0.1 Problem Description

We model a two-vehicle (the ego vehicle and the cut-in vehicle) system using the kinematic single-track model:

$$\dot{\delta} = v_{\delta}
\dot{\psi} = \frac{v}{l_{wb}} \tan(\delta)
\dot{v} = a_{1\circ ng}
\dot{s}_{x} = v \cos(\psi)
\dot{s}_{y} = v \sin(\psi)$$
(1)

And we provide the ego vehicle with a closed-loop controller that keeps the distance from a front vehicle or a cut-in vehicle. The controller is expressed in an analytical form w.r.t. the state variables in the system and is differentiable.

The cut-in vehicle is assigned the same kinematic single-track model with full control authority to perform any control sequences.

The question we seek to answer is: given a set of initial conditions of the two-vehicle system state $x_0 \in S_0$ (which is part of our ODD definition), for all the possible controls of the cut-in vehicle, will the two-vehicle system $\dot{x} = f(x)$ remain as collision-free within a predefined time window [0,T]?

0.2 Mathematical Formulation

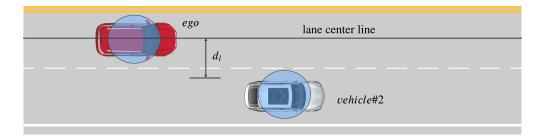
The full state of the two-vehicle system is $\mathbf{x} = [v_1, s_{x1}, s_{y1}, \psi_1, \delta_1, v_2, s_{x2}, s_{y2}, \psi_2, \delta_2]^{\mathrm{T}}$, and the state-space equations are:

$$\dot{\mathbf{x}} = \begin{bmatrix} \dot{s}_{x1} \\ \dot{s}_{y1} \\ \dot{\psi}_{1} \\ \dot{\psi}_{1} \\ \dot{v}_{1} \\ \dot{\delta}_{1} \\ \dot{s}_{x2} \\ \dot{s}_{y2} \\ \dot{\psi}_{2} \\ \dot{v}_{2} \\ \dot{\delta}_{2} \end{bmatrix} = \begin{bmatrix} v_{1} \cos(\psi_{1}) \\ v_{1} \sin(\psi_{1}) \\ v_{1} \sin(\psi_{1}) \\ v_{1} \tan(\delta_{1}) \\ a_{1} \\ v_{2} \cos(\psi_{2}) \\ v_{2} \sin(\psi_{2}) \\ v_{2} \sin(\psi_{2}) \\ v_{2} \sin(\psi_{2}) \\ a_{2} \\ v_{\delta 2} \end{bmatrix} \tag{2}$$

This is a first-order nonlinear ODE with 4 control inputs $[a_1, v_{\delta 1}, a_2, v_{\delta 2}]$. The ego vehicle's control inputs $[a_1, v_{\delta 1}]$ is based on a closed-loop control (IDM Model):

$$a_1 = a_0 \left[1 - \left(\frac{v_1}{v_0} \right)^{\delta} - \left(\frac{s^*}{s} \right)^2 \right] \tag{3}$$

where a_0 is a nominal value for acceleration to mimic everyday traffic, v_0 is a desired driving speed on a free road, δ is a pre-defined constant (typically $\delta = 4$), s is the distance from the front car, and s^* stands for the desired dynamical distance to the



Figur 1: The cut-in status determination: if vehicle #2's mass center is closer than d_l to the lane center line of the ego vehicle's lane, then the ego vehicle considers vehicle #2 as entering the cut-in status.

front car, which is calculated as:

$$s^*(v_1, \Delta v) = s_0 + \max \left[0, v_1 T_h + \frac{v_1 \Delta v}{2\sqrt{a_0 b_0}} \right]$$
 (4)

where s_0 is a minimum bumper-to-bumper distance, T_h is a time headway, $\Delta v = v_1 - v_l$ is the speed difference between the ego car and the lead car, b_0 is a reference deceleration value for stop-and-go motion.

An important detail is the determination of a cut-in action. A cut-in action is defined as vehicle #2's mass center getting closer than d_l to the ego vehicle's lane center, as depicted in Figure 1. Therefore, the distance s in the IDM model can be expressed as a piecewise function:

$$s = \begin{cases} s_{x2} - s_{x1} & \text{if } dist((s_{x2}, s_{y2}), C) < d_l \\ +\infty & \text{otherwise} \end{cases}$$
 (5)

For simplicity, we do not define any steering behavior for the ego vehicle, therefore $\delta_1 = 0$.

With this closed-loop control, the two-vehicle system is reduced to 2 control inputs $[a_2, v_{\delta 2}]$. The state-space equation can be re-written as:

$$\begin{bmatrix} \dot{s}_{x1} \\ \dot{s}_{y1} \\ \dot{\psi}_{1} \\ \dot{\psi}_{1} \\ \dot{v}_{1} \\ \dot{\delta}_{1} \\ \dot{s}_{x2} \\ \dot{s}_{y2} \\ \dot{\psi}_{2} \\ \dot{v}_{2} \\ \dot{\delta}_{2} \end{bmatrix} = \begin{bmatrix} v_{1} \cos(\psi_{1}) \\ v_{1} \sin(\psi_{1}) \\ v_{1} \sin(\psi_{1}) \\ v_{1} \sin(\psi_{1}) \\ v_{1} \sin(\psi_{1}) \\ a_{0} \left[1 - \left(\frac{v_{1}}{v_{0}} \right)^{\delta} - \left(\frac{s^{*}}{s} \right)^{2} \right] \\ 0 \\ v_{2} \cos(\psi_{2}) \\ v_{2} \sin(\psi_{2}) \\ v_{2} \sin(\psi_{2}) \\ v_{2} \sin(\psi_{2}) \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ a_{2} \\ v_{\delta 2} \end{bmatrix}$$

$$(6)$$

Given a set of initial conditions $\mathbf{x}_0 \in S_0$, the reachable states within the time interval [0,T] can be numerically approximated using a selected reachability computation tool:

$$R_{[0,T]}(S_0) = \{ \mathbf{x}(t) \in \mathbb{R}^{10} | \mathbf{x} = \int_0^t f(\mathbf{x}, \mathbf{u}), \forall t \in [0,T], \forall \mathbf{u}(\cdot) = [a_2(\cdot), v_{\delta 2}(\cdot)] \}$$
 (7)

We define a simple point-to-point version of collision freedom as:

$$\mathbf{x} \in \mathcal{X}_{cf} := \{ \mathbf{x} | \sqrt{(s_{x1} - s_{x2})^2 + (s_{y1} - s_{y2})^2} > d_{min} \}$$
 (8)

where d_{min} is a pre-defined minimum collision distance.

Initial States

If the state of the system is initially fixed, i.e.,

$$\mathbf{x}(0) = [v_1(0), s_{x1}(0), s_{y1}(0), \psi_1(0), \delta_1(0), v_2(0), s_{x2}(0), s_{y2}(0), \psi_2(0), \delta_2(0)]^{\mathrm{T}}$$

is assigned a single vector, then the system reachability within [0, T] can only represent a very specific traffic scene, and the analysis would have very limited use.

Instead, if the initial state of the system can take a range of values (ideally this range would match the ODD), then the system reachability can provide safety analysis for the ego vehicle controller across a range of scenes. For simplicity, we limit the diversity of the initial state to the range of values for $v_2(0)$, while keeping all other sub-states fixed.

0.3 Proposed Workflow

The proposed workflow consists of the following steps:

- 1. We apply the selected reachability tool to the system in (6), and obtain the over-approximated reachable states $R_{[0,T]}(S_0)$ within time [0,T] and a set of initial states $\mathbf{x} \in S_0$.;
- 2. We use the collision definition to post-process $R_{[0,T]}(S_0)$, and back-track what values of $v_2(0)$ lead to collisions.