

# Leakage reduction in fast superconducting qubit gates via optimal control: Overview

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## ① Introduction

## ② Setup and system control

## ③ Parameter optimization & Results

# Table of Contents

- 1 Introduction
- 2 Setup and system control
- 3 Parameter optimization & Results

# Introduction

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- Open-loop optimal control theory (gradient/newton-descent) offers means for states and gates realization with high fidelity.
- However, this method produces less accurate results in comparison to ion traps and NMR systems.
- As a result, pulse shaping for supercond. qubits requires closed-loop optimal control (finite, continuous space), i.e., direct optimization of the experimental system.

# Table of Contents

1 Introduction

2 Setup and system control

3 Parameter optimization & Results

## Backend comparison

Experiments are carried out on a transmon-type fixed-frequency superconducting qubit. Some numbers:

- transition frequency  $\omega_{01}/2\pi = 5.11722$  GHz;
- anharmonicity  $\Delta/2\pi = -315.28$  MHz;
- $T_1 = 105\mu s$  and  $T_2 = 39\mu s$ .

Better than armonk ( $\sim$ us). Not as good as jakarta.

## Realization of $X$ and $Y$ pulses

Drive IF signal consists of two control components,

$$\Omega = \Omega(t) \exp\{i(\omega_{ssb}t + \phi)\}, \quad (1)$$

which is up-converted to the qubit frequency  $\omega_{ij}$  and synthesized by AWG. Thus real-time control over phase, frequency, and amplitude. In a frame rotating at the qubit frequency, the transmon Hamiltonian is given by

$$\frac{\hat{H}^R}{\hbar} = \Delta|2\rangle\langle 2| + \frac{\tilde{\Omega}_x(t)}{2} \sum_{j=1}^2 \hat{\sigma}_{j,j-1}^x + \frac{\tilde{\Omega}_y(t)}{2} \sum_{j=1}^2 \hat{\sigma}_{j,j-1}^y, \quad (2)$$

where  $\Omega_{x,y}$  are the drive's IQ-components. Choosing appropriate  $\phi$  and  $\theta$  results in realization of arbitrary  $X$  and  $Y$  pulses.

## DRAG first-order correction

Since transmons have low anharmonicity, DRAG is employed to suppress leakage out of the computation subspace. To the first-order correction, a Gaussian shaped pulse

$\Omega_x(t) = A \exp\{-t^2/(2\sigma^2)\}$  with amplitude  $A$  and width  $\sigma$ , is corrected by

$$\Omega_{DRAG}(t) = \Omega_x(t) + i \frac{\beta}{\Delta} \frac{d\Omega_x(t)}{dt}, \quad (3)$$

where the imaginary component eliminates the spectral weight of the pulse at  $|1\rangle \leftrightarrow |2\rangle$  transition.

## DRAG second-order correction

DRAG pulses fail to produce high fidelity state transition when gate duration is lower than  $10/\Delta^1$ . To overcome this, higher-order correction terms  $\delta_n = a_n + ib_n$  have to be added. This results in a list of piecewise-constant control amplitudes

$$\Omega_n = \Omega_{DRAG}(n\Delta t) + \delta_n. \quad (4)$$

The time discretization  $\Delta t$  is naturally given by the sampling rate of the AWG generating the pulse envelope. Optimization parameters are amplitude corrections  $a_n$  and  $b_n$  to the  $n$ -th sample of  $\Omega_{x,y}$ .

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<sup>1</sup> $\Delta/2\pi = -315.28$  MHz

# Table of Contents

- 1 Introduction
- 2 Setup and system control
- 3 Parameter optimization & Results

## Pulse parameter optimization

- Pulse parameters are optimized using the covariance matrix adaptation-evolution strategy (CMA-ES) algorithm. Briefly,  $\mathcal{S}^k$  ( $\lambda$  sets) are generated, with  $k = 1, \dots, \lambda$  each characterized by the parametrization of the pulse shape. Each's shape-candidate is evaluated by a cost function, which generates a new set of candidate shapes.
- Randomized benchmarking as cost function ( $m$  Clifford gates,  $K$  sequences). Clifford gates are constructed by composing  $\pm X/2$  and  $\pm Y/2$  pulses (!?) based on  $\mathcal{S}^k$ .

# Fidelity estimates of optimized short pulses

- ① First round using CMA-ES to calibrate DRAG pulses,  
 $\mathcal{S} = \{A, \beta, \omega_{ssb}\}$ .
- ② Next round extending  $\mathcal{S}$  to include higher correction orders,  
namely  $a_j$  and  $b_j$ .

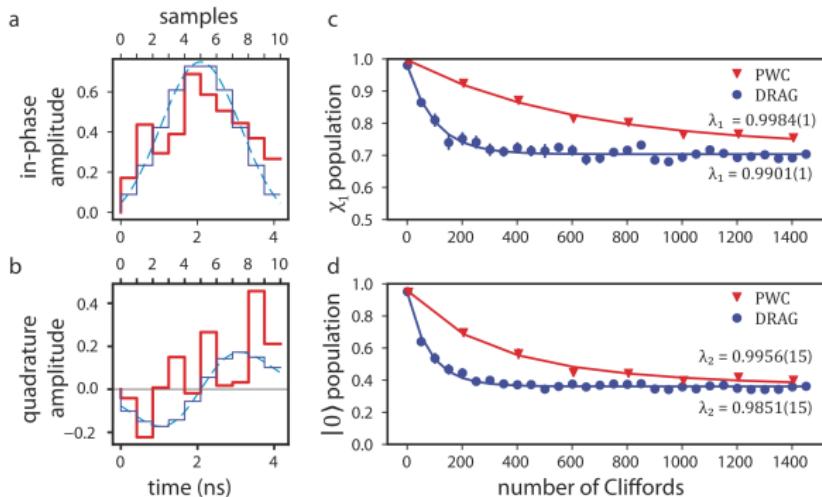


Figure: Optimized DRAG pulse.