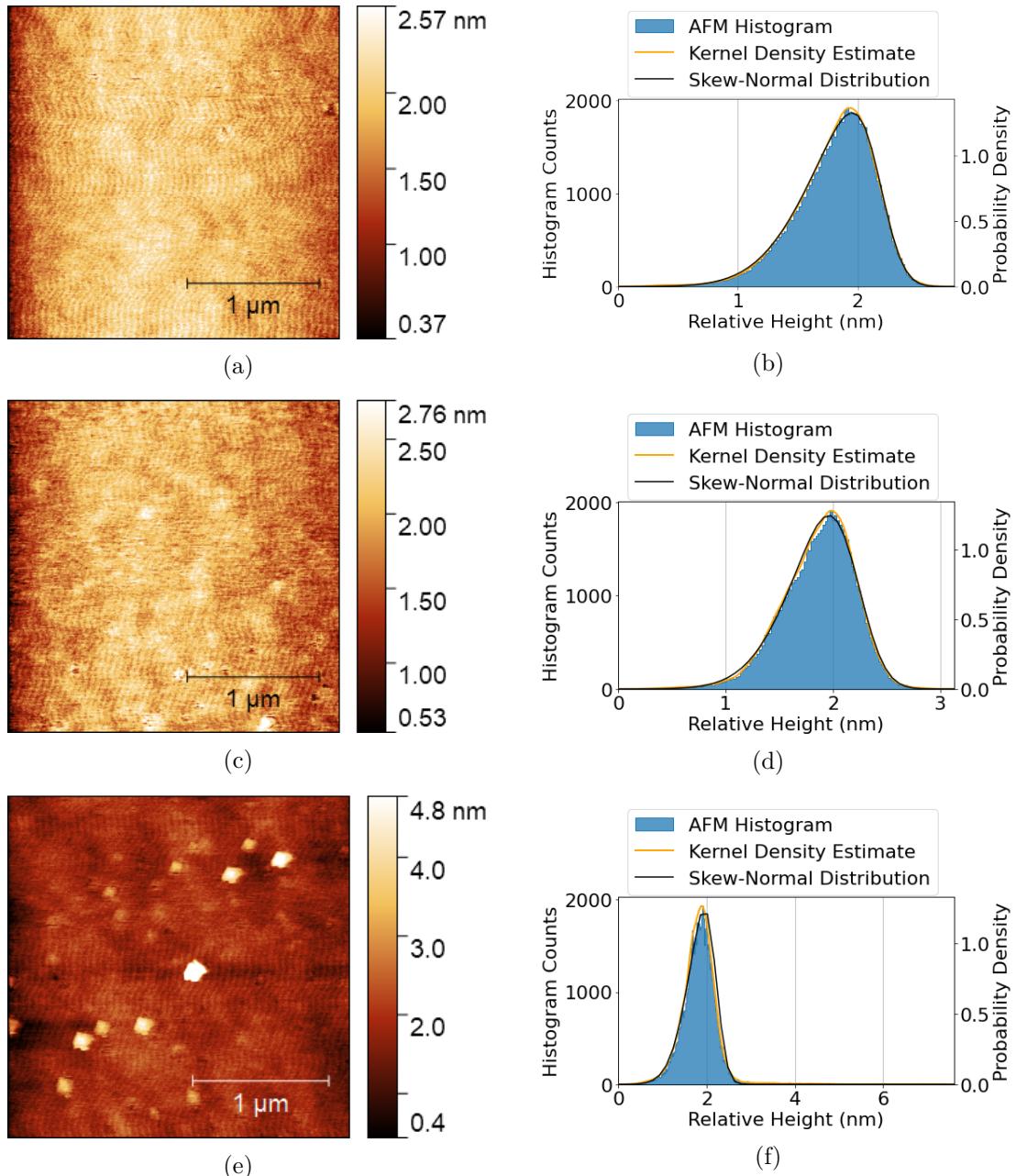


Figure 1.2.: $2.5 \mu\text{m} \times 2.5 \mu\text{m}$ atomic force microscope (AFM) images of silicon dioxide substrates alongside histogram height distributions and KDE plots corresponding to each image. The substrate in (a) and (b) was exposed to solvent, the substrate in (c) and (d) was exposed to surfactant, and the substrate in (e) and (f) was exposed to surfactant with steam present.

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has $\alpha = -3.2$, $\xi = 2.2$ nm and $\omega = 0.5$ nm, while in Figure 1.2d $\alpha = -2.2$, $\xi = 2.2$ nm and $\omega = 0.5$ nm. The close correspondence between ξ and ω for these distributions implies that the skewness is a variable imaging or processing artifact rather than a physical property of the surface. Without distortion, the roughness of a clean SiO₂ surface should follow a normal distribution [14].

Figure 1.2f has a pronounced positive skew with a long tail. The tail appears to result from the contribution of residual surfactant aggregates to surface morphology, observed in Figure 1.2e and recently discussed elsewhere in the literature [12], [15]. Attempting to fit a skew-normal distribution to this histogram fails when all three variables are allowed to vary due to the presence of the tail. Instead, previous values obtained for ξ and ω can be set fixed at ξ and ω at 2.2 nm and 0.5 nm respectively in the fitting process, assuming that these values are characteristic of the imaging process used and not the substrate. In this fitting process, therefore, only α was allowed to change. The resulting fitted distribution is shown in Figure 1.2f, with $\alpha = -2.4$. The distribution closely fits the negative tail of the histogram, but deviates slightly from the positive tail due to the presence of surfactant. This deviation is small and the fit is good quality, with an R-squared value of 0.98. The surfactant contamination identified here could have negative effects on both sensitivity of carbon nanotubes and also could damage the attached biological elements.

Using the morphology analysis technique outlined by Vobornik *et al.* [12], five successive diameter measurements of 30 carbon nanotube bundles were collected using Gwyddion. Measurements were not taken at bundle junctions. A height threshold ‘mask’ was defined in Gwyddion to determine average substrate height, as shown in Figure 1.3a. This background value was subtracted from our diameter measurements to determine the actual bundle height. The mean background heights of the solvent-deposited, surfactant-deposited and steam-assisted surfactant-deposited bundle diameter histograms were 8.8 ± 4.0 nm, 4.2 ± 1.8 nm and 3.3 ± 1.0 nm respectively. An increased maximum feature height leads to an increased mean background height, and by examining the AFM images in Figure 1.1 it appears this may be due to deep artifacts on the surface of the substrate in the vicinity of large features. The average of the five height-adjusted values for each carbon nanotube bundle was then calculated, and these 30 averages were sorted into six equal-sized bins. The binned bundle diameter measurements, alongside estimated probability density, are shown in Figure 1.3.

From Figure 1.3, it is clear that each histogram appears to follow a positively skewed normal distribution, different to the skew-free normal distribution expected from previous works [10]–[12]. The skew is likely another artifact from imaging the network with the atomic force microscope. The force of the atomic force microscope tip is known to cause larger bundles to undergo some degree of compression, and the resulting systematic underestimation of their height may be responsible for the distribution skewness [12]. The fitted skew-normal distribution in Figure 1.3b has $\alpha = 2.7$ (shape; skew), $\xi = 4.3$ nm (location; mean), $\omega = 5.9$ nm (scale; standard deviation), the distribution in Figure 1.3c has $\alpha = 2.4$, $\xi = 2.2$ nm, $\omega = 2.6$ nm, and the distribution in Figure 1.3d has

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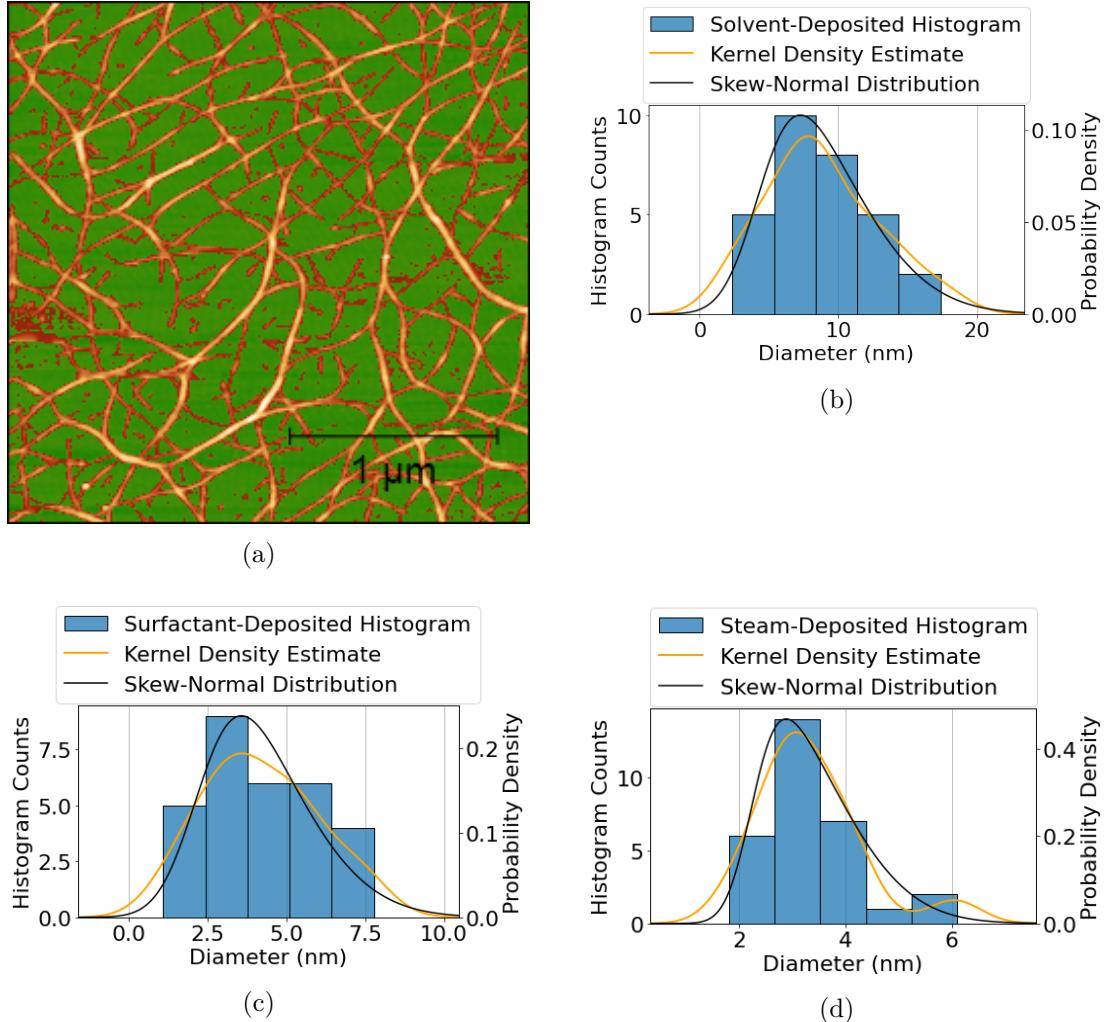


Figure 1.3.: An masked AFM image is shown in (a), where the masked carbon nanotube bundles are shaded blue. The mask sets a height threshold so that masked features are excluded from the height dataset. Histogram height distributions with corresponding KDE plots collected via the morphology analysis method outlined by Vobornik *et al.* [12] are shown in (b)-(d). The substrate in (b) was exposed to solvent, the substrate in (c) was exposed to surfactant, and the substrate in (d) was exposed to surfactant with steam present.

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$\alpha = 3.6$, $\xi = 2.2$ nm and $\omega = 1.5$ nm. The probability density for the carbon nanotube bundle histogram drops to approximately zero at or before 0 nm, which is physically appropriate.

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Warning: package 'kableExtra' was built under R version 4.3.3
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Table 1.1.: The first eight optimised ratios of 2D packed circle diameter to encompassing circle diameter, given to 3 s.f. (encompassing circle diameter = d , number of packed circles = n , approximate packed circle diameter = d_n).

n	2	3	4	5	6	7	8	9
d/d_n	2.00	2.15	2.41	2.70	3.00	3.00	3.30	3.61

Previously, analysis of the morphology of carbon nanotube networks has been simplified by assuming the component nanotubes are cylinders, follow 2D packing and are of equal diameter [2]. Table 1.1 shows the relationship between the diameter of a bundle of 2D packed cylinders and the constituent diameters of up to nine cylinders within that bundle. From looking up the relevant d/d_n packing ratios, and assuming an average carbon nanotube diameter of 1.45 nm, it is possible to use Table 1.1 to find the approximate number of nanotubes n likely to be present in the mean bundle size corresponding to each deposition type [16], [17]. These estimates are shown in Table 1.2. Also shown in Table 1.2 is an estimate of the ratio of single- to multi-tube bundles for each deposition. This estimate was obtained by taking the integral of each distribution with a lower bound of 2.9 nm, the minimum multi-tube bundle size for 1.45 nm diameter nanotubes. As the area under the curve represents the probability a bundle will have a particular diameter, this integral should give a good estimate of the relative proportion of multi-tube bundles. Table 1.2 should be interpreted as lower-limit estimates of the size and relative proportion of bundles, recalling that the distribution skewness indicates underestimation of the true bundle height.

Table 1.2.: The mean of histogram distributions for carbon nanotube films deposited using various methods, alongside estimates for the number of nanotubes present per mean bundle and the estimated proportion of multi-tubed bundles present across the network.

	Mean Bundle Diameter (nm)	Tubes per Average Bundle	% Multi-Tube Bundles
Solvent deposited	8.8 ± 4.0	28	> 96%
Surfactant deposited	4.2 ± 1.8	5	> 75%

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Surfactant deposited with steam	3.3 ± 1.0	3	> 65%
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Both the carbon nanotube bundle diameter mean and standard deviation are small for surfactant-deposited films when compared to the mean and standard deviation of solvent-deposited films. However, despite the presence of surfactant, it is apparent both from Figure 1.1 and Table 1.2 that not all surfactant-dispersed carbon nanotubes are deposited individually. Bundling may occur during the process of deposition onto the substrate, which could disrupt the repulsive forces from the surfactant coating and allow attractive forces to temporarily dominate. It is possible that the bundling of surfactant-dispersed carbon nanotubes is a consequence of dynamics introduced by the coffee-ring effect [18], [19]. The coffee-ring effect refers to a build-up of dispersed solid forming around the edges of a dispersion evaporating on a surface. This process occurs due to the dispersion edges being fixed by surface forces, leading to capillary flow outwards to replace liquid evaporating at the edges, bringing solid material along with it. The presence of vapour is known to disrupt this capillary effect [20], which may explain why mean bundle diameter is lower for the films deposited in surfactant with steam present relative to films deposited in surfactant without steam.

The discussion in this section gives us a new understanding of the histograms shown in Figure 1.1. It is now apparent that these histograms are linear combinations of skewed normal distributions. These distributions include a negatively-skewed distribution corresponding to the substrate surface and a positively-skewed distribution corresponding to the carbon nanotube bundles. X and Y junctions between overlapping nanotubes may also form a similarly skewed normal distribution as part of the full histogram [2]. The complete linear combination could be modelled mathematically in order to rapidly extract key parameters from atomic force microscope images [21], but implementing this approach is outside of the scope of this thesis. Another outcome of this discussion is awareness that carbon nanotube bundling within a network is lowered by the presence of surfactant during deposition. Introducing steam when depositing with surfactant lowers bundling even further, but also leads to residual surfactant pooling and attaching to the substrate surface. These results may both be explained by the presence of steam enabling surfactant to follow carbon nanotubes to the substrate surface, which keeps them from bundling during the attachment process. The unwanted persistence of surfactant means that higher temperature vacuum annealing may be required for robust biosensors [22].

1.2.2. Raman Spectroscopy

Raman spectroscopy was also used to analyse and compare the deposited carbon nanotube networks. Raman spectra were collected from a solvent-deposited carbon nanotube film and a steam-assisted surfactant-deposited film, both on silicon dioxide, in the manner described in ?@sec-raman-characterisation. These spectra were then

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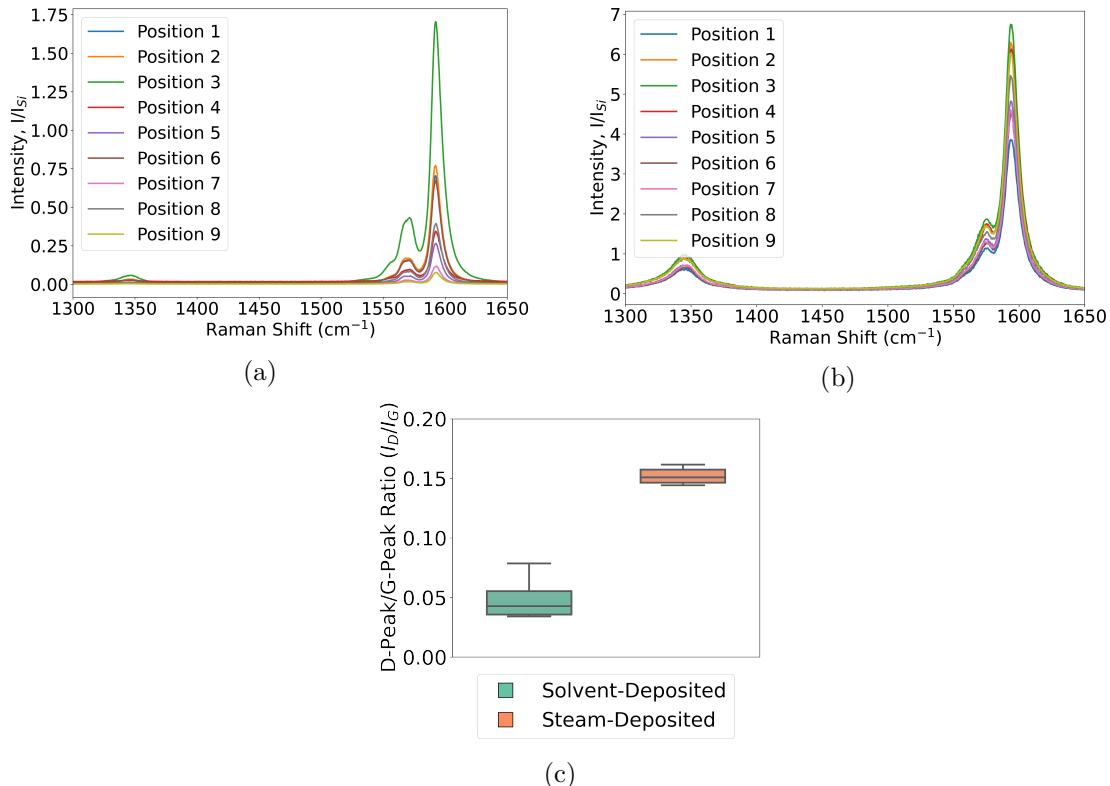


Figure 1.4.: A series of nine Raman spectra at different locations across a $40 \mu\text{m} \times 100 \mu\text{m}$ carbon nanotube film region, where (a) shows spectra from a film deposited using solvent while (b) shows spectra from a film deposited with surfactant in the presence of steam. (c) shows the spread of the D-peak/G⁺-peak spectral ratios corresponding to each film.

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processed using the Python script mentioned in Section B.3. For each location, spectra over two wavenumber ranges were collected. A peak corresponding to the silicon dioxide substrate, found in the range between 100 cm^{-1} and 650 cm^{-1} , was used as a reference peak for the normalisation of intensity across the wavenumber range between 1300 cm^{-1} and 1650 cm^{-1} . These normalised spectra are shown in Figure 1.4. In all spectra, a D-band comprising a single D-peak is observed at $\sim 1320\text{ cm}^{-1}$, and a G-band comprising two G-peaks, G^- and G^+ , is observed between $\sim 1525\text{ cm}^{-1}$ and $\sim 1650\text{ cm}^{-1}$. These features are characteristic of networks of semiconducting carbon nanotubes [23], [24].

Closer inspection of the D peak and G peaks can give us important information about network composition. G^- is a minor peak found at $\sim 1570\text{ cm}^{-1}$, while G^+ is a larger feature at $\sim 1590\text{ cm}^{-1}$. The G^+ feature describes the in-plane vibration of carbon bonds along the length of the carbon nanotubes, while the G^- feature describes the in-plane vibration of bonds about the nanotube circumference [24], [25]. The splitting between the wavenumber location of the G^- and G^+ local maxima is lower in Figure 1.4b than in Figure 1.4a, indicating more metallic nanotubes are present in the surfactant-deposited network [25]. The D-peak gives an indication of the defects present in the carbon nanotube atomic structure [24], [25]. The size of the normalised D-peak appears much lower in Figure 1.4a than in Figure 1.4b, indicating the solvent deposition process introduces less defects to the carbon nanotubes than surfactant-mediated deposition.

It is also possible to compare the relative magnitude of the D-peak and G^+ -peak intensity to quantify carbon nanotube structural disorder, which disrupts in-plane lattice vibration [23], [24]. Figure 1.4c gives a summary of the ratios between the D-peak and G^+ -peak across all nine positions for the solvent-deposited and surfactant-deposited film. It is immediately observed that I_D/I_G is significantly larger for the steam-assisted, surfactant-deposited films than for the solvent-deposited films. This is a further indication of the presence of defects across the steam-deposited network. These defects are likely introduced through the introduction of charge impurities by surfactant aggregates present around the carbon nanotubes [15]. However, at the same time, the range of values for the I_D/I_G ratio is lower for the steam-deposited network. This spatially homogeneous vibrational behaviour implies the steam-deposited network is more evenly distributed than the solvent-deposited network, which matches the discussion in Section 1.2.

1.3. Electrical Characteristics of Pristine Devices

1.3.1. Python Analysis

Analysis of electrical measurements was performed using the three modules described in Section B.4. The first of the three modules is for processing sensing datasets. This module cleans, analyses and filters sensing data and produces a variety of plots. These plots include normalised plots (type of normalisation can be set in the code config file), plots with fitted curves, plots with the linear baseline drift removed, plots of signal with

1.3. Electrical Characteristics of Pristine Devices

analyte addition, “despiked” plots and “filtered” plots. The analysis used to produce these plots is described further below. It is possible to add annotations to any of these plots using the config file, and it is possible to produce a plot with a combination of these modifications. The module can also fit exponential and linear trendlines to regions of the sensing data, and find the signal change per analyte addition; the module then returns spreadsheets containing the results of these analyses, including the standard deviation for all calculated parameters.

The `scipy.optimize.curve_fit` function is used in the first module to fit linear and exponential curves to regions of interest of the sensing data. For a linear fit $c_1 t + c_2$, initial parameters are simply set as $c_1 = 1$ and $c_2 = 0$. For an exponential fit $I_0 \exp(-t/\tau) + I_C$, rough approximations are used for the initial parameters: I_C is set as the final current measurement of the region of interest, I_0 is set as the initial current measurement minus I_C , and τ is set as the time where current has dropped to $e^{-1}I_0 + I_C$.

“Despiked” plots have had spurious datapoints removed through the use of an interquartile range rolling filter. The window size of the rolling filter used was 40 datapoints, and datapoints in each window with a z-score above ± 3 were removed from the plotted/processed data. “Filtered” plots had noise reduced using a moving median filter. The moving median filter is more effective at removing noise than a simple moving average, and has advantages over other filters (such as the Savitzky-Golay filter) when removing noise from data with sharp edges, as is the case for sensing data. Median filtering can also be used for baseline drift compensation, though this approach was not used in this thesis [26]. The moving median filter used had a window of 40 datapoints.

Plots of signal with analyte addition were constructed from current data after first removing baseline drift and applying a moving median filter. A simple difference calculation between the mean of the filtered current before an addition and the mean of the filtered current after the addition was performed at each addition. These differences were then normalised relative to the initial current. The signal with analyte addition give reasonably consistent results regardless of whether baseline drift was removed from the data, as shown in Figure 1.5. We can therefore be confident that robust signal with analyte addition plots are robust even in the presence of significant drift.

The second module creates combined and individual plots of transfer data collected from eight channels on a single device. In combined plots, channels which are non-working, due to being shorted or non-conducting, are removed via setting a maximum and minimum possible on-current in the config file. Various parameters from the transfer characteristics are saved as a spreadsheet along with standard error. These parameters include on current, off current, subthreshold slope and threshold voltage for the carbon nanotube devices, and on current, off current and major Dirac point voltage for graphene devices. The device type being analysed can be set in the config file.

The third module allows for comparison of transfer measurements taken of the same channel before and after some modification. It also calculates the shift in either threshold voltage or major Dirac voltage of the device.

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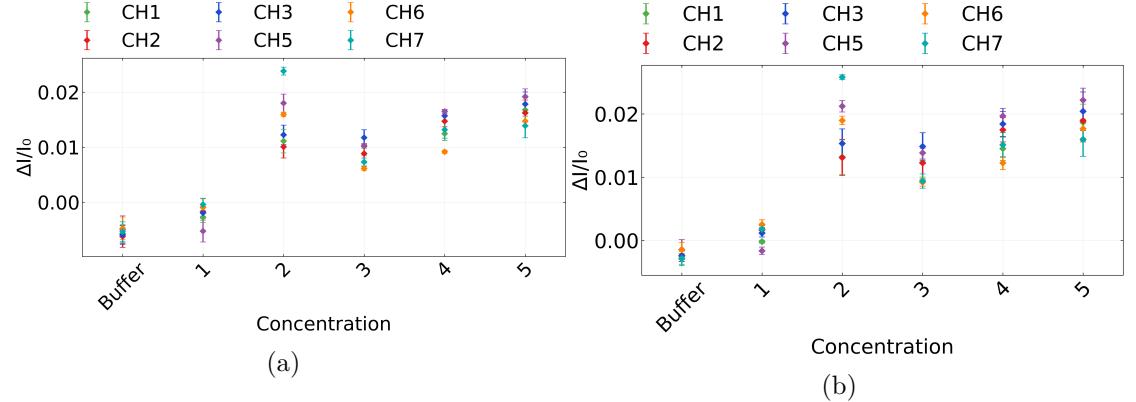


Figure 1.5.: A comparison of signal with analyte addition plots taken from the same salt concentration sensing dataset (the same dataset as used in Figure 1.11). In (a), a simple difference calculation performed on filtered data was used, while in (b) the same calculation was performed on filtered data with the baseline drift removed, the method used in the body of the thesis.

1.3.2. Graphene Devices

Graphene field-effect transistor devices were electrically characterised in the manner described in [?@sec-electrical-characterisation](#) and analysed using the Python code discussed in Section B.4.

Figure 1.6 shows the liquid-gated transfer characteristics of two graphene devices. These devices were fabricated prior to Jun 2021. Both devices exhibit the ambipolar characteristics typical of liquid-gated graphene devices [27]–[30]. As with the carbon nanotube network devices, leakage current remained below $\sim 1 \times 10^{-7}$ V across both the forward and reverse sweep. Hysteresis between the forward and reverse sweep is caused by trapping of charge within and on the surface of the SiO_2 dielectric [31]. The major Dirac point for these devices is slightly to the right of $V_{\text{Dirac}} \approx 0$ V, which indicates *p*-doping of the channel. This slight *p*-doping is a result of adsorption of oxygen and water from the air from residual resist from photolithography [30], [32], [33]. Some devices exhibited double Dirac behaviour. Here, the global minimum of the transfer characteristic is referred to as the ‘major’ Dirac point while the second Dirac point is referred to as the ‘minor’ Dirac point.

Figure 1.6 also shows the effect of $1\times$ PBS on the graphene channels. The channels were measured on exposure to $1\times$ PBS, after exposure to $1\times$ PBS for one hour, and after the device surface was rinsed and $1\times$ PBS was replaced in the well one time, two times and three times successively. A slight negative shift of the major Dirac point was observed. This effect is possibly a result of gate bias stress, where successive transfer sweeps introduce charge traps to the graphene layer and alters the current level at a given gate voltage [34], [35]. Alternatively, Kireev *et al.* found that a series of liquid-gated

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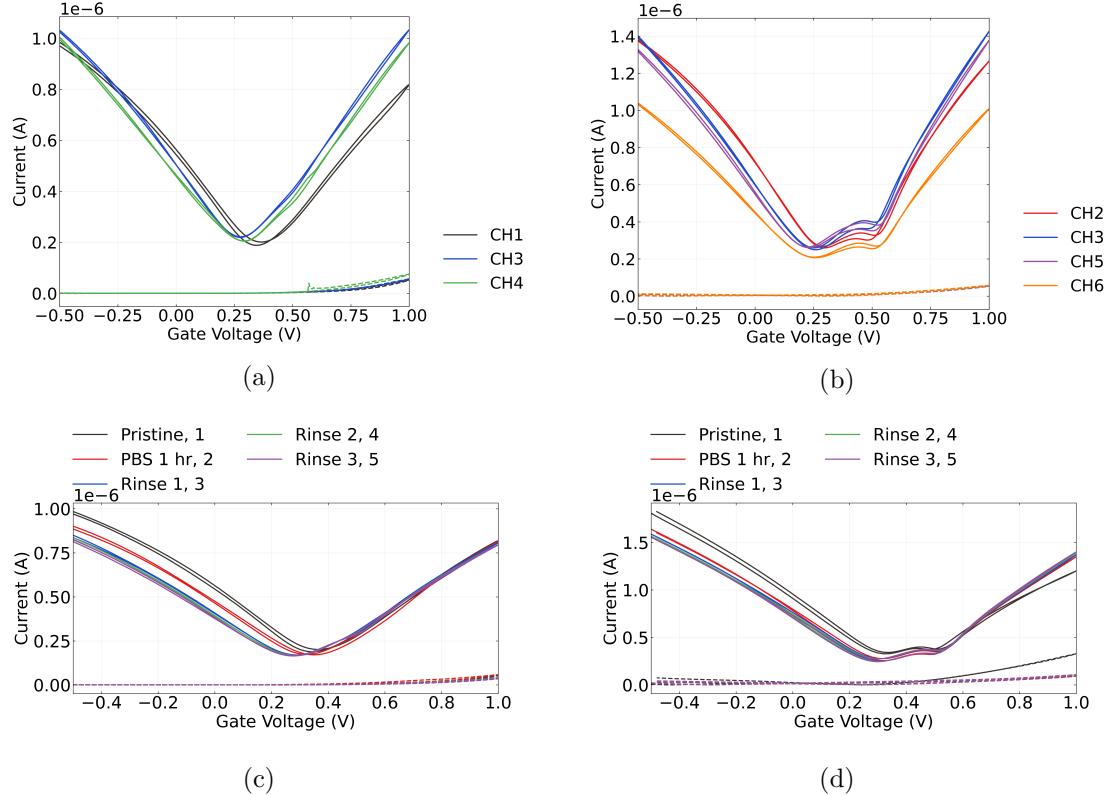


Figure 1.6.: These figures show liquid-gated transfer characteristics of channels from two AZ® 1518 encapsulated graphene devices. The characteristics of working device channels upon initial exposure to 1× PBS are shown in (a) and (b). The transfer characteristics of channel 1 in (a) and channel 5 in (b) after various degrees of exposure to 1× PBS are shown in (c) and (d) respectively, with each transfer sweep numbered in the order the sweeps were taken. The dashed lines correspond to measurements of gate leakage current.

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sweeps also reduced the size of the second Dirac point [30]. The mechanism behind this change may be the emptying of interfacial charge traps as a result of the transfer sweep. The emptying of traps can bring the Dirac points of the contact and channel region closer together, increasing the consistency of the Fermi level across the channel [30], [31], [36]. If the contaminants removed are *p*-dopants, which could be due to adsorbed oxygen or resist residues, this interpretation would also explain the negative shift of the major Dirac point.

Table 1.3.: Average on-off ratio and major Dirac point voltage for AZ® 1518 encapsulated liquid-gated graphene transistor channels at various stages of exposure to 1X PBS. Electrical characteristics were taken of 6 channels total, three channels from each of two devices.

	1XPBS: Initial	1XPBS: After 1 hr	1XPBS: Rinse
On-Off Ratio (arb.)	5.1 ± 0.3	5.0 ± 0.7	5.0 ± 0.6
Dirac Point Voltage (V)	0.28 ± 0.04	0.31 ± 0.03	0.28 ± 0.02

Table 1.3 shows the on-off ratio and major Dirac point voltage of the graphene devices. Apart from the previously-mentioned slight negative shift of the major Dirac point, these values were highly consistent before and after exposure to 1× PBS.

1.3.3. Carbon Nanotube Network Devices

Each carbon nanotube device fabricated was electrically characterised as described in [?@sec-electrical-characterisation](#), and electrical data was analysed using the Python code discussed in Section B.4. Devices with a 100 nm or 300 nm SiO₂ layer were used for liquid gated measurements, and devices with a 100 nm SiO₂ layer were used for backgated measurements. Figure 1.7 displays multi-channel measurements of representative devices fabricated as described in [?@sec-fabrication](#). To ensure a consistent comparison, each device here was encapsulated with AZ® 1518 encapsulation before measurements were taken. The channels which did not exhibit reliable transistor characteristics are not shown. These ‘non-working’ channels were either shorted, due to metal remaining on the channel after lift-off, or were very low current, due to a very sparse carbon nanotube network. Devices shown here with a solvent-deposited carbon nanotube network were fabricated prior to Jan 2022; devices with a surfactant-deposited network without steam present were fabricated prior to Jun 2021; devices with a surfactant-deposited network without steam were fabricated prior to Sep 2022.

Liquid-Gated CNTFETs

The liquid-gated devices in Figure 1.7a, Figure 1.7c and Figure 1.7e each exhibited ambipolar characteristics, commonly observed in liquid-gated carbon nanotube network

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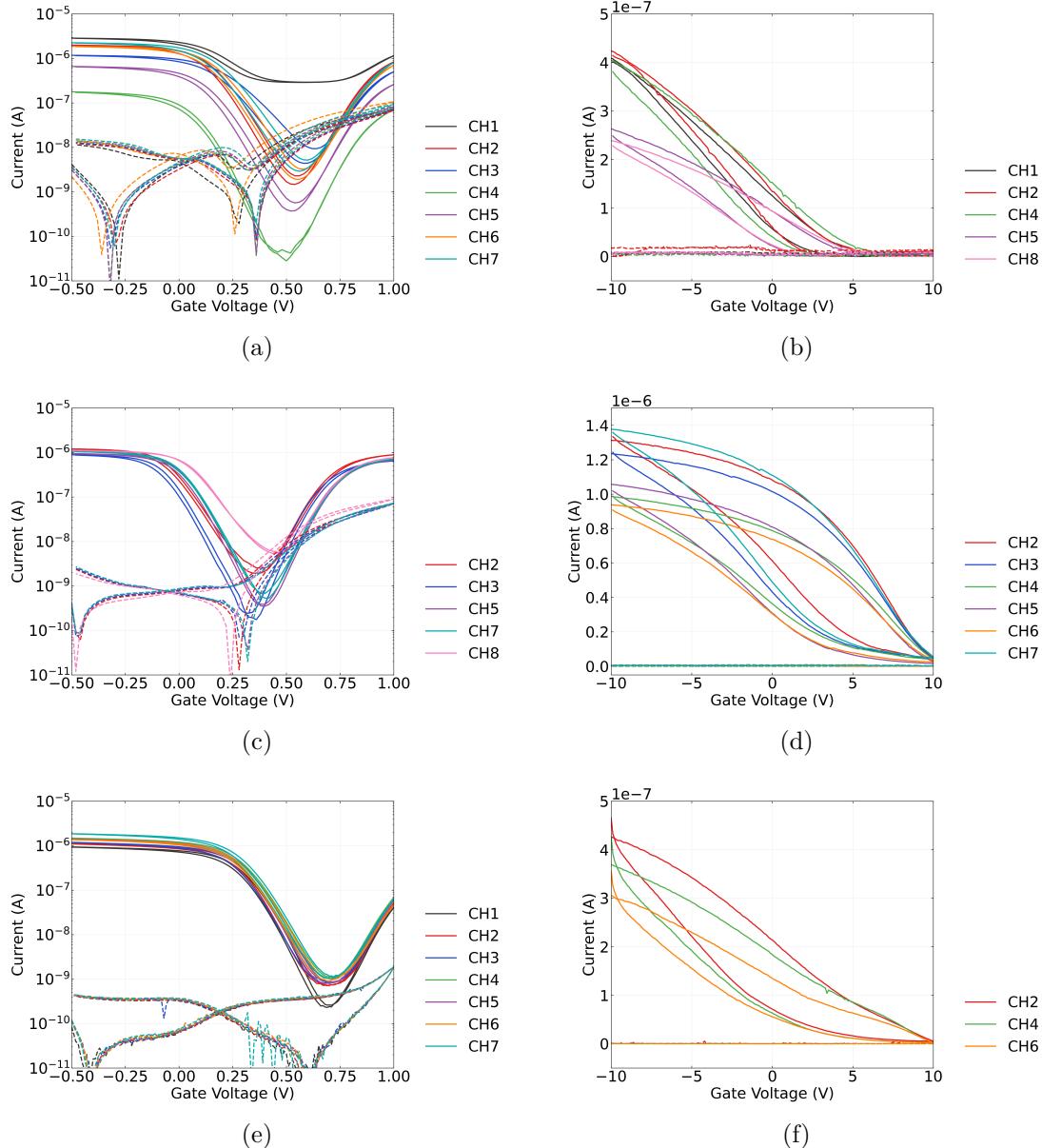


Figure 1.7.: Liquid-gated (left) and back-gated (right) transfer characteristics of AZ® 1518 encapsulated field-effect transistors, where the film was deposited with solvent in (a) and (b), deposited with surfactant in (c) and (d), and deposited with surfactant in the presence of steam in (e) and (f). A step size of 100 mV was used for the backgated sweeps in (a), (c) and (e), while a step size of 20 mV was used for the liquid-gated sweeps in (b), (d) and (f). Gate current (leakage current) is shown with a dashed line. The source-drain voltage used for all sweeps was $V_{ds} = 100\text{mV}$, and 1× PBS was used as the buffer for the liquid-gated measurements here.

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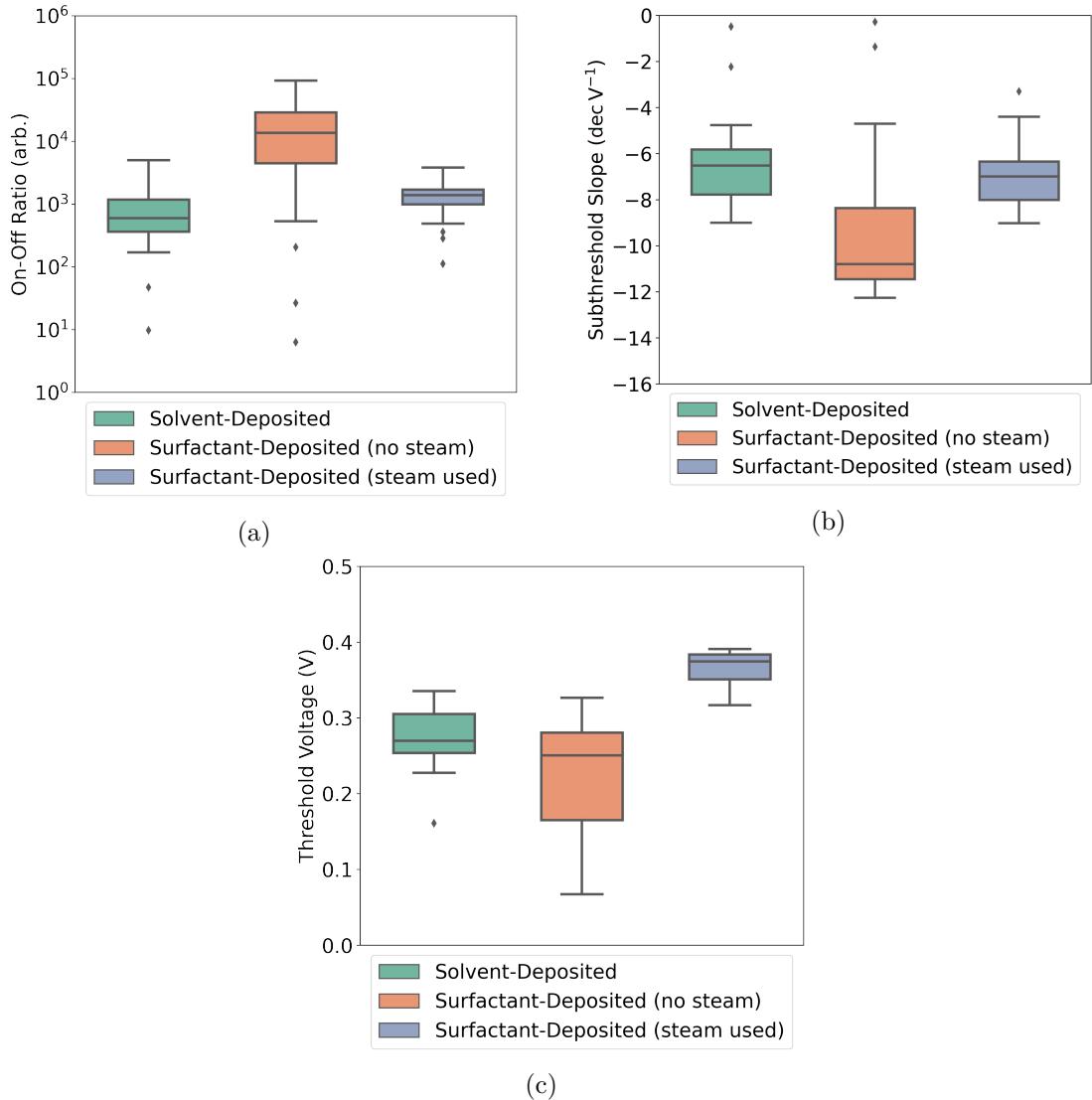


Figure 1.8.: These boxplots illustrate the statistical distribution of (a) the on-off ratio, (b) the subthreshold slope, and (c) the threshold voltage of AZ® 1518 encapsulated liquid-gated transistor channels corresponding to each type of carbon nanotube film deposition. For each deposition type, electrical characteristics were taken of 21 channels of at least three separate devices. The boxes indicate the 25th and 75th percentile of the distribution.

1.3. Electrical Characteristics of Pristine Devices

FETs [2], [37]–[41]. When devices were appropriately configured, leakage current (shown by the dashed traces) did not exceed $\sim 1 \times 10^{-7}$ V across the forward and reverse sweep. The devices shown which used steam-deposited carbon nanotube films showed the least hysteresis. Section 1.2.1 demonstrates that the mean diameter of the bundles in these films is about 0.9 nm less than the mean bundles in films deposited without steam present, and 5.5 nm less than those in films deposited in solvent. Hysteresis is known to scale roughly linearly with bundle diameter, due to trapped charge increasing as bundle density of states is increased [42]. Steam-deposited devices also showed significantly less channel-to-channel variation in electrical characteristics more generally. Channel 1 in Figure 1.7a has a much higher off-current than the other channels of the same device, which appears to be due to a uncommonly high proportion of metallic carbon nanotubes present in the network conduction pathways of this channel [43]–[45].

A summary of key parameters of pristine liquid-gated devices is shown in Figure 1.8. The full dataset consists of three sets of 21 liquid-gated transfer characteristics of working channels, with each set corresponding to the use of a particular method of carbon nanotube network deposition in the device fabrication. Measurements from at least three devices are included in each set. Each entry in the summary corresponds to the average of the specific parameter in the forward and reverse sweep direction. When steam was used for surfactant deposition of films, the resulting devices showed highly consistent channel-to-channel electrical properties. Since the carbon nanotube films on these devices are relatively dense, as seen in Figure 1.1e, the network should be well above the percolation threshold. As many carbon nanotube pathways connect across the channel in parallel, small variations in the network morphology have less of an impact on the overall channel behaviour [2]. Figure 1.3 and Table 1.2 indicate that the range of bundle sizes is relatively low in the steam-deposited films used in these devices, meaning the electrical behaviour of dominant conduction pathways is more spatially consistent. The repeatable subthreshold regime behaviour between channels seen for steam-deposited devices is a desirable attribute for reliable real-time multiplexed biosensing [37], [38], [46].

Channels from surfactant-deposited film devices usually showed a larger on-off ratio and subthreshold slope than those from solvent-deposited devices. Decreasing the ratio of gate-sensitive semiconducting carbon nanotubes to metallic nanotubes tends to decrease the on-off ratio [2], [10], [43], [45]. Section 1.2.2 seems to indicate there are more metallic nanotubes present in the surfactant-deposited films than in the solvent-deposited films. However, percolating conduction pathways dominate device behaviour and nanotube pathways across the channel with a lower degree of bundling are less likely to contain metallic tubes [2]. Therefore, the larger on-off ratio for surfactant-deposited film devices is likely a result of their reduced nanotube bundle size and reduced bundle size variation relative to other films, as discussed in Section 1.2. The larger subthreshold slope is likely due to increased mobility from a denser nanotube network in surfactant-deposited films [43], as seen in Figure 1.1e. A larger on-off ratio and subthreshold slope results in a larger change in conductance in response to changes in the transfer characteristic curve.

1. Characteristics of Pristine Carbon Nanotube & Graphene Field Effect Transistors

Therefore, the larger on-off ratio and subthreshold slope of steam-deposited devices is desirable for improved sensor performance [37], [38], [46].

All channels characterised had a positive threshold voltage (V_{th}). The threshold voltage was largest and most consistent for steam-assisted surfactant-deposited films. The relatively high values of V_{th} which correspond to channel measurements from steam-assisted surfactant-deposited devices indicates increased *p*-doping of the network relative to networks deposited via alternative processes [2], [47], [48]. As seen from Figure 1.2e-f and Figure 1.4c, the steam deposition process leads to the presence of significant, persistent surfactant aggregates. It has been previously established that residual surfactant can *p*-dope carbon nanotubes, alongside enhancing *p*-doping from adsorbed oxygen and water [15], [22], [49]. The presence of residual surfactant may also explain the lowered subthreshold slope, and therefore mobility, of the steam-deposited devices relative to devices with films deposited in surfactant without steam. The analysis by Kane *et al.* shows that the thermal annealing at 150°C used in this work to remove residual surfactant is likely inadequate for this purpose. Oxidation of devices and vacuum annealling at high temperatures (> 600°C) may be required for effective desorption of the persistent surfactant [22], [50]. Devices using films made using the alternative two methods have the advantage of not requiring careful treatment to remove surfactant.

Back-Gated CNTFETs

When characterising devices using the vapour delivery system chip carrier, the setup arrangement meant all measurements were taken using a backgate. Figure 1.7b, Figure 1.7d and Figure 1.7f show that backgated devices exhibit *p*-type transistor behaviour. Gate current leakage was negligible, as shown by the dashed line staying close to zero across the sweep. Significant hysteresis was observed. The hysteresis can be explained by the presence of defects or charge traps within and on the surface of the silicon dioxide and at interfaces between the silicon dioxide and carbon nanotubes [51]–[53]. The hysteresis observed was much greater than for the corresponding liquid-gated sweeps on the right. The devices fabricated with a solvent-based deposition were switched off at a lower voltage than the devices which used surfactant during deposition.

Transfer measurements were taken to determine whether backgated measurements could be taken of an unencapsulated device in the vapour sensor chamber with 1× PBS covering the channels. The use of a backgated configuration with channels in a liquid environment is generally considered less than ideal, since the sensitivity of the device is greatly reduced [54]. Figure 1.9 shows the behaviour of an unencapsulated backgated device with a 300 nm SiO₂ layer before and after being covered by 50 µL of 1× PBS (phosphate buffered saline). The on-off ratio and hysteresis of the channels increase significantly. The presence of water increases hysteresis through introducing charge traps at the silicon dioxide surface around the carbon nanotubes and at the surface of the nanotubes themselves [51], [53], [55], [56]. There is also a significant increase in current leakage to the backgate for larger applied voltages, despite the electrolyte having no

1.4. Aqueous Sensing of Phosphate Buffered Saline Concentration

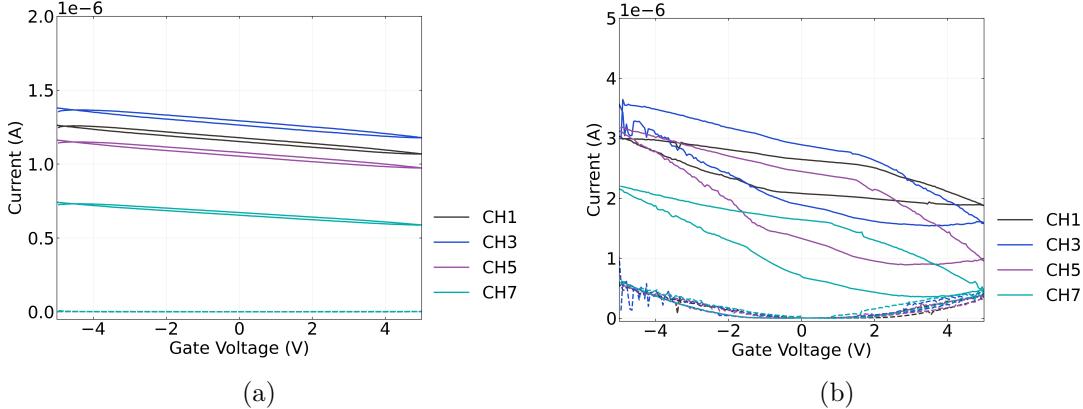


Figure 1.9.: Backgated transfer sweeps were taken of a single unencapsulated device with a 300 nm SiO_2 layer and steam assisted surfactant-deposited carbon nanotube network channels before and after being covered in 50 μL 1 \times PBS electrolyte.

visible physical contact with the silicon backgate or copper plane. This leakage current may simply be due to an increase in relative humidity around the device due to the presence of water [57].

1.4. Aqueous Sensing of Phosphate Buffered Saline Concentration

1.4.1. Control Series and Baseline Drift

Table 1.4.: The threshold voltages V_{th} of each working channel of a steam-deposited device, and the difference between each V_{th} and the mean device threshold voltage $V_{th,mean}$.

Channels	CH1	CH2	CH3	CH5	CH6	CH7
Threshold voltage (mV)	160	150	130	140	180	140
Relative to mean (mV)	10	0	-20	-10	30	-10

To verify the sensitivity of the fabricated field-effect transistors and therefore verify their suitability for sensing, control measurements replicating a typical sensing experiment were taken before functionalising the channels of a carbon nanotube network device. The first step to verifying device suitability was ensuring the device showed no response to 1 \times PBS. This sequence is referred to in this thesis as the ‘PBS control series’. The

1. Characteristics of Pristine Carbon Nanotube & Graphene Field Effect Transistors

PDMS well contained 80 μL 1 \times PBS at 0 s. The PBS control series ran over the first 1800 s, with 20 μL phosphate buffer saline (1 \times PBS) additions at 100 s, 200 s and 300 s, and 20 μL subtractions at 400 s, 500 s and 600 s. The device was left untouched over the next 1200 s to allow the current level to settle. The gate voltage was held at $V_g = 0$ V.

Figure 1.10a shows the transfer sweeps of the six working channels of a steam-assisted surfactant-deposited carbon nanotube field-effect transistor measured using the NI PXIe. The device was fabricated on a substrate with a 300 nm SiO₂ layer, the carbon nanotube film was deposited using the steam-assisted surfactant method and encapsulated with AZ® 1518 before measurement. The central feature in the transfer characteristics of channels 1 and 7 are absolute-value measurements of negative current. These are unphysical measurements due to equipment error, and can be considered as regions where zero current passes through the channel. The threshold voltages of the channels are shown in Table 1.4. Table 1.4 also shows the difference between the threshold voltage of each channel and the mean threshold voltage of the device. The mean threshold voltage was $V_{th} = 150 \pm 20$ mV. As discussed previously, the electrical characteristics are highly consistent between the channels due to the film deposition method used.

Figure 1.10b shows the PBS control series corresponding to each device channel alongside gate current. In both series, there is no clear stepwise response to any addition or subtraction of 1 \times PBS. Gate leakage current remains negligible across the entire control series, with no change in response to 1 \times PBS additions. The current has a period of short-term decay followed by much longer term baseline drift, similar to observations by Lin *et al.* and more recently Noyce *et al.* for parallel arrangements of single carbon nanotubes in air or vacuum [35], [58]. This effect results from changes in the occupancy of charge traps in and around the substrate and carbon nanotubes. The magnitude of baseline drift is lower for our devices than for those characterised by Noyce *et al.*, which may be a result of numerous device and setup differences which affect the presence of charge traps. These differences include liquid-gating instead of back-gating, the use of a network of carbon nanotubes instead of single nanotubes, a different channel length, the use of a 300 nm instead of 90 nm SiO₂ layer, a gate voltage of 0.0 V instead of -15.0 V, and the use of an asymmetric, liquid-gated transfer sweep over a shorter voltage range to characterise devices before each control series was measured [35].

Table 1.5.: The coefficients of linear fits to the PBS control series of each channel between 1200 – 1800 s, where c_1 is the gradient and c_2 is the constant term.

Channels	CH1	CH2	CH3	CH5	CH6	CH7
c_1 (pA/s)	-5.1±0.2	-7.2±0.1	-6.5±0.1	-5.0±0.1	-7.6±0.1	-5.1±0.2
c_2 (μA)	0.316	0.316	0.308	0.218	0.364	0.332

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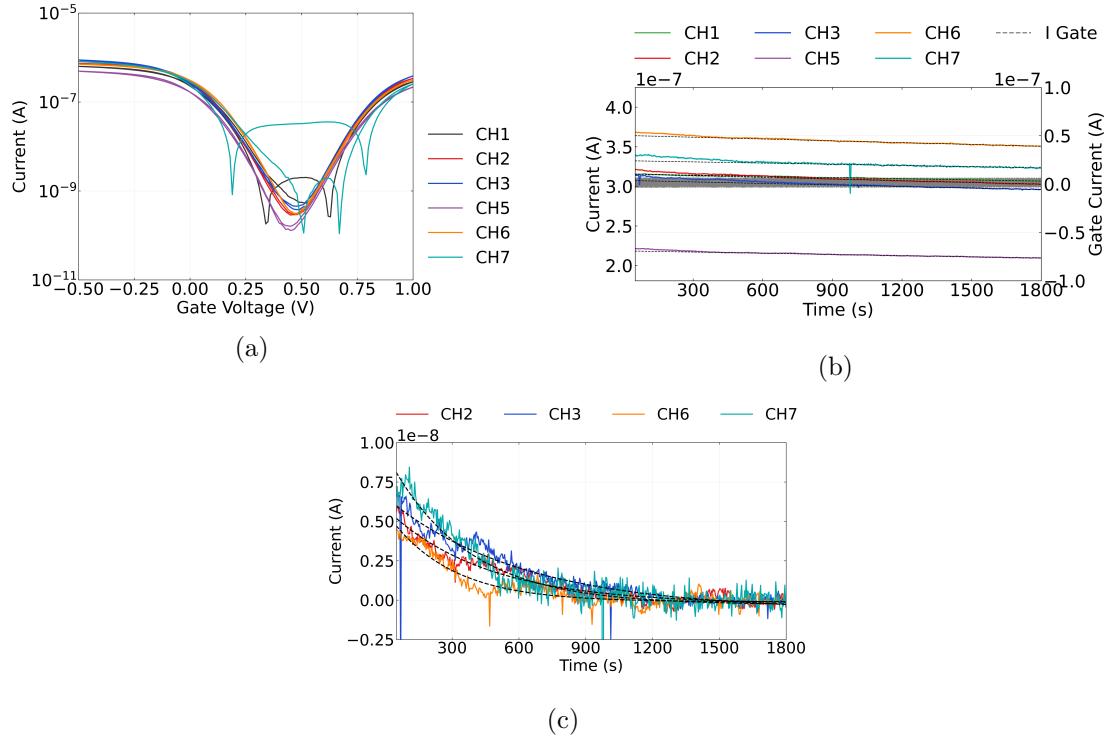


Figure 1.10.: The transfer characteristics in (a) were taken of the steam-deposited carbon nanotube field-effect transistor used here for an example of salt concentration sensing. The absolute values of measurements are shown, so that negative values resulting from measurement error can be visualised. Linear fits to the PBS control series from each channel from 1200 s onwards are shown in (b), while exponential fits to the PBS control series from 0 – 1200 with the linear fit subtracted are shown in (c). No significant response to PBS additions are seen at any of the addition times from 100 – 600 s.

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Table 1.6.: The coefficients of exponential fits to the PBS control series of each channel between 0 – 1200 s, after the linear fit has been subtracted, where I_0 is the gradient and τ is the time constant.

Channels	CH2	CH3	CH6	CH7
I_0 (nA)	6.07 ± 0.08	7.19 ± 0.11	5.75 ± 0.12	9.68 ± 0.41
τ (s)	450 ± 10	610 ± 30	280 ± 10	350 ± 30

As a first-order approximation to the longer time constant exponentials discussed by Noyce *et al.* [35], linear fits were performed on each PBS control series from 1200 – 1800 s. These fits are tangent to the curve of the sum of the larger time constant exponentials, and are a close approximation to this curve when higher order terms in the series expansion are approximately zero. This is only the case when $t \ll \tau_i$, where the time interval of interest t is much shorter than the time constants of the larger time constant exponentials, τ_i . These linear fits are shown by the dashed yellow lines in Figure 1.10b. The parameters from each fit in Figure 1.10b are shown in Table 1.5, where $I = c_1 t + c_2$. The fits for channels 1, 5 and 7 are all in parallel within error. The gradient value for each fit in Figure 1.10b is consistent within a 2.6 pA/s range across all channels. The current data from channel 1 is closely approximated by the linear across the entire control series. No short-term decay is present for this channel, indicating the channel has low net trapped charge. It is unclear why this short-term exponential decay behaviour is only absent for channel 1.

The long-term linear fits were next subtracted from the raw control series data. Figure 1.10c shows exponential fits to the remaining curve from 0 – 1800 s, which was successful for all channels except channels 1 and 5. The parameters from each fit are shown in Table 1.6, where $I = I_0 \exp(-t/\tau)$. Any constant term I_C resulting from the fit was negligible and so could be neglected. The exponential fits had characteristic time constants τ ranging between 280 – 610 s. Note that the value of peak-to-peak noise is above 5% of the initial current value for all channels. This result indicates that 3 time constants is a sufficient length of time for this short-term baseline drift to decay almost completely for each channels. At most, 1830 ± 150 s is required to minimise the drift present when sensing is performed, which is fulfilled by the chosen length of the control series.

From this analysis it appears that the baseline drift for the liquid-gated carbon nanotube devices can generally be approximated as a combination of a exponential and linear term. The lack of response to 1× PBS at any of the six PBS addition and removal times gives us confidence that this is a stable baseline which can be used for reliable chemical sensing. Furthermore, after ~ 1800 s the baseline drift can be reasonably approximated as linear, with a small gradient of less than -10 pA/s. The approximately linear current change means that it becomes easier to distinguish responses due to analyte addition. It can

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therefore be concluded that the 1800 s length of the PBS control series is appropriate for minimising baseline drift for more reliable sensing.

1.4.2. Sensing Series

A salt concentration sensing series were performed from 1800 s onwards, directly after the PBS control series. The responses to successive dilutions of the liquid-gate electrolyte were recorded to confirm the fabricated devices were sensitive to small environmental changes in their pristine state, to check for spurious signals, and to ensure gate current leakage or other confounding factors were not contributing to sensing responses. The PDMS well contained 80 μL 1 \times PBS at 1800 s. During the series, successive additions of deionised water were made to reduce the concentration of PBS in the well. An initial 1 \times PBS addition was performed at 2100s, to confirm no changes occurred during the PBS control series that would interfere with sensing. All additions to the well in the sensing series and resulting changes to the PBS concentration in the well are shown in Table 1.7.

Table 1.7.: This table shows the times at which 20 μL additions were made to the PDMS well, with 300 s between each addition. The concentration in the well after each addition and the change in concentration after each addition are also shown. The well contained 80 μL of 1 \times PBS at 1800 s.

	1X PBS Addition	DI Water Additions				
Time (s)	2100	2400	2700	3000	3300	3600
Final PBS volume (μL)	100	120	140	160	180	200
Final PBS concentration	1X	0.83X	0.71X	0.63X	0.56X	0.50X
Δ PBS concentration	0	-0.17X	-0.12X	-0.09X	-0.07X	-0.06X

Figure 1.11a shows a multiplexed salt concentration sensing series from the channels of a single AZ® 1518 encapsulated device, measured with the NI-PXIe. The gate voltage used was 0 V, which meant current measurements were well above the magnitude of the subthreshold device current. Gate current measurements did not exceed 1 nA for the SU8 encapsulated devices, and did not exceed 10 nA for the AZ® 1518 devices. At each of the deionised water addition times, the current traces for at least two out of six channels showed a sharp, transient increase in current followed by a return to an increased baseline. It is well established that changing the salt concentration of the liquid gate has an electrostatic gating effect on the carbon nanotubes or graphene, and changes the transfer characteristics of the channel. This shift in transfer characteristic leads to a real-time signal response to each addition [28], [30], [38].

Using the data in Table 1.5, the linear term approximating baseline drift ($c_1 t$) for each channel can be subtracted from the data in Figure 1.11a to account for the downward

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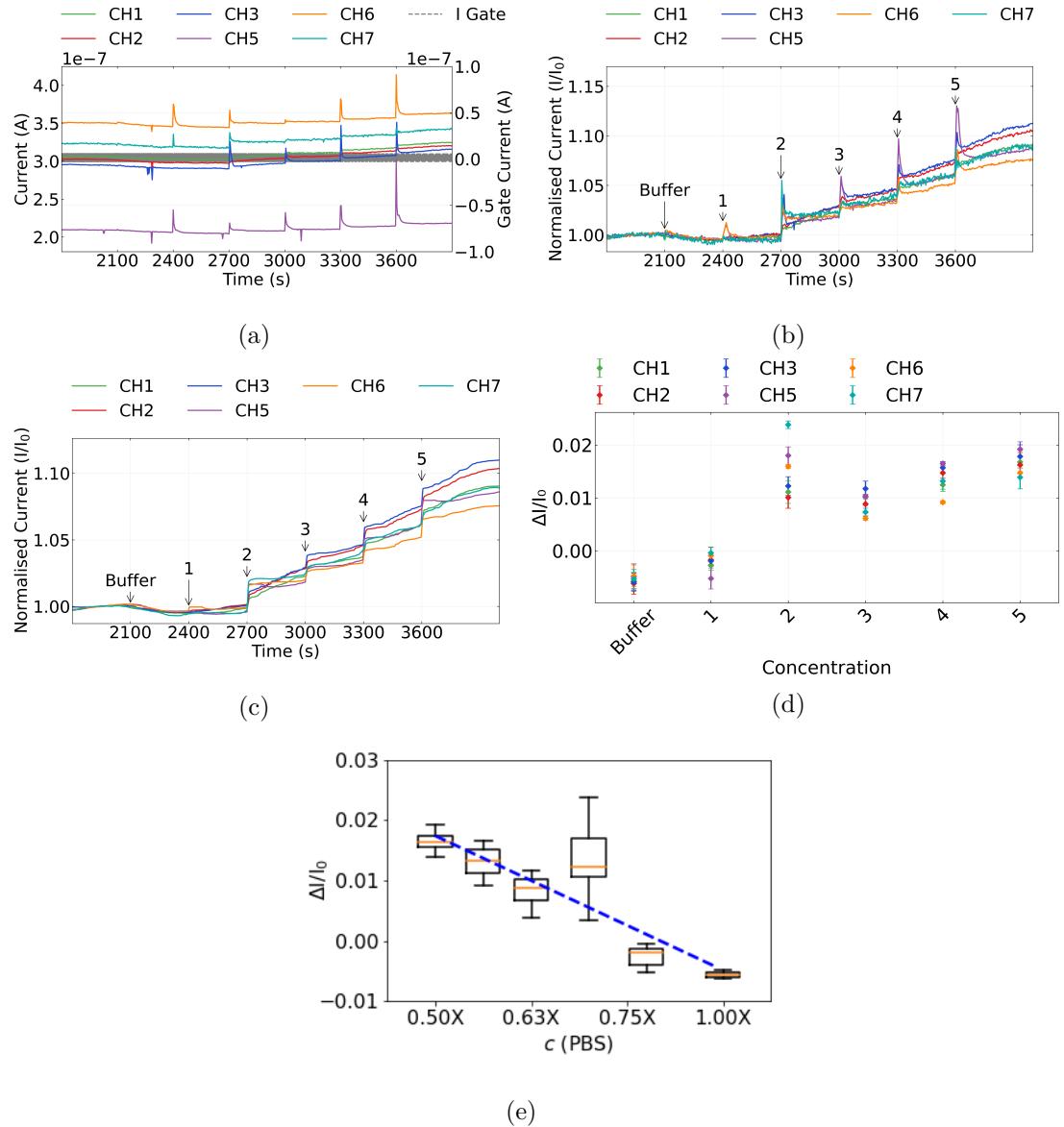


Figure 1.11.: Various visualisations of a multiplexed salt concentration sensing series taken from a single device. The source-drain voltage V_{ds} was 100 mV, and gate voltage V_g was 0 V. In (a), the raw current measurements for each channel are shown alongside gate current. The same measurements after despiking, removal of baseline drift and normalisation to initial current are shown in (b), (c) shows the data in (b) after being processed with a moving median filter, and (d) shows the signal changes in (c). The signal data in (d) is shown in box plot format in (e) alongside a fit to the median change in signal for each addition. The R squared value for the fit was 0.86.

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drift. The mean current level just before 1800 s then becomes roughly constant. Next, each channel is normalised relative to their initial mean current level I_0 . Artifacts resulting from PXIe-2737 module lag, single datapoints which fall well below the current level of the immediately preceding and succeeding datapoints, are also removed. This ‘despike’ process uses an interquartile range filter, which is described in Section 1.3.1. The resulting dataset is shown in Figure 1.11b. This figure shows that the signal-to-noise ratio remains roughly similar across all channels of the device. However, the behaviour of the initial transient increase with each addition is highly variable across channels and between additions for a single channel.

As measurement of the highly variable initial transient is not useful for robust sensing purposes, a moving median filter was applied, with the implementation of this filter discussed in Section 1.3.1. The filtered data is shown in Figure 1.11c. Noise and initial transients are removed completely, while the clearly defined step to a new current baseline is retained. Using the realtime data in Figure 1.11c, a plot of signal against addition can be created using the method described in Section 1.3.1, shown in Figure 1.11d. This presentation of the data allows us to see the increase at each step relative to I_0 .

Intriguingly, even though the largest change in PBS concentration occurred at the first deionised water addition (see Table 1.7), there was very little signal change across all channels, while a relatively large change occurred at the second addition. The logarithm of final salt concentration has previously been shown to be proportional to conductance change in the linear on-regime [28]. Figure 1.11e shows the signal change presented in terms of this logarithmic relationship. The median values of the first two additions do not line up well with the overall logarithmic trend; insufficient mixing in the tightly enclosed PDMS well environment for the first few additions may be responsible for this result. Subsequent additions may improve mixing in the well, leading to the change in concentration at the surface of the channel being more representative of the overall concentration in the well.

In Figure 1.11b and Figure 1.11c, from around the second deionised water addition onwards, the drift behaviours of individual channels begin to significantly diverge. This deviation from the baseline drift subtracted from the raw data occurs either because the linear fit is only a first-order approximation which weakens with time, or because the additions themselves affect the drift behaviour. Displaying the data as discrete signal changes, as in Figure 1.11d, is one way of excluding these deviations (see Section 1.3.1). An alternative way of presenting the signal changes, by normalising relative to both I_0 and the final current reading with the formula $(I - I_0)/(I_f - I_0)$, is shown in Figure 1.12. This approach is useful for filtering out remaining unaccounted-for drift behaviour in order to compare the short-term transient responses to additions across the device channels. Furthermore, it lets us better understand how the short-term transient responses affect the longer-term step responses discussed earlier.

Figure 1.12a and Figure 1.12c show that the transient responses to DI water additions vary significantly across the surface of the device. For example, Figure 1.12c shows that in response to the second DI water addition, channel 7 gives a large initial transient

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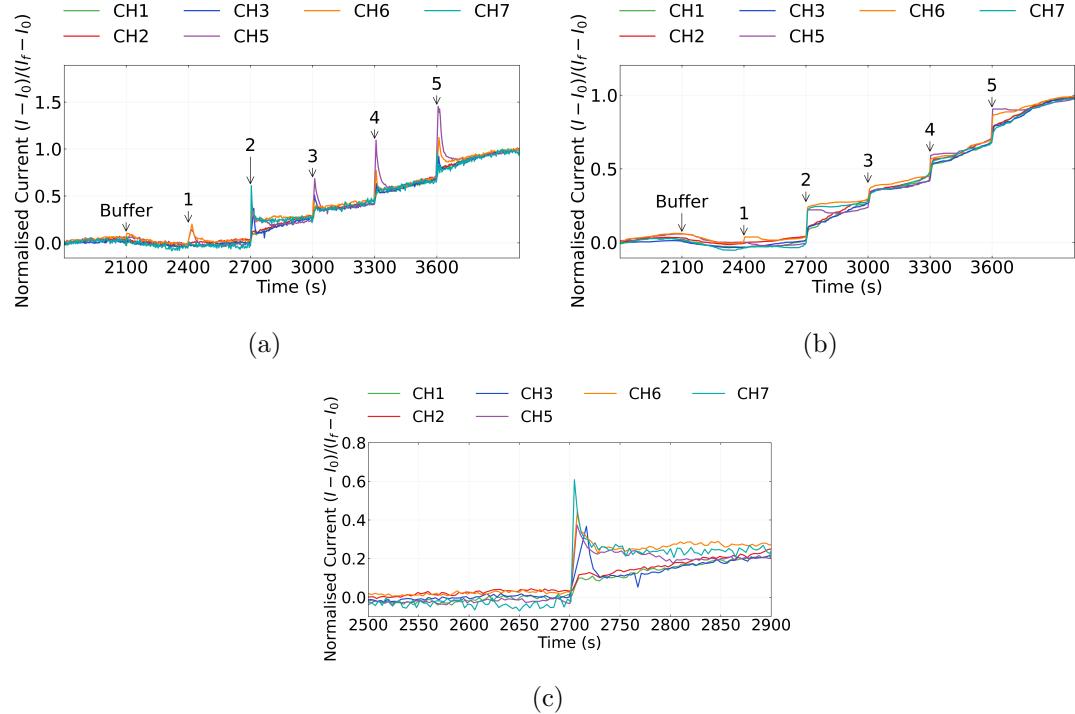


Figure 1.12.: The processed data shown in Figure 1.11b and Figure 1.11c is normalised to I_0 , but an alternative normalisation can more effectively filter out remaining drift present. This normalisation presents data relative to both I_0 and the final current reading I_f using the formula $(I - I_0)/(I_f - I_0)$. Using this normalisation, the data in Figure 1.11b and Figure 1.11c can be displayed instead as (a) and (b) respectively. (c) shows a magnified version of the step at addition 2 in (a).

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response about twice the size of the step increase between 2600 and 2800 s. Meanwhile, channels 1 and 2 show no transient response above the step increase. Figure 1.12c indicates transient size is based on location across the device, with neighbouring channels showing the most similar behaviour. This spatially-dependent behaviour may indicate transient responses are determined by the location of the channel relative to either the location of water additions or the slightly-variable location of the liquid gate. Larger and longer-lasting transient responses are not entirely removed by the moving median filter, as shown by comparing Figure 1.12a to Figure 1.11c, and so careful placement of additions is important when sensing to minimise this effect. However, even the longest-lasting transients appear to decay to zero within about 200 s, demonstrating that a 200 s spacing between additions at minimum is necessary for reliable real-time liquid-gated sensing using this setup.

Signal-to-Noise Ratio

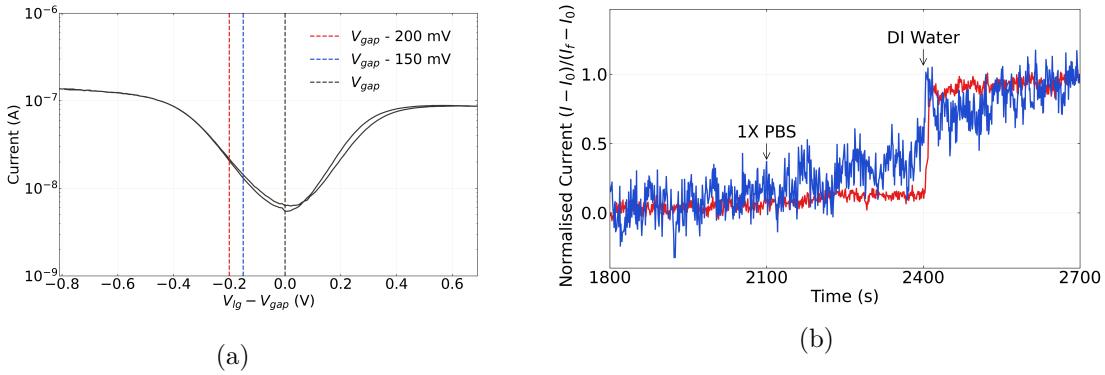


Figure 1.13.: The transfer characteristics of a single steam-deposited carbon nanotube field-effect transistor channel are shown in (a). V_{gap} is the gate voltage corresponding to the center of the transistor bandgap, found at the minimum of the characteristic curve. The signal-to-noise ratio of the channel response to a deionised water addition after a suitable control series is shown in (b). The blue current trace in (b) was performed gating the device 150 mV away from V_{gap} , while the red current was performed gating the device 200 mV away from V_{gap} .

To understand the effect of gate voltages on signal-to-noise ratio, two PBS control and salt concentration sensing series were performed with the same channel at different gate voltages. The transfer characteristics of this channel are shown in Figure 1.13a, with coloured dashed lines marking the voltages used for gating the transistor during each sensing series. Figure 1.13 shows the initial PBS and DI water additions made after 1800 s. Previous work on the signal-to-noise ratio for liquid-gated, encapsulated carbon nanotube devices suggests that gating devices close to V_{gap} should give the largest signal-to-noise ratio for salt concentration additions [38]. However, this was not what was

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observed for our carbon nanotube field-effect transistor, as Figure 1.13 shows improved signal-to-noise ratio, i.e. the signal step can be more clearly distinguished, when gated at a voltage further removed from V_{gap} . This discrepancy could be a result of the use of a network of carbon nanotubes rather than a single nanotube; gating may have less of an impact on noise when a network morphology is used. Alternatively, it could be a result of a lack of mixing in our static well setup leading to inconsistent signal sizes with concentration change. Heller *et al.* used a flow cell during their signal-to-ratio work [38]. By using a flow cell with our devices, it would be possible to confirm whether this is the case, and this might also help us reduce the size of unwanted transient responses resulting from drop-wise additions.

1.5. Vapour Sensing with Volatile Organic Compounds

1.5.1. Baseline Drift

When sensing vapour in the vapour delivery system, devices have no liquid gate, and are instead backgated when taking measurements. Therefore, the baseline drift of devices characterised in this manner should be considered separately to those characterised in an liquid-gated environment. Device baseline drift of a backgated device in the vapour sensing chamber is therefore examined here in more detail. A AZ® 1518 encapsulated carbon nanotube network device was used for this discussion. The device was fabricated on a substrate with a 300 nm SiO₂ layer, and the carbon nanotube film was deposited using the steam-assisted surfactant method. Before measurements were taken, the vapour system was purged of vapour, the total dilution flow into the chamber was set at 200 sccm as read by the Tylan mass flow controller and flow to the PID was set to 150 sccm on the flowmeter. The transfer sweep of a channel on this device (channel 6) is shown in Figure 1.14, measured using the B1500A semiconductor device analyser.

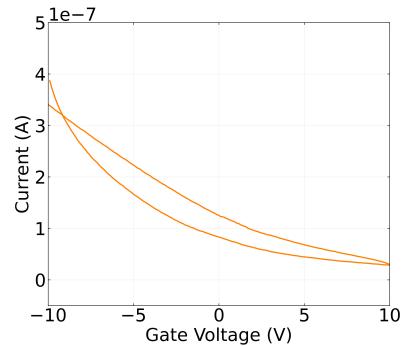
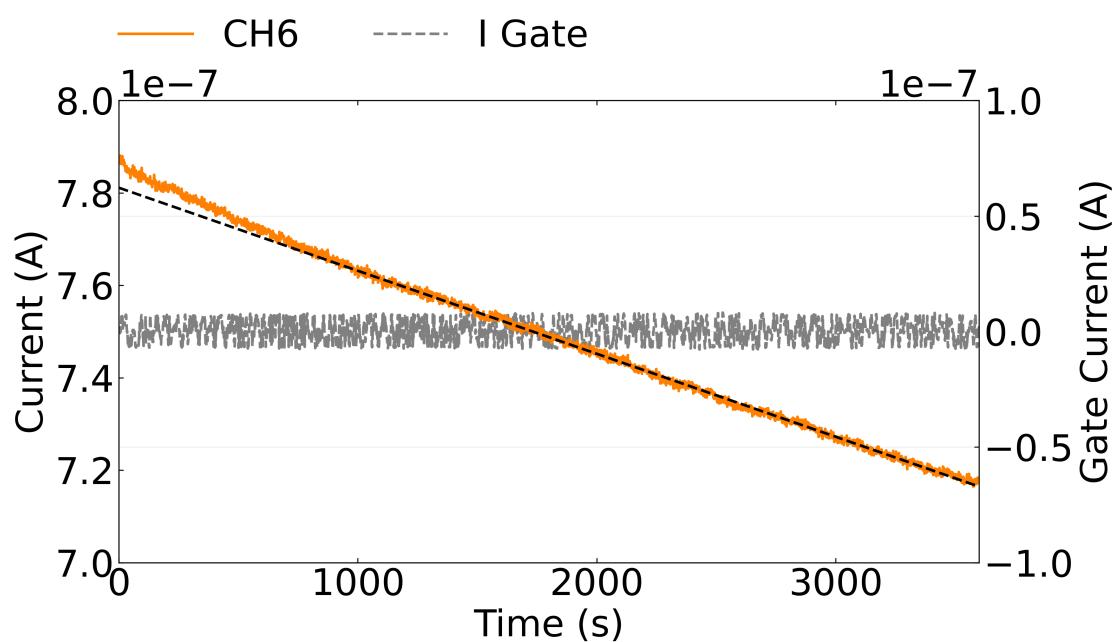


Figure 1.14.: Transfer sweep of a steam-deposited carbon nanotube network field-effect transistor, backgated in the vapour delivery system device chamber.

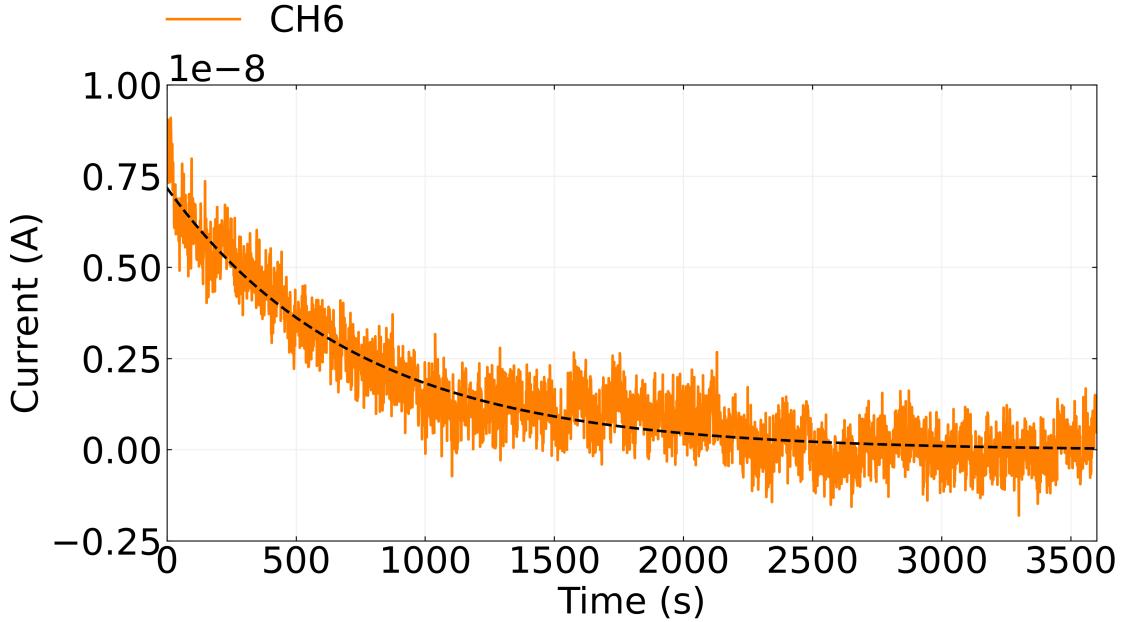
::: {#fig-bg-baseline-drift layout="[-11,3,-1,70,-15],[-11,3,-1,70,-15]" layout-valign="top"}

(a)



(b)

1. Characteristics of Pristine Carbon Nanotube & Graphene Field Effect Transistors



The source-drain and gate current measured for a backgated device channel across 3600 s, where $V_{ds} = 100$ mV and $V_g = 0$ V is shown in (a). A linear fit to the data from 2400 s onwards has been indicated on (a) with a black dashed line. The linear fit has then been subtracted from (a) to give the dataset shown in (b). An exponential fit to the dataset in (b) is also shown in black. :::

?@fig-bg-baseline-drift (a) shows 3600 s of baseline drift from the same channel when the device was backgated at $V_g = 0$ V and a source-drain voltage of $V_{ds} = 100$ mV was placed across the channel. During this period of time, a 200 sccm nitrogen flow was placed through the device chamber with the dilution mass flow controller. Gate leakage current remains negligible across the entire control series. As seen for the liquid-gated device in Section 1.4.1, there is a period of rapidly-disappearing exponential decay followed by a period of stable, approximately linear baseline drift. The baseline drift observed here appears to be significantly lower than that seen by Noyce *et al.*. This observation suggests that the higher magnitude of drift observed by Noyce *et al.* is not primarily due to backgating in air, but instead results from the use of a significantly different fabrication process for their devices [35].

A linear least-squares fit was performed on the samples taken between 2400 s – 3600 s, and the fit obtained had an R-squared value of 0.998. The constants obtained for the linear fit, where $I = c_1 t + c_2$, were $c_1 = -17.31 \pm 0.05$ pAs⁻¹ and $c_2 = 0.779$ μ A. Both linear and constant terms are higher than that of the average liquid-gated device drift. The linear fit was then subtracted from the raw data, and an exponential least-squares fit was performed on the remaining dataset. ?@fig-bg-baseline-drift (b) shows the exponential fit to this remaining dataset from 0 s – 3600 s. The constants obtained for the exponential fit $I = I_0 \exp(-t/\tau)$ were $I_0 = 7.20 \pm 0.05$ nA and $\tau = 730 \pm 10$ s. The

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exponential term is similar in size to those found for the channels of the liquid-gated device, which may indicate the magnitude of this decay behaviour is independent of the type of transistor gating. Three time constants equates to 2190 ± 30 , indicating the length of the control sequence could be safely reduced to 2400 s without the short-term exponential drift being present during sensing.

This analysis indicates that the baseline drift for the backgated carbon nanotube under nitrogen flow can be approximated as a combination of a exponential, linear and constant term. Furthermore, while only measured here for a single channel, it appears likely that we can expect backgated baseline drift behaviour to be similar to the multiplexed liquid-gated drifts observed in Section 1.4.1, except possibly with a longer time constant for the exponential term. It seems that the baseline drift behaviour in these devices is primarily due to the general nature of the carbon nanotube network. It appears possible that the type of gating used for device characterisation may affect the rate at which the exponential term decays. However, further experimentation may be needed to confirm this relationship, which is outside the scope of this thesis.

1.5.2. Sensing Series

Directly after the 3600 s control series, sensing devices were exposed to four intervals of volatile organic vapour flow from the carrier line. Two high vapour pressure compounds, ethyl hexanoate and *trans*-2-hexen-1-al, were measured separately using two different devices. 5 mL of the analyte of interest was placed into the analyte bottle on the carrier line before each sensing series. The same settings for the vapour delivery system were kept from Section 1.5.1. A total flow of 200 sccm between the two mass flow controllers was kept through the chamber at all times. During each interval 150 sccm flow was placed through the carrier line. Apart for the duration of these intervals, flow through the carrier line was kept at zero. The intervals were of varying lengths to see how the carbon nanotube device responded to various concentrations of vapour in the chamber as recorded by the PID. A 1200 s recovery period was placed between each carrier flow interval, where 200 sccm flow was placed into the chamber from the dilution line. A separate series was also performed for each device in an identical manner except without analyte in the analyte bottle. The chamber temperature was $22^\circ\text{C} \pm 3^\circ\text{C}$ for all measurements.

The results of these interval tests, both with and without analyte, are shown in Figure 1.15 (a) for *trans*-2-hexen-1-al and Figure 1.15 (b) for ethyl hexanoate. These results have been normalised, despiked and have had baseline drift corrections applied in the manner described in both Section 1.3.1 and Section 1.4.2. To more clearly discern sensing behaviour through the noise present, a moving median filter was applied to these datasets, as shown in Figure 1.15 (c) and Figure 1.15 (d) for E2Hex and EtHex respectively. Most intervals of exposure to carrier line flow correspond to a current increase. These increases have been labelled with the length of the corresponding interval used. When analyte was present in the analyte bottle on the carrier line, the response to each

1. Characteristics of Pristine Carbon Nanotube & Graphene Field Effect Transistors

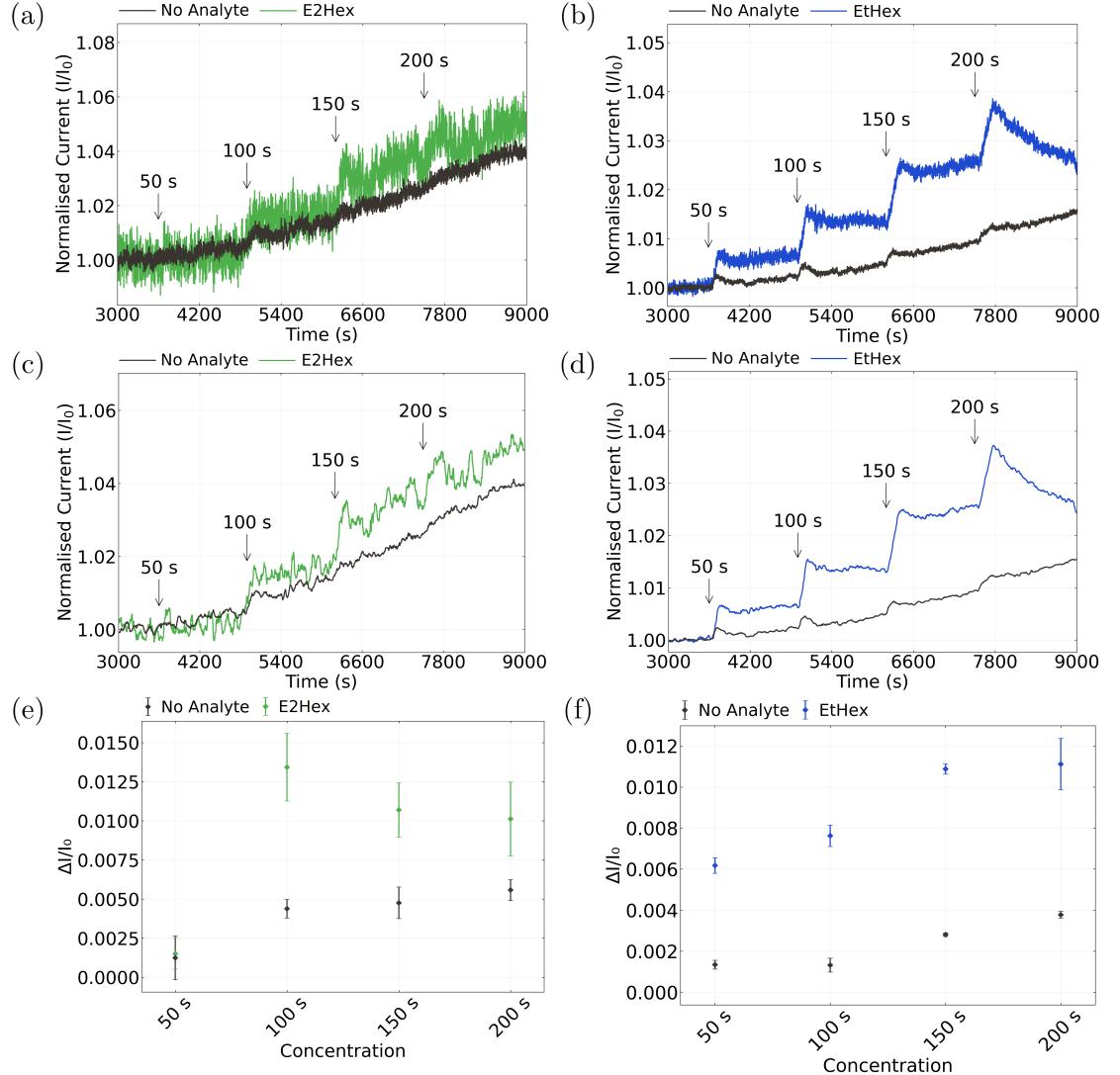


Figure 1.15.: Device channel responses to intervals of flow from the carrier line into the vapour delivery system chamber. Intervals begin at 3600 s, 4850 s, 6150 s and 7500 s. The length of each interval is indicated above the corresponding normalised current response to *trans*-2-hexen-1-al (E2Hex) in (a) and to ethyl hexanoate (EtHex) in (b). Each series is shown alongside a control series in which no analyte was present in the analyte bottle. The dataset after applying a moving median filter is shown in (c) for E2Hex and (d) for EtHex. The signal changes corresponding to the current responses to each interval are shown in (e) for E2Hex and (f) for EtHex.

1.5. Vapour Sensing with Volatile Organic Compounds

exposure interval was generally larger than the response when no analyte is present. Some response to carrier line flow is observed even when the analyte bottle is empty. As the system lines are purged with a roughing pump before sensing, and both lines are checked for vapour before sensing during the PID, it appears these small responses may be due to a slow leak of volatiles from the fumehood environment into the carrier line when not in use.

Vapour concentration measurements from PID, shown in Figure 1.16, also indicate that an ionisable gas is reaching the chamber during each interval, even when the analyte bottle is left empty. As discussed in [?@sec-responses-to-vapour](#), some baseline drift is seen after each addition, which is particularly significant for the second two carrier line intervals in Figure 1.16 (a). The baseline immediately before each peak was therefore subtracted from the maximum concentration measured during each interval to give the values shown above each peak. These values are taken to represent the nominal change in chamber concentration as a result of each exposure interval.

Each signal response corresponds to a change in conductance through the exposed carbon nanotubes within the device channel. These conductance changes occur due to the molecular adsorption of analyte vapour onto the external and internal surfaces of the nanotubes. The vapour can dope the semiconducting carbon nanotubes in the channel, causing a shift in the channel threshold voltage, and can cause carrier scattering when adsorbed onto the metallic nanotubes present. Binding of analyte to a gas sensing material can be reversible or irreversible. In general, adsorption onto carbon nanotube sensors is irreversible. This irreversibility means after a response to analyte, readings from the sensor will not return to the original baseline within the same timescale as the sensing response, even after stopping analyte flow to the chamber [59], [60]. From Figure 1.15, it is clear that the carbon nanotube sensor configuration used here is primarily irreversible, where the current level does not return to baseline within a period of 1200 s after analyte exposure.

Assuming that the signal response is directly proportional to the degree of surface coverage by adsorbed analyte on the carbon nanotube network [60], it should be possible to model the relationship between signal response (Figure 1.15) and concentration in the device chamber (Figure 1.16) with an adsorption isotherm [59]. The Freundlich adsorption isotherm (Equation 1.2) models adsorption onto a heterogeneous surface, and has previously been used to model adsorption of volatile organic molecules onto single-walled carbon nanotubes. K_F is the adsorption capacity and $1/n$ is adsorption intensity. $1/n$ can be used to understand the heterogeneity of adsorbate sites [61], [62]. The vapour response factor, which is equal to 1.6 for a 10.6 eV photoionisation detector (PID), is denoted as k_{RF} . As the PID has been run uncalibrated, a factor k_D has been included to account for linear span drift. As span drift due to window contamination can cause concentration readings to be reduced up to 30% after six months of PID operation, it is expected that k_D falls within the range of 0.2 – 1 for the sensing configuration used [63], [64].

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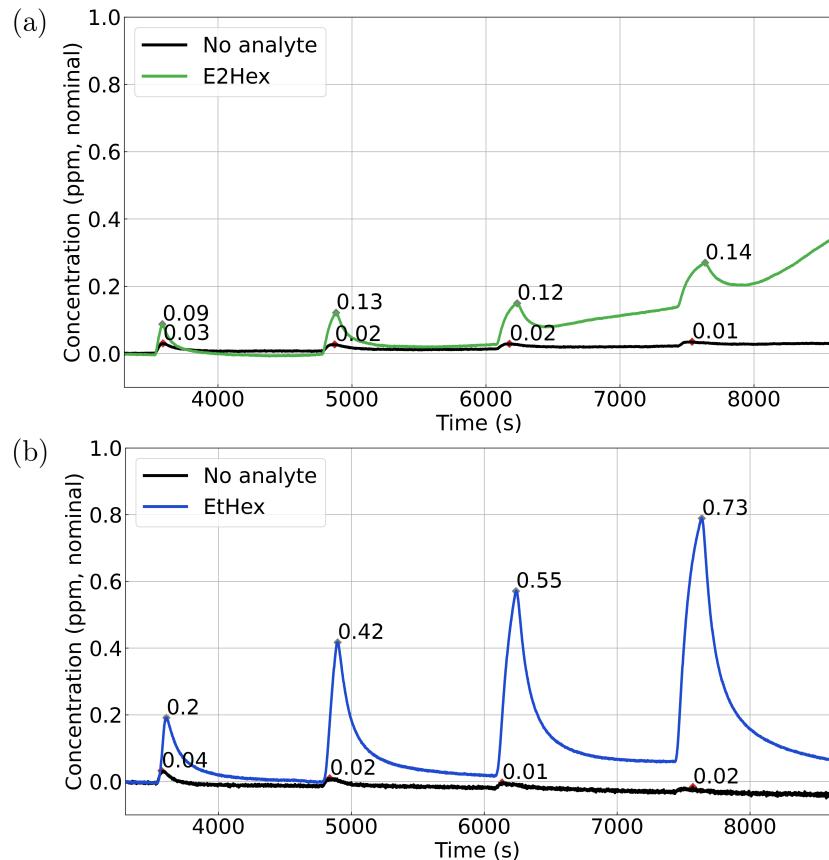


Figure 1.16.: Nominal concentration measurements by the photoionisation detector taken from the device chamber during device current sampling from 3600 s onwards. Measurements both with and without *trans*-2-hexen-1-al (E2Hex) in the analyte bottle are shown in (a), while measurements both with and without ethyl hexanoate (EtHex) are shown in (b). The maximum nominal concentration reached during each carrier flow interval is indicated above each peak.

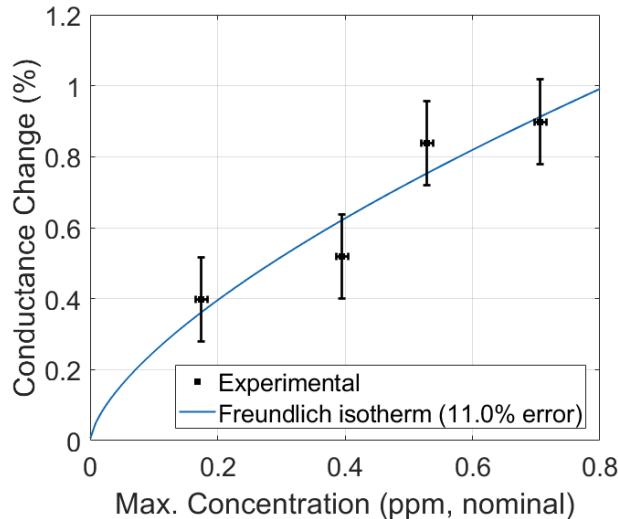


Figure 1.17.: Device response against maximum concentration measurement corresponding to each interval of carrier flow, where control responses to carrier line flow from an empty analyte bottle have been subtracted. The experimental results have been fitted with a Freundlich isotherm. The chamber temperature was $22^{\circ}\text{C} \pm 2^{\circ}\text{C}$ during collection of all data used here.

$$q_e = K_F(k_D k_{RF} C_e)^{1/n} \quad (1.2)$$

To examine only the device response directly attributable to the presence of analyte vapour, the average response resulting from carrier line exposure with no analyte present was subtracted from each device current reading. The same was then done for the vapour concentration readings from the PID. Due to the equivalence of the three final concentration measurements in Figure 1.16 (a), 0.11 ± 0.01 ppm, no isotherm could be fitted to the E2Hex dataset. An average response above control of $0.74 \pm 0.18\%$ was found for these E2Hex intervals, where the high error margin resulted from the relatively high level of noise in the collected data. The best-fit Freundlich isotherm for EtHex concentration readings against device channel responses is shown in Figure 1.17. The linear least-squares fit had an R-squared value of 0.89 and a value for $1/n$ of 0.7. A value for $1/n$ above ~ 0.2 indicates a carbon nanotube sensor has a relatively high maximum adsorption capacity. This results from using a nanotube network morphology with a relatively high external surface area [59]. The small size of the carbon nanotubes used in the network gives it a high external surface area, which explains the relatively high value obtained for $1/n$.

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1.6. Conclusion

To ensure fabricated transistors were suitable for biosensing purposes, the morphology and electrical properties of the pristine carbon nanotube and graphene transistors were investigated.

The morphology of the carbon nanotube networks were found to have a significant impact on the electrical characteristics of the devices, which was determined through comparison of the skew-normal height profile of the carbon nanotube network and the key electrical parameters of a range of carbon nanotube devices. When networks were highly bundled ($> 90\%$), there was a large range of carbon nanotube bundle diameters present in the network. This large variation in the size of conducting pathways resulted in a wide range of on-off ratios and threshold voltages for the liquid-gated devices created using these carbon nanotube films. In contrast, devices using films fabricated with a relatively low percentage of bundling ($< 75 \%$) showed highly consistent on-off ratios and threshold voltages, along with low hysteresis, due to the relatively consistent bundle diameters and high density of these networks. These low-bundling networks were found to have a mean bundle distribution height of 3.3 ± 1.0 nm. When performing multiplexed sensing, consistent channel behaviour is highly desirable since comparing sensing behaviour between channels is more straightforward.

However, atomic force microscope imaging and Raman spectroscopy also indicated that less bundled networks had the most surface contamination present. Aggregated surfactant present on the surface had a height of more than 4 nm, and introduced significant defects to the carbon nanotube network. The introduction of *p*-dopants to the carbon nanotubes by surfactant appears to have significantly increased the threshold voltage of steam-assisted surfactant-deposited network devices relative to steam-free surfactant-deposited network devices. Since the presence of surfactant could negatively impact biosensing, techniques to remove contaminants should be explored in more detail. Oxidation and thermal annealing of carbon nanotube films at high temperatures could be used to resolve this issue, and this is discussed further in [?@sec-future-work-fabrication](#). The presence of electrolyte on the surface of a backgated transistor for use in vapour sensing was also found to significantly adversely affect its electrical characteristics.

Constant voltage real-time measurements of the carbon nanotube field-effect transistor devices had a characteristic drift that could be modelled using a exponential and linear term. This was true for both liquid-gated and back-gated devices. The linear term of liquid-gated baseline drift had a reasonably consistent gradient between device channels, with a mean value of -6.1 ± 1.2 pAs⁻¹, indicating that similar drift behaviour should be reproducible between devices fabricated in the same manner. The time constant of the exponential term for liquid-gated drift ranged from $\tau = 280 \pm 10$ s to $\tau = 610 \pm 30$ s for the device characterised. The linear term of back-gated baseline drift in nitrogen found for a single channel was -17.31 ± 0.05 pAs⁻¹, higher than all measurements for liquid-gated linear drift. The exponential term found was $\tau = 730 \pm 10$ s, higher than that of the liquid-gated channels. These results indicate a control series length of

1800 s is appropriate for minimising the effects of baseline drift on liquid-gated sensing, while a control series length of 2400 s is sufficient in the case of a backgated device under nitrogen flow.

A PBS dilution sensing series indicated that the carbon nanotube transistor devices were highly sensitive to environmental changes in an aqueous environment. Successive additions of deionised water to the $1\times$ PBS present in the well gave signal responses of up to 2.5% above the control response. The signal response was found to be proportional to the logarithm of concentration, giving a fit to the median response sizes with an $R^2 = 0.86$. Deviations from this trend can possibly be explained by the enclosed sensing environment preventing sufficient mixing of electrolyte concentrations within the PDMS well, which could possibly be addressed by using a flow cell for sensing work. It was also seen that the signal size relative to baseline drift was highly consistent between channels. This is a promising result when it comes to ensuring consistent multiplexing, but it cannot be guaranteed that this behaviour carries over to sensing with biofunctionalised devices.

Furthermore, vapour sensing with *trans*-2-hexen-1-al and ethyl hexanoate using a photoionisation-based reference sensor showed that the transistor devices were highly sensitive to low concentrations of vapour. Exposure of the carbon nanotube device to parts-per-million concentrations of both compounds resulted in irreversible signal responses of up to 1% above the corresponding control measurement. Each signal response coincided with a local maximum in chamber vapour concentration as measured by the photoionisation detector. It was found that the relationship between signal response to vapour and their corresponding maximum concentration value could be modelled using a Freundlich adsorption isotherm, where the R-squared value of the model with the dataset was 0.89. An adsorption intensity of $1/n = 0.7$ was found for the sensor response to ethyl hexanoate, indicating that the carbon nanotube morphology used is particularly sensitive. Again, this is promising for the sensitivity of these devices when biofunctionalised, but may pose issues with regard to the selectivity of these devices.

Graphene field-effect transistor devices were often found to possess a double-minima feature, which appears to be the result of a lack of doping from the metal contacts in the center of the device channels. These double Dirac points are unlikely to have an significant effect on the sensing behaviour of graphene devices. The graphene device characteristics were found to be consistent after 1 hour exposure to $1\times$ PBS with minimal drift, with an on-off ratio of 5 and major Dirac point voltage of 0.3 V. There was some indications from the transfer characteristics that *p*-dopants were present on the graphene surface. Salt concentration and vapour sensing with graphene FETs is not shown in this thesis, but it is important to perform this experiment and use similar analysis techniques if there are any concerns about the sensitivity of a fabricated batch of graphene devices.

A. Vapour System Hardware

Table A.1.: Major components used in construction of the vapour delivery system described in this thesis.

Description	Part No.	Manufacturer
Mass flow controller, 20 sccm full scale	GE50A013201SBV020	MKS Instruments
Mass flow controller, 200 sccm full scale	GE50A013202SBV020	MKS Instruments
Mass flow controller, 500 sccm full scale	FC-2901V	Tylan
Analogue flowmeter, 240 sccm max. flow	116261-30	Dwyer
Micro diaphragm pump	P200-B3C5V-35000	Xavitech
Analogue flow controller, for micro diaphragm pump	X3000450	Xavitech
10 mL Schott bottle	218010802	Duran
PTFE connection cap system	Z742273	Duran
Baseline VOC-TRAQ flow cell, red	043-951	Mocon
Humidity and temperature sensor	T9602	Telaire
Enclosure, for humidity and temperature sensor	MC001189	Multicomp Pro

B. Python Code for Data Analysis

B.1. Code Repository

The code used for general analysis of field-effect transistor devices in this thesis was written with Python 3.8.8. Contributors to the code used include Erica Cassie, Erica Happe, Marissa Dierkes and Leo Browning. The code is located on GitHub and the research group OneDrive, and is available on request.

B.2. Atomic Force Microscope Histogram Analysis

The purpose of this code is to analyse atomic force microscope (AFM) images of carbon nanotube networks in .xyz format taken using an atomic force microscope and processed in Gwyddion (see [?@sec-afm-characterisation](#)). It was originally designed by Erica Happe in Matlab, and adapted by Marissa Dierkes and myself for use in Python. The code imports the .xyz data and sorts it into bins 0.15 nm in size for processing. To perform skew-normal distribution fits, both *scipy.optimize.curve_fit* and *scipy.stats.skewnorm* modules are used in this code.

B.3. Raman Spectroscopy Analysis

The purpose of this code is to analyse a series of Raman spectra taken at different points on a single film (see [?@sec-raman-characterisation](#)). Data is imported in a series of tab-delimited text files, with the low wavenumber spectrum ($100\text{ cm}^{-1} - 650\text{ cm}^{-1}$) and high wavenumber spectrum ($1300\text{ cm}^{-1} - 1650\text{ cm}^{-1}$) imported in separate datafiles for each scan location.

B.4. Field-Effect Transistor Analysis

The purpose of this code is to analyse electrical measurements taken of field-effect transistor (FET) devices. Electrical measurements were either taken from the Keysight 4156C Semiconductor Parameter Analyser, National Instruments NI-PXIe or Keysight B1500A Semiconductor Device Analyser as discussed in [?@sec-electrical-characterisation](#);

B. Python Code for Data Analysis

the code is able to analyse data in .csv format taken from all three measurement setups. The main Python file in the code base consists of three related but independent modules: the first analyses and plots sensing data from the FET devices, the second analyses and plots transfer characteristics from channels across a device, and the third compares individual channel characteristics before and after a modification or after each of several modifications. The code base also features a separate config file and style sheet which govern the behaviour of the main code. The code base was designed collaboratively by myself and Erica Cassie over GitHub using the Sourcetree Git GUI.

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