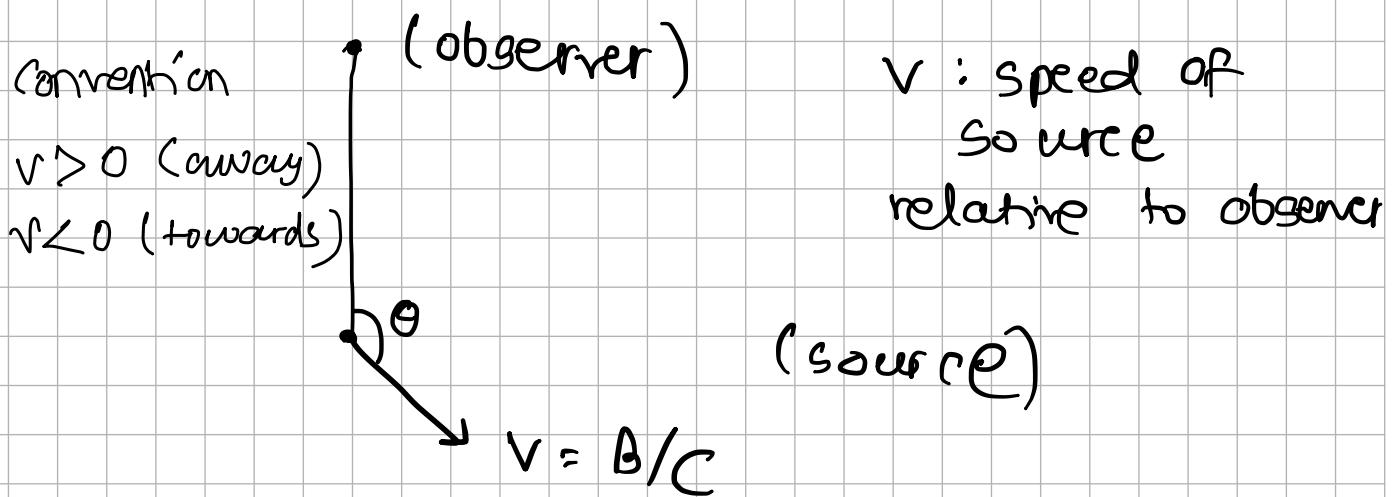


Hw 6

ASTR 589

$$1. \nu = \frac{\nu_0}{r(1 - B \cos \theta)}$$

- a)  $\nu_0$  is the frequency of the emitter moving with speed  $v$  away from the observer at an angle  $\theta$  as shown below



For cosmological redshift, the universe is isotropically expanding away from any observer, so the correct choice of

$$\underline{\underline{\theta = \pi}}$$

$$\nu = \frac{\nu_0}{r(1 - B(-1))} = \frac{\nu_0}{r(1 + B)}$$

$$\text{Now } \gamma = \frac{1}{\sqrt{1-\beta^2}}$$

$$\therefore v(\text{observed freq}) = \frac{v_0(\text{source freq})}{\sqrt{\frac{1}{(1-\beta)(1+\beta)}}} \cdot (1+\beta)$$

$$v = v_0 \sqrt{\frac{1-\beta}{1+\beta}}$$

As  $|\beta| < 1$  we can clearly see that  
 $v < v_0$ , i.e. things are getting  
 redshifted (moving to lower freq/ higher  
 wavelength)

$$\text{Now, } v = c/\lambda$$

$$\therefore \frac{v}{v_0} = \frac{\lambda_0}{\lambda} = \sqrt{\frac{1-\beta}{1+\beta}}$$

$$\text{we define } z(\text{redshift}) \text{ as } z = \frac{\lambda}{\lambda_0} - 1$$

$$\therefore z = \sqrt{\frac{1+\beta}{1-\beta}} - 1$$

$$\Rightarrow \boxed{1+z = \sqrt{\frac{1+\beta}{1-\beta}}} \quad \text{where } \beta = v/c$$

b) At a redshift  $z=1$ , we can find  $\beta$  by using the above formula, assuming we are only measuring cosmological expansion velocities and local peculiar velocities are negligible

$$1 + 1 = \sqrt{\frac{1+\beta}{1-\beta}}$$

$$\rightarrow 4(1-\beta) = 1+\beta$$

$$4 - 4\beta = 1 + \beta$$

$$\boxed{\beta = 3/5}$$

$$\Rightarrow v = \frac{3}{5} c$$

for JADES-GSZ 14-0 at  $z=14.32$   
(furthest galaxy known)

$$1 + 14.32 = \sqrt{\frac{1+\beta}{1-\beta}}$$

$$(15.32)^2 - 1 - (15.32)^2 \beta = 1 + \beta$$

$$(15.32)^2 - 1 = \beta ((15.32)^2 + 1)$$

$$233.7024 = \beta \cdot 235.7024$$

$$\boxed{\beta = \frac{233.7024}{235.7024} \sim 0.9915}$$

$$\Rightarrow v \approx 0.995 c$$

c) If we receive a collimated beam from a laser from the 214 galaxy with source power  $P_0 = \frac{h\nu_0}{t_0}$

Note that  $\frac{1}{t_0}$  transforms in the same way as  $\nu_0$

So we want to find  $\frac{P}{P_0}$  where

$$P = \frac{h\nu}{t} \quad \text{with} \quad \frac{\nu}{\nu_0} = \sqrt{\frac{1-\beta}{1+\beta}}$$

$$\text{and} \quad \frac{1/t}{1/t_0} = \sqrt{\frac{1-\beta}{1+\beta}} \quad \begin{matrix} \text{since they} \\ \text{transform} \\ \text{in same way} \end{matrix}$$

$$\therefore \frac{P}{P_0} = \frac{\frac{h\nu}{t}}{\frac{h\nu_0}{t_0}} = \frac{\nu}{\nu_0} \cdot \frac{t_0}{t}$$

$$= \sqrt{\frac{1-\beta}{1+\beta}} \cdot \sqrt{\frac{1-\beta}{1+\beta}} = \frac{1-\beta}{1+\beta}$$

$$\boxed{\frac{P}{P_0} = \frac{1-\beta}{1+\beta}} \Rightarrow \text{lower power observed.}$$

For the TADES galaxy we got

$$\beta = \frac{233 \cdot 7024}{235 \cdot 7024}$$

$$\therefore \left( \frac{P}{P_0} \right) \approx 0.00426$$

by plugging  $\beta$  in  $\frac{P}{P_0} = \frac{1-\beta}{1+\beta}$

d) we know that

$$\gamma = \frac{1}{\sqrt{1-\beta^2}}$$

$$\therefore 1-\beta^2 = \frac{1}{\gamma^2}$$

$$(1-\beta)(1+\beta) = \frac{1}{\gamma^2}$$

$$1-\beta = \frac{1}{\gamma^2(1+\beta)}$$

$$\text{for } \beta \rightarrow 1 \quad \frac{1}{1+\beta} \sim \frac{1}{2} \quad *$$

$$\therefore \boxed{1 - \beta = \frac{1}{2\gamma^2} + \text{higher order terms}}$$

\* Proof  $\frac{1}{1+\beta} = \frac{1}{1 + \beta + 1 - 1} = \frac{1}{2 + \beta - 1}$

$$= \frac{1}{2 \left( 1 + \frac{\beta - 1}{2} \right)} = \frac{1}{2} \left( 1 + \frac{\beta - 1}{2} \right)^{-1}$$

Small

$$= \frac{1}{2} \left( 1 - \left( \frac{\beta - 1}{2} \right) \right)$$

$$= \frac{1}{2} \left( 1 - \frac{\beta}{2} + \frac{1}{2} \right) = \frac{1}{2} \left( \frac{3 - \beta}{2} \right)$$

$$\beta \rightarrow 1 \quad \therefore = \frac{1}{2} \left( \frac{2}{2} \right) = \frac{1}{2}$$

$$\boxed{a = \frac{1}{2} \quad b = -2}$$

Proved

Q2.

a) collision rate

$$\boxed{\tilde{n}_c = n \sigma_c \bar{v}_{th}}$$

This makes sense because,  
if there are more atoms per unit volume,

i.e.  $n \uparrow$ , the collision rate would certainly increase as things are more densely packed.

Similarly if  $\sigma_c$  is higher, there is more chance of a collision as the interaction area  $\sigma_c$  becomes larger.

Lastly we know that  $\bar{v}_{th} \propto \sqrt{T}$  and at higher  $T$  there is more random motion among atoms, so they are more likely to collide.

Now we know the frequency of

collisions  $\nu_c = n \sigma_c \bar{v}_{th}$ . So the

approx time b/w each collision is

$$1/\nu_c = \frac{1}{n \sigma_c \bar{v}_{th}}. \text{ Now the mean}$$

free path is defined to be the distance traveled b/w each collision. Since an atom on average has speed  $\bar{v}_{th}$ , the MFP is

$$l_c = \frac{1}{\nu_c} \cdot \bar{v}_{th} = \frac{1}{n \sigma_c \bar{v}_{th}} \cdot \bar{v}_{th}$$

$$l_c = \frac{1}{n \sigma_c}$$

$\rightarrow$  This dimensionally makes sense and also we

excepted  $l_c \downarrow$  as  $n \uparrow$  or  $\sigma_c \uparrow$  as

there is more chance of collision, so atom travels less b/w each collision!

b) we are given line profile width due to collisional broadening  $\Gamma = 2\gamma k$

and doppler width  $\Delta v_D \approx v_0 \frac{v_{th,a}}{c}$

where  $v_{th,a} = \sqrt{\hbar T/m_a}$  → thermal speed of emitting atom of mass  $m_a = A m_p$

$\frac{\Gamma}{\Delta v_D}$ , the ratio of the 2 line widths is  $\frac{\Gamma}{\Delta v_D} = \frac{2 v_c}{v_0 v_{th,a} / c}$

Plugging the  $v_c$  from 2a)  
and we know  $v_0 \lambda_0 = c$

$$\therefore \frac{\Gamma}{\Delta v_D} = \frac{2 n \sigma_c \overline{v_{th}}}{\frac{1}{\lambda_0} v_{th,a}}$$

we know  $L_c = \frac{1}{n \sigma_c}$

$$\therefore \frac{\Gamma}{\Delta v_D} = \frac{2\lambda_0}{L_c} \cdot \frac{\sqrt{v_{th}}}{v_{th,a}}$$

$$\sqrt{v_{th}} \propto \sqrt{\frac{kT}{Amp}} \quad (\text{we roughly have } N \text{ atoms})$$

$$v_{th,a} \propto \sqrt{\frac{kT}{Amp}} \quad (\text{emitting atom})$$

Since we are ignoring order unity constants,

$$\boxed{\frac{\Gamma}{\Delta v_D} \approx \frac{\lambda_0}{L_c} \sqrt{A}}$$

c) For sodium doublet line,  $\lambda_0 = 589 \text{ nm}$

$$\sigma_c \sim 4\pi a_0^2 \rightarrow \text{Bohr radius}$$

$$\frac{\Gamma}{\Delta v_D} \sim \frac{\lambda_0 n \sigma}{A} \sqrt{23} \quad A_{Na} = 23$$

$$P = n k_B T \quad (\text{ideal gas law})$$

$$n = \frac{P}{k_B T}$$

$$\therefore \frac{\Gamma}{\Delta\nu_D} \sim \lambda_0 \frac{P}{k_B T} \cdot 4\pi a_0^2 \sqrt{23}$$

From HW3, we know

$$P_{\text{gas}}(T=0) = \frac{2g}{3K} \quad \text{where } g = \frac{GM}{R^2}$$

and  $K = \text{mean opacity}$   
 $= 0.3 \text{ cm}^2/\text{g}$

$$\therefore \frac{\Gamma}{\Delta\nu_D} \sim \frac{\lambda_0}{k_B T} \cdot \frac{2}{3KR} \cdot \frac{GM}{R^2} \cdot 4\pi a_0^2 \sqrt{23}$$

Plugging in appropriate values for Sun,  $a_0$ ,  $T=5800K$  we get

$$\boxed{\frac{\Gamma}{\Delta\nu_D} \sim 0.0076}$$

i.e  $\Gamma \ll \Delta\nu_D$  which means  
 that at line center doppler broadening  
 is much more important than  
 collisional broadening

Q3 Doppler :  $\Delta\nu_D$

Collisional :  $\Gamma$

$\Delta\nu = \nu - \nu_0$  relative to line center

$$\nu_0 = c/\lambda_0$$

$$\phi(\Delta\nu) = \frac{1}{\sqrt{\pi} \Delta\nu_D} H(v, a)$$

$$H(v, a) = \frac{1}{\pi} \int_{-\infty}^{\infty} \frac{ae^{-y^2}}{(v-y)^2 + a^2} dy$$

$$v = \frac{\Delta\nu}{\Delta\nu_D} \quad a = \frac{\Gamma}{4\pi \Delta\nu_D}$$

a) As  $a \rightarrow 0$ , Voigt reduces to Doppler

$$\text{Given : } \lim_{a \rightarrow 0} \left( \frac{a}{x^2 + a^2} \right) \Rightarrow \pi S(x)$$

Using this in  $H(v, a)$

$$\lim_{a \rightarrow 0} H(v, a) = \lim_{a \rightarrow 0} \frac{1}{\pi} \int_{-\infty}^{\infty} \frac{ae^{-y^2}}{(v-y)^2 + a^2} dy$$

Now we have

$$\lim_{a \rightarrow 0} \frac{a}{(v-y)^2 + a^2}$$

$$= \pi g(v-y)$$

Plugging it in,

$$\lim_{a \rightarrow 0} H(v, a) = \frac{1}{\pi} \int_{-\infty}^{\infty} \pi g(v-y) e^{-y^2} dy$$

Using

$$\int_{-\infty}^{\infty} g(v-y) e^{-y^2} dy = e^{-v^2}$$

we get

$$\lim_{a \rightarrow 0} H(v, a) = \frac{1}{\pi} \cdot \pi e^{-v^2} = e^{-v^2}$$

Plugging this in  $\phi(\Delta v)$  we get,

$$\phi(\Delta v) = \frac{1}{\sqrt{\pi \Delta v}} e^{-v^2}$$

Using  $v = \frac{\Delta v}{\Delta v_D}$  we get

$$\Phi(\Delta v) = \frac{1}{\sqrt{\pi} \Delta v_D} e^{-\frac{(\Delta v)^2}{(\Delta v_D)^2}}$$

$$\boxed{\Phi(\Delta v) = \frac{1}{\sqrt{\pi} \Delta v_D} e^{-\frac{(v - v_0)^2}{\Delta v_D^2}}}$$

This is the doppler profile hence proved  
that as  $\alpha \rightarrow 0$ , Voigt reduces to doppler

while at line wings, collisional will be more important as the dopper broadening shape is a gaussian (exponential dropoff) and for collisional it is Lorentzian, and away from their centers, Lorentzian has slower dropoff than a gaussian.

Q3 b) We know that the emergent intensity  $I_2$  through a slab of source  $S_2$ , optical depth  $\tau_2$

$$\text{is } I_2 = I_{2,b} e^{-\tau_2} + S_2 (1 - e^{-\tau_2})$$

$\hookrightarrow$  background.

Equivalent width  $EW$

$$\equiv \int \left| 1 - \frac{I_2}{I_{2,b}} \right| d\lambda$$

Plugging in  $I_2$ , we get

$$EW = \int \left| 1 - \left[ \frac{I_{2,b} e^{-\tau_2} + S_2 (1 - e^{-\tau_2})}{I_{2,b}} \right] \right| d\lambda$$

$$E\bar{W} = \int \left| \frac{I_{v,b}(1 - e^{-T_v}) - S_v(1 - e^{-T_v})}{I_{v,b}} \right| d\lambda$$

$$E\bar{W} = \int \left| \frac{(I_{v,b} - S_v)(1 - e^{-T_v})}{I_{v,b}} \right| d\lambda$$

$$E\bar{W} = \int \left| 1 - \frac{S_v}{I_{v,b}} \right| (1 - e^{-T_v}) d\lambda \quad 1 - e^{-T_v} > 0$$

always

Since the  $E\bar{W}$  integral is over a range of freq  $\ll v_0$ ,  $\Rightarrow I_{v,b}, S_v$  are constant almost in the range

$$\therefore E\bar{W} = \left| 1 - \frac{S_v}{I_{v,b}} \right| \int (1 - e^{-T_v}) d\lambda$$

range of freq  $\gg \Delta v$   $\Rightarrow \lambda \rightarrow \infty$

$$\lambda = \frac{c}{v} \quad (\text{change of variable})$$

$$\frac{d\lambda}{dv} = -\frac{c}{v^2} \quad \frac{d\lambda}{d\nu} = -\frac{\lambda}{v}$$

in the range of freq we are interested  
in  $\frac{d\lambda}{dv} \sim -\frac{\lambda_0}{v_0}$   $\lambda_0, v_0 \rightarrow \text{line center}$

$$\therefore EW = \left| 1 - \frac{S_v}{I_{v,b}} \right| \int (1 - e^{-\tau_v}) dv \left( \frac{-\lambda_0}{v_0} \right)$$

$$\therefore \boxed{\frac{EW}{\lambda_0} = - \left| 1 - \frac{S_v}{I_{v,b}} \right| \int (1 - e^{-\tau_v}) \frac{dv}{v_0}}$$

Multiplying by  $\frac{v_0}{\Delta v_D}$  we get

$$\frac{EW}{\lambda_0} \frac{v_0}{\Delta v_D} = - \left| 1 - \frac{S_v}{I_{v,b}} \right| \int (1 - e^{-\tau_v}) \frac{dv}{v_0} \frac{\Delta \lambda_D}{\Delta v_D}$$

$\left( \frac{\Delta \lambda_D}{\Delta v_D} \sim -\frac{\lambda_0}{v_0} \right)$  (because  
 $\frac{\Delta v_D}{\Delta \lambda_D} \ll \frac{v_0}{\lambda_0}$ )

$$\therefore \frac{EW}{\lambda_0} \cdot \frac{\Delta \lambda_D}{-\Delta \lambda_D \frac{\lambda_0}{v_0}} = - \frac{EW}{\Delta \lambda_D}$$

$$\therefore \text{we get } \frac{EW}{\Delta \lambda_D} = \left| 1 - \frac{S_v}{I_{v,b}} \right| \int (1 - e^{-\tau_v}) \frac{dv}{\Delta v_D}$$

we have defined  $U = \frac{\Delta v}{\Delta v_D}$

$$\therefore \frac{EW}{\Delta \lambda_D} = \left| 1 - \frac{Sv}{I_{v,b}} \right| \int (1 - e^{-tv}) du$$

c) we have

$$\Phi(\Delta v) = \frac{1}{\sqrt{\pi}} \cdot \frac{1}{\Delta v_D} H(v, a)$$

where  $H(v, a) = \frac{1}{\pi} \int_{-\infty}^{\infty} \frac{ae^{-y^2}}{(v-y)^2 + a^2} dy$

Given  $a = 0.1$

$$-4 < \frac{\Delta v}{v_D} = v < 4$$

$$\underbrace{\Phi(\Delta v) \cdot \Delta v_D}_{y} = \frac{1}{\sqrt{\pi}} H(v, a)$$

$$\underbrace{f(v, a=0.1)}_{f(v)}$$

Have to plot  $y$  vs  $f(v)$   
 $(\log scale)$

For pure doppler ,

$$\Phi(\Delta\nu) \Delta\nu_D = \frac{1}{\sqrt{\pi}} e^{-\left(\frac{\Delta\nu}{\Delta\nu_D}\right)^2}$$
$$= \frac{1}{\sqrt{\pi}} e^{-v^2}$$

For pure pressure ,

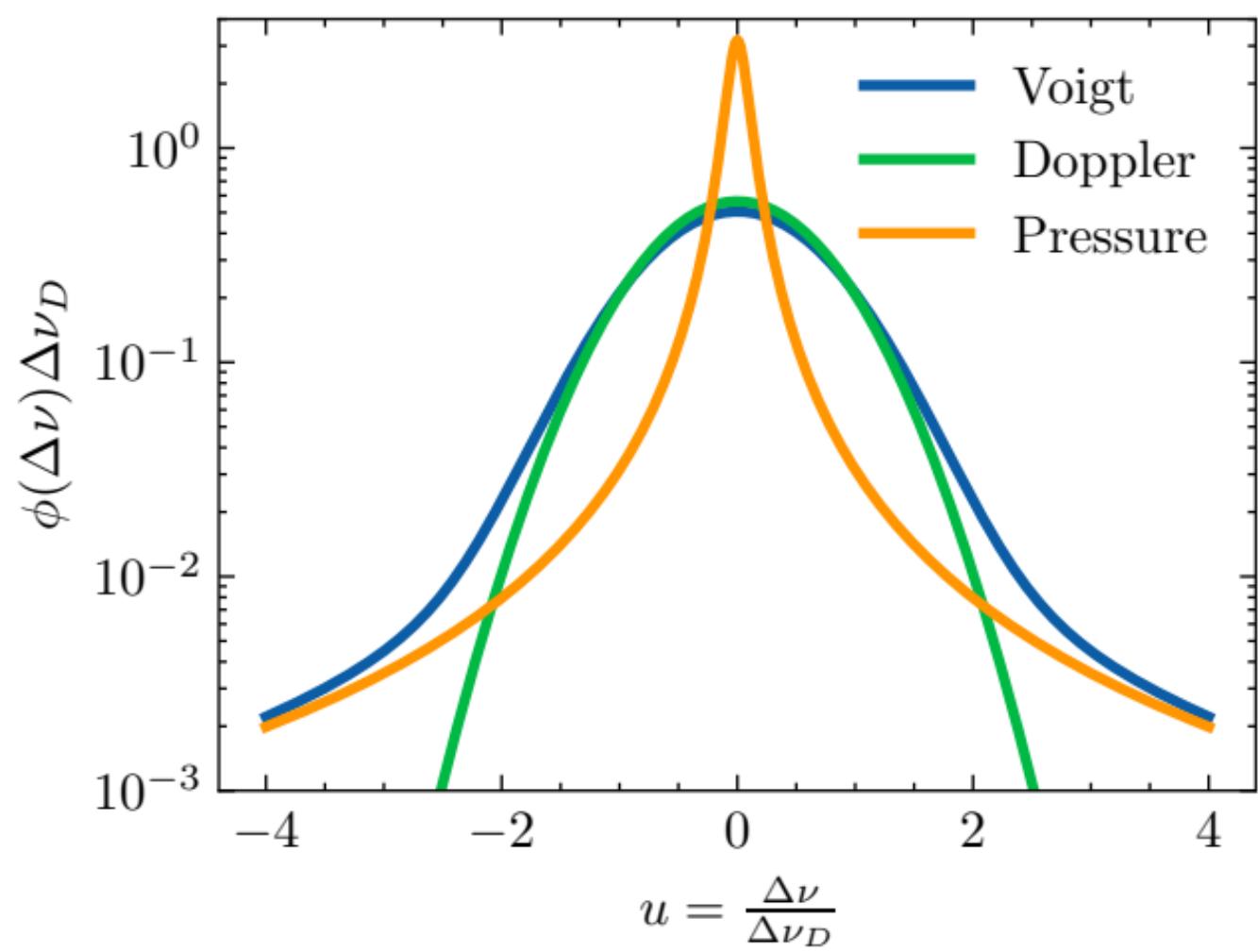
$$\Phi(\Delta\nu) = \frac{\tau / 4\pi^2}{\Delta\nu^2 + (\tau / 4\pi)^2}$$

where  $\tau = 4\pi \Delta\nu_D a$

$$\therefore \Phi(\Delta\nu) = \frac{1}{\pi} \frac{\Delta\nu_D a}{\Delta\nu^2 + (\Delta\nu_D a)^2}$$

$$\Phi(\Delta\nu) \Delta\nu_D = \frac{a/\pi}{\left(\frac{\Delta\nu}{\Delta\nu_D}\right)^2 + a^2}$$

$$= \frac{a/\pi}{v^2 + a^2}$$



we can clearly see that the tail of pressure matches voigt, and towards center, doppler matches voigt well

d) we want to plot

$$e^{-T_v} \text{ vs } v = \frac{\Delta v}{\Delta v_D}$$

$$\text{where } T_v = T_0 \frac{\phi(\Delta v)}{\phi(0)}$$

$$T_0 = 0.1, 1, 10$$

Doppler &  $\alpha = 0.3$  Voigt profile

for doppler

$$- \left( \frac{\Delta v}{\Delta v_D} \right)^2$$

$$\phi(\Delta v) = \frac{1}{\sqrt{\pi} \Delta v_D} e$$

$$\phi(0) = \frac{1}{\sqrt{\pi} \Delta v_D}$$

$$T_v = T_0 e^{-\left( \frac{\Delta v}{\Delta v_D} \right)^2} = T_0 e^{-v^2}$$

$$\text{as } U = \frac{\Delta v}{\Delta v_D}$$

Plot  $e^{-T_v}$  vs  $U$

For weight  $a = 0.3$

$$\phi(\Delta v) = \frac{1}{\sqrt{\pi} \Delta v_D} H(v, a)$$

$$\phi(0) = \frac{1}{\sqrt{\pi} \Delta v_D} H(0, a)$$

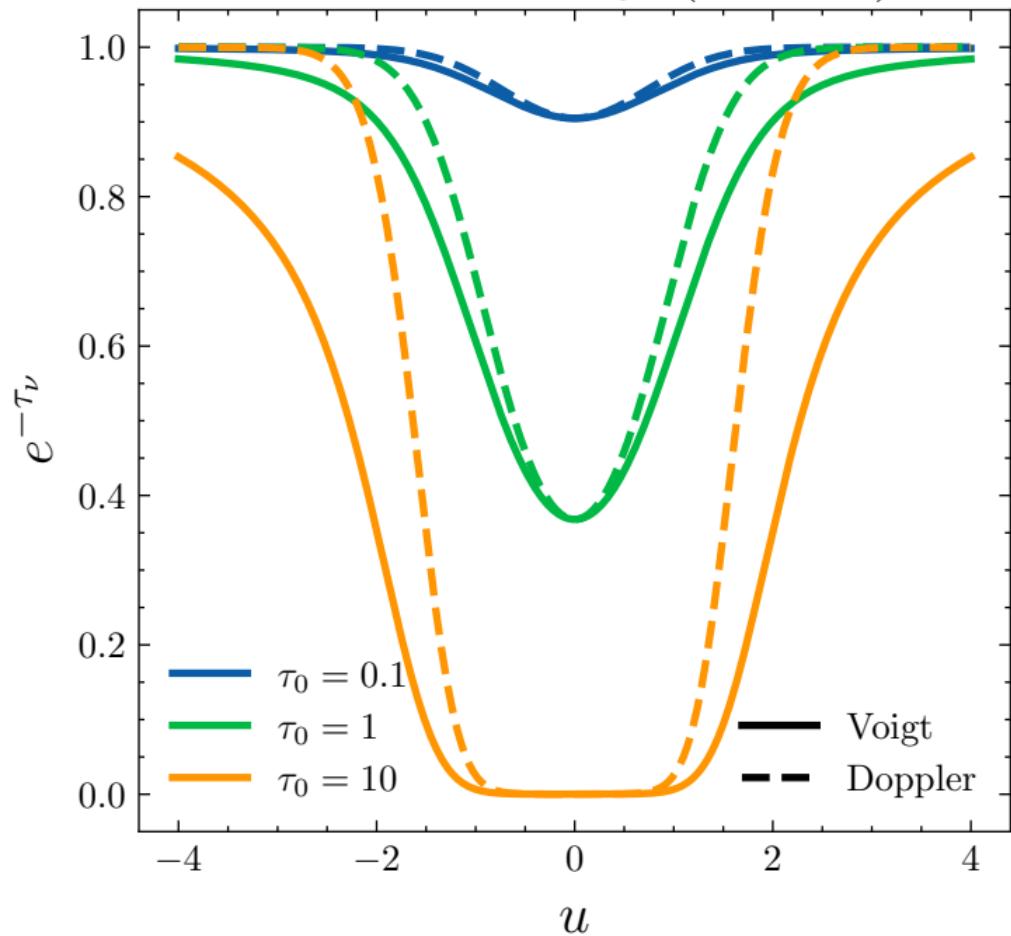
$$\therefore T_v = T_0 \frac{H(v, a)}{H(0, a)}$$

where  $a = 0.3$

Plot  $e^{-T_v}$  vs  $U$

~~for  $\alpha = 0.1$~~

# Doppler vs Voigt ( $a = 0.3$ )



e) Plot EW vs tau<sub>D</sub> for  $0.01 \leq \tau_D \leq 100$

$\alpha = 0$  (pure doppler)

$\alpha \rightarrow \infty$  (pure pressure)

$\alpha = 0.01, 0.1, 1$  Voigt

we are given  $S_v = 0$  (only

absorption & no emission)

$$\frac{EW}{\Delta\lambda} = \int_{-\infty}^{\infty} (1 - e^{-\tau_v}) du$$

Note that for doppler,

$1 - e^{-\tau_v}$  is symmetric about  $v$

$$\therefore \frac{EW}{\Delta\lambda_D} = 2 \int_0^{\infty} (1 - e^{-\tau_v}) du$$

For pressure, we are given

$$\frac{Ew}{\Delta \lambda_p} = \int_{-\infty}^{\infty} [1 - e^{-T_0/(1+y^2)}] \frac{dy}{\sqrt{\pi}}$$

Note that this  
is also symmetric by  $y$

$$\therefore \int_{-\infty}^{\infty} \rightarrow 2 \int_0^{\infty}$$

Now for Voight, we are given

$$\Delta \lambda_v = \frac{\Delta \lambda_D}{h(0, a)}$$

$$\therefore \frac{Ew}{\Delta \lambda_v} = h(0, a) \int (1 - e^{-Tu}) du$$

$$\text{where } Tu = \frac{h(u, a)}{h(0, a)} T_0$$

we have to plot

$$\frac{Ew}{\Delta \lambda_v} \text{ vs } Tu \quad \text{For } a = 0, 0.01, 0.1, 1$$

# Equivalent Width vs $\tau_0$

